

## Element Reference Manual

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## Notation.

A Cross sectional area
Ap Plastic area
As, Asy, Asz Effective shear area
$\mathbf{A}_{1} \ldots \mathbf{A}_{\mathrm{n}}$ Nodal cross sectional areas
ar Mass Rayleigh damping constant
$\alpha$ Coefficient of thermal expansion
$\alpha$ Softening parameter
$\alpha \mathbf{x}, \alpha \mathbf{y}, \alpha \mathbf{z}, \alpha \mathbf{x y}, \alpha \mathbf{x z}$, Orthotropic thermal expansion coefficients $\alpha y z$
$\alpha \mathbf{x}, \alpha \mathbf{y}, \alpha \mathbf{z}$ Angular accelerations
br Stiffness Rayleigh damping parameter
$\beta$ Shear retention factor/parameter
$\beta$ Principal stresses direction
C Specific heat capacity
$\mathbf{C i}$ (i)th hardening stiffness
$\mathbf{C}_{0}$ Neo-Hookean rubber model constant
$\mathbf{C}_{1}, \mathbf{C}_{2}$ Mooney-Rivlin rubber model constants
c Cohesion
co Initial cohesion
Dij Rigidity coefficients
du, dq Relative displacement, rotation
E Modulus of elasticity (Young's modulus)
Ep Elasto-plastic modulus$\mathbf{E x}, \mathbf{E y}, \mathbf{E z}$ Orthotropic moduli of elasticityep Strain at peak compressive strengthey, ez Eccentricity$\varepsilon \mathbf{x}, \varepsilon \mathbf{y}, \varepsilon \mathbf{z}$ Direct strains (local or global)
Es Maximum shear strain
عe Von Mises equivalent strain
عc Creep strains
عр Equivalent plastic strain
$\mathbf{F x}, \mathbf{F y}, \mathbf{F z}$ Forces (local or global)
Fyld Yield force
F Deformation gradient
fc' Compressive strength of concrete
ft' Tensile strength of concrete
$\psi \mathbf{x}, \psi \mathbf{y}, \psi \mathbf{z}$ Flexural (bending) strain resultants
$\psi \mathbf{x y}, \psi \mathbf{x z}, \psi \mathbf{y z}$ Torsional strain resultants
G Shear modulus
Gf Fracture energy
Gxy, Gxz, Gyz Orthotropic shear moduli
$\gamma \mathbf{x}, \gamma \mathbf{y}, \gamma \mathbf{z}$ Membrane strain resultants
$\gamma \mathbf{x}, \gamma \mathbf{y}, \gamma \mathbf{z}$ Field gradients (local or global)
H Enthalpy
Hi1 Isotropic hardening parameter
Hk1 Kinematic hardening parameter
hc Convective heat transfer coefficient
hf Heat fractionhr Radiative heat transfer coefficient
$\theta \mathbf{x}, \theta \mathbf{y}, \theta \mathbf{z}$ Rotations (local or global)
$\theta_{1}, \theta_{2}$ Loof node rotations (local)
$\theta \alpha, \theta \beta$ Nodal rotations for thick shells
$\theta \lambda$ Angle defining principal directions of $\lambda_{1}, \lambda_{2}$
Iy, Iz 1st moments of inertia
Iyy, Izz 2nd moments of inertia
Iyz Product moment of inertia
J Volume ratio (determinant of F)
K Spring stiffness
Kc Contact stiffness
Kl Lift-off stiffness
Ko Original gap conductance
Kt Torsional constant
k Thermal conductivity
$\mathbf{k x}, \mathbf{k y}, \mathbf{k z}$ Orthotropic thermal conductivities
kr Bulk modulus
$\kappa$ Hardening stiffness
Li Limit of (i)th hardening stiffness
$\lambda_{1}, \lambda_{2}, \lambda_{3}$ Principal stretches
M Mass
$\mathbf{M x}, \mathbf{M y}, \mathbf{M z}$ Concentrated moments (local or global)
$\mathbf{M x}, \mathbf{M y}, \mathbf{M z}, \mathbf{M}_{\theta}$ Flexural moments (local or global)
Mxy, Mxz, Myz Torsional moments (local or global)
$\mathbf{M}_{1}, \mathbf{M}_{2}$ Concentrated loof moments (local or global)
$\mathbf{m}_{\mathrm{x}}, \mathbf{m}_{\mathrm{y}}, \mathbf{m}_{\mathrm{z}}$ Mass in element local directions
$\mu$ Coulomb friction coefficient
$\mu \mathbf{r i}$, ari Ogden rubber model constants
$\mathbf{N x}, \mathbf{N y}, \mathbf{N z}, \mathbf{N} \theta$ Membrane resultants (local or global)
$\mathbf{N x}, \mathbf{N y}, \mathbf{N x y}$ Stress resultants
Nmax, Nmin Principal stress resultants
Ns Maximum shear stress resultant
Ne Von Mises equivalent stress resultant
$v$ Poisson's ratio
vxy, vxz, vyz Orthotropic Poisson's ratio
Px, Py, Pz Concentrated loads (global)
$\rho$ Mass density
Q Field loading
qa Field face loading flux/unit area
qv Field volume loading flux/unit volume
$\mathbf{q x}, \mathbf{q y}, \mathbf{q z}$ Field fluxes (local or global)$\mathbf{Q}_{\mathrm{H}}$ Rate of internal heat generation per unit volume Rate of internalmass (liquid+vapour) generation per unit volume Heat flux$\mathbf{Q}_{\mathrm{w}}$ Rate of internal heat generation per unit volume Rate of internalmass (liquid+vapour) generation per unit volume Heat flux$\mathbf{q}_{\mathrm{H}}$ Rate of internal heat generation per unit volume Rate of internalmass (liquid+vapour) generation per unit volume Heat flux
qs Stress potential parameters
$\mathbf{q}_{\mathrm{w}}$ Mass (liquid+vapour) flux Relative humidity Initial relativehumidity
RH Mass (liquid+vapour) flux Relative humidity Initial relativehumidity
$\mathbf{R H}_{0}$ Mass (liquid+vapour) flux Relative humidity Initial relativehumidity
Sp Plastic shear area
$\sigma y$ Yield stress
$\sigma y o$ Initial uniaxial yield stress
$\sigma \mathbf{x}, \sigma \mathbf{y}, \sigma \mathbf{z}$ Direct stresses (local or global)
$\sigma$ max, $\sigma$ min Principal stresses$\sigma \mathbf{x y}, \sigma \mathbf{x z}, \sigma \mathbf{y z}$ Shear stresses (local or global)os Maximum shear stress
$\sigma$ Von Mises equivalent stress
T Temperature
T, To Final, initial temperatures
$\mathbf{t}_{1} \ldots \mathbf{t}_{\mathrm{n}}$ Nodal thicknesses
U, V, W Displacements (global)
$\Phi$ Field variable
Фе External environmental temperature
$\phi$ Frictional angle
$\phi$ o Initial frictional angle
$\phi$ Body force potential
$\mathbf{V x}, \mathbf{V y}, \mathbf{V z}$ Nodal velocities (global)
V11, V12 ... V33 Left stretch tensor components
$\mathbf{W x}, \mathbf{W y}, \mathbf{W z}$ Uniformly distributed intensities
$\mathbf{X , Y , \mathbf { Z }}$ Nodal coordinates (global)
Xcbf, Ycbf, Zcbf Constant body forces (global)
Xo, Yo, Zo Offsets of finite element model coordinate system from point about which global angular acceleration and velocities are applied
$\mathbf{y}_{1}, \mathbf{z}_{1} \ldots \mathbf{y}_{4}, \mathbf{z}_{4}$ Cross sectional coordinates (local)
$\mathbf{Z y p}, \mathbf{Z z p}$ Torsional plastic moduli
Zyyp, Zzzp Flexural plastic moduli
$\omega$ Frequency of vibration
$\Omega \mathbf{x}, \Omega \mathbf{y}, \Omega \mathbf{z}$ Angular velocities (global)

## Introduction.

## Overview

The LUSAS Element Reference Manual describes the elements currently available in LUSAS Solver. It has been designed to be used in conjunction with the Solver Reference Manual and provides input/output information which is specific to each element type.
If you require:

- General theoretical information - refer to Theory Manual Volume 1
- Element related theoretical / formulation information - refer to Theory Manual Volume 2


## Element selection

Details of typical element uses are provided and, to assist you with choosing an element for a particular modelling task, three alternative selection methods are available for selecting by:
$\square$ Element type - listing just element group, sub-group and element name
$\square$ Element index - showing element name, geometry, nodal freedoms and element availability
$\square$ Element summary - showing element names, material property, loading, nonlinear, integration, and mass modelling capabilities
Of these three methods, the element summary tables provide the most detail to enable correct element selection for a particular modelling task.

## Element uses

The following brief descriptions of each element group are provided to assist you with element selection for a particular modelling task.
Additional more detailed and element-specific recommendations on use can be found by viewing the Recommendations on Use section provided within each element's listing. For an example see 3D Isoparametric Thick Beam Elements

## Bar Elements

Bar elements are used to model plane and space truss structures, cables in cable-stayed structures, and stiffening reinforcement.

- LUSAS incorporates 2 and 3-dimensional bar elements which may either be straight or curved.
- Bar elements model axial force only.


## Beam Elements

Beam elements are used to model plane frames, space frame structures, and cables in cable-stayed structures.

- LUSAS incorporates a variety of thin and thick beams in both 2 and 3-dimensions. In addition, specialised beam elements for modelling grillage or eccentrically ribbed plate structures are available.
- LUSAS beam elements may be either straight or curved and may model axial force, bending and torsional behaviour.


## 2D Continuum Elements

2D continuum elements are used to model solid structures whose behaviour may reasonably be assumed to be 2-dimensional.

- 2D continuum elements may be applied to plane stress, plane strain and axisymmetric solid problems.
- Triangular and quadrilateral elements are available.
- Fourier elements, which allow non-axisymmetric loading to be applied to axisymmetric models, are considered a special case of the 2 D continuum elements since the mesh is defined entirely in the xy-plane, but the resulting displacements, strains and stresses are fully three-dimensional.
- Special crack tip elements are available to model the singularities encountered at crack opening
- Explicit elements are available to model high speed dynamics problems efficiently.


## 3D Continuum Elements

3D continuum elements are used to model fully3-dimensional structures.

- Tetrahedral, pentahedral and hexahedral solid elements are available to model full 3-dimensional stress fields.



## Element Reference Manual

- Composites elements are available to model laminates.
- Special crack tip elements are available to model the singularities encountered at crack opening


## Plate Elements

Plate elements are used to model flat structures whose deformation can be assumed to be predominantly flexural

- LUSAS incorporates both thin and thick plate elements.

- Triangular and quadrilateral flexural plate elements are available.


## Shell Elements

Shell elements are used to model 3-dimensional structures whose behaviour is dependent upon both flexural and membrane effects.

- LUSAS incorporates both flat and curved shell elements.
- Triangular and quadrilateral elements are available
- Both thin and thick shell elements are available.


## Membrane Elements

Membrane elements are used to model 2 and 3-dimensional structures whose behaviour is dominated by in-plane membrane effects.

- LUSAS incorporates both axisymmetric and space (3-

- 

dimensional) membrane elements.

- Membrane elements incorporate in-plane (membrane) behaviour only (they include no bending behaviour).


## Joint Elements

Joint elements are used to model flexible joints between other LUSAS elements.

- LUSAS incorporates a variety of joint elements which are
 designed to match the nodal freedoms of their associated elements.
- Joint elements may also be used to model point masses, elastoplastic hinges, or smooth and frictional element contacts.


## Non-Structural Mass Elements

Non-Structural Mass elements are used to model translational mass at a point, along an edge or on a surface.

- Non-Structural Mass elements must be used with other structural

elements.


## Thermal / Field Elements

Thermal / Field elements are used to model quasi-harmonic equation problems such as thermal conduction or potential distribution.

- LUSAS incorporates bar, plane, axisymmetric solid and 3-

dimensional solid field elements.
- Thermal link elements are also available.


## Hygro-Thermal Elements

Hygro-thermal elements are used in hygro-thermal transient analyses, i.e. to model heat and moisture flow in porous media. The elements are generally used for problems involving the heat of hydration of concrete,
 and are normally used in a hygro-thermal-structural coupled analysis.

- LUSAS incorporates plane, axisymmetric solid and 3dimensional solid hygro-thermal elements
- Thermal link elements can also be used in a hygro-thermal analysis.


## Interface Elements

Mohr-Coulomb interface elements are used to model the contact behaviour between two bodies.
Delamination interface elements model delamination and crack

propagation in composites. They are positioned at places of potential delamination between continuum elements

## Rigid Elements

Rigid elements are used to define the shape of a rigid surface which is not part of the analysis model.


## Phreatic Surface Elements

Phreatic surface elements are used to define the shape of a phreatic surface. They may be used with 2D and 3D continuum and two-phase elements.


## Element Groups

The LUSAS Element Library is arranged into the following element groups:

# Bars 

$\square$ Beams

- 2D Continuum elements
$\square$ 3D Continuum elements
$\square$ Plates
$\square$ Shells
$\square$ Membranes
- Joints

Non-structural mass elements
$\square$ Thermal/Field elements
[ Hygro-thermal elements
$\square$ Interface elements
$\square$ Rigid elements
$\square$ Phreatic surface elements

## Element Sub-Groups

Each element group is also sub-divided into element sub-groups according to the type of element formulation as shown in the following table. For example, the Beam element group contains the element sub-groups: Engineering beams, Thick beams, Kirchhoff beams and Semiloof beams.
Within each sub-group elements vary according to the geometry, the number of nodes, and the properties required by each element. The individual elements are referred to by their LUSAS name, for example: BMI21 or QTS4 .

## Note

The dimensional classification of LUSAS elements is on the basis of the number of dimensions required for input of the nodal coordinates. For example, an engineering grillage element, (GRIL) requires X, Y coordinates and is hence classed as being 2-dimensional (despite having an out of plane displacement freedom).

## Element Types and Availability

| Element Group | Element Subgroup | Element Name and Software Product Version Availability |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | LT | Standard (S) | Plus (+) |
| Bars | Structural bars | $\begin{array}{\|l\|} \hline \text { BAR2, } \\ \hline \text { BRS2 } \\ \hline \end{array}$ | BAR3, BRS3 |  |
| Beams | Engineering beams | GRIL |  |  |
|  | Plain strain beams |  | BMI2N, BMI3N |  |
|  | Thick beams | $\begin{array}{\|l} \mathrm{BMI} 2, \\ \mathrm{BMI} 21 \\ \hline \end{array}$ |  | $\begin{aligned} & \begin{array}{l} \text { BMI3, BMI2X } \\ \text { BMI3X, BMI22 } \\ \text { BMI31, BMI33, } \\ \text { BMX21 } \\ \text { BMX22, } \\ \text { BMX31, BMX33 } \end{array} \end{aligned}$ |
|  | Thick crosssection beams |  |  | $\begin{aligned} & \text { BMI3, BMI2X, } \\ & \text { BMI3X, BMI22, } \\ & \text { BMI31, BMI33, } \\ & \begin{array}{l} \text { BMX22 } \end{array}, \text { BMX22, } \\ & \hline \text { BMX31, BMX33 } \end{aligned}$ |
|  | Warping beams |  |  |  |
|  | Thin (Kirchhoff) beams |  | BM3, BMX3 | BS3, BS4, BSX4 |
|  | Semiloof beams |  |  | BSL3, BSL4, BXL4 |
| 2D Continuum | Plane stress continuum |  | $\begin{aligned} & \text { TPM3, TPM6, } \\ & \text { QPM4, QPM8, } \\ & \text { QPM4M, TPK6, } \\ & \text { QPK8 } \end{aligned}$ | TPM3E, OPM4E |
|  | Plane strain continuum |  | $\begin{aligned} & \text { TPN3, TPN6, QPN4, } \\ & \text { QPN8, } \end{aligned}$ | TPN3E, QPN4E |


| Element Group | Element Subgroup | Element Name and Software Product Version Availability |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | LT | Standard (S) | Plus (+) |
|  |  |  | $\begin{aligned} & \text { QPN4L, TNK6, } \\ & \text { QNK8 } \end{aligned}$ |  |
|  | Plain strain two phase |  | TPN6P, OPN8P |  |
|  | Axisymmetric solid continuum |  | $\begin{aligned} & \text { TAX3, TAX6, QAX4, } \\ & \text { QAX8, QAX4M, } \\ & \text { QAX4L, TXK6, } \\ & \text { QXK8, TAX3F, } \\ & \begin{array}{l} \text { TAX6F, }, ~ Q A X 4 F, ~ \\ \text { QAX8F } \end{array} \end{aligned}$ | TAX3E, OAX4E |
|  | Axisymmetric solid two-phase |  |  | TAX6P, QAX8P |
|  | Fourier ring |  |  | $\begin{aligned} & \text { TAX3F, TAX6F } \\ & \text { QAX4F }, \underline{\text { QAX8F }} \end{aligned}$ |
| 3D Continuum | Solid continuum |  | $\begin{aligned} & \text { TH4 }, ~ P N 6, ~ H X 8, ~ \\ & \underline{H X 8} \end{aligned}$ | $\begin{aligned} & \text { TH10, PN12, PN15, } \\ & \begin{array}{l} \text { HX16, }, \text { HX20, } \\ \text { TH10S }, \text { PN6L } \\ \text { PN12L, HX8L, } \\ \text { HX16L, TH4E }, \\ \text { PN6E, HX8E } \end{array} \end{aligned}$ |
|  | Solid continuum crack tip |  |  | $\begin{aligned} & \text { TH10K, PN15K, } \\ & \text { HX20K } \end{aligned}$ |
|  | Solid continuum two phase |  |  | TH10P,$~$ <br> PN1512P <br> HX20P, |
| Plates | Isoflex plates <br> Mindlin plates |  | $\begin{aligned} & \text { TF3, QF4, QSC4 } \\ & \text { TTF6, QTF } 8 \end{aligned}$ |  |
| Shells | Axisymmetric thin shells |  | BXS3 |  |
|  | Axisymmetric thick shells |  | BXSI2, ${ }^{\text {BXSI3 }}$ |  |
|  | Flat thin shells |  | TS3, QSI4 | TSR6, |


| Element Group | Element <br> Subgroup | Element Name and Software Product Version Availability |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | LT | Standard (S) | Plus (+) |
|  | Semiloof shells |  |  | TSL6, OSL8 |
|  | Thick shells |  | TTS3, QTS4 | TTS6, QTS8 |
| Membranes | Axisymmetric membranes |  | BXM2, BXM3 |  |
|  | Space membranes |  | TSM3, SMI4 |  |
| Joints | 2D joints |  | $\frac{\mathrm{JNT} 3}{\mathrm{JAX3}}, \underline{\mathrm{JPH} 3}, \underline{\mathrm{JF} 3},$ |  |
|  | 3D joints |  | $\begin{aligned} & \mathrm{JNT4}, \mathrm{JL43}, ~ \mathrm{JSH} 4, \\ & \mathrm{JL46} \end{aligned}$ | JSL4 |
| Field | Thermal bars |  | $\begin{aligned} & \frac{\mathrm{BFD} 2}{}, \underline{\mathrm{BFD} 3}, \text { BFX2, } \\ & \text { BFX3 }, ~ B F S 2, ~ B F S 3 \end{aligned}$ |  |
|  | Thermal links |  | LFD2, LFX2, LFS2 |  |
|  | Plane field |  | $\begin{aligned} & \text { TFD3 } \\ & \text { QFD8 } \\ & \text { TFD6, }, ~ \text { QFD4, } \end{aligned}$ |  |
|  | Axisymmetric field |  | $\frac{\text { TXF3 }}{\text { QXF }}, ~ \text { TXF6 }, ~ \text { QXF4, }$ |  |
|  | Solid field |  | $\begin{aligned} & \text { TF4, TF10, PF6, } \\ & \text { PF12, PF15, HF8 } \end{aligned}$ | $\begin{aligned} & \begin{array}{l} \text { HF16, HF20, PF6C, } \\ \text { PF12C, } \\ \text { HF8C, TF10S } \end{array} \end{aligned}$ |
| Hygro-Thermal | Plane hygrothermal |  |  | $\begin{aligned} & \text { THT3, THT6, } \\ & \text { QHT4, QHT8 } \end{aligned}$ |
|  | Axisymmetric hygro-thermal |  |  | TXHT3, TXHT6, |
|  | Solid hygrothermal |  |  | THT4, THT10, <br> PHT6, PHT12, <br> PHT15, HHT8, <br> HHT16, ${ }^{\text {HHT20 }}$ |
| Interface | 2D Interface |  |  | $\begin{aligned} & \text { IPN4, IPN6, IPM4, } \\ & \text { IPM6, IAX4, IAX } \end{aligned}$ |
|  | 2D Two-phase interface |  |  | IPN6P, IAX6P |


| Element Group | Element Subgroup | Element Name and Software Product Version Availability |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | LT | Standard (S) | Plus (+) |
|  | 3D Interface |  |  | IS6, IS8, IS12, IS16 |
|  | 3D Two-phase interface |  |  | IS12P, IS16P |
| Mass | Point Mass |  |  | PM2, PM3 |
|  | Line Mass |  |  | LM2, LM3, LMS3, <br> LMS4 |
|  | Surface Mass |  |  | $\frac{\text { TM3 }}{\text { OM8 }},$ |
| Rigid Surface | 2D Rigid |  |  | R2D2 |
|  | 3D Rigid |  |  | R3D3, R3D4 |
| Phreatic Surface | 2D |  | PHS2 |  |
|  | 3D |  | PHS3, PHS4 |  |

For details of the compatibility of joint elements with other elements see Appendix L : $\underline{\mathbf{J o i n t}}$ Element Compatibility

## Element Index

The following element index tables provide a diagrammatic index for each element with a description of the element, the nodal freedoms, and the software product version in which it is available.
The tables are listed in the following order:
$\square$ Bar elements
$\square$ Beam elements

- 2D Continuum elements
$\square$ 3D Continuum elements
$\square$ Plate elements
$\square$ Shell elements
$\square$ Membrane elements
$\square$ Joint elements
Thermal / Field elements
$\square$ Hygro-Thermal elements
$\square$ Interface elements
$\square$ Non-Structural Mass elements
$\square$ Rigid elements
$\square$ Phreatic elements


## Bar Elements

| Name | Geometry | Title | Freedoms | Product Version |
| :--- | :--- | :--- | :--- | :---: |
| $\underline{\text { BAR2 }}$ |  | BAR element in 2D | $\mathrm{U}, \mathrm{V}$ | LT |
| BAR3 |  | BAR element in 2D | $\mathrm{U}, \mathrm{V}$ |  |



## Beam Elements

| Name | Geometry | Title | Freedoms | Product <br> Version |
| :--- | :--- | :--- | :--- | :--- |
| GRIL |  | ENGINEERING grillage thick <br> beam element in 2D | $\mathrm{W}, \mathrm{qx}, \mathrm{qy}$ |  |
| $\underline{\text { BMI2 }}$ |  | LT |  |  |
| $\underline{\text { BMI3 }}$ |  | THICK beam element in 2D <br> (co-rotational) | $\mathrm{U}, \mathrm{V}, \mathrm{qz}$ |  |
| $\underline{\text { BMI3X }}$ |  | THICK beam element in 2D <br> with quadrilateral cross-section <br> (co-rotational) | $\mathrm{U}, \mathrm{V}, \mathrm{qz}$ |  |


| BMI21 |  | THICK linear thick beam element in 3D | $\left\lvert\, \begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{qx}, \\ & \mathrm{qy}, \mathrm{qz} \end{aligned}\right.$ | LT |
| :---: | :---: | :---: | :---: | :---: |
| BMI21W |  | THICK linear thick beam element with torsional warping in 3D | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{qx}, \\ & \mathrm{qy}, \mathrm{qz}, \alpha \end{aligned}$ | Plus |
| BMX21 |  | THICK linear thick beam element in 3D with quadrilateral cross-section | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{qx}, \\ & \mathrm{qy}, \mathrm{qz} \end{aligned}$ | Standard |
| BMX21W |  | THICK linear thick beam element with torsional warping in 3D with quadrilateral crosssection | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{qx}, \\ & \mathrm{qy}, \mathrm{qz}, \alpha \end{aligned}$ | Plus |
| BMI31 |  | THICK quadratic thick beam element in 3D | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{qx}, \\ & \mathrm{qy}, \mathrm{qz} \end{aligned}$ | Plus |
| BMI31W |  | THICK quadratic thick beam element with torsional warping in 3D | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{qx}, \\ & \mathrm{qy}, \mathrm{qz}, \alpha \end{aligned}$ | Plus |


| BMX31 |  | THICK quadratic thick beam element in 3D with quadrilateral cross-section | $\left\lvert\, \begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{qx}, \\ & \mathrm{qy}, \mathrm{qz} \end{aligned}\right.$ | Plus |
| :---: | :---: | :---: | :---: | :---: |
| BMX31W |  | THICK quadratic thick beam element with torsional warping in 3D with quadrilateral crosssection | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{qx}, \\ & \mathrm{qy}, \mathrm{qz}, \alpha \end{aligned}$ | Plus |
| BMI22 |  | THICK twisted linear thick beam element in 3D | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{qx}, \\ & \mathrm{qy}, \mathrm{qz} \end{aligned}$ | Plus |
| BMI22W |  | THICK twisted linear thick beam element with torsional warping in 3D | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{qx}, \\ & \mathrm{qy}, \mathrm{qz}, \alpha \end{aligned}$ | Plus |
| BMX22 |  | THICK twisted linear thick beam element in 3D with quadrilateral cross-section | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{qx}, \\ & \mathrm{qy}, \mathrm{qz} \end{aligned}$ | Plus |
| BMX22W |  | THICK twisted linear thick beam element with torsional warping in 3D with quadrilateral cross-section | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{qx}, \\ & \mathrm{qy}, \mathrm{qz}, \alpha \end{aligned}$ | Plus |


| BMI33 |  | THICK twisted quadratic thick beam element in 3D | $\left\lvert\, \begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{qx}, \\ & \mathrm{qy}, \mathrm{qz} \end{aligned}\right.$ | Plus |
| :---: | :---: | :---: | :---: | :---: |
| BMI33W |  | THICK twisted quadratic thick beam element with torsional warping in 3D | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{qx}, \\ & \mathrm{qy}, \mathrm{qz}, \alpha \end{aligned}$ | Plus |
| BMX33 |  | THICK twisted quadratic beam element in 3D with quadrilateral cross-section | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{qx}, \\ & \mathrm{qy}, \mathrm{qz} \end{aligned}$ | Plus |
| BMX33W |  | THICK twisted quadratic beam element with torsional warping in 3D with quadrilateral crosssection | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{qx}, \\ & \mathrm{qy}, \mathrm{qz}, \alpha \end{aligned}$ | Plus |
| BM3 |  | KIRCHHOFF thin beam element in 2D | end nodes: U, V, qz mid-node: dU | Standard |
| BMX3 |  | KIRCHHOFF thin beam element in 2D with quadrilateral cross-section | $\begin{aligned} & \text { end nodes: } \\ & \text { U, V, qz } \\ & \text { mid-node: } \\ & \text { dU } \end{aligned}$ | Standard |
| BS3 |  | KIRCHHOFF thin beam element in 3D | end nodes: U, V, W, qx, qy, qz mid-node: dU, dqx | Plus |


| BS4 |  | KIRCHHOFF thin beam element in 3D | end nodes: <br> U, V, W, qx, <br> qy, qz <br> mid-node: <br> dU, dqx | Plus |
| :---: | :---: | :---: | :---: | :---: |
| BSX4 |  | KIRCHHOFF thin beam element in 3D with quadrilateral cross-section | end nodes: U, V, W, qx, qy, qz mid-node: dU, dqx | Plus |
| BSL3 |  | SEMILOOF thin beam element in 3D for use with TSL6 | $\begin{aligned} & \text { end nodes: } \\ & \text { U, V, W, qx, } \\ & \text { qy, qz } \\ & \text { mid-node: } \\ & \text { U, V, W, q1, } \\ & \text { q2 } \\ & \hline \end{aligned}$ | Plus |
| BSL4 |  | SEMILOOF thin beam element in 3D for use with QSL8 | $\begin{aligned} & \text { end nodes: } \\ & \text { U, V, W, qx, } \\ & \text { qy, qz } \\ & \text { mid-node: } \\ & \text { U, V, W, q1, } \\ & \text { q2 } \\ & \hline \end{aligned}$ | Plus |
| BXL4 |  | SEMILOOF thin beam element in 3D with quadrilateral crosssection | $\begin{aligned} & \text { end nodes: } \\ & \text { U, V, W, qx, } \\ & \text { qy, qz } \\ & \text { mid-node: } \\ & \text { U, V, W, q1, } \\ & \text { q2 } \\ & \hline \end{aligned}$ | Plus |
| BMI2N | $\underbrace{1} \rightarrow$ | Plane strain beam (co-rotational) | U, V, qz, | Standard |
| BMI3N |  | Plane strain beam (co-rotational) | U, V, qz, | Standard |

## 2D Continuum Elements

| Name | Geometry | Title | Freedoms | Product <br> Version |
| :--- | :--- | :--- | :--- | :--- |


| TPM3 |  | PLANE STRESS continuum element in 2D | U, V | Standard |
| :---: | :---: | :---: | :---: | :---: |
| TPM6 |  | PLANE STRESS continuum element in 2D | U, V | Standard |
| QPM4 |  | PLANE STRESS continuum element in 2D | U, V | Standard |
| QPM8 |  | PLANE STRESS continuum element in 2D | U, V | Standard |
| QPM4M |  | PLANE STRESS continuum element in 2D with enhanced strains | U, V | Standard |
| TPK6 |  | PLANE STRESS continuum crack tip element in 2D | U, V | Standard |
| QPK8 |  | PLANE STRESS continuum crack tip element in 2D | U, V | Standard |
| TPM3E |  | PLANE STRESS explicit dynamics element in 2D | U, V | Plus |
| QPM4E | $\square_{1}^{4}$ | PLANE STRESS explicit dynamics element in 2D | U, V | Plus |
| TPN3 | $\qquad$ | PLANE STRAIN continuum element in 2D | U, V | Standard |


| TPN6 |  | PLANE STRAIN continuum element in 2D | U, V | Standard |
| :---: | :---: | :---: | :---: | :---: |
| QPN4 | $\square$ | PLANE STRAIN continuum element in 2D | U, V | Standard |
| QPN8 |  | PLANE STRAIN continuum element in 2D | U, V | Standard |
| QPN4M | $\square$ | PLANE STRAIN continuum element in 2D with enhanced strains | U, V | Standard |
| QPN4L |  | PLANE STRAIN continuum element in 2D for large strains | U, V | Standard |
| TNK6 |  | PLANE STRAIN continuum crack tip element in 2D | U, V | Standard |
| ONK8 |  | PLANE STRAIN continuum crack tip element in 2D | U, V | Standard |
| TPN3E |  | PLANE STRAIN explicit dynamics element in 2D | U, V | Plus |
| QPN4E |  | PLANE STRAIN explicit dynamics element in 2D | U, V | Plus |
| TPN6P |  | PLANE STRAIN continuum two phase element in 2D | $\mathrm{U}, \mathrm{V}$ P: <br> corner nodes <br> U, <br> V: Midside <br> nodes | Standard |


| QPN8P | 5 | PLANE STRAIN continuum two phase element in 2D | U, V P: <br> corner nodes <br> U, <br> V: Midside <br> nodes | Standard |
| :---: | :---: | :---: | :---: | :---: |
| TAX3 |  | AXISYMMETRIC solid continuum element in 2D | U, V | Standard |
| TAX6 |  | AXISYMMETRIC solid continuum element in 2D | U, V | Standard |
| QAX4 | $\square$ | AXISYMMETRIC solid continuum element in 2D | U, V | Standard |
| QAX8 | 5 | AXISYMMETRIC solid continuum element in 2D | U, V | Standard |
| QAX4M |  | AXISYMMETRIC solid continuum element in 2D with enhanced strains | U, V | Standard |
| QAX4L | $\square$ | AXISYMMETRIC solid continuum element in 2D for large strains | U, V | Standard |
| TXK6 |  | AXISYMMETRIC solid continuum crack tip element in 2D | U, V | Standard |
| QXK8 |  | AXISYMMETRIC solid continuum crack tip element in 2D | U, V | Standard |
| TAX3E |  | AXISYMMETRIC solid explicit dynamics element in 2D | U, V | Plus |


| QAX4E |  | AXISYMMETRIC solid explicit dynamics element in 2D | U, V | Plus |
| :---: | :---: | :---: | :---: | :---: |
| TAX6P |  | AXISYMMETRIC solid two phase continuum element in 2D | $\begin{aligned} & \mathrm{U}, \mathrm{~V} \mathrm{P:} \\ & \text { corner nodes } \\ & \mathrm{U}, \\ & \mathrm{~V}: \text { Midside } \\ & \text { nodes } \end{aligned}$ | Plus |
| QAX8P |  | AXISYMMETRIC solid two phase continuum element in 2D | $\begin{aligned} & \mathrm{U}, \mathrm{~V} \mathrm{P:} \\ & \text { corner nodes } \\ & \mathrm{U}, \\ & \text { V: Midside } \\ & \text { nodes } \end{aligned}$ | Plus |
| TAX3F |  | AXISYMMETRIC Fourier ring element in 2D | U, V, W | Plus |
| TAX6F |  | AXISYMMETRIC Fourier ring element in 2D | U, V, W | Plus |
| QAX4F |  | AXISYMMETRIC Fourier ring element in 2D | U, V, W | Plus |
| QAX8F |  | AXISYMMETRIC Fourier ring element in 2D | U, V, W | Plus |

3D Continuum Elements

| Name | Geometry | Title | Freedo <br> ms | Product <br> Version |
| :--- | :--- | :--- | :--- | :--- |
| TH4 |  | SOLID CONTINUUM element in 3D | U, V, W | Standard |


| TH10 |  | \|SOLID CONTINUUM element in 3D | \|U, V, W | Plus |
| :---: | :---: | :---: | :---: | :---: |
| PN6 |  | SOLID CONTINUUM element in 3D | U, V, W | Standard |
| PN12 |  | SOLID CONTINUUM element in 3D | U, V, W | Plus |
| PN15 |  | SOLID CONTINUUM element in 3D | U, V, W | Plus |
| HX8 |  | SOLID CONTINUUM element in 3D | U, V, W | Standard |
| HX16 |  | SOLID CONTINUUM element in 3D | U, V, W | Plus |
| HX20 |  | SOLID CONTINUUM element in 3D | U, V, W | Plus |
| HX8M |  | SOLID CONTINUUM element in 3D with enhanced strains | U, V, W | Standard |
| TH10S | $\sqrt[20]{10}$ | SOLID CONTINUUM composite element in 3D | U, V, W | Plus |
| PN6L |  | SOLID CONTINUUM composite element in 3D | U, V, W | Plus |


| PN12L |  | SOLID CONTINUUM composite element in 3D | \|U, V, W | Plus |
| :---: | :---: | :---: | :---: | :---: |
| HX8L |  | SOLID CONTINUUM composite element in 3D | U, V, W | Plus |
| HX16L |  | SOLID CONTINUUM composite element in 3D | U, V, W | Plus |
| TH10K | 里 | SOLID CONTINUUM crack tip element in 3D | U, V, W | Plus |
| PN15K |  | SOLID CONTINUUM crack tip element in 3D | U, V, W | Plus |
| HX20K |  | SOLID CONTINUUM crack tip element in 3D | U, V, W | Plus |
| TH4E |  | SOLID CONTINUUM explicit dynamics element in 3D | U, V, W | Plus |
| PN6E |  | SOLID CONTINUUM explicit dynamics element in 3D | U, V, W | Plus |
| HX8E |  | SOLID CONTINUUM explicit dynamics element in 3D | U, V, W | Plus |
| TH10P | $\sqrt[s]{5}$ | SOLID CONTINUUM two phase element in 3D | U, V, W | Plus |



## Plate Elements

| Name | Geometry | Title | Freedoms | Product <br> Version |
| :--- | :--- | :--- | :--- | :--- |
| TF3 |  | ISOFLEX thin plate flexure <br> element in 2D | W, qx, qy | Standard |
| $\underline{\text { QF4 }}$ | ISOFLEX thin plate flexure <br> element in 2D | W, qx, qy | Standard |  |
| $\underline{\text { TTF6 }}$ | ISOFLEX thick plate flexure <br> element in 2D | W, qx, qy | Standard |  |
| QTF8 |  | MINDLIN thick plate flexure <br> element in 2D | W, qx, qy | Standard |

## Shell Elements

| Name | Geometry | Title | Freedoms | Product Version |
| :---: | :---: | :---: | :---: | :---: |
| BXS3 |  | AXISYMMETRIC thin shell element in 2D | end nodes: U, V, qz | Standard |
| BXSI2 |  | AXISYMMETRIC thick shell element in 2D | end nodes: $\mathrm{U}, \mathrm{V}, \mathrm{qz}$ | Standard |
| BXSI3 |  | AXISYMMETRIC thick shell element in 2D | $\begin{aligned} & \text { end nodes: } \\ & \text { U, V, qz } \\ & \text { mid-node: } \\ & \text { dU } \end{aligned}$ | Standard |
| TS3 |  | FLAT thin shell element in 3D | U, V, W, qx, qy, qz | Standard |
| QSI4 |  | FLAT thin shell element in 3D | U, V, W, qx, qy, qz | Standard |
| TSR6 |  | FLAT thin nonlinear shell element in 3D | $\begin{aligned} & \text { corner nodes: } \\ & \text { U, V, W } \\ & \text { mid-side nodes: q1 } \end{aligned}$ | Plus |
| TSL6 |  | SEMILOOF curved thin shell element in 3D | corner nodes: U, V, W mid-side nodes: U, V, W, q1, q2 | Plus |
| QSL8 |  | SEMILOOF curved thin shell element in 3D | corner nodes: <br> U, V, W mid-side nodes: $\mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{q} 1, \mathrm{q} 2$ | Plus |


| TTS3 | THICK SHELL flat <br> element in 3D | U, V, W, qa, qbor <br> $\mathrm{U}, \mathrm{V}, \mathrm{qx}, \mathrm{qy}, \mathrm{qz}$ | Standard |  |
| :--- | :--- | :--- | :--- | :--- |
| TTS6 | THICK SHELL curved <br> element in 3D | $\mathrm{U}, \mathrm{V}, \mathrm{W}, \mathrm{qa}, \mathrm{qbor}$ <br> $\mathrm{U}, \mathrm{V}, \mathrm{W}, \mathrm{qx}, \mathrm{qy}, \mathrm{qz}$ | Plus |  |
| $\mathbf{\text { QTS4 }}$ |  | THICK SHELL flat <br> element in 3D | $\mathrm{U}, \mathrm{V}, \mathrm{W}, \mathrm{qa}, \mathrm{qbor}$ <br> $\mathrm{U}, \mathrm{V}, \mathrm{W}, \mathrm{qx}, \mathrm{qy}, \mathrm{qz}$ | Standard |
| $\mathbf{\text { QTS8 }}$ |  | THICK SHELL curved <br> element in 3D | $\mathrm{U}, \mathrm{V}, \mathrm{W}, \mathrm{qa}, \mathrm{qbor}$ <br> $\mathrm{U}, \mathrm{V}, \mathrm{W}, \mathrm{qx}, \mathrm{qy}, \mathrm{qz}$ | Plus |

## Membrane Elements

| Name | Geometry | Title | Freedom <br> s | Product Version |
| :--- | :--- | :--- | :--- | :--- |
| $\underline{\text { BXM2 }}$ |  | AXISYMMETRIC membrane element <br> in 2D |  |  |
| $\underline{\text { BXM3 }}$ |  | V | Standard |  |
| $\underline{\text { TSM3 }}$ |  | SPACE membrane element in 3D | $\mathrm{U}, \mathrm{V}, \mathrm{W}$ | Standard |
| in 2D |  |  |  |  |

## Joint Elements

| Name | Geometry | Title | Freedoms | Product |
| :--- | :--- | :--- | :--- | :--- |


|  |  |  |  | Version |
| :---: | :---: | :---: | :---: | :---: |
| JNT3 |  | JOINT ELEMENT in 2D for bars, plane stress and plane strain | U, V | Standard |
| JPH3 |  | JOINT ELEMENT in 2D for engineering and Kirchhoff beams | U, V, qz | Standard |
| JF3 |  | JOINT ELEMENT in 2D for grillage beams and plates | W, qx, qy | Standard |
| JAX3 |  | JOINT ELEMENT in 2D for axisymmetric solids | U, V | Standard |
| JXS3 |  | JOINT ELEMENT in 2D for axisymmetric shells | U, V, qz | Standard |
| JNT4 |  | JOINT ELEMENT in 3D for bars, solids and space membranes | U, V, W | Standard |
| JL43 |  | JOINT ELEMENT in 3D for corner nodes of semiloof elements | U, V, W | Standard |
| $\begin{aligned} & \mathrm{JSH} 4 \\ & \underline{\mathrm{JL} 46} \end{aligned}$ |  | JOINT ELEMENT in 3D for engineering and Kirchhoff beams and the end/corner nodes of semiloof elements | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{qx}, \\ & \mathrm{qy}, \mathrm{qz} \end{aligned}$ | Standard |
| JSL4 |  | JOINT ELEMENT in 3D for mid-side nodes of semiloof elements | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{q} 1, \\ & \mathrm{q} 2 \end{aligned}$ | Plus |

Thermal / Field Elements

| Name | Geometry | Title | Freedoms | Product Version |
| :---: | :---: | :---: | :---: | :---: |
| BFD2 |  | THERMAL BAR element in 2D | F | Standard |
| BFD3 |  | THERMAL BAR element in 2D | F | Standard |
| BFX2 |  | Axisymmetric THERMAL MEMBRANE element in 2D | F | Standard |
| BFX3 |  | Axisymmetric THERMAL MEMBRANE element in 2D | F | Standard |
| BFS2 |  | THERMAL BAR element in 3D | F | Standard |
| BFS3 |  | THERMAL BAR element in 3D | F | Standard |
| LFD2 |  | THERMAL LINK element in 2D | F | Standard |
| LFX2 |  | Axisymmetric THERMAL LINK element in 2D | F | Standard |
| LFS2 |  | THERMAL LINK element in 3D | F | Standard |
| TFD3 |  | PLANE FIELD element in 2D | F | Standard |
| TFD6 |  | PLANE FIELD element in 2D | F | Standard |


| QFD4 | PLANE FIELD element in 2D | Standard |  |  |
| :--- | :--- | :--- | :--- | :--- |
| QFD8 | PLANE FIELD element in 2D | F | Standard |  |
| TF4 | SOLID FIELD element in 3D | F | Standard |  |
| PF12 | SF10 | SOLID FIELD element in 3D | F | Standard |
| PF15 | SF8 | SOLD element in 3D | Flus |  |
| HF16 |  | POLID FIELD element in 3D | F |  |


| TF10S |  | SOLID FIELD composite element in 3D | F | Plus |
| :---: | :---: | :---: | :---: | :---: |
| PF6C |  | SOLID FIELD composite element in 3D | F | Plus |
| PF12C |  | SOLID FIELD composite element in 3D | F | Plus |
| HF8C |  | SOLID FIELD composite element in 3D | F | Plus |
| HF16C |  | SOLID FIELD composite element in 3D | F | Plus |
| TXF3 |  | AXISYMMETRIC FIELD element in 2D | F | Standard |
| TXF6 |  | AXISYMMETRIC FIELD element in 2D | F | Standard |
| QXF4 |  | AXISYMMETRIC FIELD element in 2D | F | Standard |
| QXF8 |  | AXISYMMETRIC FIELD element in 2D | F | Standard |

## Hygro-Thermal Elements

| Name | Geometry | Title | Freedo <br> ms | Product <br> Version |
| :--- | :--- | :--- | :--- | :--- |


| THT3 |  | PLANE HYGRO-THERMAL element in 2D | T, Pc | Plus |
| :---: | :---: | :---: | :---: | :---: |
| THT6 |  | PLANE HYGRO-THERMAL element in 2D | T, Pc | Plus |
| OHT4 |  | PLANE HYGRO-THERMAL element in 2D | T, Pc | Plus |
| QHT8 |  | PLANE HYGRO-THERMAL element in 2D | T, Pc | Plus |
| TXHT3 |  | AXISYMMETRIC HYGRO-THERMAL element in 2D | T, Pc | Plus |
| TXHT6 |  | AXISYMMETRIC HYGRO-THERMAL element in 2D | T, Pc | Plus |
| QXHT4 |  | AXISYMMETRIC HYGRO-THERMAL element in 2D | T, Pc | Plus |
| OXHT8 |  | AXISYMMETRIC HYGRO-THERMAL element in 2D | T, Pc | Plus |
| THT4 |  | SOLID HYGRO-THERMAL element in 3D | T, Pc | Plus |
| THT10 |  | SOLID HYGRO-THERMAL element in 3D | T, Pc | Plus |


| PHT6 |  | SOLID HYGRO-THERMAL element in 3D | T, Pc | Plus |
| :---: | :---: | :---: | :---: | :---: |
| PHT12 |  | $\begin{aligned} & \text { SOLID HYGRO-THERMAL element in } \\ & \text { 3D } \end{aligned}$ | T, Pc | Plus |
| PHT15 |  | SOLID HYGRO-THERMAL element in 3D | T, Pc | Plus |
| HHT8 |  | SOLID HYGRO-THERMAL element in 3D | T, Pc | Plus |
| HHT16 |  | SOLID HYGRO-THERMAL element in 3D | T, Pc | Plus |
| HHT20 |  | SOLID HYGRO-THERMAL element in 3D | T, Pc | Plus |

## Interface Elements

| Name | Geometry | Title | Freedoms | Product <br> Version |
| :---: | :---: | :---: | :---: | :---: |
| IPN4 |  | PLANE STRAIN INTERFACE ELEMENT in 2D (Initial gap allowed for Mohr-Coulomb variant) | U, V | Plus |
| IPM4 |  | PLANE STRESS INTERFACE ELEMENT in 2D (Initial gap allowed for Mohr-Coulomb variant) | U, V | Plus |


| IAX4 |
| :--- | :--- | :--- | :--- | :--- | :--- |


| IS16 | INTERFACE ELEMENT in 3D <br> (Initial gap allowed for Mohr- <br> Coulomb variant) | U, V, W | Plus |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| IS12P | TWO PHASE INTERFACE <br> ELEMENT in 3D | U, V, W, P <br> corner nodes; <br> $\mathrm{U}, \mathrm{V}, \mathrm{W}$ midside <br> nodes | Plus |  |
| IS16P |  |  | U, V, W, P <br> corner nodes; <br> U,V, W midside <br> nodes | Plus |

Non-Structural Mass Elements

| Name | Geometry | Title | $\left\lvert\, \begin{aligned} & \text { Freedo } \\ & \mathrm{ms} \end{aligned}\right.$ | Product Version |
| :---: | :---: | :---: | :---: | :---: |
| PM2 |  | NON-STRUCTURAL MASS ELEMENT in 2D to model mass at a point | U, V | Plus |
| PM3 | $\overbrace{0}^{2 \underbrace{4 x}_{y}}$ | NON-STRUCTURAL MASS ELEMENT in 3D to model mass at a point | U, V, W | Plus |
| LMS3 |  | NON-STRUCTURAL MASS ELEMENT in 3D to model mass along an edge | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \\ & \mathrm{~W}, \mathrm{qx}, \\ & \mathrm{qy}, \mathrm{qz} \end{aligned}$ | Plus |
| LMS4 |  | NON-STRUCTURAL MASS ELEMENT in 3D to model mass along an edge | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \\ & \mathrm{~W}, \mathrm{qX}, \\ & \mathrm{qy}, \mathrm{qz} \end{aligned}$ | Plus |
| LM2 |  | NON-STRUCTURAL MASS ELEMENT in 2D to model mass along an edge | U, V | Plus |
| LM3 |  | NON-STRUCTURAL MASS ELEMENT in 2D to model mass along an edge | U, v | Plus |



Rigid Slideline Elements

| Name | Geometry | Title | Freedo <br> ms | Product <br> Version |
| :--- | :--- | :--- | :--- | :--- |
| $\underline{\text { R2D2 }}$ |  | RIGID SLIDELINE SURFACE ELEMENT in <br> 2D for modelling non-deformable surfaces in a <br> contact analysis | $\mathrm{U}, \mathrm{V}$ | Plus |
| $\underline{\text { R3D3 }}$ |  | RIGID SLIDELINE SURFACE ELEMENT in <br> 3D for modelling non-deformable surfaces in a <br> contact analysis | $\mathrm{U}, \mathrm{V}, \mathrm{W}$ | Plus |

## Phreatic Elements

| Name | Geometry | Title | lreedo <br> ms | Product <br> Version |
| :--- | :--- | :--- | :--- | :--- |
| PHS2 |  | PHREATIC SURFACE ELEMENT in 2D <br> for modelling phreatic surface. | $\mathrm{U}, \mathrm{V}$ | Plus |



## Element Summary Tables

The following element summary tables list element facilities arranged by LUSAS element group:
$\square$ Bar and Beam elements

- 2D Continuum elements
- 3D Continuum elements
$\square$ Plate, Shell and Membrane elements
$\square$ Joint elements
$\square$ Thermal/Field elements
- Hygro-Thermal elements

Interface, Non-Structural Mass, Rigid, Interface and Phreatic elements

|  |  | Bars |  | Beams |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bar and Elemen | Beam <br> t Summary |  |  | $\mid$ | $\sum_{i=1}^{N}$ |  |  |  | Non |  |  |  | $\sum_{n}^{\infty} \mid$ | $\sum_{\infty}^{\infty}$ |  |  |  | + |
| Product version | $\begin{aligned} & \text { LT, Standard (S) } \\ & \text { or Plus (+) } \end{aligned}$ | LT | LT | LT | LT | LT | S | + | + | + | + | + | S | S | + | + | + | + |
| Nodal | U, V | $\checkmark$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | U, V, W |  | $\checkmark$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| (mid-side) | U, V, qz |  |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |  |  |  |  |  |  |  |
|  | U, V, qz (dU) |  |  |  |  |  |  |  |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  |  |  |
|  | W, qx, qy |  |  | $\checkmark$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | $\begin{aligned} & \text { U, V, W, qx, qy, } \\ & \text { qz (dU, dqx) } \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  |
|  | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \text { qx, qy, } \\ & \text { qz (U, V, W,q1, } \\ & \text { q2) } \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\checkmark$ | $\checkmark$ |
|  | U, V, W, qx, qy |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{qx}, \mathrm{qy}, \\ & \mathrm{qz} \end{aligned}$ |  |  |  | $\checkmark$ |  |  |  | $\checkmark$ |  | $\checkmark$ | $\checkmark$ |  |  |  |  |  |  |
| Material | Linear (Isotropic) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Linear (Orthotropic) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Linear (Anisotropic) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Linear (Rigidities) |  |  |  | $\checkmark$ | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ |  |  | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
|  | Matrix |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Joint |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Concrete Multi- crack |  |  |  |  |  |  | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ |  |  |  |  |  |  |
|  | Stress Resultant |  |  |  | $\checkmark$ | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ |  |  | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ |  |
|  | Tresca | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ |
|  | Drucker-Prager | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ |


|  | Mohr-Coulomb | $\checkmark$ | $\checkmark$ |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Optimised Implicit Von Mises | $\checkmark$ | $\checkmark$ |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ |
|  | $\begin{array}{\|l\|} \hline \text { Volumetric } \\ \text { Crushing/Foam } \\ \hline \end{array}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Stress <br> Potential(Von <br> Mises, Modified <br> Von Mises) | $\checkmark$ | $\checkmark$ |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Creep (General) | $\checkmark$ | $\checkmark$ |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Creep (AASHTO) |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Creep (CEB-FIP) |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Creep (Chinese) |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Creep (Eurocode) |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Creep (IRC) |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Damage (Simo, Oliver) | $\checkmark$ | $\checkmark$ |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ |
|  | Viscoelastic | $\checkmark$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Shrinkage (CEB-FIP_90, Eurocode_2, General, User) | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Rubber |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Generic Polymer |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Multi-linear | $\checkmark$ | $\checkmark$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Composite |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Field |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Loading types | $\begin{array}{\|l} \hline \text { Prescribed Value } \\ \text { (PDSP,TPDSP) } \\ \hline \end{array}$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Concentrated Loads (CL) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | $\begin{aligned} & \text { Element Load } \\ & \text { (ELDS) } \end{aligned}$ |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ |
|  | $\begin{aligned} & \begin{array}{l} \text { Distributed Load } \\ \text { (UDL) } \end{array} \\ & \hline \end{aligned}$ |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | $\begin{array}{\|l\|} \hline \begin{array}{l} \text { Distributed Load } \\ \text { (FLD) } \end{array} \\ \hline \end{array}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | $\begin{aligned} & \text { Body Force } \\ & \text { (CBF) } \end{aligned}$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | $\begin{aligned} & \text { Body Force } \\ & \text { (BFP,BFPE) } \end{aligned}$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Velocity (VELO) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | $\begin{aligned} & \text { Acceleration } \\ & \text { (ACCE) } \end{aligned}$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |


|  | Initial Stress/Strain (SSI,SSIE) | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Initial Stress/Strain (SSIG) | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | $\begin{array}{\|l} \hline \begin{array}{l} \text { Residual Stress } \\ \text { (SSR,SSRE) } \end{array} \\ \hline \end{array}$ |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | $\begin{aligned} & \text { Residual Stress } \\ & \text { (SSRG) } \end{aligned}$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Target Stress/Strain (TSSIE,TSSIA) | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Target Stress/Strain (TSSIG) | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Temperature (TEMP,TMPE) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Field Loads |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Temperature Dependent Loads |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Nonlinear | Total Lagrangian | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Updated Lagrangian |  |  |  |  |  |  | $\checkmark$ |  |  |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
|  | Eulerian |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Co-rotational | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |  |  |  |
| Integration schemes | Explicitly Integrated |  |  | $\checkmark$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Numerically Integrated | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| Mass modelling | Consistent Mass (default) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Lumped Mass | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |


| 2D Continuum Element Summary |  | 2D Continuum |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | cosin | $\mid \sum_{i}^{2}$ | $\mid$ | 倥\| |  | $\stackrel{7}{2}$ | 完 |  |  |  |  | $\underset{d}{\sum}$ | $\stackrel{y}{2}$ | $\left\|\begin{array}{c} a \\ y y y \\ y \\ 0 \\ 0 \\ 0 \\ x \end{array}\right\|$ |  |  | $\begin{array}{ll} 0 \\ 0 \end{array}$ |
| Product Version | $\begin{aligned} & \text { LT, Standard (S) } \\ & \text { or Plus (+) } \end{aligned}$ | S | S | S | + | S | S | S | S | + | + | S | S | S | S | + | + | + |
| Nodal freedoms | U, V | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
|  | U, V, W |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\checkmark$ |
| (corner) | U, V, (P) |  |  |  |  |  |  |  |  |  | $\checkmark$ |  |  |  |  |  | $\checkmark$ |  |
| Material | Linear (Isotropic) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Linear (Orthotropic) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Linear (Anisotropic) | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ * |  | $\checkmark *$ |  | $\checkmark *$ | $\checkmark$ | ** |  | $\checkmark *$ |  | $\checkmark *$ |  |
|  | Linear (Rigidities) | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark *$ |  | $\checkmark *$ |  | $\checkmark *$ |  |  |  |  |  | $\checkmark *$ |  |
|  | Matrix |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Joint |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Concrete Multi- crack | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ |  |
|  | Concrete Multicrack(Transient) | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  |  |  |  |
|  | Stress Resultant |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Tresca | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
|  | Optimised Implicit Von Mises | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
|  | Mohr-Coulomb | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
|  | Modified <br> Mohr-Coulomb |  |  |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
|  | Drucker-Prager | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
|  | Modified Cam-clay |  |  |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ |  |
|  | Volumetric Crushing/Foam |  |  |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
|  | Stress Potential (Von Mises, Modified Von Mises) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |


|  | Interface (2D) | $\checkmark$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | Creep (General) | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
|  | Creep (AASHTO) | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  |  |  |
|  | Creep (CEB-FIP) | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  |  |  |
|  | Creep (Chinese) | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  |  |  |
|  | Creep (Eurocode) | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  |  |  |
|  | Creep (IRC) | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  |  |  |
|  | Damage (Simo, | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
|  | Oliver) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Viscoelastic |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
|  | Shrinkage (CEB- | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  |
|  | FIP, Eurocode. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| General, User) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


|  | (TSSIE,TSSIA) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | Target Stress/Strain <br> (TSSIG) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Temperature <br> TEMP,TMPE) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Field Load |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Temp Dependent <br> Load |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Overburden | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  |
|  | Phreatic Surface | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  |
|  | Total Lagrangian | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ |  |
| Nonlinear <br> geometry | Updated <br> Lagrangian | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ |  |
|  | Eulerian | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
|  | Co-rotational | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ |  |  |  |  |  |  |  |
|  | Explicitly <br> Integrated |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Integration |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| schemes | Numerically <br> Integrated | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Consistent Mass <br> (default) | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ |
|  | Lumped Mass | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |

* Linear anisotropic and rigidities material properties for elements marked are supported in LUSAS Solver but not supported in LUSAS Modeller.

| 3D Continuum Element Summary |  | 3D Continuum |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\|\vec{F}\|$ |  |  | $\stackrel{\text { n }}{\substack{2}}$ | $\left\|\begin{array}{c} \boldsymbol{\alpha} \\ \dot{y} \boldsymbol{y} \end{array}\right\|$ | ⿹弋工⿹勹巳u | $\sum_{i x}^{y}$ | 体 | $\stackrel{5}{7}$ |  |  |  | 翟 |
| Product Version | $\begin{aligned} & \text { LT, Standard (S) } \\ & \text { or Plus (+) } \end{aligned}$ | S | ＋ | S | ＋ | S | ＋ | S | ＋ | ＋ | ＋ | ＋ | ＋ | ＋ |
| Nodal freedoms | U，V |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | U，V，W | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
| （corner） | U，V，W（P） |  |  |  |  |  |  |  |  |  |  |  |  | $\checkmark$ |
| Material properties | Linear（Isotropic） | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Linear（Orthotropic） | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Linear（Anisotropic） | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |
|  | Linear（Rigidities） |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Matrix |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Joint |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Concrete（Multi－crack） | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |
|  | Concrete（Multi－ crack）Transient | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |  |  |  |
|  | Stress Resultant |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Tresca | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Optimised Implicit Von Mises | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Mohr－Coulomb | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Modified Mohr－Coulomb | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |  | $\checkmark$ |
|  | Drucker－Prager | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Modified Cam－clay | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |  | $\checkmark$ |
|  | Volumetric Crushing／Foam | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Stress Potential（Von Mises， <br> Modified Von Mises | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |


|  | Hill, Hoffman) |  |  |  |  |  |  |  |  |  |  |  |  |  |
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|  | Creep (General) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ |
|  | Creep (AASHTO) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
|  | Creep (CEB-FIP) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
|  | Creep (Chinese) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
|  | Creep (Eurocode) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
|  | Creep (IRC) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
|  | Damage | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Viscoelastic | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |
|  | Shrinkage (CEB-FIP, Eurocode, General, User) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |
|  | Ko Initialisation | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |  | $\checkmark$ |
|  | Elasto-plastic interface | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  |  |  |  | $\checkmark$ |
|  | Rubber (Ogden, Mooney-Rivlin, Neo- Hookean, Hencky |  |  |  |  |  |  | $\checkmark$ |  |  |  |  |  |  |
|  | Generic Polymer | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |
|  | Resin Cure Model |  |  |  |  |  |  |  | - | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
|  | Composite (Composite Solid) |  |  |  |  |  |  |  | - | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
|  | Composite (Composite Shell) |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Field |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Loading types | Prescribed Value (PDSP,TPDSP) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Concentrated Loads (CL) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Element Loads |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | $\begin{aligned} & \begin{array}{l} \text { Distributed Load } \\ \text { (UDL) } \end{array} \\ & \hline \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | $\begin{aligned} & \begin{array}{l} \text { Distributed Load } \\ \text { (FLD) } \end{array} \\ & \hline \end{aligned}$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Body Force (CBF,BFP,BFPE) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Velocity (VELO) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Acceleration (ACCE) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | $\begin{aligned} & \text { Initial Stress/Strain } \\ & \text { (SSI,SSIE) } \\ & \hline \end{aligned}$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | $\begin{aligned} & \begin{array}{l} \text { Initial Stress/Strain } \\ \text { (SSIG) } \end{array} \\ & \hline \end{aligned}$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |
|  | $\begin{aligned} & \text { Residual Stress } \\ & \text { (SSR,SSRE) } \\ & \hline \end{aligned}$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |


|  | Residual Stress (SSRG) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Target Stress/Strain (TSSIE,TSSIA) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | $\begin{aligned} & \text { Target Stress/Strain } \\ & \text { (TSSIG) } \end{aligned}$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | - | $\checkmark$ |
|  | Temperature (TEMP,TMPE) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Field Load |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Temp Dependent Load |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Overburden | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |
|  | Phreatic Surface | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |
| Nonlinear geometry | Total Lagrangian | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |  | $\checkmark$ |
|  | Updated Lagrangian | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |  | $\checkmark$ |
|  | Eulerian | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ |
|  | Co-rotational | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |
| Integration schemes | Explicitly Integrated |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Numerically Integrated | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| Mass modelling | Consistent Mass (default) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |
|  | Lumped Mass | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |


| Plate, Shell and Membrane Element Summary |  | Plates |  |  | Shells |  |  |  |  |  |  |  |  | $\begin{gathered} \text { Membrane } \\ \mathrm{s} \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & U \\ & U N \end{aligned}$ | $\begin{aligned} & \infty \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | 敛\| |  | $\left\|\begin{array}{l} \underset{N}{2} \\ \hat{n} \\ \tilde{n}_{n}^{n} \end{array}\right\|$ | $\begin{aligned} & 0 \\ & \stackrel{\rightharpoonup}{-2} \\ & \underset{\sim}{2} \end{aligned}$ |  | $\left.\begin{array}{\|c} \boldsymbol{N} \\ \hat{N} \end{array} \right\rvert\,$ | $\left\|\begin{array}{c} 6 \\ 0 \\ 0 \\ \mid \end{array}\right\|$ | $\stackrel{7}{6}$ | - | $\sum_{n}^{\infty}$ | 帱 |
| Product <br> Version | $\begin{aligned} & \text { LT, Standard (S) } \\ & \text { or Plus (+) } \end{aligned}$ | S | S | S | S | S | S | + | + | S | + | S | + | S | S |
| Nodal | U, V |  |  |  |  |  |  |  |  |  |  |  |  | $\checkmark$ |  |
| Freedoms | U, V, W |  |  |  |  |  |  |  |  |  |  |  |  |  | $\checkmark$ |
| (mid-side) | W, qx, qy |  | $\checkmark$ | $\checkmark$ |  |  |  |  |  |  |  |  |  |  |  |
|  | W, qx, qy (dq) | $\checkmark$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | U, V, W, qx, qy |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | U, V, qz |  |  |  |  | $\checkmark$ |  |  |  |  |  |  |  |  |  |
|  | U, V, qz (dU) |  |  |  | $\checkmark$ |  |  |  |  |  |  |  |  |  |  |
|  | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}, \mathrm{qx}, \mathrm{qy}, \\ & \mathrm{qz} \end{aligned}$ |  |  |  |  |  | $\checkmark$ |  |  |  |  |  |  |  |  |
|  | $\begin{aligned} & \mathrm{U}, \mathrm{~V}, \mathrm{~W}(\mathrm{U}, \mathrm{~V}, \mathrm{~W}, \\ & \mathrm{q} 1, \mathrm{q} 2) \end{aligned}$ |  |  |  |  |  |  |  | $\checkmark$ |  |  |  |  |  |  |
|  | U, V, W (q1,) |  |  |  |  |  |  | $\checkmark$ |  |  |  |  |  |  |  |
|  | $\mathrm{U}, \mathrm{V}, \mathrm{W}, ~ q a, ~ q b$ $(\mathrm{U}, \mathrm{V}, \mathrm{W}, ~ q x, ~ q y$, $\mathrm{qz})$ |  |  |  |  |  |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
| Material properties | Linear (Isotropic) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Linear (Orthotropic) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |
|  | Linear (Anisotropic) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |
|  | Linear (Rigidities) | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |  |  | $\checkmark$ |
|  | Matrix |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Joint |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Concrete (Multicrack) |  |  |  |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
|  | Stress Resultant |  |  |  | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ |  |  |  |  |  |  |
|  | Tresca |  |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
|  | Optimised Implicit Von Mises |  |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
|  | Mohr-Coulomb |  |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |


|  | Drucker-Prager |  |  |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Volumetric Crushing/Foam |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Stress Potential (Von-Mises, Modified Von Mises) |  |  |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
|  | Stress Potential(Hill, Hoffman) |  |  |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
|  | Creep (General) |  |  |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
|  | Creep (AASHTO) |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
|  | $\begin{aligned} & \text { Creep } \\ & \text { (CEB_FIP_90) } \\ & \hline \end{aligned}$ |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
|  | Creep (Chinese) |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
|  | Creep (Eurocode) |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
|  | Creep (IRC) |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
|  | Damage |  |  |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
|  | Viscoelastic |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Shrinkage (CEB- FIP_90, Eurocode_2, General, User) |  |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Ko Initialisation |  |  |  | . | . | $\cdot$ | . | $\cdot$ | . | . | . | . | . |  |  |
|  | Rubber (Ogden, Mooney-Rivlin, Neo-Hookean, Hencky) |  |  |  |  |  |  |  |  |  |  |  |  |  | $\checkmark$ |  |
|  | Generic Polymer |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Composite <br> (Composite Shell) |  |  |  |  |  |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
|  | Field |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Loading types | Prescribed Value (PDSP,TPDSP) | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Concentrated <br> Loads (CL) | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | $\begin{aligned} & \text { Element Load } \\ & \text { (ELDS) } \end{aligned}$ |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  |  |  |  |  |  |  |  |
|  | Distributed Load (UDL) | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | $\begin{aligned} & \text { Distributed Load } \\ & \text { (FLD) } \end{aligned}$ |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  |  |  |  |  |  | $\checkmark$ |  |
|  | Body Force (CBF,BFP,BFPE) | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |


|  | Velocity (VELO) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { Acceleration } \\ & \text { (ACCE) } \end{aligned}$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | $\begin{aligned} & \text { Initial } \\ & \text { Stress/Strain } \\ & \text { (SSI,SSIE) } \\ & \hline \end{aligned}$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |  |  | $\checkmark$ | $\checkmark$ |
|  | Initial <br> Stress/Strain <br> (SSIG) |  |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | $\begin{aligned} & \hline \text { Residual Stress } \\ & \text { (SSR,SSRE) } \\ & \hline \end{aligned}$ |  |  |  |  |  |  | $\checkmark$ |  |  |  |  |  |  |  |
|  | $\begin{aligned} & \text { Residual Stress } \\ & \text { (SSRG) } \end{aligned}$ |  |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
|  | Target <br> Stress/Strain <br> (TSSIE,TSSIA) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |  |  | $\checkmark$ | $\checkmark$ |
|  | Target Stress/Strain (TSSIG) |  |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Temperature (TEMP,TMPE) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Field Load |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Temp Dependent Loads |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Overburden |  |  |  |  |  |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
|  | Phreatic surface |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
| Nonlinear geometry | Total Lagrangian |  |  |  | $\checkmark$ | $\checkmark$ |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
|  | Updated Lagrangian |  |  |  | $\checkmark$ |  |  |  | $\checkmark$ |  |  |  |  |  |  |
|  | Eulerian |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Co-rotational |  |  |  |  |  |  | $\checkmark$ |  |  |  |  |  |  |  |
| Integration schemes | Explicitly Integrated |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Numerically Integrated | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| Mass modelling | Consistent Mass (default) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |
|  | Lumped Mass | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |


|  |  | Joints |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Joint Element Summary |  |  |  |  |  |  |  |  |  |
|  |  | 気 | 気 | ⿹ㅗㅅ | $\underset{y}{x}$ | － | $$ | $\stackrel{7}{7}$ | －ت |
| Product version | LT，Standard（S）or Plus（＋） | S | S | S | S | S | S | S | ＋ |
| Nodal freedoms | U，V | $\checkmark$ |  |  | $\checkmark$ |  |  |  |  |
|  | U，V，W |  |  |  |  |  | $\checkmark$ |  |  |
|  | U，V，qz |  | $\checkmark$ |  |  | $\checkmark$ |  |  |  |
|  | W，qx，qy |  |  | $\checkmark$ |  |  |  |  |  |
|  | U，V，W，qx，qy |  |  |  |  |  |  |  |  |
|  | U，V，W，qx，qy，qz |  |  |  |  |  |  | $\checkmark$ |  |
|  | U，V，W，q1，q2 |  |  |  |  |  |  |  | $\checkmark$ |
| Material properties | Linear |  |  |  |  |  |  |  |  |
|  | Matrix（Stiffness，Mass， Damping）＊ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Joint（Stiffness，General） | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Joint（Dynamic，General） | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Joint（Elasto－Plastic） | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Joint（Nonlinear Contact） | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Joint（Nonlinear Friction） | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Viscous damping | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Lead－Rubber | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Friction Pendulum | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Multilinear elastic | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Axial force dependent multilinear elastic | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Concrete |  |  |  |  |  |  |  |  |
|  | Elasto－Plastic |  |  |  |  |  |  |  |  |
|  | Creep |  |  |  |  |  |  |  |  |
|  | Damage |  |  |  |  |  |  |  |  |
|  | Viscoelastic |  |  |  |  |  |  |  |  |
|  | Shrinkage |  |  |  |  |  |  |  |  |
|  | Volumetric Crushing／Foam |  |  |  |  |  |  |  |  |
|  | Rubber |  |  |  |  |  |  |  |  |
|  | Composite |  |  |  |  |  |  |  |  |


|  | Field |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Loading types | Prescribed value (PDSP,TPDSP) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Concentrated Load (CL) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Element Load |  |  |  |  |  |  |  |  |
|  | Distributed Load |  |  |  |  |  |  |  |  |
|  | Body Force(CBF) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Body Force (BFP,BFPE) |  |  |  |  |  |  |  |  |
|  | Velocities (VELO) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Acceleration (ACCE) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Initial Stress/Strain (SSI,SSIE) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Initial Stress/Strain (SSIG) |  |  |  |  |  |  |  |  |
|  | Residual Stress |  |  |  |  |  |  |  |  |
|  | Target Stress/Strain (TSSIE,TSSIA) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Target Stress/Strain (TSSIG) |  |  |  |  |  |  |  |  |
|  | Temperature (TEMP,TMPE) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Field Load |  |  |  |  |  |  |  |  |
|  | Temp Dependent Load |  |  |  |  |  |  |  |  |
| Nonlinear | Total Lagrangian |  |  |  |  |  |  |  |  |
|  | Updated Lagrangian |  |  |  |  |  |  |  |  |
|  | Eulerian |  |  |  |  |  |  |  |  |
|  | Co-rotational |  |  |  |  |  |  |  |  |
| Integration | Explicitly Integrated |  |  |  |  |  |  |  |  |
|  | Numerically Integrated | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| Mass | Consistent Mass (default) |  |  |  |  |  |  |  |  |
|  | Lumped Mass | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |

* Supported in LUSAS Solver but not supported in LUSAS Modeller for all joints listed.

|  |  | Field |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thermal／Field Element Summary |  | Non | 枵\| | $\begin{aligned} & \text { Nan } \\ & \\ & \end{aligned}$ |  | $\left\|\begin{array}{c} \underset{y}{x} \\ \text { cin } \end{array}\right\|$ | $\left\|\begin{array}{l} \underset{y}{2} \\ \underset{y}{c} \end{array}\right\|$ |  |  | 部 | 武\| | 曷, | $\stackrel{i}{2}$ | $\left\|\begin{array}{c} \infty \\ \underline{1} \\ \mathbf{1} \end{array}\right\|$ |  | 骎 |  |  |  | $\left.\begin{array}{\|c\|} \infty \\ y_{1}^{2} \\ 0 \\ 0 \\ 0 \\ 1 \\ \end{array} \right\rvert\,$ |
| Product version | $\begin{aligned} & \text { LT, Standard (S) } \\ & \text { or Plus (+) } \end{aligned}$ | S | S | S | S | S | S | S | S | S | S | S | S | S | ＋ | ＋ | ＋ | ＋ | S | S |
| Freedoms | F | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| Material properties | Composite |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |
|  | Field（Isotropic） | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Field（Isotropic Concrete） | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Field （Orthotropic） |  |  |  |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Field（Orthotropic Concrete） |  |  |  |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Field（Linear Conv／Rad） |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Field（Arbitary Conv／Rad） |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Loading types | $\begin{aligned} & \text { Prescribed } \\ & \text { (TPDSP) } \end{aligned}$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Rate of heat inflow， concentrated （RGN） | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Face heat and water fluxes（FFL） | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | $\begin{aligned} & \text { Rate of heat } \\ & \text { inflow, per unit } \\ & \text { volume (RBC, } \\ & \text { RBV, RBVE) } \\ & \hline \end{aligned}$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Temperature <br> （TEMP， <br> TMPE） | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | $\begin{aligned} & \text { Environmental } \\ & \text { conditions (ENVT) } \end{aligned}$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | $\begin{aligned} & \hline \text { Temp Dep Load } \\ & \text { (TDET/RIHG) } \end{aligned}$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |


| Schemes | Numerically <br> Integrated | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Specific <br> heat | Consistent <br> (default) | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
|  | Lumped | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |


|  |  | Hygro-Thermal |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Hygro-Thermal |  |  |  |  |  |  |  |
| Element Summary |  |  |  |  |  |  |  |


|  |  | Interface |  |  |  |  |  |  |  | Mass |  |  |  | Rigid Slideline |  | $\begin{gathered} \text { Phreati } \\ \text { c } \\ \hline \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Interface, Non- <br> Structural Mass, Rigid <br> Slideline and Phreatic <br> Element Summary |  |  |  |  | $\left\|\begin{array}{c} \infty \\ \sqrt[n]{2} \\ \tilde{n} \\ \end{array}\right\|$ | 象 |  |  | $\left\|\underset{\sum_{a}}{ }\right\|$ | $\sum_{i=1}^{n}$ |  |  | TM3/6, OM4/8 | $\left\|\begin{array}{c} \underset{\sim}{\hat{N}} \end{array}\right\|$ |  | $\left\|\begin{array}{c} \tilde{i} \\ \underset{i}{2} \end{array}\right\|$ |  |
| Product version | $\begin{aligned} & \text { LT, Standard (S) } \\ & \text { or Plus (+) } \end{aligned}$ | + | + | + | + | + |  | + | + | + | + | + | + | + | + | + | + |
| Nodal freedoms | U, V | $\checkmark$ | $\checkmark$ |  |  |  |  |  | $\checkmark$ |  |  | $\checkmark$ |  | $\checkmark$ |  |  |  |
|  | U, V, P |  |  |  |  | $\checkmark$ |  |  |  |  |  |  |  |  |  |  |  |
|  | U, V, W |  |  | $\checkmark$ | $\checkmark$ |  |  |  |  | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  | $\checkmark$ |  |  |
|  | U,V,W, P |  |  |  |  |  |  | $\checkmark$ |  |  |  |  |  |  |  |  |  |
|  | U, V, qz |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | W, qx, qy |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | U, V, W, qx, qy |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | U, V, W, qx, qy, qz |  |  |  |  |  |  |  |  |  | $\checkmark$ |  |  |  |  |  |  |
|  | U, V, W, q1, q2 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Material properties | Linear |  |  |  |  |  |  |  |  |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  |
|  | Matrix |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Joint |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Mass |  |  |  |  |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |  |
|  | Concrete |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Elasto-Plastic |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Creep |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Damage |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Shrinkage |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Interface | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  |  |  |  |  |  |  |  |  |
|  | Rubber |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Generic Polymer |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Stress Potential |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Composite |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Field |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Loading types | Prescribed value (PDSP,TPDSP) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  |
|  | Concentrated Loads | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  | $\checkmark$ |  |  |  |  |  |  |  |  |  |


|  | (CL) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | Element Load |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Distributed Load |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Body Force (CBF) |  |  |  |  |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |  |
|  | Body Force <br> (BFP,BFPE) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Velocity (VELO) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  |
|  | Acceleration (ACCE) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |  |  |  |  | $\checkmark$ | $\checkmark$ |  |  |
|  | Initial Stress/Strain <br> (SSI,SSIE) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Initial Stress/Strain <br> SSIG) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Residual Stress |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Target Stress/Strain <br> (TSSIE,TSSIA) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Target Stress/Strain <br> (TSSIG) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Temperature <br> (TEMP,TMPE) | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |  |  |  |  |  |  |  |  |  |
|  | Field Load |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Temp Dependent Load |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  | $\checkmark *$ | $\checkmark *$ |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

* Dependent upon the other surface (deformable surface) that the element is in contact with.


## Chapter 1 : Bar Elements.

## 2D Structural Bar Elements

## General



## Element Group Bars

Element Structural Bars
Subgroup
Element Straight and curved isoparametric bar elements in 2D which can
Description accommodate varying cross sectional area.
Number Of 2 or 3 .
Nodes
Freedoms U, V at each node
Node X, Y at each node
Coordinates

## Geometric Properties

A1 ... An Cross sectional area at each node.
SF1, MF1 Optional scale factor applied to the areas in the calculation of the stiffness and mass matrices

## Material Properties

Linear Isotropic
Matrix Not applicable
Joint Not applicable
Concrete Not applicable
Elasto-Plastic Stress resultant Not applicable
Tresca:
MATERIAL PROPERTIES NONLINEAR 61


## Loading

Prescribed Value PDSP, TPDSP
Concentrated CL Loads
Element Loads Not applicable.
Distributed Loads Not applicable.
Body Forces CBF

BFP, BFPE $\quad$ Body force potentials at nodes/for element. $0,0,0$, 0, Xcbf, Ycbf
Velocities. Vx, Vy at nodes.
Acceleration Ax, Ay at nodes.
Initial stresses/strains at nodes/for element. Fx, $\varepsilon x$ x, $\sigma x, \varepsilon x$
$\left.\begin{array}{rll} & \text { SSIG } & \text { Initial stresses/strains at Gauss points. F, } \varepsilon x, \sigma x, \\ & & \varepsilon x\end{array}\right)$

## LUSAS Output

Solver Force (default): Fx
Strain: $\varepsilon x$
Modeller $\quad$ See Results Tables (Appendix K)

## Local Axes

- Standard line element


## Sign Convention

- Standard bar element


## Formulation

## Geometric Nonlinearity

$$
\begin{aligned}
\text { Total Lagrangian } & \text { For large displacements and small strains } \\
\text { Updated } & \text { Not applicable. } \\
\text { Lagrangian } &
\end{aligned}
$$

Eulerian Not applicable.<br>Co-rotational For large displacements and small strains.

## Integration Schemes

Stiffness Default.
Fine (see
Options).
Mass Default.
Fine (see Options).

1-point (BAR2), 2-point (BAR3).
2-point (BAR2).

2-point (BAR2), 3-point (BAR3).
As default.

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule for element.
55 Outputs strains as well as stresses
87 Total Lagrangian geometric nonlinearity.
105 Lumped mass matrix.
229 Co-rotational geometric nonlinearity.

## Notes on Use

1. The bar formulation is based on the standard isoparametric approach. The variation of axial force is constant for BAR2, and linear for BAR3.
2. Since the 3-noded element has no bending stiffness mechanisms may occur when used as 'stand alone' elements if the central node is not constrained in some way.
3. When the BAR2 element is used with either varying cross-sectional area or temperature dependent material properties, the 2-point Gauss rule should be utilised. This provides an improved representation of the variation of the material properties along the length of the element.
4. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties
and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command.

## Restrictions

$\square$ Ensure mid-side node centrality

- Avoid excessive element curvature


## Recommendations on Use

- The 2-node elements are the most effective bar elements for modelling 'stand-aloneelements' such as members of trusses or bars connecting two discrete structures.
- They can be used to model cables in cable-stayed structures.
- Both the 2-noded and 3-noded elements are suitable for modelling reinforcement with continuum elements e.g. BAR3 may be used with QPM8 for analysis of reinforced concrete structures, or for modelling rock bolts surrounding an excavation


## Theory

For additional information see the LUSAS Theory Manual

## 3D Structural Bar Elements

## General

Element Name
TY, V


BRS3


## Element Group <br> Bars

Element Structural Bars
Subgroup
Element Straight and curved isoparametric bar elements in 3D which can
Description accommodate varying cross-sectional area.
Number Of
2 or 3.
Nodes
Freedoms U, V, W at each node
Node X, Y, Z at each node.
Coordinates
(Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic)
Not applicable
STRESS POTENTIAL VON_MISES (Isotropic: von Mises, Modified von Mises)
CREEP PROPERTIES (Creep)
DAMAGE PROPERTIES SIMO, OLIVER (Damage)
VISCO ELASTIC PROPERTIES
SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
MATERIAL PROPERTIES NONLINEAR 104

## Loading

Prescribed Value PDSP, TPDSP Concentrated CL Loads Element Loads Not applicable

## Distributed Loads Not applicable

Body Forces CBF

BFP, BFPE
Velocities VELO
Accelerations ACCE
Initial SSI, SSIE
Stress/Strains

Prescribed variable. U, V, W at each node.
Concentrated loads. Px, Py, Pz at each node.

Constant body forces for element. Xcbf, Ycbf, Zcbf, $\Omega_{\mathrm{x}}, \Omega \mathrm{y}, \Omega_{\mathrm{z}}, \alpha \mathrm{x}, \alpha \mathrm{y}, \alpha \mathrm{z}$
Body force potentials at nodes/for element. 0, 0, 0, 0, Xcbf, Ycbf, Zcbf
Velocities. Vx, Vy, Vz at nodes.
Acceleration Ax, Ay, Az at nodes.
Initial stresses/strains at nodes/for element. Fx, $\varepsilon x, \sigma x, \varepsilon x$

|  | SSIG | Initial stresses/strains at Gauss points. F, $\varepsilon x, \sigma x$, |
| ---: | :--- | :--- |
|  |  | $\varepsilon x$ |

## LUSAS Output

Solver Force (default): Fx
Strain: Ex
Modeller See Results Tables (Appendix K)

## Local Axes

- Standard line element


## Sign Convention

- Standard bar element


## Formulation

## Geometric Nonlinearity

$$
\begin{aligned}
\text { Total Lagrangian } & \text { For large displacements and small strains } \\
\text { Updated } & \text { Not applicable. } \\
\text { Lagrangian } &
\end{aligned}
$$

Eulerian Not applicable.<br>Co-rotational For large displacements and small strains.

## Integration Schemes

Stiffness Default.
Fine (see Options).
$\begin{array}{ll}\text { Mass } & \text { Default. } \\ & \text { Fine (see Options). }\end{array}$

1-point (BRS2), 2-point (BRS3). 2-point (BRS2). 2-point (BRS2), 3-point (BRS3). As default.

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule for element.
55 Outputs strains as well as stresses
87 Total Lagrangian geometric nonlinearity.
105 Lumped mass matrix.
229 Co-rotational geometric nonlinearity.

## Notes on Use

1. The bar formulation is based on the standard
2. Since the 3-noded element has no bending stiffness, mechanisms may occur, when used as 'stand alone' elements, if the central node is not constrained in some way.
3. When the BRS2 element is used with either varying cross-sectional area or temperature dependent material properties, the 2-point Gauss rule should be utilised. This provides an improved representation of the variation of the material properties along the length of the element.
4. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command.

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature


## Recommendations on Use

- The 2-node elements are the most effective bar elements for modelling 'stand-aloneelements' such as members of trusses or bars connecting two discrete structures.
- They can be used to model cables in cable-stayed structures.
- Both the 2-noded and 3-noded elements are suitable for modelling reinforcement with continuum elements e.g. BRS3 may be used with HX20 for analysis of reinforced concrete structures, or for modelling rock bolts surrounding an excavation.


## Chapter 2: Beam Elements.

## 2D Engineering Grillage Thick Beam Element

## General

## Element Name GRIL



## Element Group Beams

Element Engineering Beams

## Subgroup

Element A straight grillage element for which shear deformations are included.
Description
The geometric properties are constant along the length.
Number Of
2 with moment release end conditions
Nodes
End Releases
The element node numbers should be followed by: R restrained (default), F free defined in the order $\theta \mathrm{y}$ at node 1 and then $\theta \mathrm{y}$ at node 2 related to local element axes
Freedoms $\mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}$ : at each node.
Node X, Y: at each node.
Coordinates

## Geometric Properties

A, Iyy, Izz, Jxx, Asz, EFW for element
ASF1,SF2,SF3,SF4, SF5,SF6 Optional scale factors applied to the geometric MF1,MF2,MF3,MF4, MF5,MF6 properties in the calculation of the stiffness and mass matrices
A Cross sectional area
Iyy, Izz 2nd moments of area about local y, z axes (see Definition and Notes)
Jxx Torsional constant
Asz Effective shear area on local yz plane in local z

directions<br>EFW Equivalent plate width

## Material Properties

Linear Isotropic:<br>Matrix Not applicable<br>Joint Not applicable<br>Concrete Not applicable<br>Elasto-Plastic Not applicable<br>Creep Not applicable<br>Damage Not applicable<br>Viscoelastic Not applicable<br>Shrinkage Not applicable<br>Rubber Not applicable<br>Generic Polymer Not applicable<br>Composite Not applicable.

## Loading

Prescribed Value PDSP, TPDSP
Concentrated CL
Loads
Element Loads ELDS

Prescribed variable. W, $\theta \mathrm{x}, \theta \mathrm{y}$ : at nodes.
Concentrated loads. Pz, Mx, My: at nodes (global).

## Element loads

LTYPE, S1, Pz, Mx, My
LTYPE=11: point loads and moments in local directions.
LTYPE=12: point loads and moments in global directions.
LTYPE, $0, \mathrm{Wz}, \mathrm{Mx}, 0$

| Distributed Loads | UDL | Uniformly distributed loads. Wz: Force/unit <br> length in local directions for element (Local z <br> and global Z are coincident). |
| ---: | :--- | ---: |
|  | FLD, FLDG | Not applicable. <br> Constant body forces for element. Zcbf |
| Body Forces | CBF | BFP, BFPE |$\quad$| Not applicable. |
| :--- |
| Velocities | VELO $\quad$| Velocities. Vz: at nodes. |
| :--- |
| Acceleration Az: at nodes. |

## Output

Solver Force (default): Fz, Mx, My: in local directions (see Notes). Element output is with respect to the beam centre line.
Modeller See Results Tables (Appendix K).

## Local Axes

- Standard line element


## Sign Convention

$\square$ 2D engineering grillage thick beam element. Positive external forces and moments acting on the element nodes are in the direction of the local element axes.

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Explicitly integrated.

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

## Notes on Use

1. The element formulation is based on the standard grillage element formulation. The force variations along the element are linear shear force, constant torsion and quadratic bending moment.
2. The displacement variations along the element are linear torsional rotations and cubic transverse flexural displacements.
3. Internal forces and moments are output at intervals of $1 / 10$ th of the element length by specifying the Gauss point option from the Output button on the File > LUSAS datafile dialog.
4. The second moment of area about local $z$, (Izz), is only required when assembling the mass matrix.
5. Strains are not available for GRIL elements.
6. Though this element cannot model nonlinear behaviour it can be mixed with other elements in a nonlinear analysis.
7. For restrictions on the use of Wood-Armer with grillages refer to the LUSAS User Guide and Theory Manual.
8. The element has constant material properties along its length. For analyses utilising temperature dependent material properties, the temperature used is the average of the nodal values.
9. A moment release option permits modelling of internal hinges (torsional rotations cannot be released). See Number of Nodes section.
10. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command.

## Restrictions

The element does not model material or geometric nonlinear effects.

## Recommendations on Use

The element can be used to model two dimensional grillage type structures. Linear, eigen, and dynamic analysis procedures can be used with GRIL elements.

## 2D Thick Beam Elements

Element Name BMI2
Element

Element 2D Thick Beams | Straight and curved isoparametric degenerate thick beam elements in 2D |
| ---: | :--- |
| for which shearing deformations are included. The elements can |
| accommodate varying geometric properties along the length. |

## Geometric Properties

A, Izz, Asy, ey for element

SF1,SF2,SF3,SF4, Optional scale factors applied to the geometric properties in the MF1,MF2,MF3,MF4 calculation of the stiffness and mass matrices
A Cross sectional area
Izz 2nd moment of area about local z-axis (see Definition)
Asy Effective shear area on local yz plane in local y directions
ey Eccentricity from beam xz-plane to nodal line (+ve in +ve local ydirection)
Note: For MATERIAL MODEL 29 additional geometric properties are appended to the previous 8 (BMI2) or 12 (BMI3) geometric properties (see Notes, Assumptions and Limitations).

## Material Properties

|  |  | MATERIAL PROPERTIES (Elastic: Isotropic) |
| :---: | :---: | :---: |
| Matrix | Not applicable |  |
| Joint | Not applicable |  |
| Concrete | Not applicable |  |
| Elasto-Plastic | Stress resultant | MATERIAL PROPERTIES NONLINEAR 29 (Elastic: Isotropic, Plastic: Resultant) (ifcode=1 or 2, see Assumptions and Limitations) |
| Creep | AASHTO | MATERIAL PROPERTIES NONLINEAR 86 AASHTO <br> (Concrete creep model to AASHTO code of Practice) |
|  | CEB-FIP | MATERIAL PROPERTIES NONLINEAR 86 CEB-FIP <br> (Concrete creep model to CEB-FIP Model Code 1990) |
|  | Chinese | MATERIAL PROPERTIES NONLINEAR 86 CHINESE <br> (Chinese creep model to Chinese Code of Practice) |
|  | Eurocode | MATERIAL PROPERTIES NONLINEAR 86 EUROCODE <br> (Concrete creep model to EUROCODE_2) |
|  | IRC | MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice) |

Damage Not applicable
Viscoelastic Not applicable

Rubber Not applicableGeneric Polymer Not applicableComposite Not applicable

SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER

## Loading

Prescribed Value PDSP, TPDSP
Concentrated CL
Loads
Element Loads ELDS
Prescribed variable. U, V, $\theta \mathrm{z}$ : at nodes. Concentrated loads. Px, Py, Mz: at nodes (global).
Element loadson nodal line (load type number

LTYPE *10 defines the corresponding element load type on beam axis, see Notes)
LTYPE, S1, Px, Py, Mz
LTYPE=11: point loads and moments in local directions.
LTYPE=12: point loads and moments in global directions.
LTYPE, $0, \mathrm{Wx}, \mathrm{Wy}, 0$
LTYPE=21: uniformly distributed loads in local directions.
LTYPE=22: uniformly distributed loads in global directions.
LTYPE=23: uniformly distributed projected loads in global directions
LTYPE, S1, Wx1, Wy1, 0, S2, Wx2, Wy2, 0
LTYPE=31: distributed loads in local directions.
LTYPE=32: distributed loads in global directions.
LTYPE=33: distributed projected loads in global directions
LTYPE, S1, Wx, Wy, 0
LTYPE=41: trapezoidal loads in local directions.
LTYPE=42: trapezoidal loads in global directions.
LTYPE=43: trapezoidal projected loads in global directions

| Distributed Loads | UDL | Uniformly distributed loads. Wx, Wy: <br> forces/unit length for element in local <br> directions. |
| ---: | :--- | :--- |
|  |  | FLD |
| Body Forces | CBF | Not applicable. <br> Constant body forces for element. |
|  |  | BFP, BFPE |
| Velocities | VELO | Not applicable. |

## LUSAS Output

Solver Stress resultants (default): Fx, Fy, Mz: axial force, shear force and moment in local directions.
Strain: $\varepsilon x, \varepsilon y, \psi z$ : Axial, shear and flexural strains in local directions. By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal
axes.
Modeller See Results Tables (Appendix K).

## Local Axes

$\square$ Standard line element

## Sign Convention

- 2D engineering beam element


## Formulation

## Geometric Nonlinearity

| Total Lagrangian | For large displacements and large rotations (see Notes) |
| ---: | :--- |
| Updated | Not applicable. |
| Lagrangian |  |
| Eulerian | Not applicable. |
| Co-rotational | For large displacements and large rotations |
| P-Delta | Displacements and rotations should be small (see Notes) |

## Integration Schemes

Stiffness Default. 1-point (BMI2), 2-point (BMI3).
Fine. Same as default.
Mass Default. 2-point (BMI2), 3-point (BMI3).
Fine. Same as default.
Note: A 3-point Newton-Cotes integration rule is also available for BMI3 using OPTION 134. This may be more applicable for infinitesimal strain, elasto-plastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory Manual.

## Mass Modelling

$\square$ Consistent mass (default).

- Lumped mass.


## Options

## 36 Follower loads

55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity. (see Notes)
102 Switch off load correction stiffness matrix due to centripetal acceleration
105 Lumped mass matrix.
134 Gauss to Newton-Cotes in plane (in the local x direction) integration for elements
157 Material model 29 (non cross-section elements), see Notes.
229 Co-rotational geometric nonlinearity.
403 Introduce residual bending flexibility correction for 2-node thick beam BMI21, see Assumptions and Limitations (on by default).
404 Compute equivalent nodal loading from equilibrium considerations for 2-node thick beam BMI21, see Assumptions and Limitations (on by default).
405 Specify geometric properties along beam centroidal axes
406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
418 Output stress resultants relative to beam centroidal axes for eccentric elements
421 P-Delta analysis, see Notes
432 Use P-Delta geometric stiffness matrix of thick beams for linear buckling analysis

## Notes, Assumptions and Limitations

1. The element is formulated from the degenerate continuum concept, i.e. enforcing directly the modified Timoshenko hypothesis for thick beams to the continuum theory. Plane cross-sections initially normal to the beam axis remain plane and undistorted (the shape of the cross-section remains unchanged) under deformation, but do not necessarily remain normal to the beam axis. Shearing deformations are included.
2. Input of geometric properties (OPTION 405) and loads (OPTION 406), and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axes. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line.
3. When OPTION 403 is specified to introduce residual bending flexibility correction (on by default), for BMI2, the axial force is constant, while the shear force and moment vary linearly along the length of the beam. For BMI3 the axial force, shear force and moment all vary linearly along the length.
4. When BMI2 is used together with OPTION 403 to introduce residual bending flexibility correction, its stiffness matrix is enhanced to the order of a cubic. Note that if OPTION 403 is used with eccentrically stacked elements, slippage can occur.
5. When BMI2 is used together with OPTION 404, loading that varies along the element length is accounted for in the force diagrams (i.e. for a beam under CBF or internal element loading). A post-processing technique has been introduced to obtain accurate quadratic bending moments for BMI3. For BMI2 (with OPTION 404) and BMI3, internal forces and moments are output at intervals of $1 / 10$ th of the element length by specifying the Gauss point option from the Output button of the LUSAS Datafile dialog.
6. The end releases for this element allow a joint to be modelled between adjacent elements. These joints allow rotation and translation of one beam with respect to another without load transferral. The rotations and translations remain in the local directions of the beam elements and support large deformations.
7. For nonlinear material model 29 the following geometric properties are appended to those already specified (see Geometric Properties).

- Ap, Zzzp, Sp at each node
- Ap Plastic area (=elastic area)
- Zzzp Plastic modulus for bending about z axes
- $\operatorname{Sp}$ Plastic area for shear $(\mathrm{Sp}=0)$.

Note that if eccentricity has been specified the plastic properties must be defined with reference to the nodal line and not the beam axes, i.e. the eccentricity is not used to automatically modify the plastic properties, they must be defined via modified geometry.
For nonlinear material model 29 the following ifcode parameters are applicable: ifcode $=1$ for circular hollow sections and ifcode $=2$ for solid rectangular sections.
8. Temperature dependent properties cannot be used with material model 29.
9. The rigidity matrix is evaluated explicitly from the geometric properties for both linear and nonlinear materials.
10. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command.
11. OPTION 36 is only applicable for use with element load types ELDS and UDL. Specifying this option makes these element loads follow the element geometry as the analysis progresses.
12. When a nonlinear material is used with this element the transverse shear stresses are excluded from the plasticity computations i.e. the transverse shear stresses are assumed to remain elastic. This means that if a nonlinear material is used in
applications where transverse shear tends to dominate the stress field the equivalent von Mises and maximum principal stresses can exceed the uniaxial yield stress.
13. When a step by step dynamic analysis is carried out using BMI elements with distributed loading, the "free body force diagrams" pertaining to applied loading, are not superimposed on the nodal values, to do so would lead to erroneous results until a steady state is reached. It should therefore be noted that different force diagrams will be obtained for BMI elements if static and dynamic analyses are directly compared.
14. OPTION 229 considers large displacements and large rotations using a co-rotational formulation. When both options 87 and 229 are true, a local Total Lagrangian formulation will be used within a global co-rotational framework. Note that OPTION 87 has no effect when specified without OPTION 229.
15. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command.
16. The P-Delta formulation is only applicable to lower order (2-noded) beams, higher order beams used in a P-Delta analysis will default to co-rotational GNL.
17. Partial fixities and rigid ends are defined via the ELEMENT TOPOLOGY data and follow on the same line after the end releases, for example:


The character $K$ is used to identify that the partial fixity stiffnesses $\widehat{k}_{12} \widehat{k}_{13}$ are being explicitly defined, while the character $N$ signifies that fixity factors, $n_{12} n_{1 a}$ are being defined. The fixity factors are used as follows:
$\hat{k}_{i j}=\frac{n_{i j}}{1-n_{i j}} \tilde{k}_{i j}$

The value of the factor $n_{i j j}$ ranges from zero for a pinned connection to 1.0 for a fully fixed connection.

The values $r_{1}$ and $r_{2}$ are the rigid end lengths at nodes 1 and 2 and $\lambda$ is the rigidity factor $(1.0=$ fully rigid, the default $)$. The factors m 1 and m 2 dictate how much mass to include for the rigid ends, full mass $=1.0$ (default $\mathrm{m}_{1}=\mathrm{m}_{2}=0.0$ ).

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature


## Recommendations on Use

- The element may be used for linear and nonlinear analysis of two dimensional beam, frame and arch structures.


## 2D Thick Beam Element with Quadrilateral Cross-Section

## General



BMI3X


## Geometric Properties

$\mathrm{y} 1, \mathrm{z} 1, \mathrm{y} 2, \mathrm{z} 2, \mathrm{y} 3, \mathrm{z} 3, \mathrm{y} 4, \mathrm{z} 4$ : local cross section coordinate pairs at each node; followed by nt 12 , nt14: specifying the number of Newton-Cotes integration points in the direction defined by the local cross-section points 1-2 and 1-4 (zero indicates default values). See Notes. Multiple quadrilateral cross-sections can be used to build up complex beam cross-sections.

Note. The coordinates of the cross section are numbered clockwise about the local $x$-axis (the beam nodal line). That is, a right-hand screw rule in the direction of increasing $x$.


## Material Properties

| Linear <br> Matrix <br> Joint | Isotropic: | Not applicable |
| ---: | :--- | :--- |
| Not applicable |  |  |$\quad$ MATERIAL PROPERTIES (Elastic: Isotropic)


|  | AASHTO | MATERIAL PROPERTIES NONLINEAR 86 AASHTO <br> (Concrete creep model to AASHTO code of Practice) |
| :---: | :---: | :---: |
|  | CEB-FIP | MATERIAL PROPERTIES NONLINEAR 86 CEBFIP <br> (Concrete creep model to CEB-FIP Model Code 1990) |
|  | Chinese | MATERIAL PROPERTIES NONLINEAR 86 CHINESE <br> (Chinese creep model to Chinese Code of Practice) |
|  | Eurocode | MATERIAL PROPERTIES NONLINEAR 86 EUROCODE <br> (Concrete creep model to EUROCODE_2) |
|  | IRC | MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice) |
| Damage |  | DAMAGE PROPERTIES SIMO, OLIVER (Damage) |
| Viscoelastic Shrinkage | Not applicable | SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER |
| Rubber Generic Polymer Composite | Not applicable <br> Not applicable <br> Not applicable |  |
| Loading |  |  |
| Prescribed Value | PDSP, TPDSP | Prescribed variable. U, V, $\theta$ z: at end nodes. dU at mid-side node. |
| Concentrated Loads | CL | Concentrated loads. Px, Py, Mz: at end nodes (global). dPx: at mid-side node (local). |
| Element Loads | ELDS | Element loads on nodal line (load type number LTYPE *10 defines the corresponding element load type on beam axis). |
|  |  | LTYPE, S1, Px, Py, Mz <br> LTYPE=11: point loads and moments in local directions. <br> LTYPE=12: point loads and moments in global directions. |



| TSSIG | Target stresses/strains at Gauss points. These <br> stresses/strains are specified in the same manner as <br> TSSIE and TSSIA. |
| ---: | :--- |
| Temperatures TEMP, TMPE | Temperatures at nodes/for element T, 0, dT/dy, 0, <br> To, 0, dTo/dy, 0 : in local directions. |
| Phreatic surface Face_Pressure | The fluid pressure is applied in the -y direction of <br> the element y axis. |
| Field Loads Not applicable. |  |

## LUSAS Output

Solver Stress resultants (default): Fx, Fy, Mz: axial force, shear forces and moment in local directions.
Continuum stresses: $\sigma x, \sigma x y$, in local directions.
Strain: $\varepsilon x, \varepsilon y, \psi z$ : Axial, shear and flexural strains in local directions.
Continuum strains: $\varepsilon x, \varepsilon x y$ in local directions.
By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal axes.
Modeller See Results Tables (Appendix K).

## Local Axes

- Standard line element


## Sign Convention

$\square$ Standard beam element

## Formulation

## Geometric Nonlinearity

Total Lagrangian
For large displacements, small rotations and small strains (see Notes).
Updated
For large displacements, large rotations and small strains.

Eulerian Not applicable.
Co-rotational For large displacements and large rotations

## P-Delta Displacements and rotations should be small (see Notes)

## Integration Schemes

| Stiffness | Default. | 1-point (BMI2X), 2-point (BMI3X). |
| :---: | :--- | :--- |
|  | Fine (see Options). | Same as default. |
| Mass | Default. | 2-point (BMI2X), 3-point (BMI3X). |
|  | Fine (see Options). | Same as default. |

A 3-point Newton-Cotes integration rule is also available for BMI3X using OPTION 134. This may be more applicable for infinitesimal strain, elasto-plastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory Manual

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

36 Follower loads
55 Output strains as well as stresses
87 Total Lagrangian geometric nonlinearity (see Notes).
102 Switch off load correction stiffness matrix due to centripetal acceleration
105 Lumped mass matrix
134 Gauss to Newton-Cotes in plane (in the local x direction) integration for elements.
139 Output yielded integration points only
229 Co-rotational geometric nonlinearity
403 Introduce residual bending flexibility correction for 2-node thick beam BMI21, see Assumptions and Limitations (on by default).
404 Compute equivalent nodal loading from equilibrium considerations for 2-node thick beam BMI2X, see Notes (on by default).
406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
418 Output stress resultants relative to beam centroidal axes for eccentric elements
421 P-Delta analysis, see Notes
432 Use P-Delta geometric stiffness matrix of thick beams for linear buckling analysis

## Notes on Use

1. The element is formulated from the degenerate continuum concept, i.e. enforcing directly the modified Timoshenko hypothesis for thick beams to the continuum theory. Plane cross-sections initially normal to the beam axis remain plane and undistorted (the shape of the cross-section remains unchanged) under deformation, but do not necessarily remain normal to the beam axis. Shearing deformations are included.
2. Input of loads (OPTION 406) and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axis. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line. Fiber stress/strain results are output at the actual location.
3. When OPTION 403 is specified to introduce residual bending flexibility correction (on by default), for BMI2X, the axial force is constant, while the shear force and moment vary linearly along the length of the beam. For BMI3X the axial force, shear force and moment all vary linearly along the length.
4. When BMI2X is used together with OPTION 403 to introduce residual bending flexibility correction, its stiffness matrix is enhanced to the order of a cubic. Note that if OPTION 403 is used with eccentrically stacked elements, slippage can occur.
5. When BMI2X is used together with OPTION 404, loading that varies along the element length is accounted for in the force diagrams (i.e. for a beam under CBF or internal element loading). Internal forces and moments are output at intervals of $1 / 10$ th of the element length by specifying the Gauss point option from the Output button of the LUSAS Datafile dialog.
6. The end releases for this element allow a joint to be modelled between adjacent elements. These joints allow rotation and translation of one beam with respect to another without load transferral. The rotations and translations remain in the local directions of the beam elements and support large deformations
7. OPTION 36 is only applicable for use with element load types ELDS and UDL. Specifying this option makes these element loads follow the element geometry as the analysis progresses.
8. OPTION 229 considers large displacements and large rotations using a co-rotational formulation. When both options 87 and 229 are true, a local Total Lagrangian formulation will be used within a global co-rotational framework. Note that OPTION 87 has no effect when specified without OPTION 229.
9. The P-Delta formulation is only applicable to lower order (2-noded) beams, higher order beams used in a P-Delta analysis will default to co-rotational GNL.
10. The Smoothed Multi Crack Concrete Model (109) can be used with this element, however, due to the "plane sections remaining plane" hypothesis, crack widths cannot be computed.
11. Partial fixities and rigid ends are defined via the ELEMENT TOPOLOGY data and follow on the same line after the end releases, for example:


The character $K$ is used to identify that the partial fixity stiffnesses $\hat{\mathrm{K}}_{12} \hat{\mathrm{k}}_{13}$ are being explicitly defined, while the character $N$ signifies that fixity factors, $n_{12} n_{1 a}$ are being defined. The fixity factors are used as follows:
$\hat{k}_{i j}=\frac{n_{i j}}{1-n_{i j}} \tilde{k}_{i j}$

The value of the factor $n_{i j j}$ ranges from zero for a pinned connection to 1.0 for a fully fixed connection.

The values $r_{1}$ and $r_{2}$ are the rigid end lengths at nodes 1 and 2 and $\lambda$ is the rigidity factor ( $1.0=$ fully rigid, the default). The factors m 1 and m 2 dictate how much mass to include for the rigid ends, full mass $=1.0\left(\right.$ default $\left.\mathrm{m}_{1}=\mathrm{m}_{2}=0.0\right)$.

## Restrictions

$\square$ Ensure mid-side node centrality

- Avoid excessive element curvature


## Recommendations on Use

The element may be used for linear and nonlinear analysis of two dimensional beam, frame and arch structures.

## 3D Thick Beam Elements

## General

Element Name


BMI21


BMI31


## BMI22



BMI33


## Element Group

Beams

## Element

Thick Beams

## Subgroup

Element Description

Straight and curved isoparametric degenerate thick beam elements in 3D for which shearing deformations are included. The elements can accommodate varying geometric properties along the length. BMI22 and BMI33 can consider initial twist.
Number Of Nodes

Freedoms
End Releases

3 (BMI21), 4 (BMI22 and BMI31) and 6 (BMI33) with end release conditions.
The orientation node(s) (3rd node of BMI21, 3rd and 4th nodes of BMI22, 4th node of BMI31, 4th, 5th and 6th nodes of BMI33) are used to define the local xy-plane.
$\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ : at each active node.
The element node numbers should be followed by: R restrained (default), F free defined in the order $\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ at node 1 and then $\mathrm{U}, \mathrm{V}$, $\mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ at node 2 and node 3 (only for BMI31 and BMI33) related to local element axes (see Notes, Assumptions and Limitations).

Partial fixity Partial fixity at each end node can be defined for all freedoms; this can take the form of a fixity reduction factor or an explicitly defined stiffness value. Partial fixities are defined with respect to the local element axes (see Notes, Assumptions and Limitations).
Rigid ends Rigid lengths $r_{1}$ and $r_{2}$ measured from each end node can be specified for these elements. If these lengths are non zero then any end release or partial fixity is applied at the inner point defining the rigid end. A rigidity factor ( $1.0>\lambda>0.0$ ) can be specified to make the ends semi-rigid, and options to include/exclude the masses of the rigid ends are also provided (see Notes, Assumptions and Limitations).
Node
$\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.

## Geometric Properties

A, Iyy, Izz, Jxx, Asz, Asy, Iyz, ez, ey At each node SF1,SF2,SF3,SF4,SF5,SF6,SF7,SF8,SF9 Optional scale factors applied to the geometric MF1,MF2,MF3,MF4, properties in the calculation of the stiffness and MF5,MF6,MF7,MF8,MF9 mass matrices<br>A Cross sectional area.<br>Iyy, Izz 2nd moment of area about local y, z directions (see Definition).<br>Jxx Torsional constant.<br>Asz, Asy Effective shear areas on local yz plane in local z, y directions (see shear areas).<br>$\mathbf{I y}, \mathbf{I z}$ 1st moment of area about local $y, z$ directions (see Definition).<br>Iyz Product moment of area about local $\mathrm{y}, \mathrm{z}$ axes (see Definition).<br>ez Eccentricity from beam xy-plane to nodal line. (+ve in the +ve local z direction). (See Notes)<br>ey Eccentricity from beam xz-plane to nodal line. (+ve in the +ve local y direction). (See Notes)

Note: For MATERIAL MODEL 29 additional geometric properties are appended to the previous 22 (BMI21 and BMI22) or 33 (BMI31 and BMI33) geometric properties (see Assumptions and Limitations).

## Material Properties

## Linear Isotropic: <br> Rigidities: <br> MATERIAL PROPERTIES (Elastic: Isotropic) RIGIDITIES 6 (Rigidities: Beam)

| Matrix Joint Concrete | Not applicable <br> Not applicable <br> Not applicable |  |
| :---: | :---: | :---: |
| Elasto-Plastic | Stress resultant: | MATERIAL PROPERTIES NONLINEAR 29 <br> (Elastic: Isotropic, Plastic: Resultant) (ifcode=1 or 2, see Assumptions and Limitations) |
| Creep | AASHTO | MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO Code of Practice) |
|  | CEB-FIP | MATERIAL PROPERTIES NONLINEAR 86 CEB-FIP (Concrete creep model to CEB-FIP Model Code 1990) |
|  | Chinese | MATERIAL PROPERTIES NONLINEAR 86 CHINESE <br> (Chinese creep model to Chinese Code of Practice) |
|  | Eurocode | MATERIAL PROPERTIES NONLINEAR 86 EUROCODE <br> (Concrete creep model to EUROCODE_2) |
|  | IRC | MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC Code of Practice) |
| Damage | Not applicable |  |
| Viscoelastic Shrinkage | Not applicable | SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER |
| Rubber | Not applicable |  |
| Generic Polymer | Not applicable |  |
| Composite | Not applicable |  |

## Loading

Prescribed Value PDSP, TPDSP

Concentrated CL
Loads

Prescribed variable. $\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ : at active nodes.
Concentrated loads in global directions. Px, $\mathrm{Py}, \mathrm{Pz}, \mathrm{Mx}, \mathrm{My}, \mathrm{Mz}$ : at active nodes.

## Element Loads ELDS

Distributed Loads UDL

FLD, FLDG
Body Forces CBF

BFP, BFPE

## Velocities VELO <br> Accelerations ACCE

Element loads on nodal line (load type number LTYPE * 10 defines the corresponding element load type on beam axis, see Assumptions and Limitations) (see Assumptions and Limitations)
LTYPE, S1, Px, Py, Pz, Mx, My, Mz LTYPE=11: point loads and moments in local directions. LTYPE=12: point loads and moments in global directions.
LTYPE, 0 , Wx, Wy, Wz, Mx, My, Mz LTYPE=21: uniformly distributed loads in local directions. LTYPE=22: uniformly distributed loads in global directions ( $\mathrm{Mx}=0$ ). LTYPE=23: uniformly distributed projected loads in global directions.
LTYPE, S1, Wx1, Wy1, Wz1, Mx1, My1, Mz1, S2, Wx2, Wy2, Wz2, Mx2, My2, Mz2
LTYPE=31: distributed loads in local directions.
LTYPE=32: distributed loads in global directions.
LTYPE=33: distributed projected loads in global directions.
LTYPE, S1, Wx, Wy, Wz, Mx, My, Mz LTYPE=41: trapezoidal loads in local directions.
LTYPE=42: trapezoidal loads in global directions.
LTYPE=43: trapezoidal projected loads in global directions.
Uniformly distributed loads. Wx, Wy, Wz, $\mathrm{Mx}, \mathrm{My}, \mathrm{Mz}$ : local forces and moments / unit length for element (see Assumptions and Limitations).
Not applicable.
Constant body forces for Element. Xcbf,
Ycbf, Zcbf, $\Omega_{\mathrm{x}}, \Omega_{\mathrm{y}}, \Omega_{\mathrm{z}}, \alpha \mathrm{x}, \alpha \mathrm{y}, \alpha \mathrm{z}$
Body force potentials at nodes/for element.
$\varphi 1, \varphi 2, \varphi 3,0$, Xcbf, Ycbf, Zcbf
Velocities. Vx, Vy, Vz: at nodes.
Acceleration. Ax, Ay, Az: at nodes

| Initial <br> Stress/Strains | SSI, SSIE | Initial stresses/strains at nodes/for element. Fx, Fy, Fz, Mx, My, Mz: axial force, shear forces, torque and moments in local directions. $\varepsilon x, \varepsilon y, \varepsilon z, \psi x, \psi y, \psi z:$ axial shear and flexural strains in local directions. |
| :---: | :---: | :---: |
|  | SSIG | Initial stresses/strains at Gauss points. These stresses/strains are specified in the same manner as SSI and SSIE. |
| Residual Stresses | SSR, SSRE | Residual stresses at nodes/for element. Resultants (for material model 29). Fx, Fy, Fz, Mx, My, Mz: axial force, shear forces, torque and moments in local directions. |
|  | SSRG | Residual stresses at Gauss points. These stresses are specified in the same manner as SSR and SSRE. |
| Target Stress/Strains | TSSIE, TSSIA | Target stresses/strains at nodes/for element. Fx, Fy, Fz, Mx, My, Mz: axial force, shear forces, torque and moments in local directions. $\varepsilon x, \varepsilon y, \varepsilon z, \psi x, \psi y, \psi z:$ axial, shear and flexural strains in local directions. |
|  | TSSIG | Target stresses/strains at Gauss points. These stresses/strains are specified in the same manner as TSSIE and TSSIA. |
| Temperatures | TEMP, TMPE | Temperatures at nodes/for element. T, 0 , $\mathrm{dT} / \mathrm{dy}, \mathrm{dT} / \mathrm{dz}, \mathrm{To}, 0, \mathrm{dTo} / \mathrm{dy}$, dTo/dz in local directions |
| Overburden | Not applicable. |  |
| Phreatic Surface | Not applicable. |  |
| Field Loads | Not applicable. |  |
| Temp Dependent | Not applicable. |  |

## LUSAS Output

Solver Stress resultants (default): Fx, Fy, Fz, Mx, My, Mz: axial force, shear forces, torque and moments in local directions.
Strain: $\varepsilon x, \varepsilon y, \varepsilon z, \psi x, \psi y, \psi z$ : Axial, shear, torsional and flexural strains in local directions.

> By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal axes.
> Modeller See $\underline{\text { Results Tables (Appendix K). }}$.

## Local Axes

- Standard line element For each element/active node, the local xy-plane is defined by the local $x$-axis and the orientation node. The local $y$-axis is perpendicular to the local x -axis and positive on the side of the element where the orientation node lies. The local y and z-axes form a right-handed set with the local x-axis. See Local Element Axes for details


## Sign Convention

- Standard beam element


## Formulation

## Geometric Nonlinearity

| Total Lagrangian | For large displacements and large rotations (see Notes) |
| ---: | :--- |
| Updated <br> Lagrangian | Not applicable. |
| Eulerian | Not applicable. |
| Co-rotational | For large displacements and large rotations |
| P-Delta | Displacements and rotations should be small (see Notes) |

## Integration Schemes

Stiffness Default. 1-point (BMI21 and BMI22), 2-point (BMI31 and BMI33).
Fine. Same as default.
Mass Default. 2-point (BMI21 and BMI22), 3-point (BMI31 and BMI33).
Fine. Same as default.
Note: A 3-point Newton-Cotes integration rule is also available for BMI31 and BMI33 using OPTION 134. This may be more applicable for infinitesimal strain, elasto-plastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory Manual.

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

36 Follower loads
55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity (see Notes).
102 Switch off load correction stiffness matrix due to centripetal acceleration
105 Lumped mass matrix.
134 Gauss to Newton-Cotes in plane (in the local x direction) integration for elements
157 Material model 29 (non cross-section elements), see Notes.
229 Co-rotational geometric nonlinearity.
403 Introduce residual bending flexibility correction for 2-node thick beam BMI21, see Assumptions and Limitations (on by default).
404 Compute equivalent nodal loading from equilibrium considerations for 2-node thick beam BMI21, see Assumptions and Limitations.
405 Specify geometric properties along beam centroidal axes (on by default).
406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
418 Output stress resultants relative to beam centroidal axes for eccentric elements
421 P-Delta analysis, see Notes
432 Use P-Delta geometric stiffness matrix of thick beams for linear buckling analysis

## Notes, Assumptions and Limitations

1. The element is formulated from the so-called degenerate continuum concept, i.e. enforcing directly the modified Timoshenko hypothesis for thick beams to the continuum theory. Plane cross-sections initially normal to the beam axis remain plane and undistorted (the shape of the cross-section remains unchanged) under deformation, but do not necessarily remain normal to the beam axis; the shear centre and centroid of cross-section coincide. Shearing deformations are included. The basic kinematic assumptions correspond to the Timoshenko beam theory and do not allow for warping effects in torsion. Although warping effects can be considered approximately by using real torsional constants, inaccuracies are likely to occur when eccentricity is present.
2. Input of geometric properties (OPTION 405) and loads (OPTION 406), and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axes. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line.
3. When OPTION 403 is specified to introduce residual bending flexibility correction (on by default), for BMI21 and BMI22, the axial force and torsion are constant, while shear forces and moments vary linearly along the length of the beam. For BMI31 and BMI33 the axial force, shear forces, moments and torsion all vary linearly along the length.
4. When BMI21 is used together with OPTION 403 to introduce residual bending flexibility correction, its stiffness matrix is enhanced to the order of a cubic. Note that if OPTION 403 is used with eccentrically stacked elements, slippage can occur.
5. When BMI21 is used together with OPTION 404, loading that varies along the element length is accounted for in the force diagrams (i.e. for a beam under CBF or internal element loading). A post-processing technique has been introduced to obtain accurate quadratic bending moments for BMI31. For BMI21 (with OPTION 404) and BMI31, internal forces and moments are output at intervals of $1 / 10$ th of the element length by specifying the Gauss point option from the Output button of the LUSAS Datafile dialog.
6. The end releases for this element allow a joint to be modelled between adjacent elements. These joints allow rotation and translation of one beam with respect to another without load transferral. The rotations and translations remain in the local directions of the beam elements and support large deformations.
7. For nonlinear material model 29 the following geometric properties are appended to those already specified (see Geometric Properties).

- $\mathrm{A}^{\mathrm{p}}, \mathrm{Zyy}^{\mathrm{p}}, \mathrm{Zzz}^{\mathrm{p}}, \mathrm{Zy}^{\mathrm{p}}, \mathrm{Zz}^{\mathrm{p}}, \mathrm{S}^{\mathrm{p}}$ at each node
- $\quad A^{p}$ Plastic area (=elastic area)
- $\mathrm{Zyy}^{\mathrm{p}}$, Zzz $^{\mathrm{p}}$ Plastic moduli for bending about $\mathrm{y}, \mathrm{z}$ axes
- $\mathrm{Zy}^{\mathrm{p}}, \mathrm{Zz}^{\mathrm{p}}$ Plastic moduli for torsion about $\mathrm{y}, \mathrm{z}$ axes.
- $\quad S^{p}$ Plastic area for shear $\left(S^{p}=0\right)$.

Where the fully plastic torsional moment $=\sigma y\left(\mathrm{Zy}^{\mathrm{p}}+\mathrm{Zz}^{\mathrm{p}}\right)$.
Note that if eccentricity has been specified the plastic properties must be defined with reference to the nodal line and not the beam axes, i.e. the eccentricity is not used to automatically modify the plastic properties, they must be defined via modified geometry.

For nonlinear material model 29 the following ifcode parameters are applicable: ifcode $=\mathbf{1}$ for circular hollow sections and ifcode $=\mathbf{2}$ for solid rectangular sections
9. Temperature dependent properties cannot be used with material model 29.
10. The rigidity matrix is evaluated explicitly from the geometric properties for both linear and nonlinear materials.
11. OPTION 36 is only applicable for use with element load types ELDS and UDL. Specifying this option makes these element loads follow the element geometry as the analysis progresses.
12. When a nonlinear material is used with this element the transverse shear stresses are excluded from the plasticity computations i.e. the transverse shear stresses are assumed to remain elastic. This means that if a nonlinear material is used in applications where transverse shear tends to dominate the stress field the equivalent von Mises and maximum principal stresses can exceed the uniaxial yield stress.
13. When a step by step dynamic analysis is carried out using BMI elements with distributed loading, the "free body force diagrams" pertaining to applied loading, are not superimposed on the nodal values, to do so would lead to erroneous results until a steady state is reached. It should therefore be noted that different force diagrams will be obtained for BMI elements if static and dynamic analyses are directly compared.
14. OPTION 87 considers large displacements and large rotations using a Total Lagrangian formulation; OPTION 229 considers large displacements and large rotations using a co-rotational formulation. In general the co-rotational formulation works better. When options 87 and 229 are true, a local Total Lagrangian formulation will be used together with a global co-rotational formulation.
15. OPTION 229 considers large displacements and large rotations using a co-rotational formulation. When both options 87 and 229 are true, a local Total Lagrangian formulation will be used within a global co-rotational framework. Note that OPTION 87 has no effect when specified without OPTION 229.
16. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command.
17. The P-Delta formulation is only applicable to lower order (2-noded) beams, higher order beams used in a P-Delta analysis will default to co-rotational GNL.
18. Partial fixities and rigid ends are defined via the ELEMENT TOPOLOGY data and follow on the same line after the end releases, for example:


The character $K$ is used to identify that the partial fixity stiffnesses $\hat{\mathrm{k}}_{12} \hat{\mathrm{k}}_{13}$ are being explicitly defined, while the character $N$ signifies that fixity factors, $n_{12} n_{1 a}$ are being defined. The fixity factors are used as follows:
$\hat{k}_{i j}=\frac{n_{i j}}{1-n_{i j}} \tilde{k}_{i j}$

The value of the factor $n_{i j}$ ranges from zero for a pinned connection to 1.0 for a fully fixed connection.

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature


## Recommendations on Use

- The elements may be used for linear and material nonlinear analysis of three dimensional beam, frame and arch structures, and can also be used to model cables in cable stayed structures. BMI21 and BMI22 may also be used as a stiffener for the QTS4 shell element; while BMI31 and BMI33 may be used as a stiffener for the QTS8 shell element, e.g. space frames.


## 3D Thick Beam Elements with Quadrilateral Cross-Section

## General



Element Group
Beams
Element
Thick Beams
Subgroup
Element Description

Straight and curved isoparametric degenerate thick beam elements in 3D for which shearing deformations are included. The element has a quadrilateral cross section which may vary along the element length. BMX22 and BMX33 can consider initial twist.
Number Of Nodes 3 (BMX21), 4 (BMX22 and BMX31) and 6 (BMX33) with end release conditions.
The orientation node(s) (3rd node of BMX21, 3rd and 4th nodes of BMX22, 4th node of BMX31, 4th, 5th and 6th nodes of BMX33) are used to define the local xy-plane.
Freedoms
End Releases
$\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ : at each active node.
The element node numbers should be followed by: R restrained (default), F free defined in the order $\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ at node 1 and then $\mathrm{U}, \mathrm{V}$,

Partial fixity

Rigid ends

Node
Coordinates
$\mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ at node 2 and node 3 (only for BMX31 and BMX33) related to local element axes (see Notes).
Partial fixity at each end node can be defined for all freedoms; this can take the form of a fixity reduction factor or an explicitly defined stiffness value. Partial fixities are defined with respect to the local element axes (see Notes, Assumptions and Limitations).
Rigid lengths $r_{1}$ and $r_{2}$ measured from each end node can be specified for these elements. If these lengths are non zero then any end release or partial fixity is applied at the inner point defining the rigid end. A rigidity factor $(1.0>\lambda>0.0)$ can be specified to make the ends semi-rigid, and options to include/exclude the masses of the rigid ends are also provided (see Notes, Assumptions and Limitations).
X, Y, Z: at each node.

## Geometric Properties

$\mathrm{y} 1, \mathrm{z} 1, \mathrm{y} 2, \mathrm{z} 2, \mathrm{y} 3, \mathrm{z} 3, \mathrm{y} 4, \mathrm{z} 4$ : local cross section coordinate pairs at each node; followed by nt 12 , nt14: number of Newton-Cotes integration points in the direction defined by the local crosssection points 1-2 and 1-4 (zero indicates default values). Multiple quadrilateral crosssections can be used to build up complex beam cross-sections.

Note. The corners of the quadrilateral are numbered clockwise about the local x -axis (the beam nodal line), that is, a right-hand screw rule in the direction of increasing $x$.


## Material Properties

Linear Isotropic:
Matrix Not applicable
Joint Not applicable

Concrete

Elasto-Plastic Stress resultant:
Tresca:

Drucker-Prager:

MATERIAL PROPERTIES (Elastic: Isotropic)

MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi Crack Concrete) Not applicable.
MATERIAL PROPERTIES NONLINEAR 61
(Elastic: Isotropic, Plastic: Tresca, Hardening:
Isotropic Hardening Gradient, Isotropic Plastic
Strain or Isotropic Total Strain)
MATERIAL PROPERTIES NONLINEAR 64


## Loading <br> Prescribed Value PDSP, TPDSP <br> Concentrated CL <br> Loads <br> Element Loads ELDS

Distributed Loads UDL

Prescribed variable. $\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ : at active nodes.
Concentrated loads in global directions. Px, $\mathrm{Py}, \mathrm{Pz}, \mathrm{Mx}, \mathrm{My}, \mathrm{Mz}$ : at active nodes (global).
Element loads on nodal line (load type number LTYPE *10 defines the corresponding element load type on beam axis, see Assumptions and Limitations)
LTYPE, S1, Px, Py, Pz, Mx, My, Mz LTYPE=11: point loads and moments in local directions. LTYPE=12: point loads and moments in global directions.
LTYPE, 0 , Wx, Wy, Wz, Mx, My, Mz LTYPE=21: uniformly distributed loads in local directions. LTYPE=22: uniformly distributed loads in global directions ( $\mathrm{Mx}=0$ ). LTYPE=23: uniformly distributed projected loads in global directions.
LTYPE, S1, Wx1, Wy1, Wz1, Mx1, My1, Mz1, S2, Wx2, Wy2, Wz2, Mx2, My2, Mz2
LTYPE=31: distributed loads in local directions.
LTYPE=32: distributed loads in global directions.
LTYPE=33: distributed projected loads in global directions.
LTYPE, S1, Wx, Wy, Wz, Mx, My, Mz
LTYPE=41: trapezoidal loads in local directions.
LTYPE=42: trapezoidal loads in global directions.
LTYPE=43: trapezoidal projected loads in global directions.
Uniformly distributed loads. Wx, Wy, Wz, Mx, My, Mz: local forces and moments / unit length for element in local directions. See Assumptions and Limitations.


## LUSAS Output

Solver Stress resultants (default): Fx, Fy, Fz, Mx, My, Mz: axial force, shear forces, torque and moments in local directions.
Continuum stresses (OPTION 172): $\sigma x, \sigma x y, \sigma x z$ : in local directions.
Strain: $\varepsilon x, \varepsilon y, \varepsilon z, \psi x, \psi y, \psi z$ : Axial, shear, torsional and flexural strains in local directions.
Continuum strains (OPTION 172): $\varepsilon x, \varepsilon x y, \varepsilon x z: ~ i n ~ l o c a l ~ d i r e c t i o n s . ~$ By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal axes.
Modeller See Results Tables (Appendix K).

## Local Axes

Standard line element For each element/active node, the local xy-plane is defined by the local $x$-axis and the orientation node. The local $y$-axis is perpendicular to the local x -axis and positive on the side of the element where the orientation node lies. The local y and z-axes form a right-handed set with the local x-axis. See Local Element Axes for details

## Sign Convention

$\square$ Standard beam element
Formulation

## Geometric Nonlinearity

Total Lagrangian
For large displacements and rotations (see Notes)
Updated
Not applicable.
Lagrangian
Eulerian
Not applicable.
Corotational For large displacements and rotations
P-Delta Displacements and rotations should be small (see Notes)

## Integration Schemes

Stiffness Default. 1-point (BMX21 and BMX22), 2-point (BMX31 and BMX33).
Fine. Same as default.
Mass Default. 2-point (BMX21 and BMX22), 3-point (BMX31 and BMX33).

Fine. Same as default.
Note: A 3-point Newton-Cotes integration rule is also available for BMX31 and BMX33 using OPTION 134. This may be more applicable for infinitesimal strain, elasto-plastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory Manual.

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

## 36 Follower loads

55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity (see Notes).
102 Switch off load correction stiffness matrix due to centripetal acceleration
105 Lumped mass matrix.
134 Gauss to Newton-Cotes in plane (in the local x direction) integration for elements.
139 Output yielded integration points only.
172 Form the rigidity matrix by numerical cross section integration.
229 Co-rotational geometric nonlinearity.
403 Introduce residual bending flexibility correction for 2-node thick beam BMI21, see Assumptions and Limitations (on by default).
404 Compute equivalent nodal loading from equilibrium considerations for 2-node thick beam BMX21, see Notes (on by default).
406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
418 Output stress resultants relative to beam centroidal axes for eccentric elements
421 P-Delta analysis, see Notes
432 Use P-Delta geometric stiffness matrix of thick beams for linear buckling analysis

## Notes, Assumptions and Limitations

1. The element is formulated from the so-called degenerate continuum concept, i.e. enforcing directly the modified Timoshenko hypothesis for thick beams to the continuum theory. Plane cross-sections initially normal to the beam axis remain plane and undistorted (the shape of the cross-section remains unchanged) under deformation, but do not necessarily remain normal to the beam axis; the shear centre and centroid of cross-section coincide. Shearing deformations are included.
2. Input of loads (OPTION 406) and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axis. CL is always input with respect to the nodal
line; displacements are output with respect to the nodal line. Fiber stress/strain results are output at the actual location.
3. When OPTION 403 is specified to introduce residual bending flexibility correction (on by default), for BMX21 and BMX22, the axial force and torsion are constant, while shear forces and moments vary linearly along the length of the beam. For BMX31 and BMX33 the axial force, shear forces, moments and torsion all vary linearly along the length.
4. When BMX21 is used together with OPTION 403 to introduce residual bending flexibility correction, its stiffness matrix is enhanced to the order of a cubic. Note that if OPTION 403 is used with eccentrically stacked elements, slippage can occur.
5. When BMX21 is used together with OPTION 404, loading that varies along the element length is accounted for in the force diagrams (i.e. for a beam under CBF or internal element loading). Internal forces and moments are output at intervals of $1 / 10$ th of the element length by specifying the Gauss point option from the Output button of the LUSAS Datafile dialog.
6. The end releases for this element allow a joint to be modelled between adjacent elements. These joints allow rotation and translation of one beam with respect to another without load transferral. The rotations and translations remain in the local directions of the beam elements and support large deformations.
7. Computation of the rigidity matrix by integration through the cross-section depth of the beam is necessary for all nonlinear material models. By default OPTION 172 is invoked automatically and a $5 * 5$ point Newton-Cotes integration rule is used. This allows the output of stresses at the numerical cross section integration points.
8. By default, the rigidity matrix is evaluated explicitly for linear materials. A 3*3 point Newton-Cotes integration rule may be invoked using OPTION 172. Numerical cross section integration enables top, middle and bottom stress output.
9. OPTION 36 is only applicable for use with element load types ELDS and UDL. Specifying this option makes these element loads follow the element geometry as the analysis progresses.
10. For nonlinear material models, fibre integration is used across the cross-sectional area of the beam. Only axial deformation is considered in the plasticity computations, any torsional deformation is assumed to remain elastic.
11. OPTION 229 considers large displacements and large rotations using a co-rotational formulation. When both options 87 and 229 are true, a local Total Lagrangian formulation will be used within a global co-rotational framework. Note that OPTION 87 has no effect when specified without OPTION 229.
12. The P-Delta formulation is only applicable to lower order (2-noded) beams, higher order beams used in a P-Delta analysis will default to co-rotational GNL.
13. The Smoothed Multi Crack Concrete Model (109) can be used with this element, however, due to the "plane sections remaining plane" hypothesis, crack widths cannot be computed.
14. The Partial fixities and rigid ends are defined via the ELEMENT TOPOLOGY data and follow on the same line after the end releases, for example:


The character $K$ is used to identify that the partial fixity stiffnesses $\hat{k}_{12} \hat{k}_{15}$ are being explicitly defined, while the character $N$ signifies that fixity factors, $n_{12} n_{15}$ are being defined. The fixity factors are used as follows:

$$
\hat{k}_{i j}=\frac{n_{i j}}{1-n_{i j}} \tilde{k}_{i j}
$$

The value of the factor $n_{i j}$ ranges from zero for a pinned connection to 1.0 for a fully fixed connection.

The values $r_{1}$ and $r_{2}$ are the rigid end lengths at nodes 1 and 2 and $\lambda$ is the rigidity factor ( $1.0=$ fully rigid, the default $)$. The factors m 1 and m 2 dictate how much mass to include for the rigid ends, full mass $=1.0$ (default $\mathrm{m}_{1}=\mathrm{m}_{2}=0.0$ ).

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature

BMX22 and BMX33 elements are not available for selection currently within LUSAS Modeller.

## Recommendations on Use

- The elements may be used for linear and nonlinear analysis of three dimensional beam, frame and arch structures. BMX21 and BMX22 may also be used as a stiffener for the QTS4 shell element; while BMX31 and BMX33 may be used as a stiffener for the QTS8 shell element.


## 3D Thick Beam Elements with Torsional Warping

## General

Element BMI21W
Name


BMI31W


BMI22W


BMI33W


Element Group
Element Subgroup

Element Description

Number Of Nodes

Freedoms
End Releases
-

Straight and curved isoparametric degenerate beam elements in 3D for which shearing deformations and torsional warping are included. The elements can accommodate varying geometric properties along the length.
BMI22W and BMI33W can consider initial twisting.
Beams
Isoparametric Degenerate Beams

3 (BMI21W), 4 (BMI22W and BMI31W) and 6 (BMI33W) with end release conditions.
The orientation node(s) (3rd node of BMI21W, 3rd and 4th nodes of BMI22W, 4th node of BMI31W, 4th, 5th and 6th nodes of BMI33W) are used to define the local xy-plane.
$\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}, \alpha$ : at each active node.
The element node numbers should be followed by: R restrained (or continuous or unreleased) (default), F free (or discontinuous or released), C discontinuous and constrained, defined in the order $\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}$,

|  | $\theta \mathrm{z}$ at node 1 and then $\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ at at node 2 and node 3 (only for BMI31W and BMI33W) related to local element axes (see Notes, Assumptions and Limitations).). |
| :---: | :---: |
| Partial fixity | Partial fixity at each end node can be defined for all freedoms; this can take the form of a fixity reduction factor or an explicitly defined stiffness value. Partial fixities are defined with respect to the local element axes (see Notes, Assumptions and Limitations). |
| Rigid ends | Rigid lengths $r_{1}$ and $r_{2}$ measured from each end node can be specified for these elements. If these lengths are non zero then any end release or partial fixity is applied at the inner point defining the rigid end. A rigidity factor ( $1.0>\lambda>0.0$ ) can be specified to make the ends semi-rigid, and options to include/exclude the masses of the rigid ends are also provided (see Notes, Assumptions and Limitations). |
| Node | X, Y, Z: at each node. |
| Coordinates |  |

## Geometric Properties

A, Iyy, Izz, Jxx, Asz, Asy, Iy, Iz, At each node
Iyz, Cw, Cwy, Cwz, Iyr, Izr, Irr,
Iwr (default) or A, Iyy, Izz, Jxx,
Asz, Asy, ez, ey, Iyz, Cw, zo, yo, Iyr,
Izr, Irr, Iwr (option 405)
SF1,SF2,SF3,SF4,SF5,SF6,SF7,SF8, Optional scale factors applied to the geometric
SF9, SF10,SF11,SF12,SF13, properties in the calculation of the stiffness and mass SF14,SF15,SF16 matrices
MF1,MF2,MF3,MF4,MF5,MF6,MF
7,MF8,
MF9,MF10,MF11,MF12,MF13,MF 14,MF15,MF16
A Cross sectional area.
Iyy, Izz 2nd moment of area about local y, z directions (see Definition).
Jxx Torsional constant.
Asz, Asy Effective shear areas on local yz plane in local z, y directions (see shear areas).
$\mathbf{I y}, \mathbf{I z}$ 1st moment of area about local $\mathrm{y}, \mathrm{z}$ directions (see Definition).
Iyz Product moment of area about local $y, z$ axes (see Definition).
Cw Warping constant (see Definition).
Cwy, Cwz 1st moment of warping about local $y, z$ directions

$$
\left.\left.\begin{array}{rl} 
& \begin{array}{l}
\text { (see Definition). } \\
\text { ez }
\end{array} \\
\text { ey } & \begin{array}{l}
\text { Eccentricity from beam xy-plane to nodal line. (+ve } \\
\text { in the +ve local z direction). (See Notes) }
\end{array} \\
\text { eccentricity from beam xz-plane to nodal line. (+ve } \\
\text { in the +ve local y direction). (See Notes) }
\end{array}\right\} \text { Zo } \begin{array}{l}
\text { z-coordinate of the shear center with respect to the } \\
\text { centroid (+ve in +ve local z-direction) }
\end{array}\right\} \begin{array}{ll}
\text { Yo } & \begin{array}{l}
\text { y-coordinate of the shear center with respect to the } \\
\text { centroid (+ve in +ve local y-direction) }
\end{array} \\
\text { Iyr, Izr, Irr, Iwr } & \text { Wagner constants. (See Notes) }
\end{array}
$$

## Material Properties

Linear Isotropic: Rigidities:
Matrix Not applicable
Joint Not applicable
Concrete Not applicable Elasto-Plastic Stress resultant:

## Creep AASHTO

CEB-FIP

Chinese

Eurocode

IRC

MATERIAL PROPERTIES (Elastic: Isotropic) RIGIDITIES 6 (Rigidities: Beam)

MATERIAL PROPERTIES NONLINEAR 29 (Elastic: Isotropic, Plastic: Resultant) (ifcode=1 or 2, see Assumptions and Limitations)

MATERIAL PROPERTIES NONLINEAR 86 AASHTO
(Concrete creep model to AASHTO code of Practice)

MATERIAL PROPERTIES NONLINEAR 86 CEB-FIP
(Concrete creep model to CEB-FIP Model Code 1990)

MATERIAL PROPERTIES NONLINEAR 86 CHINESE
(Chinese creep model to Chinese Code of Practice)

MATERIAL PROPERTIES NONLINEAR 86 EUROCODE
(Concrete creep model to EUROCODE_2)
MATERIAL PROPERTIES NONLINEAR 86 IRC
(Concrete creep model to Indian IRC code of

| Damage | Pot applicable | Practice) |
| ---: | :--- | :---: |
| Viscoelastic |  |  |
| Shrinkage | Not applicable |  |
| Rubber | Not applicable | SHRINKAGE CEB_FIP_90, EUROCODE_2, |
| GENERAL, USER |  |  |
| Generic Polymer |  |  |
| Composite | Not applicable | Not applicable |

LTYPE=42: trapezoidal loads in global directions.
LTYPE=43: trapezoidal projected loads in global directions.

|  | DLDL, DLDG | Not applicable. |
| :---: | :---: | :---: |
|  | DLEL,DLEG | Not applicable. |
|  | PLDL, PLDG | Not applicable. |
| Distributed Loads | UDL | Uniformly distributed loads. Wx, Wy, Wz, Mx, My, Mz : local forces and moments / unit length for element (see Assumptions and Limitations). |
|  | FLD, FLDG | Not applicable. |
| Body Forces | CBF | Constant body forces for Element. Xcbf, Ycbf, Zcbf, $\Omega_{\mathrm{x}}, \Omega_{\mathrm{y}}, \Omega_{\mathrm{z}}, \alpha \mathrm{x}, \alpha \mathrm{y}, \alpha_{\mathrm{z}}$ |
|  | BFP, BFPE | Body force potentials at nodes/for element. $\varphi 1, \varphi 2$, $\varphi 3,0$, Xcbf, Ycbf, Zcbf |
| Velocities | VELO | Velocities. Vx, Vy, Vz: at nodes. |
| Accelerations | ACCE | Acceleration. Ax, Ay, Az: at nodes |
| Initial Stress/Strains | SSI, SSIE | Initial stresses/strains at nodes/for element. Fx, Fy, $\mathrm{Fz}, \mathrm{Mx}, \mathrm{My}, \mathrm{Mz}, 0,0$ : axial force, shear forces, torque and moments in local directions. $\varepsilon x, \varepsilon y, \varepsilon z$, $\psi \mathrm{x}, \psi \mathrm{y}, \psi \mathrm{z}, 0,0$ : axial, shear and flexural strains in local directions. |
|  | SSIG | Initial stresses/strains at Gauss points. These stresses/strains are specified in the same manner as SSI and SSIE. |
| Residual Stresses | SSR, SSRE | Residual stresses at nodes/for element. Resultants (for material model 29). Fx, Fy, Fz, Mx, My, Mz: axial force, shear forces, torque and moments in local directions. |
|  | SSRG | Residual stresses at Gauss points. These stresses are specified in the same manner as SSR and SSRE. |
| Target Stress/Strains | TSSIE, TSSIA | Target stresses/strains at nodes/for element. Fx, Fy, $\mathrm{Fz}, \mathrm{Mx}, \mathrm{My}, \mathrm{Mz}, 0,0$ : axial force, shear forces, torque and moments in local directions. $\varepsilon x, \varepsilon y, \varepsilon z$, $\psi x, \psi y, \psi z, 0,0$ : axial, shear and flexural strains in local directions. |
|  | TSSIG | Target stresses/strains at Gauss points. These stresses/strains are specified in the same manner as TSSIE and TSSIA. |
| Temperatures | TEMP, TMPE | Temperatures at nodes/for element. T, $0, \mathrm{dT} / \mathrm{dy}$, $\mathrm{dT} / \mathrm{dz}, \mathrm{To}, 0, \mathrm{dTo} / \mathrm{dy}, \mathrm{dTo} / \mathrm{dz}$ in local directions |

Overburden Not applicable.<br>Phreatic Surface Not applicable.<br>Field Loads Not applicable.<br>Temp Dependent Not applicable.<br>Loads

## LUSAS Output

Solver Force (default): Fx, Fy, Fz, Mx, My, Mz, Fb, Mb: axial force, shear forces, torque, moments, bishear (or warping torsion) and bimoment in local directions.
Strain: $\varepsilon x, \varepsilon y, \varepsilon z, \psi x, \psi y, \psi z, \alpha, \alpha^{\prime}:$ axial, shear, torsional, flexural strains and torsional warping strains in local directions.
By default element output is with respect to the nodal line. Option 380 outputs stress/strain resultants with respect to the beam centreline.
Modeller See Results Tables (Appendix K).

## Local Axes

I Standard line element For each element/active node, the local xy-plane is defined by the local $x$-axis and the orientation node. The local $y$-axis is perpendicular to the local x -axis and positive on the side of the element where the orientation node lies. The local y and z-axes form a right-handed set with the local x-axis. See Local Element Axes for details

## Sign Convention

$\square$ Standard beam element

## Formulation

## Geometric Nonlinearity

Total Lagrangian Updated Not applicable.

## Lagrangian

Eulerian Not applicable.
Co-rotational For large displacements, large rotations and small strains.
P-Delta Displacements and rotations should be small (see Notes)

## Integration Schemes

Stiffness Default. 1-point (BMI21W and BMI22W), 2-point (BMI31W and BMI33W).
Fine. Same as default.
Mass Default. 2-point (BMI21W and BMI22W), 3-point (BMI31W and BMI33W).
Fine. Same as default.
Note: A 3-point Newton-Cotes integration rule is also available for BMI31W and BMI33W using option 134. This may be more applicable for infinitesimal strain, elastoplastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory Manual

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

36 Follower loads
55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity (see Notes).
102 Switch off load correction stiffness matrix due to centripetal acceleration
105 Lumped mass matrix.
134 Gauss to Newton-Cotes in plane (in the local x direction) integration for elements
157 Material model 29 (non cross-section elements), see Notes.
229 Co-rotational geometric nonlinearity.
380 Output stress/strain resultants relative to beam axes for eccentric elements.
403 Introduce residual bending flexibility correction for 2-node thick beam BMI21, see Assumptions and Limitations.
404 Compute equivalent nodal loading from equilibrium considerations for 2-node thick beam BMI21, see Assumptions and Limitations.
405 Specify geometric properties along beam centroidal axes
406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
421 P-Delta analysis, see Notes
424 Include the Wagner effect in the large deformation formulation for beams
432 Use P-Delta geometric stiffness matrix of thick beams for linear buckling analysis

## Notes, Assumptions and Limitations

1. The element is formulated from the so-called degenerate continuum concept, i.e. enforcing directly the modified Timoshenko hypothesis for thick beams to the continuum theory. Shearing deformations and torsional warping are included.
2. By default input of geometric properties and loads, and output of element stress/strain resultants are with respect to the nodal line. Option 405 inputs geometric properties, option 406 inputs loads, and option 380 outputs stress/strain resultants with respect to the beam centreline. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line.
3. When OPTION 403 is specified to introduce residual bending flexibility correction (on by default), for BMI21W and BMI22W, the axial force, bishear, bimoment and torsion are constant, while the other shear forces and moments vary linearly along the length of the beam. For BMI31W and BMI33W the axial force, all shear forces, all moments and torsion vary linearly along the length
4. When BMI21W is used together with OPTION 403 to introduce residual bending flexibility correction, its stiffness matrix is enhanced to the order of a cubic.
5. When BMI21W is used together with OPTION 404, loading that varies along the element length is accounted for in the force diagrams (i.e. for a beam under CBF or internal element loading). Internal forces and moments are output at intervals of $1 / 10$ th of the element length by specifying the Gauss point option from the Output button of the LUSAS Datafile dialog.
6. The end releases for this element allow a joint to be modelled between adjacent elements. These joints allow rotation and translation of one beam with respect to another without load transferral as well as different warping conditions in adjacent elements. The rotations and translations remain in the local directions of the beam elements and support large deformations.
7. The rigidity matrix is evaluated explicitly from the geometric properties for both linear and nonlinear materials.
8. Option 36 is only applicable for use with element load types ELDS and UDL. Specifying this option makes these element loads follow the element geometry as the analysis progresses.
9. For large deformation analyses the following geometric properties (Wagner constants) are required (see Geometric Properties) if Option $424=$ T: Iyr, Igr, Irr and Iwr at each node. If these constants are set to zero, the Wagner effect will be ignored, and the results may not be correct if twist rotations are not small.
10. When a step by step dynamic analysis is carried out using BMI elements with distributed loading, the "free body force diagrams" pertaining to applied loading, are not superimposed on the nodal values, to do so would lead to erroneous results until a steady state is reached. It should therefore be noted that different force diagrams will be obtained for BMI elements if static and dynamic analyses are directly compared.
11. OPTION 229 considers large displacements and large rotations using a co-rotational formulation. When both options 87 and 229 are true, a local Total Lagrangian formulation will be used within a global co-rotational framework. Note that OPTION 87 has no effect when specified without OPTION 229.
12. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command.
13. The P-Delta formulation is only applicable to lower order (2-noded) beams, higher order beams used in a P-Delta analysis will default to co-rotational GNL.
14. Partial fixities and rigid ends are defined via the ELEMENT TOPOLOGY data and follow on the same line after the end releases, for example:


1123 RFRRFRRRRRRRRR $N n_{12} n_{15}\left[\mathrm{r}_{1} \mathrm{r}_{2} \lambda \mathrm{~m}_{1} \mathrm{~m}_{2}\right]$


The character $K$ is used to identify that the partial fixity stiffnesses $\hat{\mathrm{k}}_{12} \widehat{\mathrm{k}}_{15}$ are being explicitly defined, while the character $N$ signifies that fixity factors, $n_{12} n_{15}$ are being defined. The fixity factors are used as follows:

$$
\hat{k}_{i j}=\frac{n_{i j}}{1-n_{i j}} \tilde{k}_{i j}
$$

The value of the factor $n_{i j j}$ ranges from zero for a pinned connection to 1.0 for a fully fixed connection.

The values $r_{1}$ and $r_{2}$ are the rigid end lengths at nodes 1 and 2 and $\lambda$ is the rigidity factor ( $1.0=$ fully rigid, the default). The factors m 1 and m 2 dictate how much mass to include for the rigid ends, full mass $=1.0$ (default $\mathrm{m}_{1}=\mathrm{m}_{2}=0.0$ ).

## Restrictions

Ensure mid-side node centrality

## Element Reference Manual

- Avoid excessive element curvature
$\square$ Ensure correct warping condition at connections.


## Recommendations on Use

- The elements may be used for linear and material nonlinear analysis of three dimensional beam, frame and arch structures. BMI21W and BMI22W may also be used as a stiffener for the QTS4 shell element; while BMI31W and BMI33W may be used as a stiffener for the QTS8 shell element.


## 3D Thick Beam Elements with Quadrilateral Cross-Section and Torsional Warping

## General



## Element Group

Beams
Element
Isoparametric Degenerate Beams Subgroup
Element Description

Number Of Nodes

## Freedoms

End Releases
$\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ : at each active node.

Straight and curved isoparametric degenerate beam elements in 3D for which shearing deformations and torsional warping are included. The element has a quadrilateral cross section which may vary along the element length. BMX22W and BMX33W can consider initial twisting. 3(BMX21W), 4 (BMX22W and BMX31W) and 6(BMX33W) with end release conditions. The orientation node(s) (3rd node of BMX21W, 3rd and 4th nodes of BMX22W, 4th node of BMX31W, 4th, 5th and 6th nodes of BMX33W) are used to define the local xy-plane.

The element node numbers should be followed by: R restrained (default),

F free defined in the order $\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ at node 1 and then $\mathrm{U}, \mathrm{V}$, $\mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ at node 2 and node 3 (only for BMX31 and BMX33) related to local element axes (see Notes).

The element node numbers should be followed by: R restrained (or continuous or unreleased) (default), F free (or discontinuous or released), C discontinuous and constrained, defined in the order $\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}$, $\theta \mathrm{z}, \alpha$ and then $\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}, \alpha$ at node 2 and node 3 (only for BMX31W and BMX33W) related to local element axes (see Notes).
Partial fixity at each end node can be defined for all freedoms; this can take the form of a fixity reduction factor or an explicitly defined stiffness value. Partial fixities are defined with respect to the local element axes (see Notes, Assumptions and Limitations).
Rigid ends
Rigid lengths $r_{1}$ and $r_{2}$ measured from each end node can be specified for these elements. If these lengths are non zero then any end release or partial fixity is applied at the inner point defining the rigid end. A rigidity factor $(1.0>\lambda>0.0)$ can be specified to make the ends semi-rigid, and options to include/exclude the masses of the rigid ends are also provided (see Notes, Assumptions and Limitations).
Node X, Y, Z: at each node.

## Geometric Properties

$\mathrm{y} 1, \mathrm{z} 1, \mathrm{y} 2, \mathrm{z} 2, \mathrm{y} 3, \mathrm{z} 3, \mathrm{y} 4, \mathrm{z} 4$ : local cross section coordinate pairs for a triangle at each node; followed by nt12, nt14: specifying the number of integration points nt12* nt14 (the value nt12* nt14 determines the integration rule no matter what the values nt 12 and nt14 are except when nt $12 *$ nt $14=7, \mathrm{nt} 12=1$ defines a cubic rule, while nt $12=7$ defines a quintic rule)
or
$y 1, z 1, y 2, z 2, y 3, z 3, y 4, z 4$ : local cross section coordinate pairs for a quadrilateral at each node; followed by nt12, nt14: specifying the number of Newton-Cotes integration points in the direction defined by the local cross-section points 1-2 and 1-4 (zero indicates default values). Multiple quadrilateral cross-sections can be used to build up complex beam crosssections. Number of divisions for each coarse quadrilateral (default $=5$ ) can be specified for the computation of warping of cross-section
Note. The corners of the quadrilateral are numbered clockwise about the local x -axis (the beam nodal line), that is, a right-hand screw rule in the direction of increasing $x$.


## Material Properties

| Linear <br> Matrix Joint | Isotropic: <br> Not applicable <br> Not applicable | MATERIAL PROPERTIES (Elastic: Isotropic) |
| :---: | :---: | :---: |
| Concrete |  | MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi Crack Concrete) |
| Elasto-Plastic | Stress resultant: <br> Tresca: | Not applicable. <br> MATERIAL PROPERTIES NONLINEAR 61 <br> (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain) |
|  | Drucker-Prager: | MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular) |
|  | Mohr-Coulomb: | MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation) |
|  | Optimised Implicit Von Mises: | MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic) |
|  | Volumetric Crushing: | Not applicable. |
|  | Stress Potential | STRESS POTENTIAL VON_MISES <br> (Isotropic: von Mises, Modified von Mises) |
| Creep |  | CREEP PROPERTIES (Creep) |
|  | AASHTO | MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of Practice) |
|  | CEB-FIP | MATERIAL PROPERTIES NONLINEAR 86 CEB-FIP <br> (Concrete creep model to CEB-FIP Model Code 1990) |
|  | Chinese | MATERIAL PROPERTIES NONLINEAR 86 CHINESE <br> (Chinese creep model to Chinese Code of Practice) |
|  | Eurocode | MATERIAL PROPERTIES NONLINEAR 86 EUROCODE <br> (Concrete creep model to EUROCODE_2) |

IRC

## Damage

Viscoelastic Not applicable Shrinkage

Rubber Not applicable

## Generic Polymer Not applicable

Composite Not applicable

MATERIAL PROPERTIES NONLINEAR 86 IRC
(Concrete creep model to Indian IRC code of Practice)
DAMAGE PROPERTIES SIMO, OLIVER (Damage)

SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER

## Loading

Prescribed Value PDSP, TPDSP

Concentrated CL
Loads
Element Loads ELDS

Prescribed variable. $\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ : at active nodes.
Concentrated loads in global directions. $\mathrm{Px}, \mathrm{Py}, \mathrm{Pz}$, $\mathrm{Mx}, \mathrm{My}, \mathrm{Mz}, \alpha$ : at active nodes (global).
Element loads on nodal line (load type number LTYPE * 10 defines the corresponding element load type on beam axis, see Assumptions and Limitations)
LTYPE, S1, Px, Py, Pz, Mx, My, Mz
LTYPE=11: point loads and moments in local directions.
LTYPE=12: point loads and moments in global directions.
LTYPE, 0 , Wx, Wy, Wz, Mx, My, Mz
LTYPE=21: uniformly distributed loads in local directions.
LTYPE=22: uniformly distributed loads in global directions ( $\mathrm{Mx}=0$ ).
LTYPE=23: uniformly distributed projected loads in global directions.
LTYPE, S1, Wx1, Wy1, Wz1, Mx1, My1, Mz1, S2, Wx2, Wy2, Wz2, Mx2, My2, Mz2
LTYPE=31: distributed loads in local directions.
LTYPE=32: distributed loads in global directions.
LTYPE=33: distributed projected loads in

global directions.<br>LTYPE, S1, Wx, Wy, Wz, Mx, My, Mz<br>LTYPE=41: trapezoidal loads in local directions.<br>LTYPE=42: trapezoidal loads in global directions.<br>LTYPE=43: trapezoidal projected loads in global directions.<br>DLDL, DLDG Not applicable.<br>DLEL,DLEG Not applicable.<br>PLDL, PLDG Not applicable.<br>Distributed Loads UDL<br>FLD, FLDG Not applicable.<br>Body Forces CBF<br>BFP, BFPE<br>Velocities VELO<br>Accelerations<br>ACCE<br>SSI, SSIE<br>Stress/Strains<br>SSIG<br>SSRG<br>Target TSSIE, TSSIA<br>Stress/Strains<br>Uniformly distributed loads. Wx, Wy, Wz, Mx, My, Mz : local forces and moments / unit length for element in local directions. See Assumptions and Limitations.<br>Constant body forces for Element. Xcbf, Ycbf, Zcbf, $\Omega_{\mathrm{x}}, \Omega_{\mathrm{y}}, \Omega_{\mathrm{z}}, \alpha \mathrm{x}, \alpha \mathrm{y}, \alpha z_{z}$<br>Body force potentials at nodes/for element. $\varphi 1, \varphi 2$, $\varphi 3,0$, Xcbf, Ycbf, Zcbf<br>Velocities. Vx, Vy, Vz: at nodes.<br>Acceleration. Ax, Ay, Az: at nodes<br>Initial stresses/strains at nodes/for element.<br>Components: Fx, Fy, Fz, Mx, My, Mz, 0, 0, $\varepsilon x$, $\varepsilon y, \varepsilon z, \psi x, \psi y, \psi z, 0,0,(\sigma x, \sigma x y, \sigma x z, \varepsilon x, \varepsilon x y$, $\varepsilon x z)$ Bracketed terms repeated for each fibre integration point.<br>Initial stresses/strains at Gauss points. These stresses/strains are specified in the same manner as SSI and SSIE.<br>Residual stresses at nodes/for element. Components: $0,0,0,0,0,0,0,0,0,0,0,0,(\sigma x, 0,0)$ Bracketed terms repeated for each fibre integration point.<br>Residual stresses at Gauss points. These stresses are specified in the same manner as SSR and SSRE.<br>Target stresses/strains at nodes/for<br>element.Components: Fx, Fy, Fz, Mx, My, Mz, 0, 0, $\varepsilon x, \varepsilon y, \varepsilon z, \psi x, \psi y, 0,0, \psi z,(\sigma x, \sigma x y, \sigma x z, \varepsilon x$,<br>$\varepsilon x y, \varepsilon x z)$ Bracketed terms repeated for each fibre integration point.<br>TSSIG Target stresses/strains at Gauss points. These

stresses/strains are specified in the same manner as TSSIE and TSSIA.

Temperatures TEMP, TMPE
Overburden Not applicable.
Phreatic Surface Not applicable.
Field Loads Not applicable.
Temp Dependent Not applicable.
Loads

Temperatures at nodes/for element. T, 0, dT/dy, $\mathrm{dT} / \mathrm{dz}, \mathrm{To}, 0, \mathrm{dTo} / \mathrm{dy}, \mathrm{dTo} / \mathrm{dz}$ in local directions

## LUSAS Output

Solver Force (default): Fx, Fy, Fz, Mx, My, Mz, Fb and Mb: axial force, shear forces, torque, moments, bishear and bimoments in local directions. Continuum stresses (OPTION 172): $\sigma_{x}, \sigma_{x y}, \sigma_{x z}$ in local directions. Strain: $\varepsilon x, \varepsilon y, \varepsilon z, \psi x, \psi y, \psi z, \alpha, \alpha ':$ axial, shear, torsional, flexural strains and torsional warping strainsin local directions.
Continuum strains (OPTION 172): $\varepsilon x, \varepsilon x y, \varepsilon_{x}$ : in local directions. By default element output is with respect to the nodal line. Option 380 outputs stress/strain resultants with respect to the beam centreline.
Modeller See Results Tables (Appendix K).

## Local Axes

$\square$ Standard line element For each element/active node, the local xy-plane is defined by the local $x$-axis and the orientation node. The local $y$-axis is perpendicular to the local x -axis and positive on the side of the element where the orientation node lies. The local y and z-axes form a right-handed set with the local x-axis. See Local Element Axes for details

## Sign Convention

$\square$ Standard beam element

## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements and large rotations (see Notes). Updated Not applicable.

## Lagrangian

Eulerian Not applicable.
Co-rotational For large displacements and large rotations.
P-Delta Displacements and rotations should be small (see Notes)

## Integration Schemes

Stiffness Default. 1-point (BMX21W and BMX22W), 2-point (BMX31W and BMX33W).
Fine. Same as default.
Mass Default. 2-point (BMX21W and BMX22W), 3-point (BMX31W and BMX33W).
Fine. Same as default.
Note: A 3-point Newton-Cotes integration rule is also available for BMX31W and BMX33W using option 134. This may be more applicable for infinitesimal strain, elastoplastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory manual.

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

36 Follower loads
55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity (see Notes)
102 Switch off load correction stiffness matrix due to centripetal acceleration
105 Lumped mass matrix.
134 Gauss to Newton-Cotes in plane (in the local x direction) integration for elements.
139 Output yielded integration points only.
172 Form the rigidity matrix by numerical cross section integration.
229 Co-rotational geometric nonlinearity.
380 Output stress/strain resultants relative to beam axes for eccentric elements
403 Introduce residual bending flexibility correction for 2-node thick beam BMI21, see Assumptions and Limitations (on by default).
404 Compute equivalent nodal loading from equilibrium considerations for 2-node thick beam BMX21, see Notes (on by default).
405 Specify geometric properties along beam centroidal axes.
406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes

418 Output stress resultants relative to beam centroidal axes for eccentric elements
421 P-Delta analysis, see Notes
432 Use P-Delta geometric stiffness matrix of thick beams for linear buckling analysis

## Notes, Assumptions and Limitations

1. The element is formulated from the so-called degenerate continuum concept, i.e. enforcing directly the modified Timoshenko hypothesis for thick beams to the continuum theory. Shearing deformations and torsional warping are included.
2. By default input of loads and output of element stress/strain resultants are with respect to the nodal line. Option 381 inputs loads, and option 380 outputs stress/strain resultants with respect to the beam centreline. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line.
3. When OPTION 403 is specified to introduce residual bending flexibility correction (on by default), for BMX21W and BMX22W, the axial force, torsion, bi-shear and bimoment are constant, while the other shear forces and moments vary linearly along the length of the beam. For BMX31W and BMX33W the axial force, all shear forces, all moments and the torsion vary linearly along the length.
4. When BMX21W is used together with OPTION 403 to introduce residual bending flexibility correction, its stiffness matrix is enhanced to the order of a cubic. Note that if OPTION 403 is used with eccentrically stacked elements, slippage can occur.
5. The end releases for this element allow a joint to be modelled between adjacent elements. These joints allow rotation and translation of one beam with respect to another without load transferral as well as different warping conditions in adjacent elements. The rotations and translations remain in the local directions of the beam elements and support large deformations.
6. Computation of the rigidity matrix by integration through the cross-section depth of the beam is necessary for all linear and nonlinear material models. By default OPTION 172 is invoked automatically and a $3 * 3$ and $5 * 5$ point Newton-Cotes integration rule is used respectively for linear and nonlinear materials for quadrilaterals; and a 7 point cubic rule is used for both linear and nonlinear materials for triangles. This allows the output of stresses at the numerical cross section integration points.
7. OPTION 36 is only applicable for use with element load types ELDS and UDL. Specifying this option makes these element loads follow the element geometry as the analysis progresses.
8. For large deformation analyses the following geometric properties (Wagner constants) are required (see Geometric Properties) if Option $424=$ T: Iyr, Igr, Irr and Iwr at each node. If these constants are set to zero, the Wagner effect will be ignored, and the results may not be correct if twist rotations are not small.
9. When a step by step dynamic analysis is carried out using BMI elements with distributed loading, the "free body force diagrams" pertaining to applied loading, are not superimposed on the nodal values, to do so would lead to erroneous results until a steady state is reached. It should therefore be noted that different force diagrams will be obtained for BMI elements if static and dynamic analyses are directly compared.
10. OPTION 229 considers large displacements and large rotations using a co-rotational formulation. When both options 87 and 229 are true, a local Total Lagrangian formulation will be used within a global co-rotational framework. Note that OPTION 87 has no effect when specified without OPTION 229.
11. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command.
12. The P-Delta formulation is only applicable to lower order (2-noded) beams, higher order beams used in a P-Delta analysis will default to co-rotational GNL.
13. The Smoothed Multi Crack Concrete Model (109) can be used with this element, however, due to the "plane sections remaining plane" hypothesis, crack widths cannot be computed.
14. Partial fixities and rigid ends are defined via the ELEMENT TOPOLOGY data and follow on the same line after the end releases, for example:


The character $K$ is used to identify that the partial fixity stiffnesses $\hat{k}_{12} \hat{k}_{15}$ are being explicitly defined, while the character $N$ signifies that fixity factors, $n_{12} n_{15}$ are being defined. The fixity factors are used as follows:
$\hat{k}_{i j}=\frac{n_{i j}}{1-n_{i j}} \tilde{k}_{i j}$

The value of the factor $n_{i j j}$ ranges from zero for a pinned connection to 1.0 for a fully fixed connection.

The values $r_{1}$ and $r_{2}$ are the rigid end lengths at nodes 1 and 2 and $\lambda$ is the rigidity factor ( $1.0=$ fully rigid, the default). The factors m 1 and m 2 dictate how much mass to include for the rigid ends, full mass $=1.0\left(\right.$ default $\left.\mathrm{m}_{1}=\mathrm{m}_{2}=0.0\right)$.

## Restrictions

Ensure mid-side node centrality
A Avoid excessive element curvature
BMX22 and BMX33 are not available for selection currently within LUSAS Modeller.

## Recommendations on Use

- The elements may be used for linear and nonlinear analysis of three dimensional beam, frame and arch structures. BMX21W and BMX22W may also be used as a stiffener for the QTS4 shell element; while BMX31W and BMX33W may be used as a stiffener for the QTS8 shell element.


## 2D Kirchhoff Thin Beam Elements

## General

Element Name


BM3


Beams
Kirchhoff Beams

## Subgroup

Element
Element Description

Parabolically curved thin beam element in which shear deformations are excluded. The element can accommodate varying geometric properties along the length.
Number Of 3
Nodes
Freedoms
dU : (relative displacement) at mid-side node.
Coordinates
$\mathrm{U}, \mathrm{V}, \theta \mathrm{z}$ : at end nodes.
Node X, Y: at each node.

## Geometric Properties

## A, Izz, ey At each node

SF1,SF2,SF3 Optional scale factors applied to the geometric properties in the MF1,MF2,MF3 calculation of the stiffness and mass matrices

A Cross sectional area
Izz 2nd moment of area about local z-axis (see Definition).
ey Eccentricity from beam xz-plane to nodal line (+ve in +ve local ydirection)

For a beam with eccentricity $\mathbf{e}$ from the nodal line then $\mathrm{Izz}=\mathrm{e}^{2} \mathrm{~A}+\mathrm{Ina}$ and $\mathrm{Iz}=\mathrm{eA}$ ( $\mathrm{Ina}=\mathrm{I}$ about centroidal axis).

For MATERIAL MODEL 29 additional geometric properties are appended to the previous 9 geometric properties; see Notes.

## Material Properties

| Linear .. Isotropic: |  | MATERIAL PROPERTIES (Elastic: Isotropic) RIGIDITIES 3 (Rigidities:Beam) |
| :---: | :---: | :---: |
|  | Rigidities: |  |
| Matrix | Not applicable |  |
| Joint | Not applicable |  |
| Concrete | Not applicable |  |
| Elasto-Plastic | Stress resultant: | MATERIAL PROPERTIES NONLINEAR 29 <br> (Elastic: Isotropic, Plastic: Resultant) (ifcode=1 or 2, see Notes) |
| Creep | AASHTO | CREEP PROPERTIES (Creep) |
|  |  | MATERIAL PROPERTIES NONLINEAR 86 AASHTO <br> (Concrete creep model to AASHTO code of Practice) |
|  | CEB-FIP | MATERIAL PROPERTIES NONLINEAR 86 CEBFIP (Concrete creep model to CEB-FIP Model Code 1990) |
|  | Chinese | MATERIAL PROPERTIES NONLINEAR 86 CHINESE <br> (Chinese creep model to Chinese Code of Practice) |
|  | Eurocode | MATERIAL PROPERTIES NONLINEAR 86 EUROCODE <br> (Concrete creep model to EUROCODE_2) |
|  | IRC | MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice) |
| Damage | Not applicable |  |
| Viscoelastic | Not applicable |  |
| Shrinkage |  | SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER |
| Rubber | Not applicable |  |
| Generic Polymer | Not applicable |  |
| Composite | Not applicable |  |

## Loading

Prescribed Value PDSP, TPDSP Concentrated CL Loads
Element Loads ELDS

## Distributed Loads UDL

FLD, FLDG
Body Forces CBF

BFP, BFPE

Velocities VELO
Accelerations ACCE
Initial SSI, SSIE
Stress/Strains

Prescribed variable. U, V, $\theta \mathrm{z}$ : at end nodes.
Concentrated loads. Px, Py, Mz: at end nodes. dPx: in local x direction at mid-side node.
Element loads on nodal line (load type number LTYPE *10 defines the corresponding element load type on beam axis).
LTYPE, S1, Px, Py, Mz
LTYPE=11: point loads and moments in local directions.
LTYPE=12: point loads and moments in global directions.
LTYPE, $0, \mathrm{Wx}, \mathrm{Wy}, \mathrm{Mz}$
LTYPE=21: uniformly distributed loads in local directions.
LTYPE=22: uniformly distributed loads in global directions.
LTYPE=23: uniformly distributed projected loads in global directions
LTYPE, S1, Wx1, Wy1, Mz1, S2, Wx2, Wy2, Mz2
LTYPE=31: distributed loads in local directions.
LTYPE=32: distributed loads in global directions.
LTYPE=33: distributed projected loads in global directions
LTYPE, S1, Wx, Wy, Mz
LTYPE=41: trapezoidal loads in local directions.
LTYPE=42: trapezoidal loads in global directions.
LTYPE=43: trapezoidal projected loads in global directions
Uniformly distributed loads. Wx, Wy: force/unit length in local directions.
Not applicable.
Constant body forces for element. Xcbf, Ycbf, $\Omega \mathrm{x}$, $\Omega \mathrm{y}, \Omega_{\mathrm{z}}, \alpha_{\mathrm{z}}$
Body force potentials at nodes/for element. $\varphi_{1}, \varphi_{2}, 0$, $0, \mathrm{Xcbf}, \mathrm{Ycbf}$
Velocities. Vx, Vy: at nodes.
Acceleration Ax, Ay: at nodes
Initial stresses/strains at nodes/for element. Fx, Mz,
0 : forces, moments in local directions. $\varepsilon x, \psi z, 0$ : strains in local directions.
Initial stresses/strains at Gauss points $\mathrm{Fx}, \mathrm{Mz}, 0$ :

| Residual Stresses |  | forces, moments in local directions. $\varepsilon x, \psi z, 0$ : strains in local directions. |
| :---: | :---: | :---: |
|  | SSR, SSRE | Residual stresses at nodes/for element. Fx, Mz, 0: forces, moments in local directions. |
|  | SSRG | Residual stresses at Gauss points $\mathrm{Fx}, \mathrm{Mz}, 0$ : forces, moments in local directions. |
| Temperatures | TEMP, TMPE | Temperatures at nodes/for element. T, $0, \mathrm{dT} / \mathrm{dy}, 0$, To, 0 , dTo/dy, 0 |
| Target Stress/Strains | $\begin{aligned} & \text { TSSIE, } \\ & \text { TSSIA } \end{aligned}$ | Target stresses/strains at nodes/for element. Fx, Mz, 0 : forces, moments in local directions. $\varepsilon x, \psi z, 0$ : strains in local directions. |
|  | TSSIG | Target stresses/strains at Gauss points Fx, Mz, 0 : forces, moments in local directions. $\varepsilon x, \psi z, 0$ : strains in local directions. |
| Overburden | Not applicable. |  |
| Phreatic Surface | Not applicable. |  |
| Field Loads | Not applicable. |  |
| Temp Dependent Loads | Not applicable. |  |

## LUSAS Output

Solver Force (default): Fx, Fy, Mz: forces, moments in local directions (see Notes).
Strain: $\varepsilon x, \varepsilon y, \psi z$ : axial, flexural strains in local directions.
By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal axis.
Modeller See Results Tables (Appendix K).

## Local Axes

- Standard line element


## Sign Convention

Standard beam element

## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements, small rotations and small strains.
Updated For large displacements, large rotations and small strains. Lagrangian

Eulerian Not applicable.
Co-rotational Not applicable.

## Integration Schemes

| Stiffness | Default. | 2-point. |
| :---: | :--- | :--- |
|  | Fine (see Options). | 3-point. |
| Mass | Default. | 2-point. |
|  | Fine (see Options). | 3-point. |

A 3-point Newton-Cotes integration rule is also available using option 134. This may be more applicable for infinitesimal strain, elastoplastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory manual.

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule for element.
54 Updated Lagrangian geometric nonlinearity.
55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity.
105 Lumped mass matrix
134 Gauss to Newton-Cotes in plane (in the local $x$ direction) integration for elements.
157 Material model 29 (non cross-section elements), see Notes.
170 Suppress transfer of shape function arrays to disk.
405 Specify geometric properties along beam centroidal axes
406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes.
418 Output stress resultants relative to beam centroidal axes for eccentric elements

## Notes on Use

1. The element formulation is based on the constrained super-parametric approach. The variation of axial force along the beam is linear. The variation of displacement is quadratic in the local $x$-direction and cubic in the local $y$-direction. Shear force is constant.
2. Input of geometric properties (OPTION 405) and loads (OPTION 406), and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axis. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line
3. For nonlinear material model 29 the following geometric properties are appended to those already specified (see Geometric Properties).

- $\quad \mathrm{A}^{\mathrm{p}}, \mathrm{Zzz}^{\mathrm{p}}, \mathrm{S}^{\mathrm{p}}$ at each node (i.e. nodes $1,2,3$ )
- $\quad \mathrm{A}^{\mathrm{p}}$ Plastic area (=elastic area)
- $\quad \mathrm{Zzz}{ }^{\mathrm{p}}$ Plastic modulus for bending about z axis
- $\quad S^{p}$ Plastic area for shear $\left(S^{p}=0\right)$

4. For nonlinear material model 29 the following ifcode parameters should be

- ifcode=1 for circular hollow sections.
- $\quad$ ifcode $=2$ for solid rectangular sections.

5. Temperature dependent properties cannot be used with material model 29.
6. The element should not be coupled to the face of a two dimensional continuum element because of the midside node incompatibility.
7. The rigidity matrix for BM3 is evaluated explicitly from the material and geometric properties for both linear and nonlinear materials.
8. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command

## Restrictions

Ensure mid-side node centrality
$\square$ Avoid excessive element curvature

## Recommendations on Use

The element may be used for linear and nonlinear analysis of two dimensional beam, frame and arch structures. The 2-noded straight beam (BMI2 is more effective for the linear analysis of structures containing straight members of constant cross-section, e.g. plane frames.

## 2D Kirchhoff Thin Beam Element with Quadrilateral CrossSection

## General

## Element Name

## BMX3



## Element Group <br> Beams

## Element <br> Kirchhoff Beams

Subgroup
Element
Description
Parabolically curved thin beam elements in which shear deformations are excluded. The quadrilateral cross-section may be eccentric and can vary along the element length.
Number Of 3
Nodes
Freedoms
$\mathrm{U}, \mathrm{V}, \theta \mathrm{z}$ : at end nodes.
dU: (relative displacement) at mid-side node.
Node X, Y: at each node.
Coordinates

## Geometric Properties

$\mathrm{y} 1, \mathrm{z} 1, \mathrm{y} 2, \mathrm{z} 2, \mathrm{y} 3, \mathrm{z} 3, \mathrm{y} 4, \mathrm{z4}$ : local cross section coordinate pairs at each node; followed by nt 12 , nt14: specifying the number of Newton-Cotes integration points in the direction defined by the local cross-section points 1-2 and 1-4 (zero indicates default values). See Notes. Multiple quadrilateral cross-sections can be used to build up complex beam cross-sections.
Note. The coordinates of the cross section are numbered clockwise about the local x -axis (the beam nodal line). That is, a right-hand screw rule in the direction of increasing $x$.


## Material Properties

Matrix Not applicable
Joint Not applicable
Concrete Not applicable
Elasto-Plastic Stress resultant:

Tresca:

DruckerPrager:

MohrCoulomb:

Optimised Implicit Von Mises:
Volumetric
Crushing: Stress Potential Creep

AASHTO

CEB-FIP

Chinese

Eurocode

MATERIAL PROPERTIES (Elastic: Isotropic)

MATERIAL PROPERTIES NONLINEAR 29 (Elastic: Isotropic, Plastic: Resultant) (ifcode=2, see Notes)
MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
MATERIAL PROPERTIES NONLINEAR 65
(Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
MATERIAL PROPERTIES NONLINEAR 75
(Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic)
Not applicable

STRESS POTENTIAL VON_MISES
(Isotropic: von Mises, Modified von Mises)
CREEP PROPERTIES (Creep)
MATERIAL PROPERTIES NONLINEAR 86 AASHTO
(Concrete creep model to AASHTO code of Practice)

MATERIAL PROPERTIES NONLINEAR 86 CEBFIP
(Concrete creep model to CEB-FIP Model Code 1990)

MATERIAL PROPERTIES NONLINEAR 86 CHINESE
(Chinese creep model to Chinese Code of Practice)
MATERIAL PROPERTIES NONLINEAR 86 EUROCODE
(Concrete creep model to EUROCODE_2)
MATERIAL PROPERTIES NONLINEAR 86 IRC

(Concrete creep model to Indian IRC code of Practice)<br>\section*{Damage}<br>Viscoelastic Not applicable Shrinkage<br>Rubber Not applicable<br>Generic Polymer Not applicable<br>Composite Not applicable<br>DAMAGE PROPERTIES SIMO, OLIVER (Damage)<br>SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER

## Loading

Prescribed Value PDSP, TPDSP

Concentrated CL
Loads
Element Loads ELDS

Prescribed variable. $\mathrm{U}, \mathrm{V}, \theta \mathrm{z}$ : at end nodes. dU at mid-side node.
Concentrated loads. Px, Py, Mz: at end nodes (global). dPx: at mid-side node (local).
Element loads on nodal line (load type number LTYPE *10 defines the corresponding element load type on beam axis).
LTYPE, S1, Px, Py, Mz
LTYPE=11: point loads and moments in local directions.
LTYPE=12: point loads and moments in global directions.
LTYPE, 0, Wx, Wy, Mz
LTYPE=21: uniformly distributed loads in local directions.
LTYPE=22: uniformly distributed loads in global directions.
LTYPE=23: uniformly distributed projected loads in global directions
LTYPE, S1, Wx1, Wy1, Mz1, S2, Wx2, Wy2, Mz2
LTYPE=31: distributed loads in local directions.
LTYPE=32: distributed loads in global directions.
LTYPE=33: distributed projected loads in global directions
LTYPE, S1, Wx, Wy, Mz
LTYPE=41: trapezoidal loads in local directions.
LTYPE=42: trapezoidal loads in global directions.
LTYPE=43: trapezoidal projected loads in global directions

## Distributed Loads UDL <br> FLD, FLDG <br> Body Forces CBF

BFP, BFPE

Velocities VELO
Accelerations ACCE
Initial SSI, SSIE
Stress/Strains

SSIG

Residual Stresses SSR, SSRE
SSRG

Uniformly distributed loads. Wx, Wy: force/unit length in local directions.
Not applicable.
Constant body forces for element. Xcbf, Ycbf, $\Omega_{\mathrm{x}}$, $\Omega \mathrm{y}, \Omega_{\mathrm{z}}, \alpha \mathrm{z}$

Body force potentials at nodes/for element. $\varphi_{1}, \varphi_{2}$, $0,0, \mathrm{Xcbf}, \mathrm{Ycbf}$
Velocities. Vx, Vy: at nodes.
Acceleration Ax, Ay: at nodes
Initial stresses/strains at nodes/for element. Resultants (for linear material models without numerical cross section integration and model 29, see Notes): Fx, Mz, 0: forces, moments in local
directions. $\mathcal{E x}, \psi \mathrm{z}, 0$ : strains in local directions.
Initial stresses/strains at Gauss points.
(1) Resultants (for linear material models without numerical cross section integration and model 29, see Notes). Fx, Mz, 0: forces, moments in local
directions. $\varepsilon x, \psi z, 0$ strains in local directions.
(2) Components (for linear material models with numerical cross section integration and all nonlinear material models except 29): $\mathrm{Fx}, \mathrm{Mz}, 0, \varepsilon_{x}$, $\psi z, 0,(\sigma x, \varepsilon x)$. Bracketed terms repeated at each fibre integration point.
Not applicable.
Residual stresses at Gauss points.
(1) Resultants (material model 29): Fx, Mz, 0
(2) Components (all nonlinear material models except 29 , also linear material models with numerical cross section integration): $0,0,0,0,0,0$,
( $\sigma x, \varepsilon x$ ) Bracketed term repeated for each fibre integration point.
Target TSSIE, TSSIA Stress/Strains

Target stresses/strains at nodes/for element. Resultants (for linear material models without numerical cross section integration and model 29, see Notes): Fx, Mz, 0: forces, moments in local directions. $\mathcal{E x}, \psi \mathrm{z}, 0$ : strains in local directions.
TSSIG Target stresses/strains at Gauss points.
(1) Resultants (for linear material models without numerical cross section integration and model 29, see Notes). Fx, Mz, 0: forces, moments in local
directions. $\varepsilon \mathrm{x}, \psi \mathrm{z}, 0$ strains in local directions. (2) Components (for linear material models with numerical cross section integration and all nonlinear material models except 29): Fx, Mz, 0, \&x, $\psi z, 0,(\sigma x, \varepsilon x)$. Bracketed terms repeated at each fibre integration point.
Temperatures TEMP, TMPE Temperatures at nodes/for element T, $0, \mathrm{dT} / \mathrm{dy}, 0$, To, $0, \mathrm{dTo} / \mathrm{dy}, 0$ : in local directions.
Overburden Not applicable.
Phreatic Surface Not
applicable.
Field Loads Not
applicable.
Temp Dependent Not
Loads applicable.

## LUSAS Output

Solver Force (default): Fx, Mz, Fy: forces, moment in local directions (see Notes)
Continuum stresses (OPTION 172): $\sigma x$ : in local directions.
Strain: $\mathcal{E x}, \psi z, 0$ : axial, flexural strains in local directions.
Continuum strains (OPTION 172): $\varepsilon x$ : in local directions.
By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal axis.
Modeller See Results Tables (Appendix K).

## Local Axes

- Standard line element


## Sign Convention

$\square$ Standard beam element

## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements, small rotations and small strains.
Updated For large displacements, large rotations and small strains. Lagrangian

Eulerian Not applicable.
Co-rotational Not applicable.

## Integration Schemes

| Stiffness | Default. | 2-point. |
| :---: | :--- | :--- |
|  | Fine (see Options). | 3-point. |
| Mass | Default. | 2-point. |
|  | Fine (see Options). | 3-point. |

A 3-point Newton-Cotes integration rule is also available using option 134. This may be more applicable for infinitesimal strain, elastoplastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory manual.

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule for element.
32 Suppress stress output but not resultants
54 Updated Lagrangian geometric nonlinearity.
55 Output strains as well as stresses
87 Total Lagrangian geometric nonlinearity
105 Lumped mass matrix
134 Gauss to Newton-Cotes in plane (in the local x direction) integration for elements.
157 Material model 29 (non cross-section elements), see Notes.
170 Suppress transfer of shape function arrays to disk.
172 Formulate rigidity matrix by integrating across the cross-section
406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
418 Output stress resultants relative to beam centroidal axes for eccentric elements

## Notes on Use

1. The element formulation is based on the constrained super-parametric approach. The variation of axial force along the beam is linear. The variation of displacement is quadratic in the local $x$-direction and cubic in the local $y$-direction. Shear force is constant.
2. Input of loads (OPTION 406), and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axis. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line. Fiber stress/strain results are output at the actual location
3. Initial strain resultants may be input for any material model.
4. The number of numerical cross-section integration points, nt 12 and nt14, may be specified but for improved performance the number of integration points corresponding to the y direction can be defined correctly (the beam bends about the local z -axis) and the integration rule in the other direction may be set to 1 .
5. For nonlinear material model 29 ifcode must be set to 2 for solid rectangular sections. Multiple quadrilateral cross-sections can be used to build up complex beam crosssections.
6. Temperature dependent properties cannot be used with material model 29.
7. The element should not be coupled to the face of a two dimensional continuum element because of the midside node incompatibility.
8. Computing the rigidity matrix by integration through the cross-section depth of the beam is necessary for all nonlinear material models (except 29). By default option 172 is invoked automatically and a 5 point Newton-Cotes integration rule is used.
9. By default, the rigidity matrix is evaluated explicitly for linear materials. A 3 point Newton-Cotes rule may be invoked using option 172. Numerical cross section integration enables top, middle and bottom stress output.

## Restrictions

Ensure mid-side node centrality
$\square$ Avoid excessive element curvature

## Recommendations on Use

The element may be used for linear and nonlinear analysis of two dimensional beam, frame and arch structures. The 2-noded straight beam (BMI2) is more effective for linear analysis of structures containing straight members of constant cross-section, e.g. plane frames.

## 3D Kirchhoff Thin Beam Elements

## General



Element Group Beams
Element Kirchhoff Beams
Subgroup
Element Description

Curved beam elements in 3D for which shearing deformations are
excluded. The elements can accommodate varying geometric properties along the length.
Number Of 3 (BS3).
Nodes 4 (BS4). The 4th node is used to define the local xy-plane.
Freedoms
$\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ : at end nodes (1 and 3)
$\mathrm{dU}, \mathrm{d} \theta \mathrm{x}$ :(relative displacement/rotation) at mid-length node.
Node X, Y, Z: at each node.
Coordinates

## Geometric Properties

A, Iyy, Izz, Jxx, Iy, Iz, Iyz, ez, ey At each node
SF1, SF2, SF3, SF4, SF5, SF6, SF7, Optional scale factors applied to the geometric
SF8, SF9, MF1, MF2, MF3, MF4, properties in the calculation of the stiffness and mass
MF5, MF6, MF7, MF8, MF9 matrices
A Cross sectional area
Iyy, Izz 2nd moment of area about local $y, z$ directions (see Definition)
Jxx Torsional constant.
Iy, Iz 1st moment of area about local $\mathbf{y}$, $\mathbf{z}$ directions (see Definition)
Iyz Product moment of area (see Definition)
ez Eccentricity from beam xy-plane to nodal line. (+ve in the + ve local $z$ direction). (See Notes)
ey Eccentricity from beam xz-plane to nodal line. (+ve in the +ve local y direction). (See Notes)

For MATERIAL MODEL 29 additional geometric properties are appended to the previous 21 geometric properties (see Notes).

## Material Properties

| Linear | Isotropic: <br> Rigidities: | MATERIAL PROPERTIES (Elastic: Isotropic) RIGIDITIES 6 (Rigidities: Beam) |
| :---: | :---: | :---: |
| Matrix | Not applicable |  |
| Joint | Not applicable |  |
| Concrete | Not applicable |  |
| Elasto-Plastic | Stress resultant: | MATERIAL PROPERTIES NONLINEAR 29 (Elastic: Isotropic, Plastic: Resultant) (ifcode=1 or 2, see Notes) |
| Creep | AASHTO | CREEP PROPERTIES (Creep) |
|  |  | MATERIAL PROPERTIES NONLINEAR 86 AASHTO <br> (Concrete creep model to AASHTO code of Practice) |
|  | CEB-FIP | MATERIAL PROPERTIES NONLINEAR 86 CEBFIP (Concrete creep model to CEB-FIP Model Code 1990) |
|  | Chinese | MATERIAL PROPERTIES NONLINEAR 86 CHINESE <br> (Chinese creep model to Chinese Code of Practice) |
|  | Eurocode | MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2) |
|  | IRC | MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice) |
| Damage | Not applicable |  |
| Viscoelastic | Not applicable |  |
| Shrinkage |  | SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER |
| Rubber | Not applicable |  |

# Generic Polymer <br> Not applicable 

Composite Not applicable

## Loading

Prescribed Value PDSP, TPDSP

Concentrated CL
Loads
Element Loads ELDS

Distributed Loads UDL

FLD, FLDG
Body Forces CBF

BFP, BFPE

Prescribed variable. $\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ : at end nodes ( 1 and 3 ). $\mathrm{dU}, \mathrm{d} \theta \mathrm{x}$ : at mid-length node.
Concentrated loads. Px, Py, Pz, Mx, My, Mz: at end nodes. $\mathrm{dPx}, \mathrm{dMy}$ : at mid-length node.
Element loads on nodal line (load type number LTYPE * 10 defines the corresponding element load type on beam axis)
LTYPE, S1, Px, Py, Pz, Mx, My, Mz
LTYPE=11: point loads and moments in local directions.
LTYPE=12: point loads and moments in global directions.
LTYPE, 0, Wx, Wy, Wz, Mx, My, Mz
LTYPE=21: uniformly distributed loads in local directions.
LTYPE=22: uniformly distributed loads in global directions.
LTYPE=23: uniformly distributed projected loads in global directions.
LTYPE, S1, Wx1, Wy1, Wz1, Mx1, My1, Mz1, S2, Wx2, Wy2, Wz2, Mx2, My2, Mz2
LTYPE=31: distributed loads in local directions.
LTYPE=32: distributed loads in global directions.
LTYPE=33: distributed projected loads in global directions.
LTYPE, S1, Wx, Wy, Wz, Mx, My, Mz
LTYPE=41: trapezoidal loads in local directions.
LTYPE=42: trapezoidal loads in global directions.
LTYPE=43: trapezoidal projected loads in global directions.
Uniformly distributed loads. Wx, Wy, Wz: local forces/unit length.
Not applicable.
Constant body forces for element. Xcbf, Ycbf, Zcbf, $\Omega \mathrm{x}, \Omega \mathrm{y}, \Omega_{\mathrm{z}}$

Body force potentials at nodes/for element. $\varphi_{1}, \varphi_{2}$,
$\varphi_{3}, 0$, Xcbf, Ycbf, ZcbfVelocities. Vx, Vy, Vz: at nodes.Acceleration Ax, Ay, Az: at nodes
Initial stresses/strains at nodes/for element. Fx, My,$\mathrm{Mz}, \mathrm{Txz}, \mathrm{Txy}, 0$ : axial force, moments and torquesin local directions. $\varepsilon x, \psi y, \psi z, \psi x z, \psi x y, 0:$ axial,flexural and torsional strains in local directions.
Total torque $=\mathrm{Txz}+\mathrm{Txy}$, total torsional strain $=$
$y x z+\psi x y$.
SSIG Not applicable.
Residual Stresses SSR, SSRE Not applicable.
SSRG
Target TSSIE, TSSIA Target stresses/strains at nodes/for element. Fx, My, Stress/Strains $\mathrm{Mz}, \mathrm{Txz}, \mathrm{Txy}, 0$ : axial force, moments and torques in local directions. $\varepsilon x, \psi y, \psi z, \psi x z, \psi x y, 0$ : axial, flexural and torsional strains in local directions.

$$
\text { Total torque }=\mathrm{Txz}+\mathrm{Txy} \text {, total torsional strain }=
$$

$$
y x z+\psi x y .
$$

Not applicable.
Temperatures TEMP, TMPE Temperatures at nodes/for element. T, 0 , dT/dy, dT/dz, To, 0, dTo/dy, dTo/dz
Overburden Not applicable.
Phreatic Surface Not applicable.
Field Loads Not applicable.
Temp Dependent ..... Not
Loads applicable.

## LUSAS Output

Solver Force (default): Fx, Fy, Fz, My, Mz, Txz, Txy: axial force, moments, torques and shear forces in local directions. (Total torque $=\mathrm{Txz}+\mathrm{Txy}$ ). Strain: $\varepsilon x, \psi y, \psi z, \psi x z, \psi x y, 0$ : axial, flexural and torsional strains in
local directions.
By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal axes.
Modeller See Results Tables (Appendix K).

## Local Axes

For BS3 the local xy-plane is defined by the 3 element nodes. The local y-axis is perpendicular to the local x -axis and positive on the convex side of the element. The local y and z -axes form a right handed set with the local x -axis.
For BS4 the local xy-plane is defined by the 2 end nodes of the beam and the 4th node. The local $y$-axis is perpendicular to the local $x$-axis and positive on the side of the element where the 4th node lies. The local y and z -axes form a right handed set with the local x -axis. See Local Element Axes for more details.

## Sign Convention

$\square$ Standard beam element

## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements, small rotations and small strains.
Updated For large displacements, large rotations and small strains.
Lagrangian
Eulerian Not applicable.
Co-rotational Not applicable.

## Integration Schemes

Stiffness Default. 2-point.
Fine (see 3-point. Options).
Mass Default. 2-point.
Fine (see 3-point.
Options).
A 3-point Newton-Cotes integration rule is also available using option 134. This may be more applicable for infinitesimal strain, elastoplastic analyses of plane frames with straight
members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory manual.

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule for element.
54 Updated Lagrangian geometric nonlinearity.
55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity.
102 Switch off load correction stiffness matrix due to centripetal acceleration.
105 Lumped mass matrix.
134 Gauss to Newton-Cotes in plane (in the local x direction) integration for elements.
157 Material model 29 (non cross-section elements), see Notes.
170 Suppress transfer of shape function arrays to disk.
405 Specify geometric properties along beam centroidal axes
406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
418 Output stress resultants relative to beam centroidal axes for eccentric elements

## Notes on Use

1. The element formulation is based on the Kirchhoff hypothesis for thin beams (i.e. the exclusion of shearing deformations).
2. The variation of axial force, moments and torsion along the length of the beam can be regarded as linear. Shear force variations are constant.
3. Input of geometric properties (OPTION 405) and loads (OPTION 406), and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axes. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line.
4. For nonlinear material model 29 the following geometric properties are appended to those already specified (see Geometric Properties).

- $A^{\mathrm{p}}, \mathrm{Zyy}^{\mathrm{p}}, \mathrm{Zzz}^{\mathrm{p}}, \mathrm{Zy}^{\mathrm{p}}, \mathrm{Zz}^{\mathrm{p}}, \mathrm{S}^{\mathrm{p}}$ at each node (i.e. nodes $1,2,3$ ).
- $\quad \mathrm{A}^{\mathrm{p}}$ Plastic area (=elastic area)
- $\quad \mathrm{Zyy}^{\mathrm{p}}$, Zzz $^{\mathrm{p}}$ Plastic moduli for bending about $\mathrm{y}, \mathrm{z}$ axes
- $\mathrm{Zy}^{\mathrm{p}}, \mathrm{Zz}^{\mathrm{p}}$ Plastic moduli for torsion about $\mathrm{y}, \mathrm{z}$ axes.
- $\quad S^{\mathrm{p}}$ Plastic area for shear $\left(\mathrm{S}^{\mathrm{p}}=0\right)$.

Where the fully plastic torsional moment $=\sigma y\left(\mathrm{Zy}^{\mathrm{p}}+\mathrm{Zz}^{\mathrm{p}}\right)$.
5. For nonlinear material model 29 the following ifcode parameters should be used

- $\quad$ ifcode $=1$ for circular hollow sections.
- $\quad$ ifcode $=2$ for solid rectangular sections.

6. Temperature dependent properties cannot be used with material model 29.
7. The element should not be coupled to the edges of either continuum or shell elements because of midside node incompatibility.
8. The rigidity matrix for BS3 and BS4 is evaluated explicitly from the geometric properties for both linear and nonlinear materials.
9. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command.

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature


## Recommendations on Use

The elements may be used for linear and nonlinear analysis of three dimensional beam, frame and arch structures. The 2-noded straight beam (BMI21) is more effective for linear analysis of structures containing straight members of constant cross-section, e.g. space frames.

# 3D Kirchhoff Thin Beam Element with Quadrilateral CrossSection 

## General



BSX4


## Element Group <br> Element <br> Subgroup <br> Element Description

Beams

## Kirchhoff Beams

Curved beam elements in 3D for which shearing deformations are excluded. The element has a quadrilateral cross section which may vary along the element length.
Number Of 4. The 4th node is used to define the local xy-plane.
Nodes
Freedoms

Node
$\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ : at the end nodes (1 and 3)
$\mathrm{dU}, \mathrm{d} \theta \mathrm{x}$ : (relative displacement/rotation) at the mid-length node.
$\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.
Coordinates

## Geometric Properties

$\mathrm{y} 1, \mathrm{z} 1, \mathrm{y} 2, \mathrm{z} 2, \mathrm{y} 3, \mathrm{z} 3, \mathrm{y} 4, \mathrm{z} 4$ : local cross section coordinate pairs at each node; followed by nt12, nt 14 : specifying the number of Newton-Cotes integration points in the direction defined by the local cross-section points 1-2 and 1-4 (zero indicates default values). Multiple quadrilateral cross-sections can be used to build up complex beam cross-sections.

Note. The coordinates of the cross section are numbered clockwise about the local x -axis (the beam nodal line). That is, a right-hand screw rule in the direction of increasing $x$.


## Material Properties

Linear Isotropic:Matrix Not applicableJoint Not applicable
Concrete Not applicableElasto-Plastic Stressresultant:Tresca:Drucker-Prager:
Mohr-Coulomb:OptimisedImplicit VonMises:
VolumetricCrushing:StressPotential
CreepAASHTO
CEB-FIP
Chinese

MATERIAL PROPERTIES (Elastic: Isotropic)

Not applicable.

MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
MATERIAL PROPERTIES NONLINEAR 75
(Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic)
Not applicable

STRESS POTENTIAL VON_MISES
(Isotropic: von Mises, Modified von Mises)
CREEP PROPERTIES (Creep)
MATERIAL PROPERTIES NONLINEAR 86 AASHTO
(Concrete creep model to AASHTO code of Practice)

MATERIAL PROPERTIES NONLINEAR 86 CEBFIP
(Concrete creep model to CEB-FIP Model Code 1990)

MATERIAL PROPERTIES NONLINEAR 86
CHINESE
(Chinese creep model to Chinese Code of Practice)
Eurocode
IRC
Damage
Viscoelastic Not applicable
ShrinkageRubber Not applicable
Generic Polymer Not applicable
Composite Not applicable
MATERIAL PROPERTIES NONLINEAR 86 EUROCODE
(Concrete creep model to EUROCODE_2)
MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
DAMAGE PROPERTIES SIMO, OLIVER(Damage)
SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER

## Loading

Prescribed Value PDSP, TPDSP

Concentrated CL Loads

Element Loads ELDS

Prescribed variable. $\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ : at the end nodes. $\mathrm{dU}, \mathrm{d} \theta \mathrm{x}$ : at the mid-length node.
Concentrated loads. Px, Py, Pz, Mx, My, Mz: at end nodes (global). dPx, dMx: at mid-length local node.
Element loads on nodal line (load type number LTYPE *10 defines the corresponding element load type on beam axis)
LTYPE, S1, Px, Py, Pz, Mx, My, Mz
LTYPE=11: point loads and moments in local directions.
LTYPE=12: point loads and moments in global directions.
LTYPE, 0 , Wx, Wy, Wz, Mx, My, Mz
LTYPE=21: uniformly distributed loads in local directions.
LTYPE=22: uniformly distributed loads in global directions.
LTYPE=23: uniformly distributed projected loads in global directions.
LTYPE, S1, Wx1, Wy1, Wz1, Mx1, My1, Mz1, S2, Wx2, Wy2, Wz2, Mx2, My2, Mz2

Distributed Loads UDL
FLD, FLDG
Body Forces CBF

BFP, BFPE

Velocities VELO
Accelerations ACCE
Initial SSI, SSIE Stress/Strains

SSIG

Residual Stresses SSR, SSRE

SSRG

Target TSSIE, TSSIA Stress/Strains

LTYPE=31: distributed loads in local directions. LTYPE=32: distributed loads in global directions. LTYPE=33: distributed projected loads in global directions.
LTYPE, S1, Wx, Wy, Wz, Mx, My, Mz
LTYPE=41: trapezoidal loads in local directions.
LTYPE=42: trapezoidal loads in global directions.
LTYPE=43: trapezoidal projected loads in global directions.
Uniformly distributed loads. Wx, Wy, Wz: forces/unit length in local directions.
Not applicable
Constant body forces for element. Xcbf, Ycbf, Zcbf, $\Omega_{\mathrm{x}}, \Omega_{\mathrm{y}}, \Omega_{\mathrm{z}}, \alpha_{\mathrm{x}}, \alpha \mathrm{y}, \alpha_{\mathrm{z}}$
Body force potentials at nodes/for element. $\varphi_{1}, \varphi_{2}$,甲 3,0, Xcbf, Ycbf, Zcbf
Velocities. Vx, Vy, Vz: at nodes.
Acceleration Ax, Ay, Az: at nodes
Initial stresses/strains at nodes/for element.
Components: Fx, My, Mz, $0,0,0, \varepsilon x, \psi y, \psi z, 0$, $0,0,(\sigma x, \sigma x y, \sigma x z, \sigma y z, \varepsilon y z, \varepsilon x, \varepsilon x z, \varepsilon y z)$
Bracketed terms repeated for each fibre integration point.
Initial stresses/strains at Gauss points. These stresses/strains are specified in the same manner as SSI and SSIE.
Residual stresses at nodes/for element.
Components: $0,0,0,0,0,0,0,0,0,0,0,0,(\sigma x$, $\sigma x y, \sigma x z, \sigma y z$,$) Bracketed terms repeated for each$ fibre integration point.
Residual stresses at Gauss points. These stresses are specified in the same manner as SSR and SSRE.
Target stresses/strains at nodes/for element.
Components: $\mathrm{Fx}, \mathrm{My}, \mathrm{Mz}, 0,0,0, \varepsilon x, \psi y, \psi z, 0$, $0,0,0,0,0,0,0,0,0,0,0,0,0,0,(\sigma x, \sigma x y, \sigma x z$, $\sigma y z, \varepsilon y z, \varepsilon x, \varepsilon x z, \varepsilon y z)$ Bracketed terms repeated for each fibre integration point.
TSSIG
Target stresses/strains at Gauss points. These stresses/strains are specified in the same manner as TSSIE and TSSIA.
Temperatures TEMP, TMPE Temperatures at nodes/for element. T, $0, \mathrm{dT} / \mathrm{dy}$,
$\mathrm{dT} / \mathrm{dz}, \mathrm{To}, 0, \mathrm{dTo} / \mathrm{dy}, \mathrm{dTo} / \mathrm{dz}$ : in local directions.
Overburden Not applicable.
Phreatic Surface Not
applicable.
Field Loads Not applicable
Temp Dependent Not applicable
Loads

## LUSAS Output

Solver Force (default): Fx, My, Mz, Txz, Txy, Fy, Fz: axial force, moments, torques and shear forces in local directions. (Total Torque $=\mathrm{Txz}+$ Txy).
Continuum stresses (OPTION 172): $\sigma x, \sigma x y, \sigma x z, \sigma y z:$ in local directions.
Strain: $\varepsilon x, \psi y, \psi z, \psi x z, \psi x y:$ axial, flexural and torsional strains in local directions.
Continuum strains (OPTION 172): $\varepsilon x, \varepsilon_{x y}, \varepsilon_{x z}, \varepsilon y z:$ in local directions.
By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal axes.
Modeller See Results Tables (Appendix K).

## Local Axes

Standard line element. The local xy-plane is defined by the 2 end nodes of the beam and the 4th node. The local $y$-axis is perpendicular to the $x$-axis and positive on the side of the element where the 4th node lies.
The local y and z -axes form a right-hand set with the local x -axis.

## Sign Convention

- Standard beam element


## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements, small rotations and small strains.
Updated For large displacements, large rotations and small strains. Lagrangian

Eulerian Not applicable.
Co-rotational Not applicable.

## Integration Schemes

| Stiffness | Default. | 2-point. |
| :---: | :--- | :--- |
|  | Fine (see Options). | 3-point. |
| Mass | Default. | 2-point. |
|  | Fine (see Options). | 3-point. |

A 3-point Newton-Cotes integration rule is also available using option 134. This may be more applicable for infinitesimal strain, elastoplastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory manual.

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule for element.
54 Updated Lagrangian geometric nonlinearity.
55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity.
102 Switch off load correction stiffness matrix due to centripetal acceleration.
105 Lumped mass matrix.
134 Gauss to Newton-Cotes in plane (in the local x direction) integration for elements.
139 Output yielded integration points only.
170 Suppress transfer of shape function arrays to disk.
172 Form the rigidity matrix by numerical cross section integration.
406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
418 Output stress resultants relative to beam centroidal axes for eccentric elements

## Notes, Assumptions and Limitations

1. The element formulation is based on the Kirchhoff hypothesis for thin beams (i.e. the exclusion of shearing deformations)
2. The variation of axial force, moments and torsion along the length of the beam can be regarded as linear. Shear force is constant.
3. Input of loads (OPTION 406), and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axes. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line. Fiber stress/strain results are output at their actual location
4. Computation of the rigidity matrix by integration over the thickness is necessary for all nonlinear material models. For nonlinear models a $5 \times 5$ Newton-Cotes integration rule is used as default. For linear models a $3 \times 3$ rule is used as the default. This allows the output of stresses at the numerical cross section integration points.
5. The torsional constant is estimated from the computed values for Iyy and Izz, Jxx = Iyy + Izz.
6. For nonlinear material models, fibre integration is used across the cross-sectional area of the beam. Only axial deformation is considered in the plasticity computations, any torsional deformation is assumed to remain elastic.
7. The element should not be coupled to the face of a two dimensional continuum element because of the midside node incompatibility
8. Computing the rigidity matrix by integration through the cross-section depth of the beam is necessary for all nonlinear material models (except 29). By default OPTION 172 is invoked automatically and a $5 * 5$ point Newton-Cotes integration rule is used.
9. By default, the rigidity matrix is evaluated explicitly for linear materials. A $3 * 3$ point Newton-Cotes integration rule may be invoked using OPTION 172. Numerical cross section integration enables top, middle and bottom stress output.

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature


## Recommendations on Use

The elements may be used for linear and nonlinear analysis of three dimensional beam, frame and arch structures. The 2-noded straight beam (BMI21) is more effective for linear analysis of structures containing straight members of constant cross-section, e.g. space frames.

## 3D Semiloof Thin Beam Elements

## General

Element Name
BSL3, BSL4



## Element Group Beams

Element
Subgroup Description

Number Of Nodes
Freedoms

Element Curved beam elements in 3D which can be mixed with the semiloof shell elements TSL6 and QSL8. The elements can accommodate varying geometric properties. Shearing deformations are excluded. 3 or 4 . For BSL4 the 4th node is used to define the local xy-plane.
$\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ : at end nodes (1 and 3). $\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta_{1}, \theta_{2}$ : at mid-side node (node 2) (see Notes).
X, Y, Z: at each node.
Semiloof Beams

X,Y,Z: ateach node.

## Geometric Properties

A, Iyy, Izz, Jxx, Iy, Iz, Iyz, ez, ey at nodes 1, 2 and 3
SF1,SF2,SF3,SF4,SF5,SF6,SF7,SF8,SF9 Optional scale factors applied to the MF1,MF2,MF3,MF4,MF5,MF6,MF7,MF8,MF9 geometric properties in the calculation of the stiffness and mass matrices
A Cross sectional area
Iyy, Izz 2 nd moments of area in local $y, z$ axes (see Definition)
Jxx Torsional constant.
Iy, Iz 1st moment of area in local $y, z$ axes (see Definition)
Iyz Product moment of area (see Definition).
ez Eccentricity from beam xy-plane to

For MATERIAL MODEL 29 additional geometric properties are appended to the 21 properties above; see Notes.

## Material Properties

| Linear | Isotropic: | MATERIAL PROPERTIES (Elastic: Isotropic) |
| :---: | :---: | :---: |
|  | Rigidities: | RIGIDITIES Rigidities 6 (Rigidities: Beam) |
| Matrix | Not applicable |  |
| Joint | Not applicable |  |
| Concrete | Not applicable |  |
| Elasto-Plastic | Stress resultant: | MATERIAL PROPERTIES NONLINEAR 29 <br> (Elastic: Isotropic, Plastic: Resultant) (ifcode=1 or 2, see Notes) |
| Creep | AASHTO | CREEP PROPERTIES (Creep) |
|  |  | MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of Practice) |
|  | CEB-FIP | MATERIAL PROPERTIES NONLINEAR 86 CEB FIP <br> (Concrete creep model to CEB-FIP Model Code 1990) |
|  | Chinese | MATERIAL PROPERTIES NONLINEAR 86 CHINESE <br> (Chinese creep model to Chinese Code of Practice) |
|  | Eurocode | MATERIAL PROPERTIES NONLINEAR 86 EUROCODE <br> (Concrete creep model to EUROCODE_2) |
|  | IRC | MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice) |
| Damage | Not applicable |  |
| Viscoelastic | Not applicable |  |
| Shrinkage |  | SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER |
| Rubber | Not applicable |  |

Generic Polymer Not applicable
Composite Not applicable

## Loading

Prescribed Value PDSP, TPDSP

Concentrated CL Loads

Element Loads ELDS

Distributed Loads UDL

FLD, FLDG
Body Forces CBF

Prescribed variable. U, V, W, $\theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ : at end nodes. U, V, W, $\theta_{1}, \theta_{2}$ : at mid-side node.
Concentrated loads. Px, Py, Pz, Mx, My, Mz: at end nodes (global). Px, Py, Pz, M1, M2: at mid-side node ( $\mathrm{M}_{1}$ and $\mathrm{M}_{2}$ local).
Element loads on nodal line (load type number LTYPE *10 defines the corresponding element load type on beam axis)
LTYPE, S1, Px, Py, Pz, Mx, My, Mz
LTYPE=11: point loads and moments in local directions.
LTYPE=12: point loads and moments in global directions.
LTYPE, 0, Wx, Wy, Wz, Mx, My, Mz
LTYPE=21: uniformly distributed loads in local directions.
LTYPE=22: uniformly distributed loads in global directions.
LTYPE=23: uniformly distributed projected loads in global directions.
LTYPE, S1, Wx1, Wy1, Wz1, Mx1, My1, Mz1, S2, Wx2, Wy2, Wz2, Mx2, My2, Mz2
LTYPE=31: distributed loads in local directions.
LTYPE=32: distributed loads in global directions.
LTYPE=33: distributed projected loads in global directions.
LTYPE, S1, Wx, Wy, Wz, Mx, My, Mz
LTYPE=41: trapezoidal loads in local directions.
LTYPE=42: trapezoidal loads in global directions.
LTYPE=43: trapezoidal projected loads in global directions.
Uniformly distributed loads. Wx, Wy, Wz: force/unit length in local directions for element.
Not applicable.
Constant body forces for element. Xcbf, Ycbf, Zcbf, $\Omega_{\mathrm{x}}, \Omega_{\mathrm{y}}, \Omega_{\mathrm{z},} \alpha_{\mathrm{x}}, \alpha \mathrm{y}, \alpha_{\mathrm{z}}$

BFP, BFPE Body force potentials at nodes/for element. $\varphi_{1}, \varphi_{2}$, $\varphi 3,0, \mathrm{Xcbf}, \mathrm{Ycbf}, \mathrm{Zcbf}$
Velocities. Vx, Vy, Vz: at nodes.
Accelerations. Ax, Ay, Az: at nodes.
Initial stresses/strains at nodes/for element. Fx, My, $\mathrm{Mz}, \mathrm{Txz}, \mathrm{Txy}, 0$ in local directions. $\varepsilon x, \psi y, \psi z$, $\psi \mathrm{xz}, \psi \mathrm{xy}, 0$ : in local directions. (see Notes). Total torque $=\mathrm{Txz}+\mathrm{Txy}$
Not applicable.
Residual stresses at nodes/for element. Resultants (nonlinear model 29): Fx, My, Mz, Txz, Txy, 0: in local directions.
Not applicable.
Target stresses/strains at nodes/for element. Fx, My, $\mathrm{Mz}, \mathrm{Txz}, \mathrm{Txy}, 0$ in local directions. $\varepsilon x, \psi y, \psi z$, $\psi \mathrm{xz}, \psi \mathrm{xy}, 0$ : in local directions. (see Notes). Total torque $=\mathrm{Txz}+\mathrm{Txy}$
Not applicable.
Temperatures TEMP, TMPE Temperatures at nodes/for element. T, $0, \mathrm{dT} / \mathrm{dy}$, $\mathrm{dT} / \mathrm{dz}, \mathrm{To}, 0, \mathrm{dTo} / \mathrm{dy}, \mathrm{dTo} / \mathrm{dz}$ : in local directions.
Overburden Not applicable.
Phreatic Surface Not applicable.
Field Loads Not applicable.

## Temp Dependent Not

Loads applicable.

## LUSAS Output

Solver Force (default): Fx, My, Mz, Txz, Txy, Fy, Fz: in local directions.
(Total torque $=T x z+T x y)$
Strain: $\varepsilon \mathrm{x}, \psi \mathrm{y}, \psi \mathrm{z}, \psi \mathrm{xz}, \psi \mathrm{xy}$ : in local directions. (see Notes). Total torsional strain $=\psi x z+\psi x y$
By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal axes.
Modeller See Results Tables (Appendix K).

## Local Axes

Standard line element. For BSL3 the local xy-plane is defined by the 3 element nodes. The local $y$-axis is perpendicular to the local $x$-axis and positive on the convex side of the element. The local y and z -axes form a right-hand set with the local x -axis.
For BSL4 the local xy-plane is defined by the 2 end nodes of the beam and the 4th node. The local $y$-axis is perpendicular to the $x$-axis and positive on the side of the element where the 4th node lies. The local y and z -axes form a right-hand set with the local x -axis.

## Sign Convention

$\square$ Standard beam element

## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements, small rotations and small strains.
Updated Not applicable.
Lagrangian
Eulerian Not applicable.
Co-rotational Not applicable.

## Integration Schemes

Stiffness Default. 3-point torsion, 2-point bending.
Fine. As default.
Mass Default. 3-point.
Fine. As default.

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity
102 Switch off load correction stiffness matrix due to centripetal acceleration.

105 Lumped mass matrix.
157 Material model 29 (non cross-section elements), see Notes.
170 Suppress transfer of shape function arrays to disk.
405 Specify geometric properties along beam centroidal axes
406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
418 Output stress resultants relative to beam centroidal axes for eccentric elements

## Notes on Use

1. The semiloof beam element is based on a Kirchhoff hypothesis for thin beams (i.e. the exclusion of shearing deformations).
2. The variation of axial force, moments and torsion can be regarded as linear along the length of the element. Shear forces are constant along the length of the element.
3. The loof rotations $\theta_{1}$ and $\theta_{2}$ refer to rotations about the element at the loof positions. A positive loof rotation is defined by a right-hand screw rule applied to a vector running in the local x -axis direction along the element edge.
4. Input of geometric properties (OPTION 405) and loads (OPTION 406), and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axes. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line.
5. For nonlinear material model 29 the following geometric properties are appended to those already specified (see Geometric Properties).

- $A^{\mathrm{p}}, \mathrm{Zyy}^{\mathrm{p}}, \mathrm{Zzz}^{\mathrm{p}}, \mathrm{Zy}^{\mathrm{p}}, \mathrm{Zz}^{\mathrm{p}}, \mathrm{S}^{\mathrm{p}}$ at each node (i.e. nodes $1,2,3$ ).
- $\quad A^{p}$ Plastic area (=elastic area)
- $\mathrm{Zyy}^{\mathrm{p}}$, Zzz $^{\mathrm{p}}$ Plastic moduli for bending about $\mathrm{y}, \mathrm{z}$ axes
- $\mathrm{Zy}^{\mathrm{p}}, \mathrm{Zz}^{\mathrm{p}}$ Plastic moduli for torsion about $\mathrm{y}, \mathrm{z}$ axes.
- $\quad S^{\mathrm{p}}$ Plastic area for shear $\left(\mathrm{S}^{\mathrm{p}}=0\right)$.

Where the fully plastic torsional moment $=\sigma y\left(\mathrm{Zy}^{\mathrm{p}}+\mathrm{Zz}^{\mathrm{p}}\right)$
6. For nonlinear material model 29 the following ifcode parameters should be

- ifcode $=1$ for circular hollow sections.
- $\quad$ ifcode $=2$ for solid rectangular sections.

7. Semiloof beam elements should be used with semiloof shell elements. For beam only problems, BS3/BS4 elements should be used.
8. Temperature dependent properties cannot be used with material model 29.
9. Integration of the element stiffness matrix is performed using selective integration, with a 2-point Gauss rule for the axial and flexural strain energy, and a 3-point Gauss rule for the torsional strain energy. The selective integration technique is implemented in a similar manner to the method proposed by Hughes [H4], i.e. the straindisplacement matrix for the bending and axial strains is evaluated at the reduced rule quadrature points and then extrapolated to the sampling locations of the 3-point quadrature rule. The material response is then assessed at the 3-point Gauss rule.
10. The rigidity matrix for BSL3 and BSL4 is evaluated explicitly from the geometric properties for both linear and nonlinear materials.
11. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature


## Recommendations on Use

- The primary use of this element is to provide a beam stiffener for the semiloof shell (QSL8) for analysing stiffened shell structures.
- The BS3 and BS4 elements are more effective for linear analysis of 3D frame structures with curved members and nonlinear analysis of three dimensional beam, frame and arch structures.
- The 2-noded straight beam (BMI21) is the most effective for linear analysis of structures containing straight members of constant cross-section, e.g. space frames.


## 3D Semiloof Thin Beam Element with Quadrilateral CrossSection

## General



## Geometric Properties

$\mathrm{y} 1, \mathrm{z} 1, \mathrm{y} 2, \mathrm{z} 2, \mathrm{y} 3, \mathrm{z} 3, \mathrm{y} 4, \mathrm{z} 4$ : local cross section coordinate pairs at each node; followed by nt12, nt14: number of Newton-Cotes integration points in the direction defined by the local crosssection points 1-2 and 1-4 (zero indicates default values). Multiple quadrilateral crosssections can be used to build up complex beam cross-sections.

Note. The corners of the quadrilateral are numbered clockwise about the local $x$-axis (the beam nodal line), that is, a right-hand screw rule in the direction of increasing $x$.


## Material Properties

Linear Isotropic:<br>Matrix Not applicable<br>Joint Not applicable<br>Concrete Not applicable<br>Elasto-Plastic Stress resultant: Tresca:<br>DruckerPrager:<br>MohrCoulomb:<br>Optimised Implicit Von Mises:<br>Volumetric Crushing: Stress Potential<br>\section*{Creep}<br>AASHTO<br>CEB-FIP<br>Chinese<br>Eurocode<br>IRC<br>MATERIAL PROPERTIES (Elastic: Isotropic)<br>Not applicable.<br>MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)<br>MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)<br>MATERIAL PROPERTIES NONLINEAR 65<br>(Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)<br>MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic)<br>Not applicable<br>STRESS POTENTIAL VON_MISES<br>(Isotropic: von Mises, Modified von Mises)<br>CREEP PROPERTIES (Creep)<br>MATERIAL PROPERTIES NONLINEAR 86 AASHTO<br>(Concrete creep model to AASHTO code of Practice)<br>MATERIAL PROPERTIES NONLINEAR 86 CEBFIP<br>(Concrete creep model to CEB-FIP Model Code 1990)<br>MATERIAL PROPERTIES NONLINEAR 86 CHINESE<br>(Chinese creep model to Chinese Code of Practice)<br>MATERIAL PROPERTIES NONLINEAR 86 EUROCODE<br>(Concrete creep model to EUROCODE_2)<br>MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of

## Damage

Viscoelastic Not applicable Shrinkage

Rubber Not applicable
Generic Polymer Not applicable
Composite Not applicable

Practice)
DAMAGE PROPERTIES SIMO, OLIVER (Damage)

SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER

## Loading

Prescribed Value PDSP, TPDSP

Concentrated CL Loads

Element Loads ELDS

Prescribed variable. U, V, W, $\theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ : at end nodes. U, V, W, $\theta_{1}, \theta_{2}$ at mid-side node.
Concentrated loads Px, Py, Pz, Mx, My, Mz at end nodes (global). Px, Py, Pz, M1, M2: at mid-side node ( $\mathrm{M}_{1}$ and $\mathrm{M}_{2}$ local).
Element loads on nodal line (load type number LTYPE * 10 defines the corresponding element load type on beam axis)
LTYPE, S1, Px, Py, Pz, Mx, My, Mz
LTYPE=11: point loads and moments in local directions.
LTYPE=12: point loads and moments in global directions.
LTYPE, 0 , Wx, Wy, Wz, Mx, My, Mz
LTYPE=21: uniformly distributed loads in local directions.
LTYPE=22: uniformly distributed loads in global directions.
LTYPE=23: uniformly distributed projected loads in global directions.
LTYPE, S1, Wx1, Wy1, Wz1, Mx1, My1, Mz1, S2, Wx2, Wy2, Wz2, Mx2, My2, Mz2
LTYPE=31: distributed loads in local directions.
LTYPE=32: distributed loads in global directions.
LTYPE=33: distributed projected loads in global directions.
LTYPE, S1, Wx, Wy, Wz, Mx, My, Mz
LTYPE=41: trapezoidal loads in local directions.
LTYPE=42: trapezoidal loads in global directions.
LTYPE=43: trapezoidal projected loads in global


## Temp Dependent Not

Loads applicable.

## LUSAS Output

Solver Force (default): Fx, My, Mz, Txz, Txy, Fy, Fz: in local directions. Total torque $=$ Txz+Txy.
Continuum stresses (Option 172): $\sigma x, \sigma x y, \sigma x z, \sigma y z:$ in local directions.
Strain/curvatures (default): $\varepsilon x, \psi y, \psi z, \psi x z, \psi x y, \gamma y z:$ in local directions (see Notes). Total torsional strain $=\psi x y+\psi y z$.
Continuum strains (Option 172): $\varepsilon x, \varepsilon_{x y}, \varepsilon x z, ~ \varepsilon y z: ~ i n ~ l o c a l ~ d i r e c t i o n s . ~$ By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal axes.
Modeller See Results Tables (Appendix K).

## Local Axes

$\square$ Standard line element The local xy-plane is defined by the 2 end nodes of the beam and the 4th node. The local $y$-axis is perpendicular to the $x$-axis and positive on the side of the element where the 4th node lies. The local $y$ and $z$-axes form a right-hand set with the local x -axis.

## Sign Convention

$\square$ Standard beam element

## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements, large rotations and small strains.
Updated Not applicable.
Lagrangian
Eulerian Not applicable.
Co-rotational Not applicable.

## Integration Schemes

| Stiffness | Default. | 2-point torsion, 2-point bending. |
| :---: | :--- | :--- |
|  | Fine. | As default. |
| Mass | Default. | 3-point. |
|  | Fine. | As default. |

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

32 Suppress stress output (but not stress resultant).
55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity.
102 Disable load correction stiffness matrix due to centripetal acceleration.
105 Lumped mass matrix
139 Output inelastic Gauss points only
170 Suppress transfer of shape function arrays to disk
172 Form the rigidity matrix by numerical cross section integration.
406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
418 Output stress resultants relative to beam centroidal axes for eccentric elements

## Notes, Assumptions and Limitations

1. The semiloof beam element formulation is based on a Kirchhoff hypothesis for thin beams (i.e. shearing deformations are excluded). The variation of axial force, bending and torsion along the length of the element may be considered as linear. Shear forces are constant.
2. Input of loads (OPTION 406), and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axes. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line. Fiber stress/strain results are output at their actual location.
3. The torsional constant is estimated from the computed values for Iyy and Izz, $\mathrm{Jxx}=$ Iyy + Izz.
4. For nonlinear material models, fibre integration is used across the cross-sectional area of the beam. Only axial deformation is considered in the plasticity computations, any torsional deformation is assumed to remain elastic.
5. Computing the rigidity matrix by integration through the cross-section depth of the beam is necessary for all nonlinear material models (except 29). By default option 172 is invoked automatically and a $5 * 5$ point Newton-Cotes integration rule is used.
6. By default, the rigidity matrix is evaluated explicitly for linear materials. A $3 * 3$ point Newton-Cotes integration rule may be invoked using option 172. Numerical cross section integration enables top, middle and bottom stress output.
7. Integration of the element stiffness matrix is performed using selective integration, with a 2-point Gauss rule for the axial and flexural strain energy, and a 3-point Gauss rule for the torsional strain energy. The selective integration technique is implemented in a similar manner to the method proposed by Hughes, i.e. the straindisplacement matrix for the bending and axial strains is evaluated at the reduced rule quadrature points and then extrapolated to the sampling locations of the 3-point quadrature rule. The material response is then assessed at the 3-point Gauss rule.

## Restrictions

Ensure mid-side node centrality
$\square$ Avoid excessive element curvature

## Recommendations on Use

- The element's primary use is to provide a beam stiffener for the semiloof shell (QSL8) for analysing stiffened shell structures.
- The BSX4 element is more effective for linear analysis of 3D frame structures with curved members and nonlinear analysis of three dimensional beam, frame and arch structures.
- The 2-noded straight beam (BMS21) is the most effective for linear analysis of structures containing straight members of constant cross-section, e.g. space frames.


## 2D Plane Strain Beam Elements

## General

Element Name BMI2N


## BMI3N



## Element Group Beams

Element
Plane Strain Beam
Subgroup
Element
Straight and curved isoparametric degenerate thick beam elements in 2D
Description for which shearing deformations are included. The element thickness may vary along its length.
Number Of 2 (BMI2N) 3 (BMI3N) Nodes
Freedoms
$\mathrm{U}, \mathrm{V}, \theta \mathrm{z}$ : at each node.
End Releases
The element node numbers should be followed by: R restrained (default) $F$ free defined in the order $U, V, \theta z$ for node 1 and then $U, V, \theta z$ for the other end node (node 2 for BMI2N, node 3 for BMI3N). The releases relate to the local element axes (see Assumptions and Limitations).
Node X, Y: at each node.
Coordinates

## Geometric Properties

$\mathbf{t 1}, \mathbf{t 2}, \mathbf{t 3}$ Thickness at each node.

Linear Isotropic:
MATERIAL PROPERTIES (Elastic: Isotropic)
Matrix Not applicable
Joint Not applicable
Concrete Not applicable

Elasto-Plastic Stress resultant Tresca:

Drucker-Prager:

Optimised Implicit Von Mises:

Volumetric Crushing:
Stress Potential

## Creep

AASHTO

CEB-FIP

Chinese

Eurocode

IRC

Mohr-Coulomb: MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
Not applicable.
MATERIAL PROPERTIES NONLINEAR 61
(Elastic: Isotropic, Plastic: Tresca, Hardening:
Isotropic Hardening Gradient, Isotropic Plastic
Strain or Isotropic Total Strain)
MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)

MATERIAL PROPERTIES NONLINEAR 75
(Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic)
Not applicable.
STRESS POTENTIAL VON_MISES, HILL, HOFFMAN
(Isotropic: von Mises, Modified von Mises
Orthotropic: Hill, Hoffman)
CREEP PROPERTIES (Creep)
MATERIAL PROPERTIES NONLINEAR 86 AASHTO
(Concrete creep model to AASHTO code of Practice)

MATERIAL PROPERTIES NONLINEAR 86 CEB-FIP
(Concrete creep model to CEB-FIP Model Code 1990)

MATERIAL PROPERTIES NONLINEAR 86 CHINESE
(Chinese creep model to Chinese Code of Practice)

MATERIAL PROPERTIES NONLINEAR 86 EUROCODE
(Concrete creep model to EUROCODE_2)
MATERIAL PROPERTIES NONLINEAR 86 IRC
(Concrete creep model to Indian IRC code of
Practice)
DAMAGE PROPERTIES SIMO, OLIVER(Damage)
SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Loading
Prescribed Value PDSP, TPDSP
Concentrated CLLoadsElement Loads ELDS

Prescribed variable. U, V, $\theta \mathrm{z}$ : at nodes. Concentrated loads. Px, Py, Mz: at nodes (global).

## Element loadson nodal line (load type number

LTYPE * 10 defines the corresponding element load type on beam axis, see Notes)
LTYPE, S1, Px, Py, Mz
LTYPE=11: point loads and moments in local directions.
LTYPE=12: point loads and moments in global directions.
LTYPE, 0, Wx, Wy, 0
LTYPE=21: uniformly distributed loads in local directions.
LTYPE=22: uniformly distributed loads in global directions.
LTYPE=23: uniformly distributed projected loads in global directions
LTYPE, S1, Wx1, Wy1, 0, S2, Wx2, Wy2, 0
LTYPE=31: distributed loads in local directions.
LTYPE=32: distributed loads in global directions.
LTYPE=33: distributed projected loads in global directions
LTYPE, S1, Wx, Wy, 0
LTYPE=41: trapezoidal loads in local directions.
LTYPE=42: trapezoidal loads in global directions.

Distributed Loads UDL

FLD
Body Forces CBF

BFP, BFPE

Velocities VELO
Accelerations ACCE
Initial SSI, SSIE
Stress/Strains

Residual Stresses SSR, SSRE,

SSRG

Target TSSIE, TSSIA Stress/Strains

TSSIG

Temperatures TEMP, TMPE
Phreatic surface Face_Pressure

Field Loads Not applicable.

LTYPE=43: trapezoidal projected loads in global directions
Uniformly distributed loads. Wx, Wy: forces/unit length for element in local directions.
Not applicable.
Constant body forces for element.
Xcbf, Ycbf, $\Omega \mathrm{x}, \Omega \mathrm{y}, \Omega \mathrm{z}, \alpha \mathrm{z}$
Body force potentials at nodes/for element. $\varphi 1$, $\varphi 2,0,0$, Xcbf, Ycbf
Velocities. Vx, Vy: at nodes.
Acceleration. Ax, Ay: at nodes.
Initial stresses/strains at nodes/for element.
Components: $N x, 0, M x, 0, S x y, \varepsilon x, 0, \gamma x, 0$,
$\varepsilon x y,(\sigma x, \sigma x y, \sigma z, \varepsilon x, \varepsilon x y, \varepsilon z)$ Bracketed terms repeated for each fibre integration point.
Initial stresses/strains at Gauss points. These stresses/strains are specified in the same manner as SSI and SSIE.
Residual stresses at nodes/for element.
Components: $0,0,0,0,0,0,0,0,0,0,(\sigma x$, $\sigma x y, \sigma z)$ Bracketed terms repeated for each fibre integration point.
Residual stresses at Gauss points for element..
Components: $0,0,0,0,0,0,0,0,0,0,(\sigma x$, $\sigma x y, \sigma z)$ Bracketed terms repeated for each fibre integration point.
Target stresses/strains at nodes/for element. Fx, Fy, Mz: axial force, shear force and moment
in local directions. $\varepsilon x, \varepsilon y, \psi z$ : axial, shear and flexural strains in local directions.
Target stresses/strains at Gauss points. These stresses/strains are specified in the same manner as TSSIE and TSSIA.
Temperatures at nodes/for elements. T, 0 , $\mathrm{dT} / \mathrm{dy}, 0, \mathrm{To}, 0, \mathrm{dTo} / \mathrm{dy}, 0$ in local directions. The fluid pressure is applied in the -y direction of the element $y$ axis..

## Temp Dependent Not applicable. Loads

## LUSAS Output

Solver Force. Nx, Nz, Mx, Mz, Sxy: axial and normal forces, moments/unit width in local directions, shear force. NB. The plate/shell convention is used for the moment definition.

Strain. $\varepsilon x, \varepsilon z, \gamma x, \gamma z, \varepsilon x y$ axial, normal, flexural and shear strains.
Continuum stresses: $\sigma x, \sigma x y, \sigma z$ in local directions.
Strain: $\varepsilon x, \varepsilon x y, \varepsilon_{z}$ Axial, shear and normal strains in local directions.
Modeller See Results Tables (Appendix K).

## Local Axes

The local x -axis lies along the line of the element in the direction in which the nodes are numbered. The local y and z -axes form a right-hand set with the local x -axis such that the y -axis lies in the global XY-plane with the z -axis parallel to the global Z-axis.

## Sign Convention

- Standard shell element. Axial and circumferential moments are positive for tension on element top fibre (the top fibre lies on the positive local y side of the element).


## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements, small rotations and small strains
Updated Not applicable.
Lagrangian
Eulerian Not applicable.
Co-rotational Not applicable.

## Integration Schemes

Stiffness Default. 1-point (BMI2N), 2-point (BMI3N).
Fine. Same as default.

```
Mass Default. 2-point (BMI2N), 3-point (BMI3N). Fine. Same as default.
```

Note: A 3-point Newton-Cotes integration rule is also available for BMI3N using OPTION 134. This may be more applicable for infinitesimal strain, elasto-plastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory Manual.

## Mass Modelling

- Consistent mass (default).

Lumped mass.

## Options

36 Follower loads
55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity.
102 Switch off load correction stiffness matrix due to centripetal acceleration
105 Lumped mass matrix.
134 Gauss to Newton-Cotes in plane (in the local x direction) integration for elements
139 Output yielded integration points only.
403 Introduce residual bending flexibility correction for 2-node thick beam BMI21, see Assumptions and Limitations.
404 Compute equivalent nodal loading from equilibrium considerations for 2-node thick beam BMI21, see Assumptions and Limitations.

## Notes, Assumptions and Limitations

1. The element is formulated from the degenerate continuum concept, i.e. enforcing directly the modified Timoshenko hypothesis for thick beams to the continuum theory. Plane cross-sections initially normal to the beam axis remain plane and undistorted (the shape of the cross-section remains unchanged) under deformation, but do not necessarily remain normal to the beam axis. Shearing deformations are included.
2. OPTION 36 is only applicable for use with element load types FLD, ELDS, UDL and phreatic surface pressure. Specifying this option makes these element loads follow the element geometry as the analysis progresses.
3. When OPTION 403 is specified to introduce residual bending flexibility correction (on by default), for BMI2N, the axial force is constant, while the shear force and moment vary linearly along the length of the beam. For BMI3N the axial force, shear force and moment all vary linearly along the length
4. When BMI2N is used together with OPTION 403 to introduce residual bending flexibility correction, its stiffness matrix is enhanced to the order of a cubic. As the plane strain beam can only be of rectangular cross section, a shear area based on 5/6 of the nodal thicknesses is assumed in this process.
5. When BMI2N is used together with OPTION 404, loading that varies along the element length is accounted for in the force diagrams (i.e. for a beam under CBF or internal element loading). A post-processing technique has been introduced to obtain accurate quadratic bending moments for BMI3N. For BMI2N (with OPTION 404) and BMI3, internal forces and moments are output at intervals of 1/10th of the element length by specifying the Gauss point option from the Output button of the LUSAS Datafile dialog.
6. The end releases for this element allow a joint to be modelled between adjacent elements. These joints allow rotation and translation of one beam with respect to another without load transferral. The rotations and translations remain in the local directions of the beam elements and support large deformations.
7. When a nonlinear material is used with this element the transverse shear stresses are excluded from the plasticity computations i.e. the transverse shear stresses are assumed to remain elastic. This means that if a nonlinear material is used in applications where transverse shear tends to dominate the stress field the equivalent von Mises and maximum principal stresses can exceed the uniaxial yield stress.
8. When a step by step dynamic analysis is carried out using BMI elements with distributed loading, the "free body force diagrams" pertaining to applied loading, are not superimposed on the nodal values, to do so would lead to erroneous results until a steady state is reached. It should therefore be noted that different force diagrams will be obtained for BMI elements if static and dynamic analyses are directly compared.
9. OPTION 87 considers large displacements and large rotations using a Total Lagrangian formulation; OPTION 229 considers large displacements and large rotations using a co-rotational formulation. In general the co-rotational formulation works better. When both options 87 and 229 are true, a local Total Lagrangian formulation will be used within a global co-rotational framework.
10. End releases for these elements are currently not valid for use in step-by-step dynamic analyses.

## Restrictions

$\square$ Ensure mid-side node centrality
$\square$ Avoid excessive element curvature

## Recommendations on Use

- The element may be used for linear and nonlinear analysis of two dimensional long structures of box girder cross-sections such as tunnel linings and retaining walls for which the plane strain assumption is appropriate.


## Chapter 3: 2D Continuum Elements.

## 2D Plane Stress Continuum Elements

## General



Element Group

## Element

 SubgroupElement Description

Number Of Nodes Freedoms Node
Coordinates

2D Continuum
Plane Stress Continuum

A family of 2D isoparametric elements with the higher order elements capable of modelling curved boundaries. The elements are numerically integrated.
$3,4,6$ or 8 , numbered anticlockwise.
$\mathrm{U}, \mathrm{V}$ : at each node.
$\mathrm{X}, \mathrm{Y}$ : at each node.

## Geometric Properties

t1... tn Thickness at each node.

## Material Properties

| Linear | Isotropic: | MATERIAL PROPERTIES (Elastic: Isotropic) |
| :---: | :---: | :---: |
|  | Orthotropic: | MATERIAL PROPERTIES ORTHOTROPIC <br> (Elastic: Orthotropic Plane Stress) |
|  | Anisotropic: | MATERIAL PROPERTIES ANISOTROPIC 3 (Elastic: Anisotropic Thin Plate) |
|  | Rigidities. | RIGIDITIES 3 (Rigidities: Membrane/Thin Plate) |
| Matrix | Not applicable |  |
| Joint | Not applicable |  |
| Concrete |  | MATERIAL PROPERTIES NONLINEAR 105 (Elastic: Isotropic, Plastic: Transient Smoothed Multi-Crack Concrete) |
|  |  | MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed MultiCrack Concrete) |
| Elasto-Plastic | Stress resultant: | Not applicable. |
|  | Tresca: | MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain) |
|  | Drucker-Prager: | MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular) |
|  | Mohr-Coulomb: | MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation) |
|  | Volumetric Crushing: | Not applicable |
|  | Interface: | MATERIAL PROPERTIES NONLINEAR 27 |
|  | Stress Potential | STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman) |
| Creep |  | CREEP PROPERTIES (Creep) |
|  | AASHTO | MATERIAL PROPERTIES NONLINEAR 86 AASHTO <br> (Concrete creep model to AASHTO code of Practice) |
|  | CEB-FIP | MATERIAL PROPERTIES NONLINEAR 86 |

CEB-FIP(Concrete creep model to CEB-FIP Model Code1990)
Chinese
Damage
IRC
Viscoelastic Not applicable
Shrinkage
Eurocode
Ko Initialisation Not applicableRubber Not applicableGeneric Polymer IsotropicComposite Not applicable

MATERIAL PROPERTIES NONLINEAR 86 CHINESE
(Chinese creep model to Chinese Code of Practice)
MATERIAL PROPERTIES NONLINEAR 86 EUROCODE
(Concrete creep model to EUROCODE_2)
MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
DAMAGE PROPERTIES SIMO, OLIVER (Damage)
SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
MATERIAL PROPERTIES NONLINEAR 89(Generic Polymer Model)

## Loading

Prescribed Value PDSP, TPDSP Concentrated CL Loads Element Loads Not applicable.
Distributed Loads U
UDL
FLD
FLDG
Body Forces CBF

BFP, BFPE

Velocities VELO

Prescribed variable. U, V: at nodes.
Concentrated loads. Px, Py: at nodes.

Not applicable.
Face Loads. Px, Py: Local Face Axis Pressures At Nodes.
Global Face Loads. $\sigma x, \sigma y, \sigma z x y$ at nodes
Constant body forces for element. Xcbf, Ycbf, $\Omega \mathrm{x}$, $\Omega \mathrm{y}, \Omega_{\mathrm{z}}, \alpha_{\mathrm{z}}$
Body force potentials at nodes/for element. 0, 0, 0, $\varphi 4$, Xcbf, Ycbf
Velocities. Vx, Vy: at nodes.

Accelerations ACCE
Initial SSI, SSIE
Stress/Strains
SSIG

Residual Stresses SSR, SSRE

SSRG

Target TSSIE, TSSIA Stress/Strains

TSSIG

Temperatures TEMP, TMPE
Overburden Applicable.
Phreatic Surface Applicable.
Field Loads Not applicable.
Temp Dependent Not applicable.
Loads

Accelerations. Ax, Ay: at nodes.
Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.
Initial stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$ : global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.

Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma x y$ : global stresses.
Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma x y$ : global stresses.

Target stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y$ : global stresses. $\mathcal{E x}, \varepsilon y, \gamma x y$ : global strains.
Target stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$ : global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.
Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}, 0$, 0,0

## LUSAS Output

# Solver <br> Stress resultants: Nx, Ny, Nxy, Nmax, Nmin, $\beta$, Ns, Ne <br> Stress (default): $\sigma x, \sigma y, \sigma x y, \sigma \max , \sigma \min , \beta, \sigma s, \sigma e$ (see description of principal stresses) 

Strain: $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon \max , \varepsilon \min , \beta, \varepsilon s, \varepsilon e$
Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

Standard 2D continuum element

## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements and large rotations.
Updated For large displacements and large rotations.
Lagrangian
Eulerian For large displacement, large rotations and moderately large strains.
Co-rotational For large displacements and large rotations.

## Integration Schemes

| Stiffness | Default. | 1-point (TPM3), 3-point (TPM6), 2x2 (QPM4, QPM8) |
| :---: | :--- | :--- |
|  | Fine (see Options). | 3x3 (QPM8), 3-point (TPM3). |
| Mass | Default. | 1-point (TPM3), 3-point (TPM6), 2x2 (QPM4, QPM8) |
|  | Fine (see Options). | 3x3 (QPM8), 3-point (TPM3). |

## Mass Modelling

C Consistent mass (default).

- Lumped mass.


## Options

18 Invokes fine integration rule.
34 Output element stress resultants.
36 Follower loads (see Notes)
54 Updated Lagrangian geometric nonlinearity.
55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity.
91 Invokes fine integration rule for mass matrix.
105 Lumped mass matrix.
123 Clockwise node numbering.
139 Output yielded Gauss points only
167 Eulerian geometric nonlinearity.
229 Co-rotational geometric nonlinearity

## Notes on Use

1. The element formulations are based on the standard isoparametric approach. The variation of stresses within an element can be regarded as constant for the lower order (corner node only) elements, and linear for the higher (mid-side node) elements.
2. All elements pass the patch test.
3. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the face loading (FLD).
4. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it is only applicable if every element is numbered clockwise. Surface normals should be visualised and if necessary corrected in the pre-processing stage.
5. If applying an initial stress/strain or thermal load that varies across an element, a higher order element ( 6 or 8 nodes) should be used. A limitation of the standard isoparametric approach when used for lower order elements ( 3 or 4 nodes) is that only constant stress/strain fields can be imposed correctly.

## Restrictions

$\square$ Ensure mid-side node centrality

- Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio


## Recommendations on Use

- The 8 -noded element with a $2 * 2$ Gauss rule is usually the most effective element, as the under-integration of the stiffness matrix prevents locking, which may occur either when the element is subjected to parasitic shear, or as the material reaches the incompressible limit (elasto-plasticity). The Gauss point stresses are also sampled at the most accurate locations for the element. However, the element does possess one spurious zero energy mode. This mode is very rarely activated in linear analysis, but it may occur in both materially and geometrically nonlinear analyses. Therefore, a careful examination of the solution should be performed, to check for spurious stress oscillations and peculiarities in the deformed configuration.
- The 8 -noded element with a $3 * 3$ Gauss rule may be used if a spurious mechanism is excited with the $2 * 2$ Gauss rule.
- The 4-noded element should not be used for analyses where in-plane bending effects are significant as the element tends to lock in parasitic shear [C1], e.g. if QPM4 elements are employed to model a cantilever subject to a point load, the solution obtained will be over-stiff.


## 2D Plane Stress Continuum Element with Enhanced Strains

## General

Element Name
QPM4M


## Element Group 2D Continuum

> Element

Plane Stress Continuum

## Subgroup

Element
A 2D isoparametric element with an assumed strain field. This mixed
Description assumed strain element demonstrates a superior performance to QPM4 (see Notes). The elements are numerically integrated.
Number Of
4, numbered anticlockwise.
Nodes
Freedoms U, V: at each node.
Node X, Y: at each node.
Coordinates

## Geometric Properties

> t1... tn Thickness at each node.

## Material Properties

$$
\begin{array}{llc}
\text { Linear } & \text { Isotropic: } & \text { MATERIAL PROPERTIES (Elastic: Isotropic) } \\
& \text { Orthotropic: } & \text { MATERIAL PROPERTIES ORTHOTROPIC } \\
& & \text { (Elastic: Orthotropic Plane Stress) } \\
& \text { Anisotropic: } & \text { MATERIAL PROPERTIES ANISOTROPIC } 3 \\
& & \text { (Elastic: Anisotropic Thin Plate) }
\end{array}
$$

Matrix Not applicable Joint Not applicable Concrete

Elasto-Plastic Stress resultant: Tresca:

DruckerPrager:

MohrCoulomb:

Volumetric Crushing: Stress Potential

## Creep

AASHTO

CEB-FIP

Chinese

EurocodeRigidities: RIGIDITIES 3 (Rigidities: Membrane/Thin Plate)

RIGIDITIES 3 (Rigidities: Membrane/Thin Plate)

MATERIAL PROPERTIES NONLINEAR 105
(Elastic: Isotropic, Plastic: Transient Smoothed Multi-Crack Concrete)
MATERIAL PROPERTIES NONLINEAR 109
(Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Not applicable
MATERIAL PROPERTIES NONLINEAR 61
(Elastic: Isotropic, Plastic: Tresca, Hardening:
Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
MATERIAL PROPERTIES NONLINEAR 64
(Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
Not applicable
STRESS POTENTIAL VON_MISES, HILL, HOFFMAN
(Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
CREEP PROPERTIES (Creep)
MATERIAL PROPERTIES NONLINEAR 86 AASHTO
(Concrete creep model to AASHTO code of Practice)

MATERIAL PROPERTIES NONLINEAR 86 CEBFIP
(Concrete creep model to CEB-FIP Model Code 1990)

MATERIAL PROPERTIES NONLINEAR 86 CHINESE
(Chinese creep model to Chinese Code of Practice)
MATERIAL PROPERTIES NONLINEAR 86 EUROCODE
(Concrete creep model to EUROCODE_2)
IRC
MATERIAL PROPERTIES NONLINEAR 86 IRCDamage(Concrete creep model to Indian IRC code ofPractice)DAMAGE PROPERTIES SIMO, OLIVER(Damage)
Viscoelastic Not applicableShrinkage
SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Ko Initialisation Not applicable
Rubber Ogden:Mooney-Rivlin:Neo-Hookean:MATERIAL PROPERTIES RUBBER OGDEN(Rubber: Ogden) (Rubber: Ogden)
MATERIAL PROPERTIES RUBBERMOONEY_RIVLIN (Rubber: Mooney-Rivlin)MATERIAL PROPERTIES RUBBERNEO_HOOKEAN (Rubber: Neo-Hookean)
Hencky:
Generic Polymer Isotropic
Composite Not applicable
Loading
Prescribed Value PDSP, TPDSPPrescribed variable. U, V: at nodes.
Concentrated CLLoadsElement Loads Not applicable.
Distributed Loads UDL

Not applicable.FLDFLD
Body Forces CBF
BFP, BFPE
Velocities VELO
Accelerations ACCE
Initial SSI, SSIEStress/Strains

Concentrated loads. Px, Py: at nodes.

Face loads. Px, Py: local face axis pressures at nodes.
Global Face Loads. $\sigma x, \sigma y, \sigma x y$ at nodes
Constant body forces for element. Xcbf, Ycbf, $\Omega \mathrm{x}$, $\Omega \mathrm{y}, \Omega_{\mathrm{z}, ~} \alpha_{\mathrm{z}}$
Body force potentials at nodes/for element. $0,0,0$, $\varphi 4$, Xcbf, Ycbf
Velocities. Vx, Vy: at nodes.
Accelerations. Ax, Ay: at nodes.
Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y$ : global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.

SSIG

Residual Stresses SSR, SSRE

SSRG

Target TSSIE, TSSIA Stress/Strains

TSSIG

Temperatures TEMP, TMPE

Overburden Applicable.
Phreatic Surface Applicable.
Field Loads Not applicable.
Temp Dependent Not applicable. Loads

Initial stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$ : global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.

Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma x y$ : global stresses.
Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma x y$ : global stresses.
Target stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.
Target stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$ : global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.
Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}, 0$, 0,0

## Output

| Solver | Stress resultants: Nx, Ny, Nxy, Nmax, Nmin, $\beta$, Ns, Ne |
| :---: | :---: |
|  | Stress (default): $\sigma x, \sigma y, \sigma x y, \sigma \max , \sigma \min , \beta, \sigma s, \sigma e$ (see description of principal stresses) |
|  | Strain: $\varepsilon x, \varepsilon y, \gamma \mathrm{xy}, \varepsilon \mathrm{max}, \varepsilon \mathrm{min}, \beta, \varepsilon \mathrm{s}, \varepsilon \mathrm{e}$ |
|  | Stretch (for rubber only): $\mathrm{V}_{11}, \mathrm{~V}_{22}, \mathrm{~V}_{12}, \lambda_{1}, \lambda_{2}, \lambda_{3}, \theta \lambda$, det F. Where |
|  | $\mathrm{V}_{\mathrm{ii}}$ are components of the left stretch tensors, $\lambda_{i}$ the principal stretches, |
|  | $\theta \lambda$ the angle between the maximum principal stretch and the global X axis, and $\operatorname{det} \mathrm{F}$ the determinant of the deformation gradient or volume ratio. |
| Modeller | See Results Tables (Appendix K). |

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

- Standard 2D continuum element


## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements and large rotations.
Updated For large displacements and large rotations.
Lagrangian
Eulerian For large displacements, large rotations and moderately large strains.
Co-rotational For large displacements and large rotations (large strains with rubber).

## Integration Schemes

Stiffness Default. 2x2
Fine. As default.
Mass Default. 2x2
Fine. As default.

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

34 Output element stress resultants.
36 Follower loads.
39 Stress smoothing for rubber material models.
54 Updated Lagrangian geometric nonlinearity.
55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity.
91 Invokes fine integration rule for mass matrix.
105 Lumped mass matrix.
123 Clockwise node numbering (see Notes).
139 Output yielded Gauss points only
167 Eulerian geometric nonlinearity.
225 Use alternative number of parameters for enhanced strain interpolation (see Notes).
229 Co-rotational geometric nonlinearity.

## Notes on Use

1. The variation of stresses within an element can be regarded as linear.
2. The element passes the patch test and the large strain patch test for rubber.
3. The strain field for this element consists of two parts: the compatible strains derived from an assumed displacement field and the assumed enhanced strains (see LUSAS Theory Manual). The assumed enhanced strain field is defined using 5 or 4 parameters for linear and nonlinear applications respectively. Option 225 switches on the higher 5 parameter enhanced strain interpolation function for nonlinear analysis.
4. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility. The load does not have to be normal to the face and may also vary over the face.
5. To apply a non-conservative (follower) pressure load (load type FLD) with corotational geometric nonlinearity, Option 36 must be specified. Note that this load must be normal to the face and constant for all the nodes of the element face.
6. The converged stresses for rubber are Kirchoff stresses (see LUSAS Theory Manual).
7. When using the rubber material model, converged strain output is replaced by the left stretch tensor, the principal stretches and the angle defining these principal directions.
The value of $\operatorname{det} \mathrm{F}=\lambda_{1} \lambda_{2}$ (the Volume ratio) is only available for Gauss-point output. (Refer to the LUSAS Theory Manual for more details.)
8. For rubber, the iterative values of stress and strain are output in local co-rotated directions at the Gauss points only.
9. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it is only applicable if every element is numbered clockwise. Surface normals should be visualised and if necessary corrected in the pre-processing stage.
10. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.
11. Convergence difficulties can sometimes arise when using enhanced strain elements with nonlinear materials, particularly if the material is elastic perfectly plastic or if a very shallow hardening curve is defined. In such cases it is recommended that the standard element formulation is used.
12. In analyses where significant in-plane bending is thermally induced it is recommended that a nonlinear solution is used. If a linear solution is required, then quadratic plane strain elements QPN8 are recommended.

## Restrictions

- Avoid excessive aspect ratio

Rubber material models can only be applied in conjunction with the co-rotational formulation, Option 229.

## Recommendations on Use

These elements exhibit an improved performance when compared with the parent element QPM4. The integration rules are the same as those given for QPM4, but the elements do not suffer from locking due to parasitic shear when the material approaches the incompressible limit. The elements are also free of any zero energy modes.

## 2D Plane Stress Continuum Crack Tip Elements

## General



## QPK8



Crack specified at Node 1

## Element Group 2D Continuum

Element
Subgroup
Element
Description
A family of 2D isoparametric crack tip elements where the crack tip can be located at any corner node. The mid-side nodes are moved to the quarter points to produce a singularity at the crack tip. The strains vary as the square root of $1 / R$, where $R$ is the distance from the crack tip. These elements are used at the crack tip only and should be mixed with the higher order plane strain continuum elements. The elements are

Number Of

> Nodes

End Releases

Freedoms
Node
Coordinates
numerically integrated. 6 or 8 numbered anticlockwise.
Plane Stress Continuum
$\mathrm{U}, \mathrm{V}$ : at each node.
$\mathrm{X}, \mathrm{Y}$ : at each node.

## Geometric Properties

t1... tn Thickness at each node.

## Material Properties

Linear Isotropic:
MATERIAL PROPERTIES (Elastic: Isotropic)

|  | Orthotropic | MATERIAL PROPERTIES ORTHOTROPIC <br> (Elastic: Orthotropic Plane Stress) |
| :---: | :---: | :---: |
|  | Anisotropic: | MATERIAL PROPERTIES ANISOTROPIC 3 (Elastic: Anisotropic Thin Plate) |
|  | Rigidities. | RIGIDITIES 3 (Rigidities: Membrane/Thin Plate) |
| Matrix | Not applicable |  |
| Joint | Not applicable |  |
| Concrete |  | MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete) |
| Elasto-Plastic | Stress resultant: | Not applicable. |
|  | Interface: | MATERIAL PROPERTIES NONLINEAR 27 |
|  | Tresca: | MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain) |
|  | Drucker- <br> Prager: | MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular) |
|  | Mohr- <br> Coulomb: | MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation) |
|  | Volumetric Crushing: | Not applicable. |
|  | Stress Potential | ```STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)``` |
| Creep | AASHTO | CREEP PROPERTIES (Creep) |
|  |  | MATERIAL PROPERTIES NONLINEAR 86 AASHTO <br> (Concrete creep model to AASHTO code of Practice) |
|  | CEB-FIP | MATERIAL PROPERTIES NONLINEAR 86 CEB FIP <br> (Concrete creep model to CEB-FIP Model Code 1990) |
|  | Chinese | MATERIAL PROPERTIES NONLINEAR 86 CHINESE <br> (Chinese creep model to Chinese Code of Practice) |
|  | Eurocode | MATERIAL PROPERTIES NONLINEAR 86 |

EUROCODE
(Concrete creep model to EUROCODE_2)

## Damage

Viscoelastic Not applicable Shrinkage
Ko Initialisation Not applicable Rubber Not applicable Generic Polymer IsotropicComposite Not applicable

MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
DAMAGE PROPERTIES SIMO, OLIVER (Damage)

SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER

MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)

## Loading

Prescribed Value PDSP, TPDSP Concentrated CL Loads Element Loads Not applicable.
Distributed Loads UDL Not applicable. FLD

FLDG
Body Forces CBF

BFP, BFPE

Velocities VELO
Accelerations ACCE
Initial SSI, SSIE Stress/Strains

SSIG

Residual Stresses SSR, SSRE nodes. $\Omega y, \Omega_{z}, \alpha z$ $\varphi 4$, Xcbf, Ycbf

Prescribed variable. U, V: at nodes.
Concentrated loads. Px, Py: at nodes.

Face loads. Px, Py: local face axis pressures at

Global Face Loads. $\sigma x, \sigma y, \sigma x y$ at nodes
Constant body forces for element. Xcbf, Ycbf, $\Omega_{\mathrm{x}}$,

Body force potentials at nodes/for element. $0,0,0$,

Velocities. Vx, Vy: at nodes.
Accelerations. Ax, Ay: at nodes.
Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y$ : global stresses. $\mathcal{E x}, \varepsilon y, \gamma x y$ : global strains.
Initial stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$ : global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.
Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma x y$ : global stresses.
SSRG Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma x y$ : global stresses.

Target TSSIE, TSSIA Stress/Strains

TSSIG
Target stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y$ : global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.
Target stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$ : global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.
Temperatures TEMP, TMPE Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}, 0$, 0,0
Overburden Applicable. Phreatic Surface Applicable.
Field Loads Not applicable.
Temp Dependent Not applicable.
Loads

## LUSAS Output

Solver Stress resultants: Nx, Ny, Nxy, Nmax, Nmin, $\beta, \mathrm{Ns}, \mathrm{Ne}$
Stress (default): $\sigma x, \sigma y, \sigma x y, \sigma \max , \sigma \min , \beta, \sigma s, \sigma e$ (see description of principal stresses)
Strain: $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon \max , \varepsilon \min , \beta, \varepsilon s, \varepsilon \mathrm{e}$
Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

- Standard 2D continuum element


## Formulation

## Geometric Nonlinearity

$$
\begin{aligned}
\text { Total Lagrangian } & \text { For large displacements and large rotations. } \\
\text { Updated } & \text { For large displacements and large rotations. } \\
\text { Lagrangian } & \\
\text { Eulerian } & \text { For large displacements, large rotations and moderately large strains. }
\end{aligned}
$$

Co-rotational For large displacements and large rotations.

## Integration Schemes

| Stiffness | Default. | 6-point (TPK6), 3x3 (QPK8) |
| :---: | :--- | :--- |
|  | Fine (see Options). | 12-point (TPK6). |
| Mass | Default. | 6-point (TPK6), 3x3 (QPK8) |
|  | Fine (see Options). | 12-point (TPK6). |

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes finer integration rule.
34 Output element stress resultants.
54 Updated Lagrangian geometric nonlinearity.
55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity.
91 Invokes fine integration rule for mass matrix.
105 Lumped mass matrix.
123 Clockwise node numbering.
139 Output yielded Gauss points only.
167 Eulerian geometric nonlinearity.
229 Co-rotational geometric nonlinearity.

## Notes on Use

1. The element formulations are based on the standard isoparametric approach. Moving the mid-side nodes to the quarter points creates a singularity with theoretically infinite stress at the corner node.
2. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility.
3. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it is only applicable if every element is numbered clockwise. Surface normals should be visualised and if necessary corrected in the pre-processing stage.
4. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.

## Restrictions

- Avoid excessive element curvature
- Avoid excessive aspect ratio


## Recommendations on Use

The QPK8 and TPK6 elements are specifically designed for application to fracture mechanics problems and may used to model the singularities that occur at the crack tip. The mid-side nodes near the crack tip are shifted to the quarter point. This ensures a singularity is present at the crack tip and that the strains vary as 1 /square root of $r$ where $r$ is the distance from the crack tip. The triangular TPK6 element is more effective than the quadrilateral element.

## 2D Plane Stress Explicit Dynamics Elements

## General

Element Name
TPM3E



## Element Group <br> 2D Continuum

Element
Subgroup
Element
Description
A family of 2D isoparametric elements for explicit dynamic analyses. The

Number Of

End Releases
Freedoms

Coordinates
elements are numerically integrated.
3 or 4 numbered anticlockwise.
$\mathrm{U}, \mathrm{V}$ : at each node.
Node X, Y: at each node.
Plane Stress Continuum

## Geometric Properties

$$
\text { t1... } \mathbf{t n} \quad \text { Thickness at each node. }
$$

## Material Properties

$$
\begin{array}{llc}
\text { Linear } & \text { Isotropic: } & \text { MATERIAL PROPERTIES (Elastic: Isotropic) } \\
& \text { Orthotropic: } & \text { MATERIAL PROPERTIES ORTHOTROPIC } \\
& & \text { (Elastic: Orthotropic Plane Stress) } \\
& \text { Anisotropic: } & \text { Not applicable } \\
& \text { Rigidities. } & \text { Not applicable }
\end{array}
$$

    Matrix Not applicable
    Joint Not applicable
    Concrete Not applicable
    Elasto-Plastic Stress Not applicable
        resultant:
        Tresca:
        Drucker-
        Prager:
    Mohr-
    Coulomb:
    Volumetric
    Crushing:
    Stress Potential STRESS POTENTIAL VON_MISES, HILL,
        HOFFMAN
        (Isotropic: von Mises, Modified von Mises
        Orthotropic: Hill, Hoffman)
        Creep Not applicable
        Damage Not applicable
        Viscoelastic Not applicable
        Shrinkage Not applicable
    Ko Initialisation Not applicable
        Rubber Not applicable
    Generic Polymer Not applicable
Composite Not applicable

## Loading

| Prescribed Value Concentrated Loads | PDSP, TPDSP CL | Prescribed variable. U, V: at each node. Concentrated loads. Px, Py: at each node. |
| :---: | :---: | :---: |
| Element Loads | Not applicable. |  |
| Distributed Loads | UDL | Not applicable. |
|  | FLD | $\frac{\text { Face loads. Px, Py: local face axis pressures at }}{\text { nodes. }}$ |
|  | FLDG | Not applicable. |


| Body Forces | CBF | Constant body forces for element. Xcbf, Ycbf, $\Omega \mathrm{x}$, $\Omega \mathrm{y}, \Omega_{\mathrm{z}, \alpha \mathrm{z}}$ |
| :---: | :---: | :---: |
|  | BFP, BFPE | Body force potentials at nodes/for element. $0,0,0$, $\varphi 4, \mathrm{Xcbf}, \mathrm{Ycbf}$ |
| Velocities | VELO | Velocities. Vx, Vy: at nodes. |
| Accelerations | ACCE | Accelerations. Ax, Ay: at nodes. |
| Initial Stress/Strains | SSI, SSIE | Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y$ : global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains. |
| Residual Stresses | SSIG | Initial stresses/strains at Gauss points $\sigma x, \sigma y, \sigma x y$ : global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains. |
|  | SSR, SSRE | Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma x y$ : global stresses. |
|  | SSRG | Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma x y$ : global stresses. |
| Target | Not |  |
| Stress/Strains | applicable. |  |
| Temperatures | TEMP, TMPE | Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}, 0$, 0,0 |
| Overburden | Not applicable. |  |
| Phreatic Surface | Not applicable. |  |
| Field Loads | Not applicable. |  |
| Temp Dependent Loads | Not applicable. |  |

## LUSAS Output

Solver $\quad$ Stress (default): $\sigma x, \sigma y, \sigma_{x y}, \sigma \max , \sigma \min , \beta, \sigma s, \sigma e$ (see description of principal stresses)
Strain: $\varepsilon x, \varepsilon y, \gamma \mathrm{xy}, \varepsilon \max , \varepsilon \min , \beta, \varepsilon \mathrm{s}, \varepsilon \mathrm{e}$
Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

- Standard 2D continuum element


## Formulation

## Geometric Nonlinearity

$$
\begin{aligned}
\text { Total Lagrangian } & \text { Not applicable. } \\
\text { Updated } & \text { Not applicable. } \\
\text { Lagrangian } & \\
\text { Eulerian } & \text { For large displacements, large rotations and moderately large strains. } \\
\text { Co-rotational } & \text { For large displacements and large rotations. }
\end{aligned}
$$

## Integration Schemes

Stiffness Default. 1-point (see Notes).
Fine. As default.
Mass Default. 1-point (see Notes).
Fine. As default.

## Mass Modelling

Lumped mass only (see Notes).

## Options

34 Output element stress resultants.
55 Output strains as well as stresses.
105 Lumped mass matrix (see Notes).
139 Output yielded Gauss points only.

## Notes on Use

1. The element formulations are based on the standard isoparametric approach. The variation of stresses within an element can be regarded as constant.
2. The system parameter HGVISC is used to restrict element mechanisms due to underintegration. The default value is usually sufficient.
3. The bulk viscosity coefficients are used to restrict numerical oscillations due to the traversal of stress waves. The default bulk viscosity coefficients (BULKLF and BULKQF) may be altered as SYSTEM parameters.
4. These elements must be used with the dynamic central difference scheme and a lumped mass matrix.
5. These elements are not applicable. for static or eigenvalue analyses.
6. Automatic time step calculations are implemented.
7. As the element geometry is always updated in an explicit dynamic analysis, a nonlinear solution is obtained. When using explicit dynamics elements nonlinear control must be specified.
8. If creep properties are defined, explicit time integration must be specified.
9. Non-conservative loading is invoked when the FLD loading facility is applied.
10. Rayleigh damping coefficients are not supported by these elements.
11. Constraint equations are not available for use with these elements.
12. Nodes must be specified in an anticlockwise order. Option 123 is not applicable for this element. When using Modeller ensure surface normal is in the +ve z direction.

## Restrictions

Avoid excessive aspect ratio

## Recommendations on Use

Explicit dynamics elements may be used to define surface boundaries which will be active in a slideline analysis.

## 2D Plane Strain Continuum Elements

## General



## Element Group 2D Continuum

## Element <br> Plane Strain Continuum

## Subgroup

Element
A family of 2D isoparametric elements with higher order models capable
Description of modelling curved boundaries. The elements are numerically integrated.
Number Of $3,4,6$, or 8 numbered anticlockwise.
Nodes
Freedoms
$\mathrm{U}, \mathrm{V}$ : at each node.
Node X, Y: at each node.
Coordinates

## Geometric Properties

Not applicable (a unit thickness is assumed).

## Material Properties

Linear Isotropic:
Orthotropic:
Anisotropic:

Rigidities.
Matrix Not applicable
Joint Not applicable Concrete

Elasto-Plastic Stress resultant: Tresca:

DruckerPrager:

MohrCoulomb:

Modified
Mohr-
Coulomb:

Modified
Cam-clay
Optimised Implicit Von Mises:

Volumetric
Crushing:
Interface:
Stress
Potential

MATERIAL PROPERTIES (Elastic: Isotropic)
MATERIAL PROPERTIES ORTHOTROPIC PLANE STRAIN (Elastic: Orthotropic Plane Strain)
MATERIAL PROPERTIES ANISOTROPIC 4 (Not supported in LUSAS Modeller)
RIGIDITIES 4 (Not supported in LUSAS Modeller)

MATERIAL PROPERTIES NONLINEAR 105
(Elastic: Isotropic, Plastic: Transient Smoothed MultiCrack Concrete)
MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Not applicable.
MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
MATERIAL PROPERTIES
MODIFIED MOHR_COULOMB (Elastic:
Isotropic, Plastic: Mohr-Coulomb/Tresca, nonassociative Hardening with tension/compression cut-off)
MATERIAL PROPERTIES CAM_CLAY MODIFIED (Elastic: Isotropic, Plastic)
MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic)
MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam)
MATERIAL PROPERTIES NONLINEAR 27
STRESS POTENTIAL VON_MISES, HILL, HOFFMAN
(Isotropic: von Mises, Modified von Mises
Orthotropic: Hill, Hoffman)

Creep
AASHTO
CEB-FIP
Chinese
Eurocode
IRC
Damage
Viscoelastic
Shrinkage
Ko Initialisation Applicable
Rubber Not applicable
Generic Polymer IsotropicComposite Not applicable
CREEP PROPERTIES (Creep)
MATERIAL PROPERTIES NONLINEAR 86
AASHTO
(Concrete creep model to AASHTO code of
Practice)
MATERIAL PROPERTIES NONLINEAR 86 CEB-
FIP(Concrete creep model to CEB-FIP Model Code1990)
MATERIAL PROPERTIES NONLINEAR 86 CHINESE(Chinese creep model to Chinese Code of Practice)
MATERIAL PROPERTIES NONLINEAR 86EUROCODE
(Concrete creep model to EUROCODE_2)
MATERIAL PROPERTIES NONLINEAR 86 IRC
(Concrete creep model to Indian IRC code of
Practice)
DAMAGE PROPERTIES SIMO, OLIVER (Damage)
VISCO ELASTIC PROPERTIES
SHRINKAGE CEB_FIP_90, EUROCODE_2,
GENERAL, USER
MATERIAL PROPERTIES NONLINEAR 89(Generic Polymer Model)

## Loading

Prescribed Value PDSP, TPDSP Prescribed variable. U, V: at nodes.
Concentrated CL Loads Element Loads Not applicable.
Distributed Loads UDL Not applicable.
FLD Face Loads. Px, Py: local face axis pressures at nodes.
FLDG
Global Face Loads. $\sigma x, \sigma y, \sigma x y$ at nodes

Body Forces CBF

BFP, BFPE

Velocities VELO
Accelerations ACCE
Initial SSI, SSIE
Stress/Strains

SSIG

Residual Stresses SSR, SSRE

SSRG

Target TSSIE, TSSIA Stress/Strains

TSSIG

Temperatures TEMP, TMPE

Overburden Applicable.
Phreatic Surface Applicable.
Field Loads Not applicable.
Temp Dependent Not applicable. Loads

Constant body forces for element. Xcbf, Ycbf, 0,0 , $\Omega \mathrm{z}, \alpha \mathrm{z}$
Body force potentials at nodes/for element. 0, 0, 0, $\varphi 4$, Xcbf, Ycbf
Velocities. Vx, Vy: at nodes.
Acceleration Ax, Ay: at nodes.
Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y, \sigma z:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.

Initial stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}$ : global stresses. $\varepsilon x, \varepsilon y, \gamma \mathrm{xy}$ : global strains.

Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma x y$, $\sigma$ z: global stresses.
Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma x y, \sigma z$ global stresses.

Target stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y, \sigma z:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.

Target stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}$ : global stresses. $\varepsilon x, \varepsilon y, \gamma \mathrm{xy}$ : global strains.
Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}, 0$, 0,0

## LUSAS Output

## Solver <br> Stress (default): $\sigma x, \sigma y, \sigma x y, \sigma z, \sigma \max , \sigma \min , \beta, \sigma s, \sigma e$ (see description of principal stresses)

Strain: $\varepsilon \mathrm{x}, \varepsilon \mathrm{y}, \gamma \mathrm{xy}, \varepsilon z=0, \varepsilon \max , \varepsilon \min , \beta, \varepsilon s, \varepsilon \mathrm{e}$
Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

- Standard 2D continuum element


## Formulation

## Geometric Nonlinearity

$$
\begin{aligned}
\text { Total Lagrangian } & \text { For large displacements and large rotations. } \\
\text { Updated } & \text { For large displacements and large rotations. } \\
\text { Lagrangian } & \\
\text { Eulerian } & \text { For large displacements, large rotations and moderately large strains. } \\
\text { Co-rotational } & \text { For large displacements and large rotations. }
\end{aligned}
$$

## Integration Schemes

Stiffness Default. 1-point (TPN3), 3-point (TPN6), 2x2 (QPN4, QPN8)
Fine (see Options). $3 \times 3$ (QPN8), 3-point (TPN3).
Mass Default. 1-point (TPN3), 3-point (TPN6), 2x2 (QPN4, QPN8) Fine (see Options). $3 \times 3$ (QPN8), 3-point (TPN3).

## Mass Modelling

- Consistent mass (default).
$\square$ Lumped mass.


## Options

18 Invokes finer integration rule.
36 Follower loads.
54 Updated Lagrangian geometric nonlinearity
55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity.
91 Invokes fine integration rule for mass matrix.
105 Lumped mass matrix.
123 Clockwise node numbering.

139 Output yielded Gauss points only.
167 Eulerian geometric nonlinearity.
229 Co-rotational geometric nonlinearity

## Notes on Use

1. The element formulations are based on the standard isoparametric approach. The variation of stresses within an element can be regarded as constant for the lower order (corner node only) elements, and linear for the higher order (mid-side node) elements.
2. All elements pass the patch test.
3. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility.
4. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it is only applicable if every element is numbered clockwise. Surface normals should be visualised and if necessary corrected in the pre-processing stage.
5. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.
6. If applying an initial stress/strain or thermal load that varies across an element, a higher order element ( 6 or 8 nodes) should be used. A limitation of the standard isoparametric approach when used for lower order elements ( 3 or 4 nodes) is that only constant stress/strain fields can be imposed correctly.

## Restrictions

Ensure mid-side node centrality
I Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio

## Recommendations on Use

- The 8 -noded element with a $2 * 2$ Gauss rule is usually the most effective element, as the under-integration of the stiffness matrix prevents locking, which may occur either when the element is subjected to parasitic shear, or as the material reaches the incompressible limit (elasto-plasticity). The Gauss point stresses are also sampled at the most accurate locations for the element. However, the element does possess one spurious zero energy mode. This mode is very rarely activated in linear analysis, but it may occur in both materially and geometrically nonlinear analyses. Therefore, a careful examination of the solution should be performed, to check for spurious stress oscillations and peculiarities in the deformed configuration.
- The 8 -noded element with a $3 * 3$ Gauss rule may be used if a spurious mechanism is excited with the $2 * 2$ Gauss rule.
- The 4-noded element should not be used for analyses where in-plane bending effects are significant as the element tends to lock in parasitic shear, e.g. if QPN4 elements are employed to model a cantilever subject to a point load, the solution obtained will be over-stiff.


## 2D Plane Strain Continuum Element with Enhanced Strains

## General

## Element Name <br> 

QPN4M


## Element Group 2D Continuum

Element
Plane Strain Continuum
Subgroup
Element
A 2D isoparametric element with an assumed strain field. This mixed
Description assumed strain element demonstrates a superior performance to QPN4 (see Notes). The element is numerically integrated.
Number Of
4, numbered anticlockwise.
Nodes
Freedoms
$\mathrm{U}, \mathrm{V}$ : at each node.
Node X, Y: at each node.
Coordinates

## Geometric Properties

Not applicable (a unit thickness is assumed).

## Material Properties

| Linear | Isotropic: | MATERIAL PROPERTIES (Elastic: Isotropic) |
| :--- | :--- | :--- |
|  | Orthotropic: | MATERIAL PROPERTIES ORTHOTROPIC |
|  |  | PLANE STRAIN (Elastic: Orthotropic Plane Strain) |
|  | Anisotropic: | MATERIAL PROPERTIES ANISOTROPIC 4 (Not |
|  |  | supported in LUSAS Modeller) |
| Rigidities. | RIGIDITIES 4 (Not supported in LUSAS Modeller) |  |
| Matrix | Not applicable |  |


| JointConcrete | Not applicable |  |
| :---: | :---: | :---: |
|  |  | MATERIAL PROPERTIES NONLINEAR 105 (Elastic: Isotropic, Plastic: Transient Smoothed Multi Crack Concrete) |
|  |  | MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete) |
| Elasto-Plastic | Stress resultant: | Not applicable. |
|  | Tresca: | MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain) |
|  | Drucker- <br> Prager: | MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular) |
|  | Modified | MATERIAL PROPERTIES |
|  | Mohr- | MODIFIED MOHR_COULOMB (Elastic: |
|  | Coulomb: | Isotropic, Plastic: Mohr-Coulomb/Tresca, nonassociative Hardening with tension/compression cut-off) |
|  | Modified | MATERIAL PROPERTIES CAM_CLAY |
|  | Cam-clay | MODIFIED (Elastic: Isotropic, Plastic) |
|  | Optimised Implicit Von Mises: | MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic) |
|  | Volumetric Crushing: | MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam) |
|  | Stress | STRESS POTENTIAL VON_MISES, HILL, |
|  | Potential | HOFFMAN <br> (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman) |
| Creep | AASHTO | MATERIAL PROPERTIES NONLINEAR 86 AASHTO <br> (Concrete creep model to AASHTO code of Practice) |
|  | CEB-FIP | MATERIAL PROPERTIES NONLINEAR 86 CEBFIP (Concrete creep model to CEB-FIP Model Code 1990) |
|  | Chinese | MATERIAL PROPERTIES NONLINEAR 86 CHINESE |



Accelerations ACCE
Initial SSI, SSIE
Stress/Strains

SSIG

Residual Stresses SSR, SSRE

SSRG

Target TSSIE TSSIA Stress/Strains

TSSIG

Temperatures TEMP, TMPE Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}, 0$,

0,0
Acceleration Ax, Ay: at nodes.
Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y, \sigma z:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.
Initial stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}$ : global stresses. $\varepsilon x, \varepsilon y, \gamma \mathrm{xy}$ : global strains.
Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}$ : global stresses.
Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma x y, \sigma z$ global stresses.
Target stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y, \sigma z:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.

Target stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}$ : global stresses. $\varepsilon x, \varepsilon y, \gamma \mathrm{xy}$ : global strains.
Overburden Applicable.
Phreatic Surface Applicable.
Field Loads Not applicable.
Temp Dependent Not applicable.
Loads

## LUSAS Output

Solver
Stress (default): $\sigma x, \sigma y, \sigma x y, \sigma z, \sigma \max , \sigma \min , \beta, \sigma s, \sigma e$ (see description of principal stresses)
Strain: $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon z=0, \varepsilon$ max, $\varepsilon$ min, $\beta, \varepsilon s, \varepsilon \mathrm{e}$
Stretch (for rubber only): $\mathrm{V}_{11}, \mathrm{~V}_{22}, \mathrm{~V}_{12}, \lambda_{1}, \lambda_{2}, \lambda_{3}=1, \theta \lambda$, det F. Where
$V_{i i}$ are components of the left stretch tensors, $\lambda_{i}$ the principal stretches,
$\theta \lambda$ the angle between the maximum principal stretch and the global X axis, and det $F$ the determinant of the deformation gradient or volume ratio.

Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

- Standard 2D continuum element


## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements and large rotations.
Updated For large displacements and large rotations.
Lagrangian
Eulerian For large displacements, large rotations and moderately large strains.
Co-rotational For large displacements and large rotations (large strains with rubber).

## Integration Schemes

## Stiffness Default. 2x2

Fine. As default.
Mass Default. 2x2
Fine. As default.

## Mass Modelling <br> $\square$ Consistent mass (default). <br> $\square$ Lumped mass.

## Output

36 Follower loads.
39 Stress smoothing for rubber material models.
54 Updated Lagrangian geometric nonlinearity.
55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity.
91 Invokes fine integration rule for mass matrix.
105 Lumped mass matrix.
123 Clockwise node numbering.

139 Output yielded Gauss points only
167 Eulerian geometric nonlinearity.
225 Use alternative number of parameters for enhanced strain interpolation (see Notes).
229 Co-rotational geometric nonlinearity.

## Notes on Use

1. The variation of stresses within an element can be regarded as linear.
2. The element passes the patch test and the large strain patch test for rubber.
3. The strain field for this element consists of two parts: the compatible strains derived from an assumed displacement field and the assumed enhanced strains; see LUSAS Theory Manual. The assumed enhanced strain field is defined using 5 or 4 parameters for linear and nonlinear applications respectively. Option 225 switches on the higher 5 parameter enhanced strain interpolation function for nonlinear analysis.
4. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility. The load does not have to be normal to the face and may also vary over the face.
5. To apply a non-conservative (follower) pressure load (load type FLD) with corotational geometric nonlinearity, Option 36 must be specified. Note that this load should be normal to the face and constant for all the nodes of the element face.
6. The converged stresses for rubber are Kirchhoff stresses (see LUSAS Theory Manual).
7. Option 39 is used to smooth the stress output. It is particularly useful when the rubber material model is applied and the element is under very high compression where oscillatory stresses may appear (checker-board pattern).
8. When using the rubber material model, converged strain output is replaced by the left stretch tensor, the principal stretches and the angle defining these principal directions.
The value of $\operatorname{det} \mathrm{F}=\lambda_{1} \lambda_{2}$ (the Volume ratio) is only available for Gauss-point output. (Refer to the LUSAS Theory Manual for more details.)
9. For rubber, the iterative values of stress and strain are output in local co-rotated directions at the Gauss points only.
10. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it is only applicable if every element is numbered clockwise. Surface normals should be visualised and if necessary corrected in the pre-processing stage.
11. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.
12. Convergence difficulties can sometimes arise when using enhanced strain elements with nonlinear materials, particularly if the material is elastic-perfectly plastic or if a very shallow hardening curve is defined. In such cases it is recommended that the standard element formulation is used.
13. In analyses where significant in-plane bending is thermally induced it is recommended that a nonlinear solution is used. If a linear solution is required, then quadratic plane strain elements QPN8 are recommended.

## Restrictions

Rubber material models can only be applied in conjunction with the co-rotational formulation, Option 229.
$\square$ Avoid excessive aspect ratio

## Recommendations on Use

These elements exhibit an improved performance when compared with the parent element QPN4. The integration rules are the same as the parent element. The elements do not suffer from locking due to parasitic shear or when the material approaches the incompressible limit. The elements are also free of any zero energy modes.

## 2D Plane Strain Continuum Element for Large Strains

## General

## Element Name

QPN4L


Element Group 2D Continuum
Element
Subgroup
Element
Description
A 2D isoparametric element incorporating an internal pressure variable.
This element should be used for analyses involving large strains. The element is numerically integrated
Number Of
4, numbered anticlockwise.
Nodes
Freedoms
Node X, Y: at each node.
Coordinates
Plane Strain Continuum
$\mathrm{U}, \mathrm{V}$ : at each node.

## Geometric Properties

Not applicable (a unit thickness is assumed).

## Material Properties

## Linear Not applicable

Matrix Not applicable
Joint Not applicable
Concrete Not applicable

Elasto-Plastic Implicit Optimised Von Mises
Stress

MATERIAL PROPERTIES NONLINEAR 75
(Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic)
STRESS POTENTIAL VON_MISES (Isotropic: von
Potential Mises)
Creep Not applicableDamage Not applicableViscoelastic Not applicableShrinkage Not applicableKo Initialisation Not applicableRubber Ogden

Mooney-
Rivlin
Neo-Hookean

Hencky
Generic Polymer Not applicable Composite Not applicable

## MATERIAL PROPERTIES RUBBER OGDEN (Rubber: Ogden) <br> MATERIAL PROPERTIES RUBBER MOONEY_RIVLIN (Rubber: Mooney-Rivlin) <br> MATERIAL PROPERTIES RUBBER NEO_HOOKEAN (Rubber: Neo-Hookean) <br> MATERIAL PROPERTIES RUBBER HENCKY (Rubber: Hencky)

## Loading

Prescribed Value PDSP, TPDSP Concentrated CL Loads Element Loads Not applicable. Distributed Load UDL FLD

FLDG
Body Forces CBF

BFP, BFPE

Velocities VELO
Accelerations ACCE
Initial SSI, SSIE
Stress/Strains
SSIG
Residual Stresses SSR, SSRE

Prescribed variable. U, V: at nodes.
Concentrated loads. Px, Py: at nodes.

Not applicable.
Face loads. Px, Py: local face axis pressures at nodes.

Global Face Loads. $\sigma x, \sigma y, \sigma x y$ at nodes
Constant body forces for element. Xcbf, Ycbf, 0,0, $\Omega \mathrm{z}, \alpha \mathrm{z}$
Body force potentials at nodes/for element. 0, 0, 0, $\varphi 4$, Xcbf, Ycbf
Velocities. Vx, Vy: at nodes.
Acceleration Ax, Ay: at nodes.
Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y, \sigma z$ : global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.

Initial stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$, $\sigma z$ : global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.
Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma x y$,
$\sigma \mathrm{z}$ : global stresses.

Overburden Applicable.
Phreatic Surface Applicable.
Field Loads Not applicable.
Temp Dependent Not applicable. Loads

Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma x y, \sigma z$ global stresses.
Target TSSIE, TSSIA Stress/Strains

TSSIG

Temperatures TEMP, TMPE Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}, 0$,
SSRG 0,0
Target stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y, \sigma z:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.
Target stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}$ : global stresses. $\varepsilon x, \varepsilon y, \gamma \mathrm{xy}$ : global strains.
Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}, 0$,

Overburden Applicable

## LUSAS Output

## Solver <br> Stress (default): $\sigma x, \sigma y, \sigma x y, \sigma z, \sigma \max , \sigma \min , \beta, \sigma s, \sigma e$ (see description of principal stresses)

Principal stretches, $\lambda_{1}, \lambda_{2}, \lambda_{3}=1, \theta \lambda$, $\operatorname{det} F$. Where $V_{i i}$ are components of the left stretch tensors, $\lambda_{i}$ the principal stretches, $\theta \lambda$ the angle between the maximum principal stretch and the global X axis, and $\operatorname{det} \mathrm{F}$ the determinant of the deformation gradient or volume ratio.
Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

$\square$ Standard 2D continuum element

## Formulation

## Geometric Nonlinearity

Total Lagrangian Not applicable.
Updated Not applicable.
Lagrangian
Eulerian For large displacements and large strains.
Co-rotational For large displacements and large rotations.

## Integration Schemes

| Stiffness | Default. | $2 \times 2$ |
| :---: | :--- | :--- |
|  | Fine. | As default. |
| Mass | Default. | $2 \times 2$ |
|  | Fine. | As default. |

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

55 Output stretches as well as stresses.
91 Invokes fine integration rule for mass matrix.
105 Lumped mass matrix.
123 Clockwise node numbering.

## Notes on Use

1. The element formulations are based on the standard isoparametric approach. The variation of stresses within an element can be regarded as linear.
2. The element passes the large strain patch test for rubber.
3. Non-conservative loading is available with this element when using FLD loading.
4. The stresses output are Kirchhoff stresses (see LUSAS Theory Manual).
5. Stretch output consists of the principal stretches and the angle defining the principal directions. The value of det $\mathrm{F}=\lambda_{1} \lambda_{2}$ is also output. (Refer to the LUSAS Theory Manual.)
6. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it is only applicable if every element is numbered clockwise. Surface normals should be visualised and if necessary corrected in the pre-processing stage.
7. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.
8. This element is based on a formulation that tackles the problem of volumetric locking in a different way to that used in QPN4M. It should be preferred to the QPN4M in cases where Eulerian description (with a current configuration taken as reference) is more appropriate than the co-rotational description (e.g. inflation problems).

## Restrictions

- Avoid excessive aspect ratio
- Avoid non-uniform initial and thermal strains with coarse meshes.


## 2D Plane Strain Continuum Crack Tip Elements

## General



TNK6


Crack specified at Node 1

QNK8

Crack specified at Node 1


## Element Group 2D Continuum

Element Subgroup Element Description

Number Of
Nodes
Freedoms
Node

A family of 2D isoparametric crack tip elements where the crack tip can be located at any corner node. The mid-side nodes are moved to the quarter points to produce a singularity at the crack tip. The strains vary as the square root of $1 / R$, where $R$ is the distance from the crack tip. These elements are used at the crack tip only and should be mixed with the higher order plane strain continuum elements. The elements are numerically integrated. 6 or 8 , numbered anticlockwise.

U, V: at each node.
$\mathrm{X}, \mathrm{Y}$ : at each node.
Plane Strain Continuum

Coordinates

|  | Orthotropic: | MATERIAL PROPERTIES ORTHOTROPIC PLANE STRAIN (Elastic: Orthotropic Plane Strain) |
| :---: | :---: | :---: |
|  | Anisotropic: | MATERIAL PROPERTIES ANISOTROPIC 4 (Not supported in LUSAS Modeller) |
|  | Rigidities. | RIGIDITIES 4 (Not supported in LUSAS Modeller) |
| Matrix | Not applicable |  |
| Joint | Not applicable |  |
| Concrete |  | MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete) |
| Elasto-Plastic | Stress resultant: | Not applicable. |
|  | Interface: | MATERIAL PROPERTIES NONLINEAR 27 |
|  | Tresca: | MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain) |
|  | Drucker-Prager: | MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular) |
|  | Mohr-Coulomb: | MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation) |
|  | Modified MohrCoulomb: | MATERIAL PROPERTIES MODIFIED MOHR_COULOMB (Elastic: Isotropic, Plastic: Mohr-Coulomb/Tresca, nonassociative Hardening with tension/compression cut-off) |
|  | Modified Camclay | MATERIAL PROPERTIES CAM_CLAY MODIFIED (Elastic: Isotropic, Plastic) |
|  | Optimised Implicit Von Mises: | MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic) |
|  | Volumetric Crushing: | MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam) |

Stress PotentialCreepAASHTO
CEB-FIPChineseEurocode
DamageIRC
Viscoelastic
Shrinkage
Ko Initialisation Applicable
Rubber Not applicable
Generic Polymer Isotropic
MATERIAL PROPERTIES NONLINEAR 89(Generic Polymer Model)
Composite Not applicable
LoadingPrescribed Value PDSP, TPDSPConcentrated CLLoadsElement Loads Not applicable.Distributed Loads UDLFLDFLDGBody Forces CBFBFP, BFPEVelocities VELOAccelerations ACCEInitial SSI, SSIE
Stress/StrainsSSIG
Residual Stresses SSR, SSRE
SSRGTarget TSSIE, TSSIAStress/Strains

Temperatures TEMP, TMPE

Overburden Applicable.
Phreatic Surface Applicable.
Field Loads Not applicable.
Temp Dependent Not applicable. Loads

Prescribed variable. U, V: at nodes. Concentrated loads. Px, Py: at nodes.

Not applicable.
Face loads. Px, Py: local face axis pressures at nodes.

Global Face Loads. $\sigma x, \sigma y, \sigma x y$ at nodes
Constant body forces for element. Xcbf, Ycbf, 0, 0 , $\Omega \mathrm{z}, \alpha \mathrm{z}$
Body force potentials at nodes/for element. 0, 0, 0, $\varphi 4, \mathrm{Xcbf}, \mathrm{Ycbf}$
Velocities. Vx, Vy: at nodes.
Acceleration Ax, Ay: at nodes.
Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y, \sigma z:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.

Initial stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}$ : global stresses. $\varepsilon x, \varepsilon y, \gamma \mathrm{xy}$ : global strains.

Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma x y$, $\sigma$ : global stresses.

Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma x y, \sigma z:$ global stresses.
Target stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y, \sigma z:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.

Target stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$, $\sigma z:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y$ : global strains.
Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}, 0$, 0,0

## LUSAS Output

Solver Stress (default): $\sigma x, \sigma y, \sigma x y, \sigma \max , \sigma \min , \beta, \sigma s, \sigma e$ (see description of principal stresses)

Strain: $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon \max , \varepsilon \min , \beta, \varepsilon s, \varepsilon e$
Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

- Standard 2D continuum element


## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements and large rotations.
Updated For large displacements and large rotations.
Lagrangian
Eulerian For large displacements, large rotations and moderately large strains.
Co-rotational For large displacements and large rotations.

## Integration Schemes

| Stiffness | Default. | 6-point (TNK6), 3x3 (QNK8) |
| :---: | :--- | :--- |
|  | Fine (see Options). | 12-point (TNK6) |
| Mass | Default. | 6-point (TNK6), 3x3 (QNK8) |
|  | Fine (see Options). | 12-point (TNK6) |

## Mass Modelling

Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes finer integration rule.

$$
\begin{aligned}
\mathbf{5 4} & \text { Updated Lagrangian geometric nonlinearity. } \\
\mathbf{5 5} & \text { Output strains as well as stresses. } \\
\mathbf{8 7} & \text { Total Lagrangian geometric nonlinearity. } \\
\mathbf{9 1} & \text { Invokes fine integration rule for mass matrix. } \\
\mathbf{1 0 5} & \text { Lumped mass matrix. } \\
\mathbf{1 2 3} & \text { Clockwise node numbering. } \\
\mathbf{1 3 9} & \text { Output yielded Gauss points only. } \\
\mathbf{1 6 7} & \text { Eulerian geometric nonlinearity. } \\
\mathbf{2 2 9} & \text { Co-rotational geometric nonlinearity. }
\end{aligned}
$$

## Notes on Use

1. The element formulations are based on the standard isoparametric approach. Moving the mid-side nodes to the quarter points creates a singularity with theoretically infinite stress at the corner node.
2. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility.
3. Option 123 will not operate on a mesh with a mixture of clockwise and anticlockwise elements, it is only applicable if every element is numbered clockwise. Surface normals should be visualised and if necessary corrected in the pre-processing stage.
4. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.

## Restrictions

- Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio


## Recommendations on Use

Elements QNK8 and TNK6 are specifically designed for application to fracture mechanics problems and may be used to model the singularities that occur at the crack tip. The mid-side nodes near the crack tip are shifted to the quarter point. This ensures a singularity is present at the crack tip and that the strains vary as 1 /square root of $r$ where $r$ is the distance from the crack tip.The triangular TNK6 element is more effective than the quadrilateral element.

## 2D Plane Strain Explicit Dynamics Elements

## General

Element Name


TPN3E


## Element Group

2D Continuum
Element
Subgroup
Element
Description
A family of 2D isoparametric elements for explicit dynamic analyses. The

Number Of
Nodes
Freedoms
Node
elements are numerically integrated.
3 or 4 numbered anticlockwise.
$\mathrm{U}, \mathrm{V}$ : at each node.
$\mathrm{X}, \mathrm{Y}$ : at each node.
Plane Strain Continuum


## Geometric Properties

Not applicable (a unit thickness is assumed).

## Material Properties

Linear Isotropic:
Orthotropic
MATERIAL PROPERTIES (Elastic: Isotropic)
MATERIAL PROPERTIES ORTHOTROPIC
PLANE STRAIN (Elastic: Orthotropic Plane Strain)
Anisotropic: Not applicable.
Rigidities. Not applicable.
Matrix Not applicable
Joint Not applicable
Concrete Not applicable

| Elasto-Plastic | Stress resultant: | Not applicable. |
| :---: | :---: | :---: |
|  | Tresca: | MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain) |
|  | Drucker- <br> Prager: | MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular) |
|  | MohrCoulomb: | MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation) |
|  | Modified | MATERIAL PROPERTIES |
|  | Mohr- | MODIFIED MOHR_COULOMB (Elastic: |
|  | Coulomb: | Isotropic, Plastic: Mohr-Coulomb/Tresca, nonassociative Hardening with tension/compression cut-off) |
|  | Optimised Implicit Von Mises: | MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic) |
|  | Volumetric Crushing: | MATERIAL PROPERTIES NONLINEAR 81 <br> (Volumetric Crushing or Crushable Foam) |
|  | Stress | STRESS POTENTIAL VON_MISES, HILL, |
|  | Potential | HOFFMAN (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman) |
| Creep |  | CREEP PROPERTIES (Creep) (see Notes) |
| Damage |  | DAMAGE PROPERTIES SIMO, OLIVER (Damage) |
| Viscoelastic |  | VISCO ELASTIC PROPERTIES |
| Shrinkage | Not applicable |  |
| Ko Initialisation | Not applicable |  |
| Rubber | Not applicable |  |
| Generic Polymer | Not applicable |  |
| Composite | Not applicable |  |

## Loading

| Prescribed Value | PDSP, TPDSP |
| ---: | :--- |
| Concentrated | CL |
| Loads |  |
| Element Loads | Not |
|  | applicable. |

Prescribed variable. U, V: at each node.
Concentrated loads. Px, Py: at each node.

| Distributed Loads | UDL | Not applicable. |
| ---: | :--- | :--- |
|  | FLD | Face loads. Px, Py: local face axis pressures at |

## LUSAS Output

## Solver

Stress (default): $\sigma x, \sigma y, \sigma x y, \sigma z, \sigma \max , \sigma \min , \beta, \sigma s, \sigma e$ (see description of principal stresses)

Strain: $\varepsilon x, \varepsilon y, \gamma \mathrm{xy}, \varepsilon \max , \varepsilon \min , \beta, \varepsilon s, \varepsilon \mathrm{e}$

# Modeller See Results Tables (Appendix K). 

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

Standard 2D continuum element

## Formulation

## Geometric Nonlinearity

Total Lagrangian Not applicable.
Updated Not applicable.
Lagrangian
Eulerian For large displacements, large rotations and moderately large strains.
Co-rotational For large displacements and large rotations.

## Integration Schemes

Stiffness Default. 1-point (see Notes).
Fine. As default.
Mass Default. 1-point (see Notes).
Fine. As default.

## Mass Modelling

L Lumped mass only (see Notes).

## Options

55 Output strains as well as stresses.
105 Lumped mass matrix (see Notes).
139 Output yielded Gauss points only.

## Notes on Use

1. The element formulations are based on the standard
2. The system parameter HGVISC is used to restrict element mechanisms due to underintegration. The default value is usually sufficient.
3. The bulk viscosity coefficients are used to restrict numerical oscillations due to the traversal of stress waves. The default bulk viscosity coefficients (BULKLF and BULKQF) may be altered as SYSTEM parameters.
4. These elements must be used with a dynamic central difference scheme and a lumped mass matrix in order to obtain the maximum efficiency from the numerical algorithms.
5. These elements are not applicable for static or eigenvalue analyses.
6. Automatic time step calculations are implemented.
7. As the element geometry is always updated in an explicit dynamic analysis, a nonlinear solution is obtained. When using explicit dynamics elements NONLINEAR CONTROL must be specified.
8. If CREEP PROPERTIES are defined, explicit time integration must be specified in VISCOUS CONTROL.
9. Non-conservative loading is invoked when the FLD loading facility is applied.
10. Rayleigh damping coefficients are not supported by these elements.
11. Constraint equations are not available for use with these elements.
12. Nodes must be specified in an anticlockwise order. Option 123 is not applicable for this element. When using Modeller ensure surface normal is in the +ve z direction.

## Restrictions

$\square$ Avoid excessive aspect ratio

## Recommendations on Use

Explicit dynamics elements may be used to define surface boundaries which will be active in a slideline analysis.

## 2D Plane Strain Two Phase Continuum Elements

## General

Element Name


TPN6P


QPN8P


## Element Group 2D Continuum

Element
Plane Strain Continuum
Subgroup
Element
A family of 2D isoparametric elements with higher order models capable
Description of modelling curved boundaries. The elements are numerically integrated.
Number Of
6 or 8 numbered anticlockwise.
Nodes
Freedoms
Node
$\mathrm{U}, \mathrm{V}, \mathrm{P}$ at corner nodes. $\mathrm{U}, \mathrm{V}$ at midside nodes.
$\mathrm{X}, \mathrm{Y}$ : at each node.
Coordinates

## Geometric Properties

Not applicable (a unit thickness is assumed).

## Material Properties

Linear Isotropic:
MATERIAL PROPERTIES (Elastic: Isotropic)
Orthotropic:
Anisotropic:
MATERIAL PROPERTIES ORTHOTROPIC PLANE STRAIN (Elastic: Orthotropic Plane Strain)
MATERIAL PROPERTIES ANISOTROPIC 4 (Not supported in LUSAS Modeller)
Rigidities.
Matrix Not applicable
Joint Not applicable
Concrete
MATERIAL PROPERTIES NONLINEAR 109

Elasto-Plastic Stress resultant: Tresca:

DruckerPrager:

MohrCoulomb:

Modified MohrCoulomb:

Modified
Cam-clay
Optimised Implicit Von Mises:

Volumetric
Crushing:
Interface
Stress
Potential
(Elastic: Isotropic, Plastic: Smoothed Multi Crack Concrete)
Not applicable.
MATERIAL PROPERTIES NONLINEAR 61
(Elastic: Isotropic, Plastic: Tresca, Hardening:
Isotropic Hardening Gradient, Isotropic Plastic
Strain or Isotropic Total Strain)
MATERIAL PROPERTIES NONLINEAR 64
(Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
MATERIAL PROPERTIES MODIFIED MOHR_COULOMB (Elastic: Isotropic, Plastic: Mohr-Coulomb/Tresca, nonassociative Hardening with tension/compression cut-off)
MATERIAL PROPERTIES CAM_CLAY MODIFIED (Elastic: Isotropic, Plastic)
MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic)
MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam)
MATERIAL PROPERTIES NONLINEAR 27
STRESS POTENTIAL VON_MISES, HILL, HOFFMAN
(Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
CREEP PROPERTIES (Creep)
DAMAGE PROPERTIES SIMO, OLIVER (Damage)
VISCOELASTIC PROPERTIES
SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER

Ko Initialisation Not applicable Rubber Not applicable Generic Polymer

MATERIAL PROPERTIES NONLINEAR 89
(Generic Polymer Model)

## Loading

Prescribed Value PDSP, TPDSP
Concentrated CL Loads
Element Loads Not applicable. Distributed Loads UDL FLD

FLDG
Body Forces CBF

BFP, BFPE

Velocities VELO
Accelerations ACCE
Initial SSI, SSIE
Stress/Strains

SSIG

Residual Stresses SSR, SSRE

SSRG

Target TSSIE, TSSIA Stress/Strains

TSSIG

Temperatures TEMP, TMPE
Overburden Applicable.

Prescribed variable. U, V, P at corner nodes. U, V at midside nodes.
Concentrated loads. Px, Py, Q at corner nodes. Px, Py at midside nodes.

Not applicable.
Face Loads. Px, Py, Q: face pressures/flux per unit area at corner nodes relative to local face axes. Px, Py: face pressures at midside nodes relative to local face axes.
Global Face Loads. $\sigma x, \sigma y, \sigma x y$ at nodes
Constant body forces for element. Xcbf, Ycbf, 0, 0 , $\Omega \mathrm{z}, \alpha \mathrm{z}, \mathrm{gx}, \mathrm{gy}$ (see Notes on Use)
Body force potentials at nodes/for element. 0, 0, 0, $\varphi 4, \mathrm{Xcbf}, \mathrm{Ycbf}, \mathrm{gx}, \mathrm{gy}$ (see Notes on Use)
Velocities. Vx, Vy: at nodes.
Acceleration Ax, Ay: at nodes.
Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma \mathrm{xy}, \sigma \mathrm{z}, \sigma \mathrm{p}$ global stresses. $\mathcal{\varepsilon}, \varepsilon \mathrm{y}, \gamma \mathrm{xy}$ : global strains.

Initial stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}, \sigma \mathrm{p}:$ global stresses. $\varepsilon \mathrm{x}, \varepsilon \mathrm{y}, \gamma \mathrm{xy}$ : global strains.
Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}, \sigma \mathrm{p}$ : global stresses.
Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma x y, \sigma z$, $\sigma$ p global stresses.
Target stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma \mathrm{xy}, \sigma \mathrm{z}, \sigma \mathrm{p}$ global stresses. $\varepsilon \mathrm{x}, \varepsilon \mathrm{y}, \gamma \mathrm{xy}$ : global strains.

Target stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}, \sigma \mathrm{p}:$ global stresses. $\varepsilon \mathrm{x}, \varepsilon \mathrm{y}, \gamma \mathrm{xy}$ : global strains.
Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}, 0$, 0,0
Phreatic Surface Applicable.
Field Loads Not applicable.
Temp Dependent Not applicable.
Loads

## LUSAS Output

# Solver <br> Stress (default): $\sigma x, \sigma y, \sigma x y, \sigma z, \sigma p, \sigma \max , \sigma \min , \beta, \sigma s, \sigma e$ (see description of principal stresses) 

Strain: $\varepsilon x, \varepsilon y, \gamma \mathrm{xy}, \varepsilon z=0, \varepsilon \mathrm{v}, \varepsilon \max , \varepsilon \mathrm{min}, \beta, \varepsilon \mathrm{s}, \varepsilon \mathrm{e}$
Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

$\square$ Standard 2D continuum element

## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements and large rotations.
Updated For large displacements and large rotations.
Lagrangian
Eulerian For large displacements, large rotations and moderately large strains.
Co-rotational For large displacements and large rotations.

## Integration Schemes

| Stiffness | Default. | 3-point (TPN6P), 2x2 (QPN8P) |
| :---: | :--- | :--- |
|  | Fine (see Options). | 3x3 (QPN8P) |
| Mass | Default. | 3-point (TPN6P), 2x2 (QPN8P) |
|  | Fine (see Options). | $3 \times 3$ (QPN8P) |

Mass Modelling
$\square$ Consistent mass (default).
$\square$ Lumped mass.
Options
18 Invokes finer integration rule.
36 Follower loads.
54 Updated Lagrangian geometric nonlinearity
55 Output strains as well as stresses
87 Total Lagrangian geometric nonlinearity.
91 Invokes fine integration rule for mass matrix.
105 Lumped mass matrix.
123 Clockwise node numbering.
139 Output yielded Gauss points only.
167 Eulerian geometric nonlinearity.
229 Co-rotational geometric nonlinearity.

## Notes on Use

1. Two phase material parameters must be used with these elements for undrained and consolidation analysis.
2. The element formulations are based on the standard isoparametric approach. The variation of isoparametric stresses and pore pressures within an element can be considered linear.
3. All elements pass the patch test.
4. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it is only applicable if every element is numbered clockwise. Surface normals should be visualised and if necessary corrected in the pre-processing stage. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.
5. Non-conservative loading is available with these elements when using Updated Lagrangian, Eulerian or co-rotational (with OPTION 36) geometric nonlinear formulations together with the FLD loading facility.
6. The global components of gravity acting on the fluid phase are defined by $g x$ and gy under CBF and BFP loading.

## Restrictions

Ensure mid-side node centrality
$\square$ Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio

## 2D Axisymmetric Solid Continuum Elements

## General



TAX3


QAX4


TAX6


QAX8


## Element Group 2D Continuum

## Element Axisymmetric Solid

## Subgroup

Element
Description
A family of 2D isoparametric elements with higher order models capable of modelling curved boundaries. The formulations apply over a unit radian segment of the structure and the loading and boundary conditions are axisymmetric. By default, the Y -axis is taken as the axis of symmetry. The elements are numerically integrated.
Number Of
$3,4,6$, or 8 numbered anticlockwise.
Nodes
Freedoms U, V: at each node.
Node X, Y: at each node.
Coordinates

## Geometric Properties

Not applicable (a unit radian segment is assumed).

## Material Properties

Linear Isotropic:
Orthotropic:

Anisotropic:

Rigidities.
Matrix Not applicable Joint Not applicable Concrete

Llasto-Plastic
Stress resultant:
Interface:
Tresca:

Drucker-Prager:

Mohr-Coulomb:

Modified MohrCoulomb:

Modified Cam-
clay
Optimised Implicit Von
Mises:
Volumetric

MATERIAL PROPERTIES (Elastic: Isotropic) MATERIAL PROPERTIES ORTHOTROPIC AXISYMMETRIC (Elastic: orthotropic Axisymmetric)
MATERIAL PROPERTIES ANISOTROPIC 4 (Not supported in LUSAS Modeller)
Not applicable.

MATERIAL PROPERTIES NONLINEAR 105
(Elastic: Isotropic, Plastic: Transient Smoothed Multi-Crack Concrete)
MATERIAL PROPERTIES NONLINEAR 109
(Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Not applicable.
MATERIAL PROPERTIES NONLINEAR 27.
MATERIAL PROPERTIES NONLINEAR 61
(Elastic: Isotropic, Plastic: Tresca, Hardening:
Isotropic Hardening Gradient, Isotropic Plastic
Strain or Isotropic Total Strain)
MATERIAL PROPERTIES NONLINEAR 64
(Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
MATERIAL PROPERTIES
MODIFIED MOHR_COULOMB (Elastic:
Isotropic, Plastic: Mohr-Coulomb/Tresca, nonassociative Hardening with tension/compression cut-off)
MATERIAL PROPERTIES CAM CLAY MODIFIED (Elastic: Isotropic, Plastic)
MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic)
MATERIAL PROPERTIES NONLINEAR 81

|  | Crushing: <br> Stress Potential | (Volumetric Crushing or Crushable Foam) STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman) |
| :---: | :---: | :---: |
| Creep |  | CREEP PROPERTIES (Creep) |
|  | CEB-FIP | MATERIAL PROPERTIES NONLINEAR 86 CEBFIP <br> (Concrete creep model to CEB-FIP Model Code 1990) |
|  | AASHTO | MATERIAL PROPERTIES NONLINEAR 86 AASHTO <br> (Concrete creep model to AASHTO code of Practice) |
|  | CEB-FIP | MATERIAL PROPERTIES NONLINEAR 86 CEBFIP <br> (Concrete creep model to CEB-FIP Model Code 1990) |
|  | Chinese | MATERIAL PROPERTIES NONLINEAR 86 CHINESE <br> (Chinese creep model to Chinese Code of Practice) |
|  | Eurocode | MATERIAL PROPERTIES NONLINEAR 86 EUROCODE <br> (Concrete creep model to EUROCODE_2) |
|  | IRC | MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice) |
| Damage |  | DAMAGE PROPERTIES SIMO, OLIVER (Damage) |
| Viscoelastic |  | VISCO ELASTIC PROPERTIES |
| Shrinkage |  | SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER |
| Ko Initialisation | Applicable |  |
| Rubber | Not applicable |  |
| Generic Polymer | Isotropic | MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model) |
| Composite | Not applicable |  |

Loading

Prescribed Value PDSP, TPDSP Concentrated CL Loads
Element Loads Not applicable.
Distributed Loads UDL
FLD

FLDG
Body Forces CBF

BFP, BFPE

## Velocities VELO <br> Accelerations ACCE <br> Initial SSI, SSIE <br> Stress/Strains

SSIG

Residual Stresses SSR, SSRE

SSRG

Target TSSIE, TSSIA Stress/Strains

TSSIG

Temperatures TEMP, TMPE

Overburden Applicable.
Phreatic Surface Applicable.
Field Loads Not applicable.
Temp Dependent Not applicable. Loads

Prescribed variable. U, V: at nodes.
Concentrated loads. Px, Py: force per unit radian at nodes.

Not available.
Face loads. Px, Py: local face pressures at nodes (force per unit area).

Global Face Loads. $\sigma x, \sigma y, \sigma x y$ at nodes
Constant body forces for element. Xcbf, Ycbf, $\Omega x$,
$\Omega \mathrm{y}$ (angular velocity must be applied about axis of symmetry), 0, 0 .
Body force potentials at nodes/for element. 0, 0, 0, $\varphi 4, \mathrm{Xcbf}, \mathrm{Ycbf}$
Velocities. Vx, Vy: at nodes.
Acceleration Ax, Ay: at nodes.
Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y, \sigma z:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon z:$ global strains.

Initial stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}$ : global stresses. $\varepsilon \mathrm{x}, \varepsilon \mathrm{y}, \gamma \mathrm{xy}, \varepsilon \mathrm{z}$ : global strains.
Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma x y$, $\sigma$ z: global stresses.

Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma x y, \sigma z$ : global stresses.
Target stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y, \sigma z:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon z:$ global strains.

Target stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}$ : global stresses. $\varepsilon x, \varepsilon y, \gamma \mathrm{xy}, \varepsilon z$ : global strains.
Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}, 0$, 0, 0

## LUSAS Output

Solver
Stress (default): $\sigma x, \sigma y, \sigma x y, \sigma z, \sigma \max , \sigma \min , \beta, \sigma s, \sigma e$ (see description of principal stresses)
Strain: $\varepsilon \mathrm{x}, \varepsilon \mathrm{y}, \gamma \mathrm{xy}, \varepsilon \mathrm{z}, \varepsilon \max , \varepsilon \mathrm{min}, \beta, \varepsilon \mathrm{s}, \varepsilon \mathrm{e}$
Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

- Standard 2D continuum element


## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements and large rotations.
Updated For large displacements and large rotations.
Lagrangian
Eulerian For large displacements, large rotations and moderately large strains.
Co-rotational Not applicable.

## Integration Schemes

Stiffness Default. 1-point (TAX3), 3-point (TAX6), 2x2 (QAX4, QAX8)
Fine (see Options). $\quad 3 \times 3$ (QAX8), 3-point (TAX3).
Mass Default. 1-point (TAX3), 3-point (TAX6), 2x2 (QAX4, QAX8)
Fine (see Options). $3 \times 3$ (QAX8), 3-point (TAX3).

## Mass Modelling

$\square$ Consistent mass (default).

- Lumped mass.


## Options

18 Invokes finer integration rule.
$47 \quad$ X-axis taken as axis of symmetry
54 Updated Lagrangian geometric nonlinearity.
55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity.
91 Invokes fine integration rule for mass matrix.
105 Lumped mass matrix.
123 Clockwise node numbering.
139 Output yielded Gauss points only.
167 Eulerian geometric nonlinearity.

## Notes on Use

1. The element formulations are based on the standard isoparametric approach. The variation of stresses within an element can be regarded as constant for the lower order (corner node only) elements, and linear for the higher order (mid-side node) elements.
2. All elements pass the patch test.
3. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility.
4. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it is only applicable if every element is numbered clockwise. Surface normals should be visualised and if necessary corrected in the pre-processing stage.
5. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.
6. The maximum and minimum principal stress computations for axisymmetric elements do not include the $\sigma \mathrm{z}$ term as this is implicitly a principal stress in a biaxial stress field.
7. An initial stress/strain or thermal load that varies across an element should not be applied to this element. A limitation of the standard isoparametric approach when used for lower order elements is that only constant stress/strain fields can be imposed correctly.

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature
- Avoid excessive aspect ratio


## Recommendations on Use

- The 8 -noded element with a $2 * 2$ Gauss rule is usually the most effective element, as the under-integration of the stiffness matrix prevents locking, which may occur either when the element is subjected to parasitic shear, or as the material reaches the incompressible limit (elasto-plasticity). The Gauss point stresses are also sampled at the most accurate locations for the element. However, the element does possess one spurious zero energy mode. This mode is very rarely activated in linear analysis, but it may occur in both materially and geometrically nonlinear analyses. Therefore, a careful examination of the solution should be performed, to check for spurious stress oscillations and peculiarities in the deformed configuration.
- The 8 -noded element with a $3 * 3$ Gauss rule may be used if a spurious mechanism is excited with the $2 * 2$ Gauss rule.
- The 4-noded element should not be used for analyses where in-plane bending effects are significant as the element tends to lock in parasitic shear.


## 2D Axisymmetric Solid Continuum Element with Enhanced Strains

## General



QAX4M


## Element Group Element Subgroup <br> Element

Description
A 2D isoparametric element with an assumed strain field. This mixed assumed strain element demonstrates a superior performance to QAX4 (see Notes). The formulations apply over a unit radian segment of the structure, and the loading and boundary conditions are axisymmetric. By default, the Y -axis is taken as the axis of symmetry. The element is numerically integrated.
4, numbered anticlockwise. Nodes Freedoms
Node
$\mathrm{U}, \mathrm{V}$ : at each node.
$\mathrm{X}, \mathrm{Y}$ : at each node.
2D Continuum
Axisymmetric Solid

Number Of

X, Y: at each node.
Coordinates

## Geometric Properties

Not applicable (a unit radian segment is assumed).

## Material Properties

## Linear Isotropic: <br> MATERIAL PROPERTIES (Elastic: Isotropic) <br> Orthotropic: MATERIAL PROPERTIES ORTHOTROPIC AXISYMMETRIC (Elastic: Orthotropic Axisymmetric)

|  | Anisotropic: | MATERIAL PROPERTIES ANISOTROPIC 4 (Not supported in LUSAS Modeller) |
| :---: | :---: | :---: |
|  | Rigidities. | Not applicable |
| Matrix | Not applicable |  |
| Joint | Not applicable |  |
| Concrete |  | MATERIAL PROPERTIES NONLINEAR 105 |
|  |  | (Elastic: Isotropic, Plastic: Transient Smoothed Multi- |
|  |  | Crack Concrete) |
|  |  | MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete) |
| Elasto-Plastic | Stress <br> resultant: | Not applicable. |
|  | Tresca: | MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain) |
|  | DruckerPrager: | MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular) |
|  | MohrCoulomb: | MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation) |
|  | Modified | MATERIAL PROPERTIES |
|  | Mohr- | MODIFIED MOHR_COULOMB (Elastic: |
|  | Coulomb: | Isotropic, Plastic: Mohr-Coulomb/Tresca, nonassociative Hardening with tension/compression cut-off) |
|  | Modified | MATERIAL PROPERTIES CAM_CLAY |
|  | Cam-clay | MODIFIED (Elastic: Isotropic, Plastic) |
|  | Optimised | MATERIAL PROPERTIES NONLINEAR 75 |
|  | Implicit Von | (Elastic: Isotropic, Plastic: Von Mises, Hardening: |
|  | Mises: | Isotropic \& Kinematic) |
|  | Volumetric | MATERIAL PROPERTIES NONLINEAR 81 |
|  | Crushing: | (Volumetric Crushing or Crushable Foam) |
|  | Stress | STRESS POTENTIAL VON_MISES, HILL, |
|  | Potential | HOFFMAN |
|  |  | (Isotropic: von Mises, Modified von Mises |
|  |  | Orthotropic: Hill, Hoffman) |
| Creep |  | CREEP PROPERTIES (Creep) |
|  | AASHTO | MATERIAL PROPERTIES NONLINEAR 86 |
|  |  | AASHTO |
|  |  | (Concrete creep model to AASHTO code of |Practice)CEB-FIP

IRC
Damage
Viscoelastic
Shrinkage
Ko Initialisation Applicable
Rubber Not applicableGeneric Polymer Isotropic
Chinese
Eurocode
MATERIAL PROPERTIES NONLINEAR 86 CEB-FIP(Concrete creep model to CEB-FIP Model Code1990)
MATERIAL PROPERTIES NONLINEAR 86CHINESE(Chinese creep model to Chinese Code of Practice)
MATERIAL PROPERTIES NONLINEAR 86EUROCODE
(Concrete creep model to EUROCODE_2)
MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
DAMAGE PROPERTIES SIMO, OLIVER (Damage)
VISCO ELASTIC PROPERTIES GENERAL, USER
MATERIAL PROPERTIES NONLINEAR 89(Generic Polymer Model)

## Loading

Prescribed Value PDSP, TPDSP Prescribed variable. U, V: at nodes.
Concentrated CLLoadsConcentrated loads. Px, Py: force per unit radian atnodes.
Element Loads Not applicable.
Distributed Loads UDL Not available.FLDFace loads. Px, Py: local face pressures at nodes(force per unit area).
FLDG
Body Forces CBF
Global Face Loads. $\sigma x, \sigma y, \sigma x y$ at nodesConstant body forces for element. Xcbf, Ycbf, $\Omega$ x,$\Omega \mathrm{y}$ (angular velocity must be applied about axis ofsymmetry), 0,0.
BFP, BFPE Body force potentials at nodes/for element. 0, 0, 0,$\varphi 4$, Xcbf, Ycbf

Velocities VELO
Accelerations ACCE
Initial SSI, SSIE
Stress/Strains

SSIG

Residual Stresses SSR, SSRE

SSRG

Target TSSIE, TSSIA Stress/Strains

TSSIG

Temperatures TEMP, TMPE
Overburden Applicable.
Phreatic Surface Applicable.
Field Loads Not applicable.
Temp Dependent Not applicable.
Loads

Velocities. Vx, Vy: at nodes.
Acceleration Ax, Ay: at nodes.
Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma \mathrm{xy}, \sigma \mathrm{z}$ : global stresses. $\varepsilon \mathrm{x}, \varepsilon \mathrm{y}, \gamma \mathrm{xy}, \varepsilon \mathrm{z}:$ global strains.

Initial stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}$ : global stresses. $\varepsilon \mathrm{x}, \varepsilon \mathrm{y}, \gamma \mathrm{xy}, \varepsilon \mathrm{z}$ : global strains.
Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}$ : global stresses.
Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma x y, \sigma z$ : global stresses.
Target stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y, \sigma z:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon z:$ global strains.
Target stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}$ : global stresses. $\varepsilon \mathrm{x}, \varepsilon \mathrm{y}, \gamma \mathrm{xy}, \varepsilon \mathrm{z}$ : global strains.
Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}, 0$, 0,0

## LUSAS Output

Solver

Stress (default): $\sigma x, \sigma y, \sigma x y, \sigma z, \sigma \max , \sigma m i n, \beta, \sigma s, \sigma e$ (see description of principal stresses)
Strain: $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon z, \varepsilon m a x, \varepsilon m i n, \beta, \varepsilon s, \varepsilon e$
Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).
Sign ConventionStandard 2D continuum element
Formulation
Geometric Nonlinearity
Total Lagrangian For large displacements and large rotations.
Updated For large displacements and large rotations.
LagrangianCo-rotational Not applicable.
Integration Schemes
Stiffness Default. ..... $2 \times 2$
Fine. As default.
Mass Default. ..... 2x2
Fine. ..... As default.
Mass Modelling
$\square$ Consistent mass (default).
$\square$ Lumped mass.
Options
$47 \quad$ X-axis taken as axis of symmetry
54 Updated Lagrangian geometric nonlinearity
55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity.
91 Invokes fine integration rule for mass matrix.
105 Lumped mass matrix.
123 Clockwise node numbering.
139 Output yielded Gauss points only.
167 Eulerian geometric nonlinearity.Eulerian For large displacements, large rotations and moderately large strains.

## Notes on Use

1. The element formulations are based on the standard isoparametric approach. The variation of stresses within an element can be regarded as linear.
2. All elements pass the patch test.
3. The strain field for this element consists of two parts: the compatible strains derived from an assumed displacement field and the assumed enhanced strains; see LUSAS Theory Manual. The assumed enhanced strain field is defined using 5 parameters for both linear and nonlinear applications.
4. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility.
5. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it will only work if every element is numbered clockwise. The best way to avoid a mixture is to check and appropriately reverse the surface definitions in the pre-processing stage of modelling.
6. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.
7. The maximum and minimum principal stress computations for axisymmetric elements do not include the $\sigma z$ term as this is implicitly a principal stress in a biaxial stress field.
8. Convergence difficulties can sometimes arise when using enhanced strain elements with nonlinear materials, particularly if the material is elastic-perfectly plastic or if a very shallow hardening curve is defined. In such cases it is recommended that the standard element formulation is used.
9. This element exhibits an improved performance when compared with its parent element QAX4. The integration rules are the same as the parent element. The elements do not suffer from locking due to parasitic shear or when the material approaches the incompressible limit. The elements are also free of any zero energy modes.
10. In analyses where significant in-plane bending is thermally induced it is recommended that a nonlinear solution is used. If a linear solution is required, then quadratic plane strain elements QPN8 are recommended.

## Restrictions

$\square$ Avoid excessive aspect ratio

## 2D Axisymmetric Solid Continuum Element for Large Strains

## General

## Element Name

## QAX4L



## Element Group

2D Continuum
Axisymmetric Solid
Subgroup
Element
Description
A 2D isoparametric element incorporating an internal pressure variable.
This element should be used for analyses involving large strains. The
formulations apply over a unit radian segment of the structure and the
loading and boundary conditions are axisymmetric. By default, the Y-axis is taken as the axis of symmetry. The element is numerically integrated.
Number Of
4, numbered anticlockwise.
Nodes
Freedoms U, V: at each node.
Node X, Y: at each node.
Coordinates

## Geometric Properties

Not applicable (a unit radian segment is assumed).

## Material Properties

Linear Not applicable
Matrix Not applicable
Joint Not applicable
Concrete Not applicable
Elasto-Plastic Implicit MATERIAL PROPERTIES NONLINEAR 75

Optimised<br>Von Mises<br>Stress<br>Potential<br>Creep Not applicable<br>Damage Not applicable<br>Viscoelastic Not applicable<br>Shrinkage Not applicable<br>Ko Initialisation Not applicable Rubber Ogden<br>Mooney-<br>Rivlin<br>Neo-Hookean<br>Hencky<br>Generic Polymer Not applicable<br>Composite Not applicable<br>(Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic )<br>STRESS POTENTIAL VON_MISES (Isotropic: von Mises)<br>\section*{MATERIAL PROPERTIES RUBBER OGDEN (Rubber: Ogden)<br><br>MATERIAL PROPERTIES RUBBER MOONEY_RIVLIN (Rubber: Mooney-Rivlin)<br><br>MATERIAL PROPERTIES RUBBER NEO_HOOKEAN (Rubber: Neo-Hookean)<br><br>MATERIAL PROPERTIES RUBBER HENCKY (Rubber: Hencky)}<br>\section*{Loading}<br>Prescribed Value PDSP, TPDSP<br>Concentrated CL<br>Loads<br>Element Loads Not applicable.<br>Distributed Loads U<br>FLD<br>FLDG<br>Body Forces CBF<br>BFP, BFPE<br>Velocities VELO<br>Accelerations ACCE<br>Initial SSI, SSIE<br>Stress/Strains<br>Prescribed variable. U, V: at nodes.<br>Concentrated loads. Px, Py: force per unit radian at nodes.<br>Not available.<br>Face loads. Px, Py: local face pressures at nodes (force per unit area).<br>Global Face Loads. $\sigma x, \sigma y, \sigma x y$ at nodes<br>Constant body forces for element. Xcbf, Ycbf, $\Omega$ x, $\Omega y$, (angular velocity must be applied about axis of symmetry), 0,0.<br>Body force potentials at nodes/for element. 0, 0, 0, $\varphi 4, \mathrm{Xcbf}, \mathrm{Ycbf}$<br>Velocities. Vx, Vy: at nodes.<br>Acceleration Ax, Ay: at nodes.<br>Initial stresses/strains at nodes/for element. $\sigma x$, $\sigma y, \sigma x y, \sigma z:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon z:$

global strains.
SSIG Initial stresses/strains at Gauss points. $\sigma x, \sigma y$, $\sigma x y, \sigma z$ : global stresses. $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon z:$ global strains.

Residual Stresses SSR, SSRE

SSRG

Target TSSIE, TSSIA Stress/Strains

TSSIG

Temperatures TEMP, TMPE

Overburden Applicable.
Phreatic Surface Applicable.
Field Loads Not applicable.
Temp Dependent Not applicable.
Loads
Residual stresses at nodes/for element. $\sigma x, \sigma y$, $\sigma x y, \sigma z:$ global stresses.
Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}$ : global stresses.
Target stresses/strains at nodes/for element. $\sigma x$, $\sigma y, \sigma x y, \sigma z:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon z:$ global strains.
Target stresses/strains at Gauss points. $\sigma x, \sigma y$, $\sigma x y, \sigma z:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon z:$ global strains.
Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}$, $0,0,0$

## LUSAS Output

## Solver $\quad$ Stress (default): $\sigma x, \sigma y, \sigma x y, \sigma z, \sigma \max , \sigma \min , \beta, \sigma s, \sigma e$ (see description of principal stresses)

Principal stretches, $\lambda_{1}, \lambda_{2}, \lambda_{3} 1, \theta \lambda$, det F. Where $\lambda_{i}$ are the principal stretches, $\theta \lambda$ the angle between the maximum principal stretch and the global X axis, and $\operatorname{det} \mathrm{F}$ the determinant of the deformation gradient or volume ratio.
Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

Standard 2D continuum element

## Formulation

## Geometric Nonlinearity

Total Lagrangian Not applicable.
Updated Not applicable.
Lagrangian
Eulerian For large displacements and large strains.
Co-rotational Not applicable.

## Integration Schemes

Stiffness Default. 2x2
Fine. As default.
Mass Default. 2x2
Fine. As default.

## Mass Modelling

$\square$ Consistent mass (default).

- Lumped mass.


## Options

47 X-axis taken as axis of symmetry.
55 Output stretches as well as stresses.
91 Invokes fine integration rule for mass matrix.
105 Lumped mass matrix
123 Clockwise node numbering.

## Notes on Use

1. The element formulations are based on the standard isoparametric approach. The variation of stresses within an element can be regarded as linear.
2. The element passes the large strain patch test for rubber.
3. Non-conservative loading is available with this element when using FLD loading.
4. The stresses output are Kirchhoff stresses (see LUSAS Theory Manual).
5. Stretch output consists of the principal stretches and the angle defining the principal directions. The value of $\operatorname{det} \mathrm{F}=\lambda_{1} \lambda_{2}$ is also output. (Refer to the LUSAS Theory Manual for more details.)
6. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it will only work if every element is numbered clockwise. The best way to avoid a mixture is to check and appropriately reverse the surface definitions in the pre-processing stage of modelling.
7. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.
8. The maximum and minimum principal stress computations for axisymmetric elements do not include the $\sigma z$ term as this is implicitly a principal stress in a biaxial stress field.

## Restrictions

Avoid excessive aspect ratio
Avoid non-uniform initial and thermal strains with coarse meshes

## 2D Axisymmetric Solid Continuum Crack Tip Elements

## General

Element Name


TXK6


Crack specified at Node 1

QXK8


Crack specified at Node 1

## Element Group

Element
Subgroup
Element
Description
A family of 2D isoparametric crack tip elements where the crack tip can be located at any node. The mid-side nodes are moved to the quarter points to produce a singularity at the crack tip. The strains vary as the square root of $1 / \mathrm{R}$, where R is the distance from the crack tip. These elements are used at the crack tip only and should be mixed with the higher order axisymmetric solid continuum elements. The formulations apply over a unit radian segment of the structure, and the loading and boundary conditions are axisymmetric. By default, the Y-axis is taken as the axis of symmetry. The elements are numerically integrated.
Number Of Nodes
Freedoms U, V: at each node.
Node $\mathrm{X}, \mathrm{Y}$ : at each node.
2D Continuum
Axisymmetric Solid

6 or 8 numbered anticlockwise.

Coordinates

## Geometric Properties

Not applicable (a unit radian segment is assumed).

## Material Properties

Linear Isotropic:
Orthotropic:
MATERIAL PROPERTIES (Elastic: Isotropic)
MATERIAL PROPERTIES ORTHOTROPIC

AXISYMMETRIC (Elastic: Orthotropic Axisymmetric)
Anisotropic: MATERIAL PROPERTIES ANISOTROPIC 4 (Not supported in LUSAS Modeller)
Rigidities. Not applicable.
Matrix Not applicable
Joint Not applicable Concrete

## Elasto-Plastic

Stress resultant:
Interface:
Tresca:
Tresca.
MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Not applicable.
MATERIAL PROPERTIES NONLINEAR 27
MATERIAL PROPERTIES NONLINEAR 61
(Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
Drucker-Prager: MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
Mohr-Coulomb: MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
Modified Mohr- MATERIAL PROPERTIES
Coulomb:

Modified Cam-
clay
Optimised
Implicit Von
Mises:
Volumetric
Crushing:
Stress Potential

Creep
AASHTO

MODIFIED MOHR_COULOMB (Elastic: Isotropic, Plastic: Mohr-Coulomb/Tresca, nonassociative Hardening with tension/compression cut-off)
MATERIAL PROPERTIES CAM_CLAY MODIFIED (Elastic: Isotropic, Plastic)
MATERIAL PROPERTIES NONLINEAR 75
(Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic)
MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam)
STRESS POTENTIAL VON_MISES, HILL, HOFFMAN
(Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
CREEP PROPERTIES (Creep)
MATERIAL PROPERTIES NONLINEAR 86 AASHTO
(Concrete creep model to AASHTO code of Practice)

CEB-FIP

## Damage

IRC
Eurocode
Chinese

Viscoelastic
Shrinkage
Shrinkage Applicable
Rubber Not applicable Generic Polymer Isotropic

Composite Not applicable

MATERIAL PROPERTIES NONLINEAR 86 CEBFIP
(Concrete creep model to CEB-FIP Model Code 1990)

MATERIAL PROPERTIES NONLINEAR 86 CHINESE
(Chinese creep model to Chinese Code of Practice)
MATERIAL PROPERTIES NONLINEAR 86 EUROCODE
(Concrete creep model to EUROCODE_2)
MATERIAL PROPERTIES NONLINEAR 86 IRC
(Concrete creep model to Indian IRC code of Practice)
DAMAGE PROPERTIES SIMO, OLIVER (Damage)
VISCO ELASTIC PROPERTIES
SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER

MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)

## Loading

Prescribed PDSP, TPDSP Prescribed variable. U, V: at nodes.
Value
Concentrated CL Concentrated loads. Px, Py: at nodes. Loads
Element Loads Not applicable.
Distributed UDL Not applicable.
Loads
FLD
FLDG
Body Forces CBF

BFP, BFPE Body force potentials at nodes/for element. $0,0,0, \varphi_{4}$,

|  |  | Xcbf, Ycbf |
| :---: | :---: | :---: |
| Velocities | VELO | Velocities. Vx, Vy: at nodes. |
| Accelerations | ACCE | Acceleration Ax, Ay: at nodes. |
| Initial Stress/Strains | SSI, SSIE | Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma \mathrm{xy}, \sigma \mathrm{z}$ : global stresses. $\varepsilon \mathrm{x}, \varepsilon \mathrm{y}, \gamma \mathrm{xy}, \varepsilon z$ : global strains. |
|  | SSIG | Initial stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y, \sigma z:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon z: ~ g l o b a l ~ s t r a i n s . ~$ |
| Residual Stresses | SSR, SSRE | Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}$ : global stresses. |
|  | SSRG | Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma x y, \sigma z:$ global stresses. |
| Target Stress/Strains | TSSIE, TSSIA | Target stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y, \sigma z:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon z:$ global strains. |
|  | TSSIG | Target stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}$ : global stresses. $\varepsilon x, \varepsilon y, \gamma \mathrm{xy}, \varepsilon z$ : global strains. |
| Temperatures | TEMP, TMPE | Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}, 0,0,0$ |
| Overburden | Applicable. |  |
| Phreatic Surface | Applicable. |  |
| Field Loads | Not applicable. |  |
| Temp | Not applicable. |  |
| Dependent Loads |  |  |

## LUSAS Output

## Solver $\quad$ Stress (default): $\sigma x, \sigma y, \sigma x y, \sigma z, \sigma \max , \sigma \min , \beta, \sigma s, \sigma e$ (see description of principal stresses)

Strain: $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon z, \varepsilon m a x, \varepsilon m i n, \beta, \varepsilon s, \varepsilon e$
Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

- Standard 2D continuum element


## Formulation

## Geometric Nonlinearity

$$
\begin{aligned}
\text { Total Lagrangian } & \text { For large displacements and large rotations. } \\
\text { Updated } & \text { For large displacements and large rotations. } \\
\text { Lagrangian } & \\
\text { Eulerian } & \text { For large displacements, large rotations and moderately large strains. } \\
\text { Co-rotational } & \text { Not applicable. }
\end{aligned}
$$

## Integration Schemes

| Stiffness | Default. | 6-point (TXK6), 3x3 (QXK8) |
| :---: | :--- | :--- |
|  | Fine (see Options). | 12-point (TXK6). |
| Mass (QXK8) |  |  |
|  | Default. | 6-point (TXK6), 3x3 (QX8) |
|  | Fine (see Options). | 12-point (TXK6). |

## Mass Modelling

$\square$ Consistent mass (default).

- Lumped mass.


## Options

18 Invokes finer integration rule.
$47 \quad \mathrm{X}$-axis taken as axis of symmetry.
54 Updated Lagrangian geometric nonlinearity.
55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity.
91 Invokes fine integration rule for mass matrix.
105 Lumped mass matrix
123 Clockwise node numbering.
139 Output yielded Gauss points only.
167 Eulerian geometric nonlinearity.

## Notes on Use

1. The element formulations are based on the standard isoparametric approach. Moving the mid-side nodes to the quarter points creates a singularity with theoretically infinite stress at the corner node.
2. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility.
3. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it will only work if every element is numbered clockwise. The best way to avoid a mixture is to check and appropriately reverse the surface definitions in the pre-processing stage of modelling.
4. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.
5. The maximum and minimum principal stress computations for axisymmetric elements do not include the $\sigma z$ term as this is implicitly a principal stress in a biaxial stress field.

## Restrictions

- Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio


## Recommendations on Use

The QXK8 and TXK6 elements are specifically designed for application to fracture mechanics problems and may used to model the singularities that occur at the crack tip. The mid-side nodes near the crack tip are shifted to the quarter point. This ensures a singularity is present at the crack tip and that the strains vary as 1 /square root of $r$ where $r$ is the distance from the crack tip. The triangular TPK6 element is more effective than the quadrilateral element.

## 2D Axisymmetric Solid Explicit Dynamics Elements

## General

Element Name
TAX3E


QAX4E


## Element Group

2D Continuum
Element
Subgroup
Element
Description
Axisymmetric Solid Continuum
A family of 2D isoparametric elements for explicit dynamic analyses.
The formulations apply over a unit radian segment of structure and loading boundary conditions are axisymmetric. By default, the Y-axis is taken as the axis of symmetry. The elements are numerically integrated.
Number Of 3 or 4 numbered anticlockwise.
Nodes
Freedoms U, V: at each node.
Node $\mathrm{X}, \mathrm{Y}$ : at each node.
Coordinates

## Geometric Properties

Not applicable (a unit radian segment is assumed).

## Material Properties

| Linear | Isotropic: | MATERIAL PROPERTIES (Elastic: Isotropic) |
| :--- | :--- | :--- |
|  | Orthotropic: | MATERIAL PROPERTIES ORTHOTROPIC |
|  |  | AXISYMMETRIC (Elastic: Orthotropic |
|  |  | Axisymmetric) |
|  | Anisotropic: | Not applicable |
| Rigidities. | Not applicable |  |

Matrix Not applicable
Joint Not applicable
Concrete Not applicable
Elasto-Plastic Stress Not applicable
resultant:
Tresca:
Drucker-
Prager:
Mohr-
Coulomb:
Modified
Mohr-
Coulomb:
Optimised Implicit Von
Mises:
Volumetric
Crushing:
Stress
Potential
Creep
AASHTO
CEB-FIP
Chinese

MATERIAL PROPERTIES NONLINEAR 61
(Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
MATERIAL PROPERTIES NONLINEAR 64
(Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
MATERIAL PROPERTIES MODIFIED MOHR_COULOMB (Elastic:
Isotropic, Plastic: Mohr-Coulomb/Tresca, nonassociative Hardening with tension/compression cut-off)
MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic)
MATERIAL PROPERTIES NONLINEAR 81
(Volumetric Crushing or Crushable Foam)
STRESS POTENTIAL VON_MISES, HILL, HOFFMAN
(Isotropic: von Mises, Modified von Mises
Orthotropic: Hill, Hoffman)
CREEP PROPERTIES (Creep) (See Notes)
MATERIAL PROPERTIES NONLINEAR 86 AASHTO
(Concrete creep model to AASHTO code of Practice)

MATERIAL PROPERTIES NONLINEAR 86 CEBFIP
(Concrete creep model to CEB-FIP Model Code 1990)

MATERIAL PROPERTIES NONLINEAR 86 CHINESE
(Chinese creep model to Chinese Code of Practice)
Eurocode

IRC

Damage
Viscoelastic
Shrinkage
Not applicable

## Ko Initialisation

Rubber
Applicable
Not applicable
Generic Polymer Not applicable
Composite Not applicable
MATERIAL PROPERTIES NONLINEAR 86 EUROCODE
(Concrete creep model to EUROCODE_2)MATERIAL PROPERTIES NONLINEAR 86 IRC(Concrete creep model to Indian IRC code ofPractice)
DAMAGE PROPERTIES SIMO, OLIVER (Damage)

## Loading

| Prescribed Value Concentrated Loads | $\begin{aligned} & \text { PDSP, TPDSP } \\ & \text { CL } \end{aligned}$ | Prescribed variable. U, V: at each node. Concentrated loads. Px, Py: at each node. |
| :---: | :---: | :---: |
| Element Loads | Not applicable. |  |
| Distributed Loads | UDL | Not applicable. |
|  | FLD | Face loads. Px, Py: local face axis pressures at nodes. |
|  | FLDG | Not applicable. |
| Body Forces | CBF | Constant body forces for element. Xcbf, Ycbf, $\Omega$ x, $\Omega y$ (angular velocity must be applied about axis of symmetry), 0,0. |
|  | BFP, BFPE | Body force potentials at nodes/for element. $0,0,0$, $\varphi 4$, Xcbf, Ycbf |
| Velocities | VELO | Velocities. Vx, Vy at nodes. |
| Accelerations | ACCE | Acceleration. Ax, Ay at nodes. |
| Initial <br> Stress/Strains | SSI, SSIE | Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y, \sigma z:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon z$ : global strains. |
|  | SSIG | Initial stress/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}$ : global stress. $\varepsilon \mathrm{x}, \varepsilon \mathrm{y}, \gamma \mathrm{xy}, \varepsilon \mathrm{z}$ : global strains. |

Prescribed ValueConcentratedCLNotapplicable.LoadsFLDG
Body ForcesVelocitiesVELOAccelerationsACCESSI, SSIE

Not applicable.
Face loads. Px, Py: local face axis pressures at nodes.
Not applicable.
Constant body forces for element. Xcbf, Ycbf, $\Omega \mathrm{x}$,
$\Omega y$ (angular velocity must be applied about axis of symmetry), 0,0.
Body force potentials at nodes/for element. $0,0,0$, $\varphi 4$, Xcbf, Ycbf
Velocities. Vx, Vy at nodes.
Acceleration. Ax, Ay at nodes.
Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y, \sigma z:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon z$ : global strains.

Initial stress/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$, $\sigma z$ : global stress. $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon z:$ global strains.
Residual Stresses SSR, SSRE
SSRG
Target Not
Stress/Strains applicable.
Temperatures TEMP, TMPETemperatures at nodes/for element. T, $0,0,0, \mathrm{To}, 0$,0,0

Residual stresses at nodes/for element $\sigma x, \sigma y, \sigma x y$, $\sigma$ z: global stresses.

Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma x y, \sigma z$ : global stresses.

$$
0,0
$$

Overburden Not applicable
Phreatic Surface
Not applicable.
Field Loads Not applicable.
Temp Dependent Not
Loads applicable.

## LUSAS Output

# Solver <br> Stress (default): $\sigma x, \sigma y, \sigma x y, \sigma z, \sigma \max , \sigma \min , \beta, \sigma \mathrm{~s}, \sigma \mathrm{e}$ (see description of principal stresses) 

Strain: $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon z, \varepsilon m a x, \varepsilon m i n, \beta, \varepsilon s, \varepsilon e$
Modeller See Results Tables (Appendix K)

## Local Axes

Not applicable.

## Sign Convention

- Standard 2D continuum element


## Formulation

## Geometric Nonlinearity

Total Lagrangian Not applicable.
Updated Not applicable.
Lagrangian
Eulerian For large displacements, large rotations and moderately large strains. Co-rotational Not applicable.

## Integration Schemes

| Stiffness | Default. <br>  <br> Mass <br> Fine. | 1-point (see Notes) |
| :---: | :--- | :--- |
|  | Default. | 1-point (see Notes) |
|  | Fine. | As default. |

## Mass Modelling

$\square$ Lumped mass (see Notes).

## Options

$47 \quad \mathrm{X}$-axis taken as axis of symmetry
55 Output strains as well as stresses.
105 Lumped mass matrix (see Notes).
139 Output yielded Gauss points only.

## Notes on Use

1. The element formulations are based on the standard
2. The system parameter HGVISC is used to restrict element mechanisms due to underintegration. The default value is usually sufficient.
3. The bulk viscosity coefficients are used to restrict numerical oscillations due to the traversal of stress waves. The default bulk viscosity coefficients (BULKLF and BULKQF) may be altered as a SYSTEM parameter.
4. These elements must be used with a dynamic central difference scheme and a lumped mass matrix.
5. These elements are not applicable to static or eigenvalue analyses.
6. Automatic time step calculations are implemented.
7. As the element geometry is always updated in an explicit dynamic analysis, a nonlinear solution is obtained. When using explicit dynamics elements Nonlinear Control must be specified.

## 8. If CREEP PROPERITES are defined explicit time integration must be specified in VISCOUS CONTROL.

9. Non-conservative loading is invoked when the face loading (FLD) is applied.
10. Rayleigh damping coefficients are not supported by these elements.
11. Constraint equations are not available for use with these elements.
12. Nodes must be specified in an anticlockwise order. Option 123 is not applicable for this element. When using Modeller ensure surface normal is in the +ve z direction.
13. The maximum and minimum principal stress computations for axisymmetric elements do not include the $\sigma z$ term as this is implicitly a principal stress in a biaxial stress field.

## Restrictions

$\square$ Avoid excessive aspect ratio

## Recommendations on Use

Explicit dynamics elements may be used to define surface boundaries which will be active in a slideline analysis.

## 2D Axisymmetric Solid Two Phase Continuum Elements

## General



## Element Group 2D Continuum

Element Axisymmetric Solid
Subgroup
Element Description

A family of 2D isoparametric elements with higher order models capable of modelling curved boundaries. The formulations apply over a unit radian segment of the structure and the loading and boundary conditions are axisymmetric. By default, the Y -axis is taken as the axis of symmetry. The elements are numerically integrated.
Number Of
6 or 8 numbered anticlockwise.
Nodes
Freedoms
Node
$\mathrm{U}, \mathrm{V}, \mathrm{P}$ : at corner nodes. $\mathrm{U}, \mathrm{V}$ : at midside nodes.
$\mathrm{X}, \mathrm{Y}$ : at each node.

Coordinates

QAX8P


## Geometric Properties

Not applicable (a unit radian segment is assumed).

## Material Properties

| Linear | Isotropic: | MATERIAL PROPERTIES (Elastic: Isotropic) |
| :--- | :--- | :--- |
|  | Orthotropic: | MATERIAL PROPERTIES ORTHOTROPIC |
|  |  | AXISYMMETRIC (Elastic: orthotropic, |
|  |  | Axisymmetric) |

Not applicable.Matrix Not applicableJoint Not applicableConcreteElasto-Plastic Stress resultant:Interface:Tresca:Drucker-Prager:Mohr-Coulomb:
CreepModified Cam-clayOptimisedImplicit Von
Mises:VolumetricCrushing:Stress PotentialModified Mohr-Coulomb:
Damage
Viscoelastic
Shrinkage
Ko Initialisation ApplicableRubber Not applicableGeneric Polymer Isotropic
MATERIAL PROPERTIES NONLINEAR 109(Elastic: Isotropic, Plastic: Smoothed Multi-CrackConcrete)
Not applicable.
MATERIAL PROPERTIES NONLINEAR 27.
MATERIAL PROPERTIES NONLINEAR 61 ..... 61
(Elastic: Isotropic, Plastic: Tresca, Hardening:Isotropic Hardening Gradient, Isotropic PlasticStrain or Isotropic Total Strain)
MATERIAL PROPERTIES NONLINEAR 64(Elastic: Isotropic, Plastic: Drucker-Prager,Hardening: Granular)
MATERIAL PROPERTIES NONLINEAR 65(Elastic: Isotropic, Plastic: Mohr-Coulomb,Hardening: Granular with Dilation)
MATERIAL PROPERTIESMODIFIED MOHR_COULOMB (Elastic:Isotropic, Plastic: Mohr-Coulomb/Tresca, non-associative Hardening with tension/compressioncut-off)MATERIAL PROPERTIES CAM CLAYMODIFIED (Elastic: Isotropic, Plastic)
MATERIAL PROPERTIES NONLINEAR 75(Elastic: Isotropic, Plastic: Von Mises, Hardening:Isotropic \& Kinematic)
MATERIAL PROPERTIES NONLINEAR 81(Volumetric Crushing or Crushable Foam)STRESS POTENTIAL VON_MISES, HILL,HOFFMAN
(Isotropic: von Mises, Modified von MisesOrthotropic: Hill, Hoffman)
CREEP PROPERTIES (Creep)
DAMAGE PROPERTIES SIMO, OLIVER(Damage)
VISCO ELASTIC PROPERTIES
SHRINKAGE CEB_FIP_90, EUROCODE_2,GENERAL, USER
MATERIAL PROPERTIES NONLINEAR 89

# (Generic Polymer Model) 

Composite Not applicable

## Loading

Prescribed Value PDSP, TPDSP

Concentrated CL Loads

Element Loads Not applicable. Distributed Loads UDL

FLD

FLDG
Body Forces CBF

BFP, BFPE

## Velocities VELO <br> Accelerations ACCE <br> Initial SSI, SSIE <br> Stress/Strains

SSIG

Residual Stresses SSR, SSRE

SSRG

Target TSSIE, TSSIA Stress/Strains

Prescribed variable. U, V, P: at corner nodes. U, V:at midsaide nodes.
Concentrated loads. Px, Py, Q: force/flux per unit radian at corner nodes. Px,Py: force per unit radian at midside nodes.

Not available.
Face loads. Px, Py, Q: local face pressures/flux at corner nodes (force/flux per unit area). Px, Py: local face pressures at midside nodes.
Global Face Loads. $\sigma x, \sigma y, \sigma x y$ at nodes
Constant body forces for element. Xcbf, Ycbf, $\Omega x$, $\Omega \mathrm{y}$ (angular velocity must be applied about axis of symmetry), 0, 0, gx, gy. (See Notes on Use)
Body force potentials at nodes/for element. 0, 0, 0, $\varphi 4, \mathrm{Xcbf}, \mathrm{Ycbf}, \mathrm{gx}, \mathrm{gy}$. (See Notes on Use)
Velocities. Vx, Vy: at nodes.
Acceleration Ax, Ay: at nodes.
Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma \mathrm{xy}, \sigma \mathrm{z}, \sigma \mathrm{p}$ : global stresses. $\varepsilon \mathrm{x}, \varepsilon \mathrm{y}, \gamma \mathrm{xy}, \varepsilon z$ : global strains.
Initial stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$, $\sigma \mathrm{z}, \sigma \mathrm{p}:$ global stresses. $\varepsilon \mathrm{x}, \varepsilon \mathrm{y}, \gamma \mathrm{xy}, \varepsilon z$ : global strains.

Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma x y$, $\sigma z, \sigma p:$ global stresses.

Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma x y, \sigma z$, $\sigma$ p: global stresses.

Target stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma x y, \sigma z, \sigma p:$ global stresses. $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon z:$ global strains.
Target stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma x y$,
$\sigma \mathrm{z}, \sigma \mathrm{p}:$ global stresses. $\varepsilon \mathrm{x}, \varepsilon \mathrm{y}, \gamma \mathrm{xy}, \varepsilon z:$ global strains.
Temperatures TEMP, TMPE Temperatures at nodes/for element. T, 0, 0, 0, To, 0 , 0,0
Overburden Applicable.
Phreatic Surface Applicable.
Field Loads Not applicable.
Temp Dependent Not applicable.
Loads

## LUSAS Output

Solver
Stress (default): $\sigma x, \sigma y, \sigma x y, \sigma z, \sigma p, \sigma m a x, \sigma \min , \beta, \sigma s, \sigma e$ (see description of principal stresses)

Strain: $\varepsilon x, \varepsilon y, \gamma x y, \varepsilon z, \varepsilon m a x, \varepsilon m i n, ~ \beta, \varepsilon s, \varepsilon e$
Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

- Standard 2D continuum element


## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements and large rotations.
Updated For large displacements and large rotations.
Lagrangian
Eulerian For large displacements, large rotations and moderately large strains.
Co-rotational Not applicable.

## Integration Schemes

| Stiffness | Default. | 3-point (TAX6P), 2x2 (QAX8P) |
| :---: | :--- | :--- |
|  | Fine (see Options). | $3 \times 3$ (QAX8P) |
| Mass | Default. | 3-point (TAX6P), 2x2 (QAX8P) |
|  | Fine (see Options). | $3 \times 3$ (QAX8P) |

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes finer integration rule.
$47 \quad$ X-axis taken as axis of symmetry
54 Updated Lagrangian geometric nonlinearity.
55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity.
91 Invokes fine integration rule for mass matrix.
105 Lumped mass matrix.
123 Clockwise node numbering.
139 Output yielded Gauss points only.
167 Eulerian geometric nonlinearity.

## Notes on Use

1. Two phase material parameters must be used with these elements for undrained and consolidation analysis.
2. The element formulations are based on the standard isoparametric approach. The variation of isoparametric stresses and pore pressures within an element can be regarded as linear.
3. All elements pass the patch test.
4. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility.
5. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it is only applicable if every element is numbered clockwise. Surface normals should be visualised and if necessary corrected in the pre-processing stage.
6. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.
7. The global components of gravity acting on the fluid phase are defined by $g x$ and gy under CBF and BFP loading.
8. The maximum and minimum principal stress computations for axisymmetric elements do not include the $\square \mathrm{z}$ term as this is implicitly a principal stress in a biaxial stress field.

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio


## Recommendations on Use

- The 8 -noded element with a $2 * 2$ Gauss rule is usually the most effective element, as the under-integration of the stiffness matrix prevents locking, which may occur either when the element is subjected to parasitic shear, or as the material reaches the incompressible limit (elasto-plasticity). The Gauss point stresses are also sampled at the most accurate locations for the element. However, the element does possess one spurious zero energy mode. This mode is very rarely activated in linear analysis, but it may occur in both materially and geometrically nonlinear analyses. Therefore, a careful examination of the solution should be performed, to check for spurious stress oscillations and peculiarities in the deformed configuration.
- The 8 -noded element with a $3 * 3$ Gauss rule may be used if a spurious mechanism is excited with the $2 * 2$ Gauss rule.


## 2D Axisymmetric Fourier Ring Elements

## General



## Element Group 2D Continuum

Element Subgroup

Element
Description

Number Of
Nodes
Freedoms

A family of 2D isoparametric elements with higher order models capable of modelling curved boundaries. The structure must be axisymmetric but
the loading need not be. By default the Y-axis is taken to be the axis of of modelling curved boundaries. The structure must be axisymmetric but
the loading need not be. By default the Y-axis is taken to be the axis of symmetry. The elements are numerically integrated.
$3,4,6$ or 8 numbered anticlockwise.

Node X, Y: at each node.
Fourier Ring

U, V, W: at each node (in cylindrical coordinates, see local coordinates).

## Geometric Properties

Not applicable.

## Material Properties

Linear Isotropic:
Orthotropic:

Anisotropic:
Rigidities.
Matrix Not applicable
Joint Not applicable
Concrete Not applicable
Elasto-Plastic Not applicable
Creep Not applicable
Damage Not applicable
Viscoelastic Not applicable
Shrinkage Not applicable
Ko Initialisation Not applicable
Rubber Not applicable
Generic Polymer Not applicable
Composite Not applicable
MATERIAL PROPERTIES (Elastic: Isotropic)
MATERIAL PROPERTIES ORTHOTROPIC
(Elastic: Orthotropic Plane Stress)
MATERIAL PROPERTIES ORTHOTROPIC
SOLID (Elastic: Orthotropic Solid)
Not applicable
Not applicable

MATERIAL PROPERTIES (Elastic: Isotropic) MATERIAL PROPERTIES ORTHOTROPIC (Elastic: Orthotropic Plane Stress) MATERIAL PROPERTIES ORTHOTROPIC SOLID (Elastic: Orthotropic Solid) Not applicable Not applicable

## Loading

Prescribed Value PDSP, TPDSP
Concentrated CL Loads
Element Loads Not applicable.
Distributed Loads UDL FLD

FLDG
Body Forces CBF

Prescribed variable. U, V, W: at each node.
Concentrated loads. Px, Py, Pz: at each node (global, may also be applied locally, see options).

Not applicable.
Face loads. Px, Py, Pz: local face axis pressures at nodes Pz in the direction of increasing $\theta$.
Not applicable.
Constant body forces for element (see Notes). Xcbf, Ycbf, Zcbf, $\Omega_{\mathrm{x}}, \Omega_{\mathrm{y}} \Omega_{\mathrm{z}}, \alpha_{\mathrm{x}}, \alpha \mathrm{y}, \alpha_{\mathrm{z}}, \mathrm{Xo}, \mathrm{Yo}, \mathrm{Zo}$, d $\theta / d t$
Body force potentials at nodes/for element. Xcbf,
Ycbf, Zcbf

Velocities VELO
Accelerations ACCE
Initial SSI, SSIE
Stress/Strains

## Residual Stresses Not

 applicable.Target Not
Stress/Strains applicable.
Temperatures TEMP, TMPE Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}, 0$, 0,0
Overburden Not applicable.
Phreatic Surface Not applicable.
Field Loads Not applicable.
Temp Dependent Not
Loads applicable.

## LUSAS Output

Solver
Stress (default): $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z, \sigma \max , \sigma \min , \beta, \sigma s, \sigma e$ (see description of principal stresses)
Strain: $\varepsilon x, \varepsilon y, \varepsilon z, \gamma_{\mathrm{xy}}, \gamma_{\mathrm{yz}}, \gamma_{\mathrm{xz}}, \varepsilon \max , \varepsilon \min , \beta, \varepsilon s, \varepsilon e$
Use LUSAS Modeller to access results at various angles around the structure. See Local and Global Results in the Modeller User Manual
Modeller See Results Tables (Appendix K).

## Local Axes

- Cylindrical coordinates (see Appendix F).
$\square$ The element axes are defined in the cylindrical coordinate system $\mathrm{x}, \mathrm{y}, \mathrm{z}$, with associated displacements $\mathrm{u}, \mathrm{v}, \mathrm{w}$. The tangential displacement w is positive in the direction of increasing $\theta$, where $\theta$ is the positive rotation defined by the right-hand coordinate system about the axis of symmetry. $u$ and $v$ are positive in the direction of increasing $x$ and $y$ respectively and may be either axial or radial displacements depending on the definition of the axis of symmetry.


## Sign Convention

- Standard 3D continuum element


## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Stiffness Default. 1-point (TAX3F), 3-point (TAX6F), 2x2 (QAX4F, QAX8F)
Fine (see Options). 3x3 (QAX8F), 3-point (TAX3F)
Mass Default.
1-point (TAX3F), 3-point (TAX6F), 2x2 (QAX4F, QAX8F)
Fine (see Options). 3x3 (QAX8F), 3-point (TAX3F)

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule.
47 X -axis taken as axis of symmetry.
55 Output strains as well as stresses.
102 Switch off load correction stiffness matrix due to centripetal acceleration.
105 Lumped mass matrix.
202 Apply concentrated loads in cylindrical coordinates.

## Notes on Use

1. CBF loads are always applied as acceleration loading. Xo, Yo, Zo, permit a shift in the original point of the global coordinate system (about which the rotations are applied). $\mathrm{d} \theta / \mathrm{dt}$ is the local angular velocity about the finite element coordinate system.
2. The application of the CBF loading depends on the particular element material model selected. See the description of Fourier analysis in Chapter 2 of the LUSAS User Guide.
3. If CBF loads are used the structure must be axisymmetric about the X-axis (option 47).
4. Fourier elements cannot be mixed with other element types.
5. Temperature fields cannot be used in dynamic or harmonic response analyses.
6. Centripetal load stiffening has been applied to the $\mathrm{n}=0$ term, but there is no nonlinear stress stiffening contribution. The centripetal load stiffening matrix, contrary, to its name, actually decreases the stiffness of the structure. Centripetal forces are proportional to the angular rotation squared and the lever arm of the mass from the centre of rotation. As the body spins, the lever arm is lengthened by positive displacements, which increases the applied load. This may, conversely, be thought of as reducing the stiffness. The centripetal load stiffness is applied by default, but is may be omitted by setting option 102.
7. The maximum and minimum principal stress computations for axisymmetric elements do not include the $\sigma z$ term as this is implicitly a principal stress in a biaxial stress field.

## Restrictions

Ensure mid-side node centrality
$\square$ Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio

## Recommendations on Use

- The element is designed to model fairly solid structures, but it also performs well in comparison to standard shell analyses and may be an effective alternative for axisymmetric problems. The QAX8F is the most effective element of the family.
- If eigenvalues are required from a thin shelled structure such as a cylinder, the Fourier elements provide an efficient means of checking a range of circumferential harmonics and will indicate the permissible coarseness of a finite element mesh which will adequately represent the 3D variation.


## Chapter 4 : 3D Continuum Elements.

## 3D Solid Continuum Elements

## General



TH10


PN12


PN15


HX8


HX16


HX20


## Element Group 3D Continuum

## Element

Solid Continuum
Subgroup
Element A family of 3D isoparametric solid continuum elements with higher order Description

Number Of Nodes

Freedoms
Node
Coordinates
numerically integrated.

4 or 10 (tetrahedra). 6,12 or 15 (pentahedra). 8,16 or 20 (hexahedra).
The elements are numbered according to a right-hand screw rule in the local z-direction.
$\mathrm{U}, \mathrm{V}, \mathrm{W}$ : at each node.
$\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.

## Geometric Properties

Not applicable.

## Material Properties

Linear Isotropic:
Orthotropic: MATERIAL PROPERTIES ORTHOTROPIC SOLID (Elastic: Orthotropic Solid)
Anisotropic: MATERIAL PROPERTIES ANISOTROPIC SOLID (Elastic: Anisotropic Solid)
Rigidities. Not applicable.
Matrix Not applicable.
Joint Not applicable.

## Concrete

Elasto-Plastic Stress
resultant:
Tresca: MATERIAL PROPERTIES NONLINEAR 61
(Elastic: Isotropic, Plastic: Tresca, Hardening:
Isotropic Hardening Gradient, Isotropic Plastic
Strain or Isotropic Total Strain)
Drucker- MATERIAL PROPERTIES NONLINEAR 64
Prager: (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
Mohr- MATERIAL PROPERTIES NONLINEAR 65
Coulomb: (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)


Ko Initialisation Applicable

## Elasto- Plastic

 InterfaceRubber Not
applicable.
Generic Polymer Isotropic

Composite Not applicable

MATERIAL PROPERTIES NONLINEAR 26

MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)

## Loading

Prescribed Value
PDSP, TPDSP Concentrated CL Loads Element Loads Not applicable.
Distributed Loads UDL FLD

FLDG

Body Forces CBF

BFP, BFPE

Velocities VELO
Accelerations ACCE
Initial SSI, SSIE
Stress/Strains

SSIG

Residual Stresses SSR, SSRE

SSRG

Prescribed variable. U, V, W: at each node.
Concentrated loads. Px, Py, Pz: at each node.

Not applicable.
Face Loads. Px, Py, Pz: local face pressures at nodes.

Global Face Loads. $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z$ at nodes
Constant body forces for element. Xcbf, Ycbf, Zcbf, $\Omega \mathrm{x}, \Omega_{\mathrm{y}}, \Omega_{\mathrm{z}}, \alpha \mathrm{x}, \alpha \mathrm{y}, \alpha \mathrm{z}$
Body force potentials at nodes/for element. $0,0,0$, $\varphi_{4}$, Xcbf, Ycbf, Zcbf
Velocities. Vx, Vy, Vz: at nodes.
Acceleration Ax, Ay, Az: at nodes.
Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma z, \sigma x y, \sigma y z, \sigma x z:$ global stresses. $\varepsilon x, \varepsilon y, \varepsilon z$, $\gamma_{\mathrm{xy}}, \gamma \mathrm{yz}, \gamma_{\mathrm{xz}}$ : global strains.
Initial stresses/strains at Gauss points $\sigma x, \sigma y, \sigma z$, $\sigma x y, \sigma y z, \sigma x z:$ global stresses. $\varepsilon x, \varepsilon y, \varepsilon z, \gamma x y$, $\gamma \mathrm{yz}, \gamma \mathrm{xz}$ : global strains.
Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma z$, $\sigma x y, \sigma y z, \sigma x z:$ global stresses.
Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma z, \sigma x y$, $\sigma y z, \sigma x z$ global stresses.
Target TSSIE, TSSIA Target stresses/strains at nodes/for element. $\sigma x, \sigma y$,

Stress/Strains

TSSIG

Temperatures TEMP, TMPE
$\begin{aligned} \text { Overburden } & \text { Applicable. } \\ \text { Fieatic Surface } & \text { Applicable. } \\ \text { Loads } & \text { Not applicable. } \\ \text { Dependent } & \text { Not applicable. }\end{aligned}$
$\begin{array}{rll}\text { Overburden } & \text { Applicable. } \\ \text { Phreatic Surface } & \text { Applicable. } \\ \text { Field Loads } & \text { Not applicable. } \\ \text { Temp Dependent } & \text { Not applicable. }\end{array}$
$\begin{aligned} \text { Overburden } & \text { Applicable. } \\ \text { Fieatic Surface } & \text { Applicable. } \\ \text { Loads } & \text { Not applicable. } \\ \text { Dependent } & \text { Not applicable. }\end{aligned}$
$\begin{array}{rll}\text { Overburden } & \text { Applicable. } \\ \text { Phreatic Surface } & \text { Applicable. } \\ \text { Field Loads } & \text { Not applicable. } \\ \text { Temp Dependent } & \text { Not applicable. }\end{array}$
Loads
$\sigma z, \sigma x y, \sigma y z, \sigma x z:$ global stresses. $\varepsilon x, \varepsilon y, \varepsilon z$, $\gamma \mathrm{xy}, \gamma \mathrm{yz}, \gamma \mathrm{xz}$ : global strains.
Target stresses/strains at Gauss points $\sigma x, \sigma y, \sigma z$, $\sigma x y, \sigma y z, \sigma x z:$ global stresses. $\varepsilon x, \varepsilon y, \varepsilon z, \gamma x y$, $\gamma \mathrm{yz}, \gamma \mathrm{xz}$ : global strains.
Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}, 0$, 0,0

## LUSAS Output

Solver
Stress (default): $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z, \sigma e:$ global stresses.
Strain: $\varepsilon x, \varepsilon y, \varepsilon z, \gamma \mathrm{xy}, \gamma \mathrm{yz}, \gamma \mathrm{xz}, \varepsilon_{\mathrm{e}}$ global strains.
For optional principal stress/strain output, together with the corresponding direction cosines, use Option 77.
Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

- Standard 3D continuum element


## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements and large rotations.
Updated For large displacements and large rotations.

## Lagrangian

Eulerian For large displacements, large rotations and moderately large strains.

## Co-rotational For large displacements and large rotations.

## Integration Schemes

| Stiffness | Default. | 1-point (TH4), 4-point (TH10), 3x2 (PN6, PN12, <br> PN15), 2x2x2 (HX8, HX16, HX20) |
| :---: | :--- | :--- |
|  | Fine (see <br> Options). <br> Coarse (see <br> Options) | 5-point (TH10), 3x3x2 (HX16), 3x3x3 (HX20) |
| Mass | 13-point (HX20), 14-point (HX20) |  |
| Default. | 1-point (TH4), 4-point (TH10), 3x2 (PN6, PN12, |  |
|  | PN15), 2x2x2 (HX8, HX16, HX20) |  |
|  | Fine (see | 4-point (TH4) 11-point (TH10), 14-point (TH10) |
| Options). | 3x3x2 (HX16), 3x3x3 (HX20) |  |
| Coarse (see | 13-point (HX20), 14-point (HX20) |  |
| Options) |  |  |

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule.
36 Follower loads
54 Updated Lagrangian geometric nonlinearity
55 Output strains as well as stresses.
77 Output principal stresses and direction cosines.
87 Total Lagrangian geometric nonlinearity.
91 Invoke finer integration of the mass matrix.
102 Switch off load correction stiffness due to centripetal acceleration.
105 Lumped mass matrix.
139 Output yielded Gauss points only.
155 Use 14-point integration rule for HX20.
156 Use 13-point integration rule for HX20.
167 Eulerian geometric nonlinearity.
229 Co-rotational geometric nonlinearity.
395 Use 14-point integration rule for mass matrix of TH10 (used together with Option 91).

398 For HX20 and HX16 with fine integration use all integration points for stress extrapolation.

## Notes on Use

1. The elements are based on the standard isoparametric approach. The variation of stresses within an element may be regarded as constant for the lower order elements (corner nodes only), and linear for the higher order elements (with mid-side nodes).
2. All elements pass the patch test.
3. When using table input format for temperature dependent ORTHOTROPIC SOLID or ANISOTROPIC SOLID material properties, the value of nset used is that defined in the first line of the property table.
4. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility.

## Restrictions

Ensure mid-side node centrality
A Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio

## Recommendations on Use

- The 3D solid elements should be used if the stress field is fully 3D, i.e. it cannot be approximated with any of the 2D elements, e.g. as for a non-axisymmetric pressure vessel.
- For linear materials, the 20 -noded element with a $2 * 2 * 2$ Gauss rule is usually the most effective element, as this under-integration of the stiffness matrix prevents locking, i.e. over-stiff solutions will occur if the elements are used with a $3 * 3 * 3$ Gauss integration rule to model structures subjected to bending. However, the element possesses six zero energy modes. Therefore, a careful examination of the solution should be performed to check for spurious stress oscillations and peculiarities in the deformed configuration. Either the 14 -point or $3 * 3 * 3$ Gauss rules should be used for materially nonlinear problems or materially linear problems that exhibit spurious deformations.
- The 8-noded element should not be used for analyses where bending effects are significant as the element tends to lock in parasitic shear [C1]. The 8 -noded element will perform poorly if it is highly distorted. The 4-noded tetrahedron TH4 element is generally not effective and should only be used if the geometry requires elements of this shape.


## 3D Solid Continuum Element with Enhanced Strains

## General

Element Name
HX8M



## Element Group 3D Continuum

## Element <br> Solid Continuum

Subgroup
Element
Description
A 3D isoparametric solid element with an incompatible strain field. This mixed assumed strain element demonstrates a much superior performance to that of the HX8 element.
Number Of 8 . The element is numbered according to a right-hand screw rule in the
Nodes local z-direction.
Freedoms U, V, W: at each node.
Node $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.
Coordinates

## Geometric Properties

Not applicable.

## Material Properties

| Linear | Isotropic: | MATERIAL PROPERTIES (Elastic: Isotropic) |
| :--- | :--- | :--- |
|  | Orthotropic: | MATERIAL PROPERTIES ORTHOTROPIC SOLID |
|  |  | (Elastic: Orthotropic Solid) |
|  | Anisotropic: | MATERIAL PROPERTIES ANISOTROPIC SOLID <br> (Elastic: Anisotropic Solid) |
|  | Rigidities. | Not applicable. |
| Matrix | Not <br> applicable. |  |
|  |  |  |

Joint Not applicable.

## Concrete

Elasto-Plastic Stress resultant: Tresca:

DruckerPrager:

MohrCoulomb:

Modified MohrCoulomb:

Modified
Cam-clay
Optimised Implicit Von Mises:
Volumetric
Crushing:
Stress Potential

Creep AASHTO

CEB-FIP

MATERIAL PROPERTIES NONLINEAR 105
(Elastic: Isotropic, Plastic: Transient Smoothed MultiCrack Concrete)
MATERIAL PROPERTIES NONLINEAR 109
(Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Not applicable.
MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
MATERIAL PROPERTIES NONLINEAR 64
(Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
MATERIAL PROPERTIES NONLINEAR 65
(Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
MATERIAL PROPERTIES MODIFIED MOHR_COULOMB (Elastic: Isotropic, Plastic: Mohr-Coulomb/Tresca, nonassociative Hardening with tension/compression cut-off)
MATERIAL PROPERTIES CAM_CLAY MODIFIED (Elastic: Isotropic, Plastic)
MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic)
MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam)
STRESS POTENTIAL VON_MISES, HILL, HOFFMAN
(Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)

MATERIAL PROPERTIES NONLINEAR 86 AASHTO
(Concrete creep model to AASHTO code of Practice)

MATERIAL PROPERTIES NONLINEAR 86 CEBFIP
(Concrete creep model to CEB-FIP Model Code
1990)
Chinese
EurocodeDamageViscoelastic
Shrinkage
Ko Initialisation Applicable Rubber Ogden:
IRC MATERIAL PROPERTIES NONLINEAR 86 IRC
MATERIAL PROPERTIES NONLINEAR 86CHINESE(Chinese creep model to Chinese Code of Practice)
MATERIAL PROPERTIES NONLINEAR 86 EUROCODE
(Concrete creep model to EUROCODE_2)(Concrete creep model to Indian IRC code ofPractice)
DAMAGE PROPERTIES SIMO, OLIVER (Damage)
VISCO ELASTIC PROPERTIES
SHRINKAGE CEB_FIP_90, EUROCODE_2,GENERAL, USER
MATERIAL PROPERTIES RUBBER OGDEN(Rubber: Ogden)
Mooney- MATERIAL PROPERTIES RUBBER
Rivlin: MOONEY_RIVLIN (Rubber: Mooney-Rivlin)Neo-Hookean: MATERIAL PROPERTIES RUBBERNEO_HOOKEAN (Rubber: Neo-Hookean)
Hencky: MATERIAL PROPERTIES RUBBER HENCKY(Rubber: Hencky)
MATERIAL PROPERTIES NONLINEAR 89(Generic Polymer Model)
Composite Not

## Loading

Prescribed Value PDSP, TPDSP
Concentrated CL Loads Element Loads Not applicable.
Distributed Loads UDL
FLD

FLDG

Body Forces CBF

Prescribed variable. U, V, W: at each node. Concentrated loads. Px, Py, Pz: at each node.

Not applicable.
Face Loads. Px, Py, Pz: local face pressures at nodes.

Global Face Loads. $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z$ at nodes
Constant body forces for element. Xcbf, Ycbf, Zcbf,

|  |  | $\Omega_{\mathrm{x}}, \Omega_{\mathrm{y}}, \Omega_{\mathrm{z}}, \alpha_{\mathrm{x}}, \alpha_{\mathrm{y}}, \alpha_{\mathrm{z}}$ |
| :---: | :---: | :---: |
|  | BFP, BFPE | Body force potentials at nodes/for element. $0,0,0$, $\varphi_{4}, \mathrm{Xcbf}, \mathrm{Ycbf}, \mathrm{Zcbf}$ |
| Velocities | VELO | Velocities. Vx, Vy, Vz: at nodes. |
| Accelerations | ACCE | Acceleration Ax, Ay, Az: at nodes. |
| Initial <br> Stress/Strains | SSI, SSIE | Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma \mathrm{z}, \sigma \mathrm{xy}, \sigma \mathrm{yz}, \sigma \mathrm{xz}:$ global stresses. $\varepsilon \mathrm{x}, \varepsilon \mathrm{y}, \varepsilon \mathrm{z}$, $\gamma \mathrm{xy}, \gamma \mathrm{yz}, \gamma \mathrm{xz}$ : global strains. |
|  | SSIG | Initial stresses/strains at Gauss points $\sigma x, \sigma y, \sigma z$, $\sigma x y, \sigma y z, \sigma x z:$ global stresses. $\varepsilon x, \varepsilon y, \varepsilon z, \gamma x y$, $\gamma \mathrm{yz}, \gamma \mathrm{xz}$ : global strains. |
| Residual Stresses | SSR, SSRE | Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma z$, $\sigma x y, \sigma y z, \sigma x z:$ global stresses. |
|  | SSRG | Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma z, \sigma x y$, $\sigma y z, \sigma x z$ global stresses. |
| Target Stress/Strains | TSSIE, TSSIA | Target stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma \mathrm{z}, \sigma \mathrm{xy}, \sigma \mathrm{yz}, \sigma \mathrm{xz}:$ global stresses. $\varepsilon \mathrm{x}, \varepsilon \mathrm{y}, \varepsilon \mathrm{z}$, $\gamma \mathrm{xy}, \gamma \mathrm{yz}, \gamma \mathrm{xz}$ : global strains. |
|  | TSSIG | Target stresses/strains at Gauss points $\sigma x, \sigma y, \sigma z$, $\sigma x y, \sigma y z, \sigma x z:$ global stresses. $\varepsilon x, \varepsilon y, \varepsilon z, \gamma x y$, $\gamma \mathrm{yz}, \gamma \mathrm{xz}$ : global strains. |
| Temperatures | TEMP, TMPE | Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}, 0$, 0,0 |
| Overburden | Applicable. |  |
| Phreatic Surface | Applicable. |  |
| Field Loads | Not applicable. |  |
| Temp Dependent Loads | Not applicable. |  |

## LUSAS Output

Solver Stress (default): $\sigma \mathrm{x}, \sigma \mathrm{y}, \sigma \mathrm{z}, \sigma \mathrm{xy}, \sigma \mathrm{yz}, \sigma \mathrm{xz}, \sigma \mathrm{e}$ : global stresses.
Strain: $\varepsilon x, \varepsilon y, \varepsilon z, \gamma \mathrm{xy}, \gamma_{\mathrm{yz}}, \gamma_{\mathrm{xz}}, \varepsilon_{\mathrm{e}}$ global strains.
Stretch (for rubber only): $\mathrm{V}_{11}, \mathrm{~V}_{22}, \mathrm{~V}_{33}, \mathrm{~V}_{12}, \mathrm{~V}_{23}, \mathrm{~V}_{13}, \lambda_{1}, \lambda_{2}, \lambda_{3}, \operatorname{det} \mathrm{~F}$.

Where $\mathrm{V}_{\mathrm{ii}}$ are components of the left stretch tensors, $\lambda_{\mathrm{i}}$ the principal stretches, $\theta \lambda$ the angle between the maximum principal stretch and the global X axis, and $\operatorname{det} \mathrm{F}$ the determinant of the deformation gradient or volume ratio.

For optional principal stress/strain output, together with the corresponding direction cosines, use Option 77.

Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

- Standard 3D continuum element


## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements and large rotations.
Updated For large displacements and large rotations.
Lagrangian
Eulerian For large displacements, large rotations and moderately large strains.
Co-rotational For large displacements and large rotations (large strains with the rubber material model).

## Integration Schemes

| Stiffness | Default. <br>  <br> Mass | $2 \times 2 \times 2$ |
| :---: | :--- | :--- |
|  | Fine. | As default. |
|  | Dine. | $2 \times 2 \times 2$ |
|  | As default. |  |

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

39 Stress smoothing for rubber material models.
54 Updated Lagrangian geometric nonlinearity.
55 Output strains as well as stresses.
77 Output principal stresses and direction cosines.
87 Total Lagrangian geometric nonlinearity.
102 Switch off load correction stiffness due to centripetal acceleration.
105 Lumped mass matrix.
139 Output yielded Gauss points only.
167 Eulerian geometric nonlinearity.
225 Use alternative number of parameters for enhanced strain interpolation (see Notes).
229 Co-rotational geometric nonlinearity.

## Notes on Use

1. The element is based on the standard isoparametric approach. The variation of stresses within an element may be regarded as linear.
2. The strain field for this element consists of two parts: the compatible strains derived from the assumed displacement field and the assumed enhanced strains; see LUSAS Theory Manual. By default, 18 parameters are used to define the assumed enhanced strain. In general, the default number of parameters should be used. However, 9 parameters may be specified using Option 225. In most cases the use of 9 or 18 parameters will give an equivalent solution. However, in some instances a better response may be obtained using more parameters at the expense of increased computation time.
3. The element passes the patch test and the large strain patch test for rubber.
4. When using table input format for temperature dependent ORTHOTROPIC SOLID or ANISOTROPIC SOLID material properties, the value of nset used is that defined in the first line of the property table.
5. Non-conservative (follower) loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility. The load does not have to be normal to the face and may also vary over the face.
6. To apply a non-conservative (follower) pressure load (load type FLD) with corotational geometric nonlinearity, Option 36 must be specified. Note that this load must be normal to the face and constant for all the nodes of the element face.
7. The converged stresses for the rubber material model are Kirchhoff stresses (see LUSAS Theory Manual).
8. Option 39 is used to smooth the stress output. It is particularly useful when the rubber material model is applied and the element is under very high compression where oscillatory stresses may appear (checker-board pattern).
9. For the rubber material model, converged values for strain output are replaced by the left stretch tensor V, the principal stretches of the vectors defining these principal directions. The principal stretches and directions can be obtained using Option 77. The value of $\operatorname{det} \mathrm{F}=\lambda_{1} \lambda_{2} \lambda_{3}$ (the volume ratio) is only available for Gauss point output.
10. For the rubber material model, the iterative values of stress and strain are output in local co-rotated directions at the Gauss points only.
11. Convergence difficulties can sometimes arise when using enhanced strain elements with nonlinear materials, particularly if the material is elastic-perfectly plastic or if a very shallow hardening curve is defined. In such cases it is recommended that the standard element formulation is used.

## Restrictions

Avoid excessive aspect ratio
Rubber material models can only be applied in conjunction with the co-rotational formulation, Option 229.

## Recommendations on Use

This element exhibits an improved performance when compared with the parent element HX8. The integration rules are the same as the parent element. The HX8M element does not suffer from locking due to parasitic shear or when the material approaches the incompressible limit. No zero energy modes exist for this element.

## 3D Solid Continuum Crack Tip Elements

## General



Crack specified at Node 1

## PN15K



Crack specified at Node 1
HX20K


Crack specified at Node 1


Crack specified along edge 1-2-3


Crack specified along edge 1-2-3


Crack specified along edge 1-2-3

## Element Group 3D Continuum

Element
Solid Continuum
Subgroup
Element A family of 3D isoparametric crack tip elements where the crack tip can Description be located at any corner node or along any edge of an element. The mid-
side nodes are moved to the quarter points to produce a singularity at the crack tip. The strains vary as the square root of $1 / R$, where $R$ is the distance from the crack tip. These elements are used at the crack tip only. The elements are numerically integrated.
Number Of
10 (tetrahedra). 15 (pentahedra). 20 (hexahedra). The elements are
Nodes
numbered according to a right-hand screw rule in the local z-direction.
Freedoms U, V, W: at each node.
Node X, Y, Z: at each node.
Coordinates

## Geometric Properties

Not applicable.

## Material Properties

| Linear | Isotropic: <br> Orthotropic: | MATERIAL PROPERTIES (Elastic: Isotropic) <br> MATERIAL PROPERTIES ORTHOTROPIC SOLID <br> (Elastic: Orthotropic Solid) |
| :---: | :--- | :--- |
|  | Anisotropic: | MATERIAL PROPERTIES ANISOTROPIC SOLID <br> (Elastic: Anisotropic Solid) |
|  | Rigidities. | Not applicable. |



Ko Initialisation Elasto- Plastic Interface

Applicable

MODIFIED MOHR_COULOMB (Elastic: Isotropic, Plastic: Mohr-Coulomb/Tresca, nonassociative Hardening with tension/compression cut-off)
MATERIAL PROPERTIES CAM_CLAY MODIFIED (Elastic: Isotropic, Plastic) MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic)
MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam)
STRESS POTENTIAL VON_MISES, HILL, HOFFMAN
(Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
CREEP PROPERTIES (Creep)
MATERIAL PROPERTIES NONLINEAR 86 AASHTO
(Concrete creep model to AASHTO code of Practice)

## MATERIAL PROPERTIES NONLINEAR 86 CEB-

 FIP(Concrete creep model to CEB-FIP Model Code 1990)

MATERIAL PROPERTIES NONLINEAR 86 CHINESE
(Chinese creep model to Chinese Code of Practice)
MATERIAL PROPERTIES NONLINEAR 86 EUROCODE
(Concrete creep model to EUROCODE_2)
MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
DAMAGE PROPERTIES SIMO, OLIVER (Damage)
VISCO ELASTIC PROPERTIES

SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER

MATERIAL PROPERTIES NONLINEAR 26

# Rubber Not <br> applicable. 

Generic Polymer Isotropic
MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)

Composite Not applicable

## Loading

Prescribed Value PDSP, TPDSP Concentrated CL Loads Element Loads Not applicable.
Distributed Loads UDL
FLD

FLDG

Body Forces CBF

BFP, BFPE

Velocities VELO
Accelerations ACCE
Initial SSI, SSIE Stress/Strains

SSIG

Residual Stresses SSR, SSRE

SSRG

Target TSSIE, TSSIA Stress/Strains

Prescribed variable. U, V, W: at each node.
Concentrated loads. Px, Py, Pz: at each node.

Not applicable.
Face Loads. Px, Py, Pz: local face pressures at nodes.

Global Face Loads. $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z$ at nodes
Constant body forces for element. Xcbf, Ycbf, Zcbf, $\Omega_{\mathrm{x}}, \Omega_{\mathrm{y}}, \Omega_{\mathrm{z}}, \alpha \mathrm{x}, \alpha \mathrm{y}, \alpha \mathrm{z}$
Body force potentials at nodes/for element. 0, 0, 0, $\varphi_{4}$, Xcbf, Ycbf, Zcbf
Velocities. Vx, Vy, Vz: at nodes.
Acceleration Ax, Ay, Az: at nodes.
Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma z, \sigma x y, \sigma y z, \sigma x z: ~ g l o b a l ~ s t r e s s e s . ~ \varepsilon x, ~ \varepsilon y, ~ \varepsilon z, ~$ $\gamma \mathrm{xy}, \gamma \mathrm{yz}, \gamma \mathrm{xz}$ : global strains.

Initial stresses/strains at Gauss points $\sigma x, \sigma y, \sigma z$, $\sigma x y, \sigma y z, \sigma x z:$ global stresses. $\varepsilon x, \varepsilon y, \varepsilon z, \gamma x y$, $\gamma \mathrm{yz}, \gamma \mathrm{xz}$ : global strains.
Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma z$, $\sigma x y, \sigma y z, \sigma x z:$ global stresses.

Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma z, \sigma x y$, $\sigma y z, \sigma x z$ global stresses.
Target stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma z, \sigma x y, \sigma y z, \sigma x z:$ global stresses. $\varepsilon x, \varepsilon y, \varepsilon z$,


## LUSAS Output

Solver Stress (default): $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z, \sigma e:$ global stresses.
Strain: $\varepsilon x, \varepsilon y, \varepsilon z, \gamma x y, \gamma y z, \gamma x z, \varepsilon e$ : global strains.
For optional principal stress/strain output, together with the corresponding direction cosines, use Option 77.
Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

Standard 3D continuum element

## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements and large rotations.
Updated For large displacements and large rotations.
Lagrangian
Eulerian For large displacements, large rotations and moderately large strains.
Co-rotational For large displacements and large rotations.

## Integration Schemes

| Stiffness | Default. | 4-point (TH10K), 6x3 (PN15K), 3x3x3 <br> (HX20K) |
| :---: | :--- | :--- |
|  | Fine (see Options). | 11-point (TH10K), 12×4 (HX15K) |
| Mass | Default. | 4-point (TH10K), $6 \times 3$ (PN15K), $3 \times 3 \times 3$ <br> (HX20K) |
|  | Fine (see Options). | 11-point (TH10K), 14-point (TH10K), 12×4 <br> (HX15K) |

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule.
36 Follower loads
54 Updated Lagrangian geometric nonlinearity
55 Output strains as well as stresses.
77 Output principal stresses and direction cosines.
87 Total Lagrangian geometric nonlinearity.
91 Invoke finer integration of the mass matrix.
102 Switch off load correction stiffness due to centripetal acceleration.
105 Lumped mass matrix.
139 Output yielded Gauss points only.
167 Eulerian geometric nonlinearity.
229 Co-rotational geometric nonlinearity.
395 Use 14-point integration rule for mass matrix of TH10 (used together with Option 91).
398 For HX20 and HX16 with fine integration use all integration points for stress extrapolation.

## Notes on Use

1. The elements are based on the standard isoparametric approach. Moving the mid-side nodes to the quarter points creates a singularity with theoretically infinite stress at the crack tip.
2. When using table input format for temperature dependent ORTHOTROPIC SOLID or ANISOTROPIC SOLID material properties, the value of nset used is that defined in the first line of the property table.
3. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility.

## Restrictions

- Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio


## Recommendations on Use

- The 3D solid crack tip elements should be used if the stress field is fully 3D, i.e. it cannot be approximated with any of the 2D crack tip elements.
- Elements TH10K, PN15K and HX20K are specifically designed for application to fracture mechanics problems and may be used to model the singularities that occur at the crack tip. The mid-side nodes near the crack tip are shifted to the quarter point. This ensures a singularity is present at the crack tip and that strains vary as 1 over the square root of $r$ - where $r$ is the distance from the crack tip.


## 3D Solid Continuum Composite Elements (Tetrahedral)

## General

Element Name
TH10S



## Element Group 3D Continuum

Element Solid Continuum
Subgroup
Element
Description
A 3D tetrahedral element capable of modelling curved boundaries. The element can be arbitrarily oriented with respect to the laminate and allows for the fully automatic mesh generation of laminate geometric models imported from CAD packages.
Number Of 10. The element is numbered according to a right-hand screw rule in the Nodes local z-direction.
Freedoms U, V, W: at each node.
Node $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.

|  | applicable. |  |
| :---: | :---: | :---: |
| Joint | Not applicable. |  |
| Concrete |  | MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete) |
| Elasto-Plastic | Stress resultant: | Not applicable. |
|  | Tresca: | MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain) |
|  | DruckerPrager: | MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular) |
|  | Mohr- <br> Coulomb: | MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation) |
|  | Modified | MATERIAL PROPERTIES |
|  | Mohr- <br> Coulomb: | MODIFIED MOHR_COULOMB (Elastic: Isotropic, Plastic: Mohr-Coulomb/Tresca, nonassociative Hardening with tension/compression cut-off) |
|  | Volumetric Crushing: | Not applicable. |
|  | Stress <br> Potential | STRESS POTENTIAL VON_MISES, HILL, HOFFMAN <br> (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman) |
| Creep | AASHTO | MATERIAL PROPERTIES NONLINEAR 86 AASHTO <br> (Concrete creep model to AASHTO code of Practice) |
|  | CEB-FIP | MATERIAL PROPERTIES NONLINEAR 86 CEB- <br> FIP <br> (Concrete creep model to CEB-FIP Model Code 1990) |
|  | Chinese | MATERIAL PROPERTIES NONLINEAR 86 CHINESE <br> (Chinese creep model to Chinese Code of Practice) |
|  | Eurocode | MATERIAL PROPERTIES NONLINEAR 86 |

EUROCODE(Concrete creep model to EUROCODE_2)
Damage
Viscoelastic
Shrinkage
IRC
Ko Initialisation Not applicable
Rubber Not
applicable.
Generic PolymerResin CureModelComposite Compositesolid:

MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)MATERIAL PROPERTIES NONLINEAR CURELAYER, FIBRE_RESINCOMPOSITE PROPERTIES (Elastic: OrthotropicSolid)

## Loading

Prescribed Value PDSP, TPDSP Concentrated Loads Element Loads Not applicable.
Distributed Loads
UDL
FLD

FLDG

Body Forces CBF

BFP, BFPE Body force potentials at nodes/for element. 0, 0, 0, $\varphi_{4}$, Xcbf, Ycbf, Zcbf
Velocities. Vx, Vy, Vz: at nodes.
Acceleration Ax, Ay, Az: at nodes.
Initial stresses/strains at nodes/for element.
$\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z:$ global stresses.
$\varepsilon x, \varepsilon y, \varepsilon z, \gamma x y, \gamma y z, \gamma x z:$ global strains.

SSIG

Residual Stresses SSR, SSRE

SSRG

Target TSSIE, TSSIA Stress/Strains

TSSIG

Temperatures TEMP, TMPE
Overburden Applicable.
Phreatic Surface Applicable.
Field Loads Not applicable.
Temp Dependent Not applicable. Loads

Initial stresses/strains at Gauss points (see Notes). $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z:$ global stresses. $\varepsilon x, \varepsilon y, \varepsilon z, \gamma x y, \gamma y z, \gamma x z:$ global strains. Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z:$ global stresses. Residual stresses at Gauss points (see Notes). $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z$ global stresses. Target stresses/strains at nodes/for element. $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z:$ global stresses. $\varepsilon x, \varepsilon y, \varepsilon z, \gamma x y, \gamma y z, \gamma x z:$ global strains. Target stresses/strains at Gauss points (see Notes). $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z:$ global stresses. $\varepsilon x, \varepsilon y, \varepsilon z, \gamma x y, \gamma y z, \gamma x z:$ global strains.
Temperatures at nodes/for element.

$$
\mathrm{T}, 0,0,0, \mathrm{To}, 0,0,0
$$

## LUSAS Output

## Solver

Stress (default): $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z:$ local stresses.
Strain: $\varepsilon x, \varepsilon y, \varepsilon z, \gamma x y, \gamma y z, \gamma x z:$ local strains.
Stresses and strains are output at the Gauss and corner points of the subdivision(s) of each layer. For optional principal stress/strain output, together with the corresponding direction cosines, use Option 77.
Modeller See Results Tables (Appendix K).

## Local Axes

The local axes for each layer are defined by the LAMINAR DIRECTIONS specified for its bottom surface. The three node set in LAMINAR DIRECTIONS define the local Cartesian set origin, the x -axis and the positive quadrant of the xy-plane respectively. The local z -axis forms an orthonormal coordinate system with x and y .

## Sign Convention

$\square$ Standard 3D continuum element

## Formulation

## Geometric Nonlinearity

Total Lagrangian Not applicable.
Updated Not applicable.
Lagrangian
Eulerian Not applicable.
Co-rotational For large displacements and large rotations.

## Integration Schemes

| Stiffness | Default. | 1-point for a tetrahedral subdivision (see Notes), 3-point for a pentahedral/pyramid subdivision, $2 \times 2$ for a hexahedral/wrick subdivision |
| :---: | :---: | :---: |
|  | Fine (see Options). | 1-point for a tetrahedral subdivision (see Notes), $3 \times 2$ for a pentahedral/pyramid subdivision, $2 \times 2 \times 2$ for a hexahedral/wrick subdivision |
| Mass | Default | 5-point for the whole element or (see Options) 1-point for a tetrahedral subdivision, $3 \times 2$ for a pentahedral/pyramid subdivision, $2 \times 2 \times 2$ for a hexahedral/wrick subdivision |
|  | Fine (see Options). | 11-point or (see Options) 14 -point for the whole element |

## Mass Modelling

Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule.
36 Follower loads.
55 Output strains as well as stresses.
77 Output principal stresses and direction cosines.
91 Formulate element mass with fine integration.
105 Lumped mass matrix.
139 Output yielded Gauss points only.

229 Co-rotational geometric nonlinearity.
266 Layer by layer computation of mass matrix.
394 Lamina directions supported.
395 Use 14-point fine integration rule for mass matrix of TH10 family (used together with 91).

## Notes on Use

1. The element is based on the standard isoparametric approach. The variation of strains within an element may be regarded as linear.
2. All elements pass the patch test.
3. The LAMINAR DIRECTIONS and COMPOSITE PROPERTIES data chapters must be used with this element in conjunction with the COMPOSITE ASSIGNMENTS data chapter.
4. The stresses obtained from a geometric nonlinear analysis are Kirchhoff stresses.
5. If the whole tetrahedral element is embedded in a single lamina, a 4-point integration rule will be used for this tetrahedral subdivision; otherwise a 1-point rule will be used.
6. The mass matrix can be computed using a layer by layer integration (OPTION 266), however this should only be used when the densities of the layers vary considerably because the computation time can be greatly increased when this OPTION is specified.
7. Numerical integration through the thickness is performed. The integration points are located in the subdivisions of each layer. Each subdivision forms the shape of a regular 3D solid continuum element and the integration points are located accordingly within the subdivision as described above.
8. SSIG and SSRG loads have to be applied at the Gauss point positions for the subdivision(s) of each layer.
9. Layer 1 is always the bottom layer.

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio


## Recommendations on Use

- 3D solid composite elements should be used for modelling thick composite structures comprising laminae of differing material properties where the computational cost of modelling each lamina with an individual solid element would be prohibitive.
- As these elements can be arbitrarily oriented with respect to the laminate, they are particularly aimed at the use of fully automatic mesh generation of laminate geometric models imported from CAD packages.


## 3D Solid Continuum Composite Elements (Pentahedral and Hexahedral)

## General



HX8L


PN12L


HX16L


## Element Group 3D Continuum

Element Solid Continuum
Subgroup
Element 3D isoparametric pentahedral and hexahedral solid elements with higher Description order models capable of modelling curved boundaries. The element can be used to model a laminate, where lamina planes are defined by the top and bottom surfaces of the element. The elements are numerically integrated.
Number Of 6 or 12 (pentahedra), 8 or 16 (hexahedra). The elements are numbered Nodes according to a right-hand screw rule in the local z-direction.
Freedoms
$\mathrm{U}, \mathrm{V}, \mathrm{W}$ : at each node.

Node $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.
Coordinates

## Geometric Properties

See Composites in the Modeller Reference Manual

## Material Properties

Linear Isotropic.
Orthotropic: MATERIAL PROPERTIES ORTHOTROPIC SOLID (Elastic: Orthotropic Solid)
Anisotropic: MATERIAL PROPERTIES ANISOTROPIC SOLID (Elastic: Anisotropic Solid)
Rigidities. Not applicable.
Matrix Not applicable.
Joint Not applicable.
Concrete

Elasto-Plastic Stress resultant:

Prager:

Mohr-
Coulomb:

Modified
Mohr-
Coulomb:

Volumetric Not applicable.
Crushing: Potential HOFFMAN

Tresca: MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
Drucker- MATERIAL PROPERTIES NONLINEAR 64

Stress STRESS POTENTIAL VON_MISES, HILL,
MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Not applicable.
(Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
MATERIAL PROPERTIES NONLINEAR 65
(Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
MATERIAL PROPERTIES
MODIFIED MOHR_COULOMB (Elastic:
Isotropic, Plastic: Mohr-Coulomb/Tresca, nonassociative Hardening with tension/compression cut-off)

| Creep | AASHTO | (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman) |
| :---: | :---: | :---: |
|  |  | MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of Practice) |
|  | CEB-FIP | MATERIAL PROPERTIES NONLINEAR 86 CEB- <br> FIP <br> (Concrete creep model to CEB-FIP Model Code 1990) |
|  | Chinese | MATERIAL PROPERTIES NONLINEAR 86 CHINESE <br> (Chinese creep model to Chinese Code of Practice) |
|  | Eurocode | MATERIAL PROPERTIES NONLINEAR 86 EUROCODE <br> (Concrete creep model to EUROCODE_2) |
|  | IRC | MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice) |
| Damage |  | DAMAGE PROPERTIES SIMO, OLIVER (Damage) |
| Viscoelastic |  | VISCO ELASTIC PROPERTIES |
| Shrinkage |  | SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER |
| Ko Initialisation Rubber | Not applicable Not applicable. |  |
| Generic Polymer |  | MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model) |
| Resin Cure <br> Model |  | MATERIAL PROPERTIES NONLINEAR CURE LAYER, FIBRE_RESIN |
| Composite | Composite solid: | COMPOSITE PROPERTIES (Elastic: Orthotropic Solid) |

## Loading

| Prescribed Value | PDSP, TPDSP |
| ---: | :--- |
| Concentrated | PL |
| Loads |  |
| Concentrated loads. Px, Py, Pz: at each node. |  |

Element Loads Not applicable.

| Distributed Loads | UDL | Not applicable. |
| :---: | :---: | :---: |
|  | FLD | Face Loads. Px, Py, Pz: local face pressures at nodes. |
|  | FLDG | Global Face Loads. $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z$ at nodes |
| Body Forces | CBF | Constant body forces for element. Xcbf, Ycbf, Zcbf, $\Omega_{\mathrm{x}}, \Omega_{\mathrm{y}}, \Omega_{\mathrm{z},} \alpha_{\mathrm{x}}, \alpha_{\mathrm{y}}, \alpha_{\mathrm{z}}$ |
|  | BFP, BFPE | Body force potentials at nodes/for element. $0,0,0$, $\varphi_{4}$, Xcbf, Ycbf, Zcbf |
| Velocities | VELO | Velocities. Vx, Vy, Vz: at nodes. |
| Accelerations | ACCE | Acceleration Ax, Ay, Az: at nodes. |
| Initial | SSI, SSIE | Initial stresses/strains at nodes/for element. |
| Stress/Strains |  | $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z:$ global stresses. <br> $\varepsilon x, \varepsilon y, \varepsilon z, \gamma_{\mathrm{xy}}, \gamma_{\mathrm{yz}}, \gamma_{\mathrm{xz}}$ : global strains. |
|  | SSIG | Initial stresses/strains at Gauss points (see Notes). $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z:$ global stresses. |
|  |  | $\varepsilon x, \varepsilon y, \varepsilon z, \gamma \mathrm{xy}, \gamma \mathrm{yz}, \gamma_{\mathrm{xz}}$ : global strains. |
| Residual Stresses | SSR, SSRE | Residual stresses at nodes/for element. |
|  | SSRG | $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z:$ global stresses. Residual stresses at Gauss points (see Notes). |
|  |  | $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z$ global stresses. Target stresses/strains at nodes/for element. |
| Target Stress/Strains | TSSIE, TSSIA | Target stresses/strains at nodes/for element. $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z:$ global stresses. |
|  |  | $\varepsilon x, \varepsilon y, \varepsilon z, \gamma \mathrm{xy}, \gamma_{\mathrm{yz}}, \gamma \mathrm{xz}$ : global strains. |
|  | TSSIG | Target stresses/strains at Gauss points (see Notes). |
|  |  | $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z:$ global stresses. |
|  |  | $\varepsilon x, \varepsilon y, \varepsilon z, \gamma x y, \gamma y z, \gamma x z:$ global strains. |
| Temperatures | TEMP, TMPE | Temperatures at nodes/for element. T, $0,0,0$, To, $0,0,0$ |
| Overburden | Applicable. |  |
| Phreatic Surface | Applicable. |  |
| Field Loads | Not applicable. |  |
| Temp Dependent | Not applicable. |  |

## LUSAS Output

$$
\begin{aligned}
& \text { Solver } \text { Stress (default): } \sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z: \text { local stresses. } \\
& \text { Strain: } \varepsilon x, \varepsilon y, \varepsilon z, \gamma x y, \gamma y z, \gamma x z: \text { local strains. } \\
& \text { Stresses and strains are output at the top and bottom of each layer. For } \\
& \text { optional principal stress/strain output, together with the corresponding } \\
& \text { direction cosines, use Option } 77 .
\end{aligned}
$$

## Local Axes

The local axes for each layer are defined using the convention for standard area elements. Local axes are computed at the top and bottom surfaces (at the Gauss points) and average values are interpolated for the mid-surface. The top and bottom faces of the element are as shown, e.g. nodes 1, 2, 3, 4 define the bottom face of HX8L. Every layer uses the same averaged values.

## Sign Convention

$\square$ Standard 3D continuum element

## Formulation

## Geometric Nonlinearity

## Total Lagrangian

Updated
Lagrangian
Eulerian
Co-rotational

Not applicable.
Not applicable.
Not applicable.
For large displacements and large rotations.

## Integration Schemes

Stiffness Default. 1-point for each layer (PN6L), 3-point for each layer (PN12L), 2x2 for each layer (HX8L,HX16L)
Fine (see 3-point for each layer (PN6L), 3x3 for each layer (HX16L) Options).
Mass Default $3 \times 2$ for the whole element (PN6L,PN12L) or (see Options) 1-point for each layer (PN6L), 3-point for each layer (PN12L), $2 \times 2 \times 2$ for the
whole element or $2 \times 2$ for each layer (HX8L,HX16L)
Fine (see $3 \times 2$ for the whole element or 3-point for each layer (PN6L), $3 \times 3 \times 2$ for Options). the whole element or $3 \times 3$ for each layer (HX16L)
Mass Modelling
$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule.
36 Follower loads.
55 Output strains as well as stresses.
77 Output principal stresses and direction cosines.
105 Lumped mass matrix.
139 Output yielded Gauss points only.
229 Co-rotational geometric nonlinearity.
266 Layer by layer computation of mass matrix.
303 Exclude incompatible modes for solid composite elements.

## Notes on Use

1. The elements are based on the standard isoparametric approach. The variation of stresses within an element may be regarded as constant for the lower order elements (corner nodes only), and linear in the plane of the quadratic element faces for the higher order elements.
2. All elements pass the patch test.
3. The COMPOSITE GEOMETRY and COMPOSITE PROPERTIES data chapters must be used with this element in conjunction with the COMPOSITE ASSIGNMENTS data chapter.
4. The stresses obtained from a geometric nonlinear analysis are Kirchhoff stresses.
5. The mass matrix can be computed using a layer by layer integration (Option 266), however this should only be used when the densities of the layers vary considerably because the computation time can be greatly increased applying this option.
6. Numerical integration through the thickness is performed. The integration points are located at the top and bottom surface of each layer.
7. SSIG and SSRG loads have to be applied at the Gauss point positions for the top and bottom surfaces of each layer.
8. Layer 1 is always the bottom layer.

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio


## Recommendations on Use

- The 3D solid composite elements should be used for modelling thick composite structures comprising laminae of differing material properties where the computational cost of modelling each lamina with an individual solid element would be prohibitive.
- Because of the numerical integration through the thickness, by increasing the number of layers the accuracy of solution will increase. This can be achieved by dividing each single layer into two or three identical layers.


## 3D Solid Continuum Explicit Dynamics Elements

## General



## Element Group 3D Continuum

## Element Solid Continuum

Subgroup
Element Description

A family of 3D isoparametric solid elements for explicit dynamic analyses. The elements are numerically integrated.
Number Of
4 (tetrahedra), 6 (pentahedra), 8 (hexahedra).
Nodes The elements are numbered according to a right-hand screw rule in the local z-direction.
Freedoms
U, V, W: at each node.
Node $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.
Coordinates

## Geometric Properties

Not applicable.

## Material Properties

Linear .. Isotropic:
Orthotropic:
MATERIAL PROPERTIES (Elastic: Isotropic)
MATERIAL PROPERTIES ORTHOTROPIC SOLID (Elastic: Orthotropic Solid)
Anisotropic: Not applicable.
Rigidities. Not applicable.
Matrix Not applicable

| Joint <br> Concrete | Not applicable Not applicable |  |
| :---: | :---: | :---: |
| Elasto-Plastic | Stress resultant: | Not applicable. |
|  | Tresca: | MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain) |
|  | Drucker- <br> Prager: | MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular) |
|  | Mohr- <br> Coulomb: | MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation) |
|  | Modified | MATERIAL PROPERTIES |
|  | Mohr- | MODIFIED MOHR_COULOMB (Elastic: |
|  | Coulomb: | Isotropic, Plastic: Mohr-Coulomb/Tresca, nonassociative Hardening with tension/compression cut-off) |
|  | Modified | MATERIAL PROPERTIES CAM_CLAY |
|  | Cam-clay | MODIFIED (Elastic: Isotropic, Plastic) |
|  | Optimised Implicit Von Mises: | MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic) |
|  | Volumetric Crushing: | MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam) |
|  | Stress | STRESS POTENTIAL VON_MISES, HILL, |
|  | Potential | HOFFMAN (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman) |
| Creep |  | CREEP PROPERTIES (Creep) (see Notes) |
| Damage |  | DAMAGE PROPERTIES SIMO, OLIVER (Damage) |
| Viscoelastic |  | VISCO ELASTIC PROPERTIES |
| Shrinkage | Not applicable |  |
| Ko Initialisation | Not applicable |  |
| Rubber | Not applicable |  |
| Generic Polymer | Not applicable |  |
| Composite | Not applicable |  |

LoadingPrescribed Value PDSP, TPDSPConcentrated CLLoads
Element Loads ..... Not
applicable.
Distributed Loads UDL

Not applicable.FLDFLDGBody Forces CBFBFP, BFPE
Velocities VELO
Accelerations ACCE
Initial SSI, SSIEStress/StrainsSSIG
Residual Stresses SSR, SSRESSRGTarget Not
Stress/Strains applicable.
Temperatures TEMP, TMPE Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}, 0$,

$$
0,0
$$ 0,0

Overburden ..... Not

Overburden Not applicable.Phreatic Surface Notapplicable.
Field Loads Notapplicable.
Temp Dependent Not

Loads applicable.

Prescribed variable. U, V, W: at each node.
Concentrated loads. Px, Py, Pz: at each node.

Face Loads. Px, Py, Pz: local face pressures at nodes.
Not applicable
Constant body forces for element. Xcbf, Ycbf, Zcbf, $\Omega_{\mathrm{x}}, \Omega_{\mathrm{y}}, \Omega_{\mathrm{z},} \alpha_{\mathrm{x}}, \alpha \mathrm{y}, \alpha_{\mathrm{z}}$
Body force potentials at nodes/for element. 0, 0, 0, $\varphi_{4}$, Xcbf, Ycbf, Zcbf
Velocities. Vx, Vy, Vz: at nodes.
Acceleration Ax, Ay, Az: at nodes.
Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma z, \sigma x y, \sigma y z, \sigma x z: ~ g l o b a l ~ s t r e s s e s . ~ \varepsilon x, ~ \varepsilon y, ~ \varepsilon z, ~$ $\gamma \mathrm{xy}, \gamma \mathrm{yz}, \gamma \mathrm{xz}$ : global strains.
Not applicable.
Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma z$, $\sigma x y, \sigma y z, \sigma x z:$ global stresses.

Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma z, \sigma x y$, $\sigma y z, \sigma x z:$ global stresses.

Phreatic Surface Not applicable. applicable.

## LUSAS Output

Solver $\operatorname{Stress}($ default): $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z, \sigma e$ : global stresses. Strain: not available (see Notes).<br>For optional principal stress output, together with the corresponding direction cosines, use Option 77.<br>Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

Standard 3D continuum element

## Formulation

## Geometric Nonlinearity

Total Lagrangian Not applicable.
Updated Not applicable.
Lagrangian
Eulerian For large displacements, large rotations and moderately large strains.
Co-rotational For large displacements and large rotations.

## Integration Schemes

| Stiffness | Default. | 1-point (see Notes). |
| :---: | :--- | :--- |
|  | Fine. | As default. |
| Mass | Default. | 1-point (see Notes). |
|  | Fine. | As default. |

## Mass Modelling

$\square$ Lumped mass only (see Notes).

## Options

77 Output principal stresses and direction cosines.

105 Lumped mass matrix.
139 Output yielded Gauss points only.

## Notes on Use

1. The elements are based on the standard isoparametric approach. Stresses within an element may be regarded as constant.
2. When using tabular input for ORTHOTROPIC SOLID the value of nset used is that defined in the first line of the property table.
3. The system parameter HGVISC is used to restrict element mechanisms due to underintegration. The default value is usually sufficient.
4. The bulk viscosity coefficients are used to restrict numerical oscillations due to the traversal of stress waves. The default bulk viscosity coefficients (BULKLF and BULKQF) may be altered as SYSTEM parameters.
5. These elements must be used with a dynamic central difference scheme and a lumped mass matrix.
6. These element are Not applicable. for static or eigenvalue analyses.
7. Automatic time step length calculations are implemented.
8. As element geometry is always updated in an explicit dynamic analysis, the solution is nonlinear. When using explicit dynamic elements NONLINEAR CONTROL must be specified.
9. If CREEP PROPERTIES are defined, explicit time integration must be specified in VISCOUS CONTROL.
10. Strains are computed incrementally and therefore total strains are not available for output.
11. Non-conservative loading is invoked when the FLD loading facility is applied.
12. Rayleigh damping coefficients are not supported by these elements.
13. Constraint equations are not available for use with these elements.

## Restrictions

$\square$ Avoid excessive aspect ratio

## Recommendations on Use

- Explicit dynamics elements may be used to define surface boundaries which will be active in a slideline analysis.


## Element Reference Manual

- The 3D explicit dynamics elements should be used if the stress field is fully 3D, i.e. it cannot be approximated with any of the 2D elements, e.g. a non-axisymmetric pressure vessel.


## 3D Solid Two Phase Continuum Elements

## General



PN12P


HX16P


PN15P


HX20P


## Element Group 3D Continuum

Element
Solid Continuum

## Subgroup

Element
A family of 3D isoparametric solid two phase continuum elements Description capable of modelling curved boundaries. The elements are numerically integrated.
Number Of 10 (tetrahedra). 12 or 15 (pentahedra). 16 or 20 (hexahedra). The elements

Nodes are numbered according to a right-hand screw rule in the local z-direction.
Freedoms U, V, W, P: at corner nodes, U, V, W at mid-side nodes.
Node $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.
Coordinates

## Geometric Properties

Not applicable.

## Material Properties

Linear Isotropic:
Orthotropic:
Anisotropic:
Rigidities. Not applicable.
Matrix Not applicable.
Joint Not applicable.

## Concrete

Elasto-Plastic Stress resultant: Tresca: MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
MATERIAL PROPERTIES NONLINEAR 64
(Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
MATERIAL PROPERTIES NONLINEAR 65
(Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
Modified MATERIAL PROPERTIES Mohr- MODIFIED MOHR_COULOMB (Elastic: Coulomb: Isotropic, Plastic: Mohr-Coulomb/Tresca, nonassociative Hardening with tension/compression cut-off)
MATERIAL PROPERTIES CAM_CLAY

Optimised Implicit Von Mises:
Volumetric Crushing:
Stress
Potential:

Cam-clay

MODIFIED (Elastic: Isotropic, Plastic)

MATERIAL PROPERTIES NONLINEAR 75
(Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic)
MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam)
STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
CREEP PROPERTIES (Creep)
DAMAGE PROPERTIES SIMO, OLIVER (Damage)
VISCO ELASTIC PROPERTIES
SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER

Ko Initialisation Applicable
Elasto- Plastic Interface Rubber

Not

Creep
Damage
Viscoelastic
Shrinkage applicable.

Generic Polymer Isotropic

MATERIAL PROPERTIES NONLINEAR 26

MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)
Composite Not applicable

## Loading

Prescribed Value PDSP, TPDSP

Concentrated CL
Loads
Element Loads Not applicable.
Distributed Loads UDL FLD

FLDG

Prescribed variable. U, V, W, P: at corner nodes, U, $\mathrm{V}, \mathrm{W}$ at mid-side nodes.
Concentrated loads. Px, Py, Pz, Q: at corner nodes, .Px, Py, Pz at mid-side nodes.

Not applicable.
Face Loads. Px, Py, Pz, Q: face pressures/flux per unit area at corner nodes relative to local face axes. $\mathrm{Px}, \mathrm{Py}, \mathrm{Pz}$ : face pressures at midside nodes relative to local face axes.

Global Face Loads. $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z$ at nodes

Body Forces CBF

BFP, BFPE

SSIG

## Residual Stresses SSR, SSRE

SSRG

Target TSSIE, TSSIA Stress/Strains

TSSIG

Temperatures TEMP, TMPE
Overburden Applicable.
Phreatic Surface Applicable.
Field Loads Not applicable.
Temp Dependent Not applicable. Loads

Constant body forces for element. Xcbf, Ycbf, Zcbf, $\Omega_{\mathrm{x}}, \Omega_{\mathrm{y}}, \Omega_{\mathrm{z},} \alpha_{\mathrm{x}}, \alpha \mathrm{y}, \alpha \mathrm{z}, \mathrm{gx}, \mathrm{gy}, \mathrm{gz}$. (See notes on use)
Body force potentials at nodes/for element. $0,0,0$, $\varphi 4, \mathrm{Xcbf}, \mathrm{Ycbf}, \mathrm{Zcbf}, \mathrm{gx}, \mathrm{gy}, \mathrm{gz}$. (See notes on use)
Velocities. Vx, Vy, Vz: at nodes.
Acceleration Ax, Ay, Az: at nodes.
Initial stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma z, \sigma x y, \sigma y z, \sigma x z, \sigma p$ global stresses. $\varepsilon x, \varepsilon y, \varepsilon z$, $\gamma_{\mathrm{xy}}, \gamma_{\mathrm{yz}}, \gamma \mathrm{xz}$ : global strains.
Initial stresses/strains at Gauss points $\sigma x, \sigma y, \sigma z$, $\sigma x y, \sigma y z, \sigma x z, \sigma p:$ global stresses. $\varepsilon x, \varepsilon y, \varepsilon z$, $\gamma_{\mathrm{xy}}, \gamma_{\mathrm{yz}}, \gamma_{\mathrm{xz}}$ : global strains.
Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma z$, $\sigma x y, \sigma y z, \sigma x z, \sigma p:$ global stresses.
Residual stresses at Gauss points. $\sigma x, \sigma y, \sigma z, \sigma x y$, $\sigma y z, \sigma x z, \sigma p$ global stresses.
Target stresses/strains at nodes/for element. $\sigma x, \sigma y$, $\sigma z, \sigma x y, \sigma y z, \sigma x z, \sigma$ p global stresses. $\varepsilon x, \varepsilon y, \varepsilon z$, $\gamma \mathrm{xy}, \gamma \mathrm{yz}, \gamma \mathrm{xz}$ : global strains.
Target stresses/strains at Gauss points $\sigma x, \sigma y, \sigma z$, $\sigma x y, \sigma y z, \sigma x z, \sigma p:$ global stresses. $\varepsilon x, \varepsilon y, \varepsilon z$, $\gamma \mathrm{xy}, \gamma \mathrm{yz}, \gamma \mathrm{xz}$ : global strains.
Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}, 0$, 0,0

## LUSAS Output

Solver
Stress (default): $\sigma x, \sigma y, \sigma z, \sigma x y, \sigma y z, \sigma x z, \sigma p, \sigma e:$ global stresses.

Strain: $\varepsilon x, \varepsilon y, \varepsilon z, \gamma \mathrm{xy}, \gamma \mathrm{yz}, \gamma \mathrm{xz}, \varepsilon \mathrm{v}, \varepsilon_{\mathrm{e}}$ : global strains.
For optional principal stress/strain output, together with the corresponding direction cosines, use Option 77.

Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

$\square$ Standard 3D continuum element

## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements and large rotations.
Updated For large displacements and large rotations.
Lagrangian
Eulerian For large displacements, large rotations and moderately large strains.
Co-rotational For large displacements and large rotations.

## Integration Schemes

Stiffness Default.

Fine (see Options).
Coarse (see Options)
Mass Default.

Fine (see Options). Coarse (see Options)

4-point (TH10P), 3x2 (PN12P, PN15P), 2x2x2 (HX16P, HX20P)
5 -point (TH10P), $3 \times 3 \times 2$ (HX16P), $3 \times 3 \times 3$ (HX20P)
13-point (HX20P), 14-point (HX20P)

4-point (TH10P), 3x2 (PN12P, PN15P), 2x2x2 (HX16P, HX20P)
11-point (TH10P), 14-point (TH10P), $3 \times 3 \times 2$ (HX16P), 3x3x3 (HX20P)
13-point (HX20P), 14-point (HX20P)

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule.
36 Follower loads
54 Updated Lagrangian geometric nonlinearity
55 Output strains as well as stresses.
77 Output principal stresses and direction cosines.
87 Total Lagrangian geometric nonlinearity.
91 Invoke finer integration of the mass matrix.
102 Switch off load correction stiffness due to centripetal acceleration.
105 Lumped mass matrix.
139 Output yielded Gauss points only.
155 Use 14-point integration rule for HX20P.
156 Use 13-point integration rule for HX20P.
167 Eulerian geometric nonlinearity.
229 Co-rotational geometric nonlinearity.
398 For HX20P and HX16P with fine integration use all integration points for stress extrapolation.

## Notes on Use

1. Two phase material parameters must be used with these elements for undrained and consolidation analysis.
2. The elements are based on the standard isoparametric approach. The variation of stresses and pore pressures within an element may be regarded linear, except for elements PN12P and HX16P where the stress is constant in the z direction.
3. All elements pass the patch test.
4. When using table input format for temperature dependent ORTHOTROPIC SOLID or ANISOTROPIC SOLID material properties, the value of nset used is that defined in the first line of the property table.
5. Non-conservative loading is available with these elements when using Updated Lagrangian, Eulerian or co-rotational (with OPTION 36) geometric nonlinear formulations together with the FLD loading facility.
6. The global components of gravity acting on the fluid phase are defined by gx and gy under CBF and BF loading.

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio


## Recommendations on Use

- The 3D solid two phase elements should be used if the stress field is fully 3D, i.e. it cannot be approximated with any of the 2D elements, e.g. a non-axisymmetric pressure vessel.
- For linear materials, the 20 -noded element with a $2 * 2 * 2$ Gauss rule is usually the most effective element, as this under-integration of the stiffness matrix prevents locking, i.e. over-stiff solutions will occur if the elements are used with a $3 * 3 * 3$ Gauss integration rule to model structures subjected to bending. However, the element possesses six zero energy modes. Therefore, a careful examination of the solution should be performed to check for spurious stress oscillations and peculiarities in the deformed configuration. Either the 14-point or $3 * 3 * 3$ Gauss rules should be used for materially nonlinear problems or materially linear problems that exhibit spurious deformations.
- In general, PN15P and HX20P give the best performance; TH10P is less accurate and needs to be used with a finer mesh. HX16P and PN12P should only be used to overcome connectivity problems when meshing.


## Chapter 5: Plate Elements.

## 2D Isoflex Thin Plate Flexure Elements

## General

Element Name


TF3


QF4


## Element Group Plates

Element
Isoflex Plates
Subgroup
Element
Description
A family of thin plate flexure elements in 2D with higher order models capable of modelling curved boundaries. The element formulation takes account of varying thickness and anisotropic properties. As required by thin plate theory, transverse shearing effects are excluded.
Number Of 3 or 4 numbered anticlockwise. Nodes Freedoms

Node $\mathrm{X}, \mathrm{Y}$ : at each node.

## Geometric Properties

t1 ... tn Thickness at each node.

## Material Properties

Linear Isotropic: MATERIAL PROPERTIES (Elastic: Isotropic)
Orthotropic: MATERIAL PROPERTIES ORTHOTROPIC (Elastic: Orthotropic Plane Stress)
Anisotropic: MATERIAL PROPERTIES ANISOTROPIC 3 (Elastic: Anisotropic Thin Plate)

Rigidities.
Matrix Not applicable
Joint Not applicable
Concrete Not applicable
Elasto-Plastic Not applicable
Creep Not applicable
Damage Not applicable
Viscoelastic Not applicable
Shrinkage Not applicable
Rubber Not applicable
Generic Polymer Not applicable
Composite Not applicable

RIGIDITIES 3 (Rigidities: Membrane/Thin Plate)

## Loading

Prescribed Value PDSP, TPDSP
Concentrated CL
Loads
Element Loads Not applicable.
Distributed Loads UDL

FLD, FLDG
Body Forces CBF
BFP, BFPE
Velocities VELO
Accelerations ACCE
Initial SSI, SSIE
Stress/Strains

SSIG
Residual Stresses Not applicable.
Target TSSIE, TSSIA
Stress/Strains

TSSIG
Temperatures TEMP, TMPE

Prescribed variable. W, $\theta \mathrm{x}, \theta \mathrm{y}$ : at the corner nodes.
Concentrated loads. Pz, Mx, My: at corner nodes.

Uniformly distributed loads. Wz: normal pressure for element (global).
Not applicable.
Constant body forces for element. Zcbf
Body force potentials at nodes/for element. $\varphi 1, \mathrm{Zcbf}$
Velocities. Vz: at nodes.
Accelerations. Az: at nodes.
Initial stresses/strains at nodes/for element. Mx, My, Mxy: moments/unit width (global).
$\psi x, \psi y, \psi x y:$ flexural strains (global).
Not applicable.

Target stresses/strains at nodes/for element. Mx, My, Mxy: moments/unit width (global).
$\psi x, \psi y, \psi x y:$ flexural strains (global).
Not applicable.
Temperatures at nodes/for element. $0,0,0, \mathrm{dT} / \mathrm{dz}, 0,0,0, \mathrm{dTo} / \mathrm{dz}$
Overburden Not applicable.
Phreatic Surface Not applicable.
Field Loads Not applicable.
Temp Dependent Not
Loads applicable.

## LUSAS Output

Solver Stress resultant: Mx, My, Mxy: moments/unit width (global).
Strain: $\psi x, \psi y, \psi x y:$ flexural strains (global).
Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

$\square$ Standard plate element

## Formulation

## Geometric Nonlinearity

Not applicable.
Integration Schemes

| Stiffness | Default. | 3-point (TF3), 2x2 (QF4). |
| :---: | :--- | :--- |
|  | Fine. | As default. |
| Mass | Default. | 3-point (TF3), 2x2 (QF4). |
|  | Fine. | As default. |

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule for element.
55 Output strains as well as stresses.
143 Output shear forces for low order thin plate bending elements.
170 Suppress transfer of shape function arrays to disk.

## Notes on Use

1. The element formulations are based on an Kirchhoff hypothesis for thin plates.
2. The variation of moments within the elements can be regarded as linear.
3. The elements pass the patch test for convergence for mixed triangular and quadrilateral element geometry.
4. The averaged nodal values produced with ELEMENT OUTPUT do not include the thin isoflex plate shear stresses if Option 143 is invoked.
5. When Option 143 is invoked shear stresses are only computed for the low order isoflex elements (QF4,TF3).

## Restrictions

$\square$ Avoid excessive aspect ratio

## Recommendations on Use

- This element may be used to analyse any 2D plate type structures where transverse shear effects do not influence the solution, e.g. thin cantilever plates.
- The thick plate elements QTF8 and TTF6 are recommended for thick plates where transverse shear strains are no longer negligible.

The following element combinations should be used for ribbed plates;

## Ribs with small or no eccentricity

QSI4/TS3 elements with BMI21 elements,
Q QTS4/TTS3 elements with BMI21 elements.

## Ribs with large eccentricity

Q QSL8/TSL6 elements with BSL3/BSL4/BXL4 elements.
$\square$ QTS4/TTS3 elements with BMI21 elements.
The through thickness integration is performed explicitly.

## 2D Isoflex Thick Plate Flexure Element



## Geometric Properties

t1... tn At each node.

## Material Properties

Linear Isotropic:
MATERIAL PROPERTIES (Elastic: Isotropic)
Orthotropic: MATERIAL PROPERTIES ORTHOTROPIC THICK (Elastic: Orthotropic Thick)
Anisotropic: MATERIAL PROPERTIES ANISOTROPIC 5 (Elastic: Anisotropic Thick Plate)
Rigidities: RIGIDITIES 5 (Rigidities: Thick Plate)
Matrix Not applicabl
Joint Not applicable
Concrete Not applicable
Elasto-Plastic Not applicableCreep Not applicable.
Damage Not applicable
Viscoelastic Not applicable
Shrinkage Not applicable
Rubber Not applicable
Generic Polymer Not applicable
Composite Not applicable
Loading
Prescribed Value PDSP, TPDSP
Concentrated ..... CL
Loads
Element Loads ..... Notapplicable.
Distributed Loads UDLFLD, FLDGBody Forces CBFBFP, BFPEVelocities VELOAccelerations ACCEInitial SSI, SSIE
Stress/Strains
SSIG
Residual Stresses Notapplicable.Target TSSIE, TSSIAStress/Strains
TSSIGTemperatures TEMP, TMPE
Overburden Notapplicable.Phreatic Surface Not

Prescribed variable. W, $\theta \mathrm{x}, \theta \mathrm{y}$ : at nodes. Concentrated loads. Pz, Mx, My: at nodes.
Uniformly distributed loads. Wz: normal pressurefor element (global).
Not applicable.
Constant body forces for element. Zcbf
Body force potentials at nodes/for element. $\varphi_{1}$,Zcbf
Velocities. Vz: at nodes.
Accelerations. Az: at nodes.
Initial stresses/strains at nodes/for element.Mx, My, Mxy: moments/unit width (global).$\psi x, \psi y, \psi x y$ : flexural strains (global).
Not applicable.
Target stresses/strains at nodes/for element.Mx, My, Mxy: moments/unit width (global).$\psi x, \psi y, \psi x y$ : flexural strains (global).
Not applicable.Temperatures at nodes/for element. $0,0,0, \mathrm{dT} / \mathrm{dz}$,$0,0,0, \mathrm{dTo} / \mathrm{dz}$
applicable.
Field Loads Not applicable.
Temp Dependent Not
Loads applicable.

## LUSAS Output

Solver Stress resultant: Mx, My, Mxy, Sx, Sy: moments, shear forces/unit width (global)

Strain: $\psi \mathrm{x}, \psi \mathrm{y}, \psi \mathrm{xy}, \gamma \mathrm{xz}, \gamma \mathrm{yz}:$ flexural, shear strains (global).
Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

Standard plate element

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

| Stiffness | Default. | $2 \times 2$ |
| :---: | :--- | :--- |
| Mass | Fine. | Default. |

## Mass Modelling

$\square$ Consistent mass (default).

- Lumped mass.


## Options

55 Output strains as well as stresses.
105 Lumped mass matrix.
170 Suppress transfer of shape function arrays to disk.

## Notes on Use

1. The element formulation involves imposing an assumed bi-linear shear strain field on the isoflex thin plate element QF4.
2. Though this element cannot model nonlinear behaviour, it can be mixed with other elements in a nonlinear analysis.
3. The element passes the patch test for convergence with rectangular and parallelogram element geometry.
4. The QF4, QF8,TF3,TF8 elements are usually more effective elements for thin plate analyses.
5. The QTF8 and TTF6 elements are usually more effective for thick plate analyses, and in such cases should be preferred to QSC4.
6. 3D solid elements should be used if the normal stress in the transverse direction is not insignificant in comparison with the in-plane stresses.
7. The following element combinations should be used for ribbed plates

Ribs with small or no eccentricity

- QSI4/TS3 elements with BMI21 elements,
- QTS4/TTS3 elements with BMI21 elements.

Ribs with large eccentricity

- QSL8/TSL6 elements with BSL3/BSL4/BXL4 elements,
- QTS4/TTS3 elements with BMI21 elements.

8. The through-thickness integration is performed explicitly.

## Restrictions

$\square$ Avoid excessive aspect ratio

## Recommendations on Use

This element may be used to analyse any 2D plate type structures where transverse shear effects influence the solution, e.g. perforated thick plates.

## 2D Mindlin Thick Plate Flexure Element

## General

Element Name


TTF6


QTF8


## Element Group Plates

## Element Mindlin Plates

## Subgroup

Element A family of thick plate flexure elements based on a Mindlin plate Description formulation. The elements can accommodate curved boundaries and varying thicknesses. Transverse shear deformations are included.
Number Of 6 or 8 , numbered anticlockwise.
Nodes
Freedoms $\mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}$ : at each node.
Node X, Y: at each node.
Coordinates

## Geometric Properties

t1... tn Thickness at each node.

## Material Properties

Linear Isotropic:
MATERIAL PROPERTIES (Elastic: Isotropic)
Orthotropic:
Anisotropic:
MATERIAL PROPERTIES ORTHOTROPIC
THICK (Elastic: Orthotropic Thick)
MATERIAL PROPERTIES ANISOTROPIC 5
(Elastic: Anisotropic Thick Plate)
Rigidities.
RIGIDITIES 5 (Rigidities: Thick Plate)
Matrix Not applicable
Joint Not applicable
Concrete Not applicable
Elasto-Plastic Not applicableCreep Not applicableDamage Not applicable
Viscoelastic Not applicable
Shrinkage Not applicableRubber Not applicable
Generic Polymer Not applicable
Composite Not applicable
Loading
Prescribed Value PDSP, TPDSPConcentrated CLLoadsElement Loads Notapplicable.
Distributed Loads UDL Uniformly distributed loads. Wz: normal pressureFLD, FLDGBody Forces CBFBFP, BFPE
Velocities VELO
Accelerations ACCEInitial SSI, SSIEStress/Strains
Residual Stresses Notapplicable.Target TSSIE, TSSIAStress/Strains

TSSIG
Temperatures TEMP, TMPEfor element (global).
Not applicable.
Constant body forces for element. Zcbf

Constant body forces for element. Zcbf
Body force potentials at nodes/for element. $\varphi 1$, Zcbf

Body force potentials at nodes/for element. $\varphi_{1}$, Zcbf
Velocities. Vz: at nodes.
Accelerations. Az: at nodes.
Initial stresses/strains at nodes/for element.

Initial stresses/strains at nodes/for element.Mx, My, Mxy, Sx, Sy: moments, shear forces/unitwidth (global)
$\psi \mathrm{x}, \psi \mathrm{y}, \psi \mathrm{xy}, \gamma \mathrm{xz}, \gamma \mathrm{yz}:$ flexural, shear strains /unit width (global).

$\psi x, \psi y, \psi x y, \gamma x z, \gamma y z:$ flexural, shear strains
Not applicable.
Not applicable.

Prescribed variable. W, $\theta \mathrm{x}, \theta \mathrm{y}$ : at nodes.
Concentrated loads. $\mathrm{Pz}, \mathrm{Mx}, \mathrm{My}$ : at nodes.
for element (global).

Accelerations. Az: at nodes.

Mx, My, Mxy, Sx, Sy: moments, shear forces/unit width (global).

Target stresses/strains at nodes/for element. Mx, My, Mxy, Sx, Sy: moments, shear forces/unit width (global).
$\psi \mathrm{x}, \psi \mathrm{y}, \psi \mathrm{xy}, \gamma \mathrm{xz}, \gamma \mathrm{yz}:$ flexural, shear strains /unit width (global).
Not applicable.
Temperatures at nodes/for element. $0,0,0, \mathrm{dT} / \mathrm{dz}, 0,0,0, \mathrm{dTo} / \mathrm{dz}$
Overburden Not applicable.
Phreatic Surface Not applicable.
Field Loads Not applicable.
Temp Dependent Not
Loads applicable.

## Output

Solver Stress resultant: Mx, My, Mxy, Sx, Sy: moments, shear forces/unit width (global).

Strain: $\psi x, \psi y, \psi x y, \gamma x z, \gamma y z:$ flexural, shear strains /unit width (global).
Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

- Standard plate element


## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

| Stiffness | Default. | 3-point (TTF6), 2x2 (QTF8) |
| :---: | :--- | :--- |
|  | Fine (see Options). | $3 \times 3$ (QTF8). |
| Mass | Default. | 3-point (TTF6), 2x2 (QTF8) |
|  | Fine (see Options). | $3 \times 3$ (QTF8). |

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule for element.
55 Output strains as well as stresses.
105 Lumped mass matrix.
170 Suppress transfer of shape function arrays to disk.

## Notes on Use

1. The element formulations are based on an isoparametric approach. The variation of moments and shears within the element may be regarded as linear.
2. Though this element cannot model nonlinear behaviour, it can be mixed with other elements in a nonlinear analysis.
3. The elements pass the patch test for convergence with triangular and parallelogram element geometry.
4. These elements are usually more effective than the QSC4 thick shell element (section 7.6.2).
5. The elements tend to lock as the plate thickness approaches the thin plate limit since shear strain energy dominates the element stiffness. Therefore, a thin plate or shell element should be used when the depth/span ratio exceeds $1 / 50$.
6. 3D solid elements should be used if the normal stress in the transverse direction is not insignificant in comparison with the in-plane stresses.
7. The following element combinations should be used for ribbed plates

Ribs with small or no eccentricity

- QSI4/TS3 elements with BMI21 elements,
- QTS4/TTS3 elements with BMI21 elements.

Ribs with large eccentricity

- QSL8/TSL6 elements with BSL3/BSL4/BXL4 elements,
- QTS4/TTS3 elements with BMI21 elements.

8. The QTF8 element with $2 * 2$ Gauss quadrature is generally more effective than the $3 * 3$ rule. The $2 * 2$ rule does, however, exhibit one zero energy mode which can be eliminated using option 18.
9. The through-thickness integration is performed explicitly.

## Restrictions

$\square$ Ensure mid-side node centrality

- Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio


## Recommendations on Use

These elements may be used to analyse any 2D plate type structures where transverse shear effects influence the solution, e.g. perforated thick plates.

## Chapter 6 : Shell Elements.

## 2D Axisymmetric Thin Shell Element

## General



Element Group Shells
Subgroup
Element A parabolically curved axisymmetric thin shell element in 2D in which Description shear deformations are excluded. The geometric properties may vary

Number Of
Nodes
End Releases
Freedoms
dU : (relative local in-plane displacement) at the mid-length node.

Element Axisymmetric Shells along the length of the element.
3.
$\mathrm{U}, \mathrm{V}, \theta \mathrm{z}$ : at end nodes.
Node X, Y: at each node.
BXS3


## Geometric Properties

$\mathbf{t}, \mathbf{t}, \mathbf{t}_{3}$ Thickness at each node.

## Material Properties

| Linear | Isotropic: | MATERIAL PROPERTIES (Elastic: Isotropic) |
| :--- | :--- | :---: |
|  | Orthotropic: | MATERIAL PROPERTIES ORTHOTROPIC |
|  |  | (Elastic: Orthotropic Plane Stress) |
|  |  | MATERIAL PROPERTIES ORTHOTROPIC |
|  |  | SOLID (Elastic: Orthotropic Thick) |

```
Anisotropic: MATERIAL PROPERTIES ANISOTROPIC 2 (Not
    supported in LUSAS Modeller)
    Rigidities: Not applicable.
    Matrix Not applicable.
    Joint Not applicable.
    Concrete Not applicable.
Elasto-Plastic Stress
    resultant:
    Tresca:
    Drucker-
    Prager:
    Mohr-
    Coulomb:
    Optimised
    Implicit Von
    Mises:
    Volumetric Not applicable.
    Crushing:
    Stress Potentia
    Creep
    AASHTO
CEB-FIP
Chinese
Eurocode
```

MATERIAL PROPERTIES NONLINEAR 29
(Elastic: Isotropic, Plastic: Resultant) (ifcode not required)
MATERIAL PROPERTIES NONLINEAR 61
(Elastic: Isotropic, Plastic: Tresca, Hardening:
Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
MATERIAL PROPERTIES NONLINEAR 64
(Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic)
Not applicable.

STRESS POTENTIAL VON_MISES, HILL, HOFFMAN
(Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
CREEP PROPERTIES (Creep)
MATERIAL PROPERTIES NONLINEAR 86 AASHTO
(Concrete creep model to AASHTO Code of Practice)

MATERIAL PROPERTIES NONLINEAR 86 CEBFIP
(Concrete creep model to CEB-FIP Model Code 1990)

Chinese

Eurocode

MATERIAL PROPERTIES NONLINEAR 86 CHINESE
(Chinese creep model to Chinese Code of Practice)
MATERIAL PROPERTIES NONLINEAR 86 EUROCODE

IRC

## Damage

Viscoelastic Not applicable. Shrinkage

Rubber Not applicable. Generic Polymer Not applicable

Composite Not applicable.
(Concrete creep model to EUROCODE_2)
MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC Code of Practice)
DAMAGE PROPERTIES SIMO, OLIVER (Damage)

SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER

## Loading

Prescribed Value PDSP, TPDSP
Concentrated CL
Loads
Element Loads ELDS

Prescribed variable. $\mathrm{U}, \mathrm{V}, \theta \mathrm{z}$ : at end nodes. dU : at the mid-length node.
Concentrated loads. Px, Py, Mx: point loads, moments/unit length/radian at end nodes (global). DPx: point load/unit length/radian at mid-length node (local).

## Element loads

LTYPE, S1, Px, Py, Mx
LTYPE=11: point loads and moments in local directions.
LTYPE=12: point loads and moments in global directions.
LTYPE, $0, \mathrm{Wx}$, Wy, Mx
LTYPE=21: uniformly distributed loads in local directions.
LTYPE=22: uniformly distributed loads in global directions.
LTYPE=23: uniformly distributed projected loads in global directions
LTYPE, S1, Wx1, Wy1, Mx1, S2, Wx2, Wy2, Mx2
LTYPE=31: distributed loads in local directions.
LTYPE=32: distributed loads in global directions.
LTYPE=33: distributed projected loads in global directions
LTYPE, S1, Wx, Wy, Mx
LTYPE=41: trapezoidal loads in local directions.
LTYPE=42: trapezoidal loads in global directions.

Distributed Loads UDL

FLD
FLDG
Body Forces CBF

BFP, BFPE

Velocities VELO
Accelerations ACCE
Initial SSI, SSIE
Stress/Strains

Residual Stresses
SSR, SSRE
SSRG

LTYPE=43: trapezoidal projected loads in global directions
Uniformly distributed loads. Wx, Wy: forces/unit length/radian in local $x$, $y$ directions for element.
Face Loads. Px, Py: local face pressures at nodes.
Not applicable.
Constant body forces for element. Xcbf, Ycbf, $\Omega \mathrm{x}$, $\Omega_{y}, \Omega_{z}, \alpha_{z}$
Body force potentials at nodes/for element. $\varphi_{1}, \varphi_{2}$, $0,0, \mathrm{Xcbf}, \mathrm{Ycbf}$
Velocities. Vx, Vy: at nodes.
Accelerations. Ax, Ay: at nodes.
Initial stresses/strains at nodes/for element.
Resultants (for linear material models without cross section integration and material model 29). $\mathrm{Nx}, \mathrm{N} \theta, \mathrm{Mx}, \mathrm{M} \theta, 0$ : axial and circumferential forces, moments/unit width. $\varepsilon x, \varepsilon_{\theta}, \psi x, \psi{ }_{\theta}, 0$, axial and circumferential strains (all models).
Initial stresses/strains at Gauss points.
(1) Resultants (for linear material models without cross section integration and material model 29). $\mathrm{Nx}, \mathrm{N} \theta, \mathrm{Mx}, \mathrm{M} \theta, 0$ : axial and circumferential forces, moments/unit width. $\varepsilon_{x}, \varepsilon_{\theta}, \psi \mathrm{x}, \psi \theta, 0$ : axial and circumferential strains (all models).
(2) Components (for linear material models with cross section integration and all nonlinear material models except 29). $0,0,0,0,0,0,0,0,0,0,(\sigma x$, $\left.\sigma_{\theta}, \varepsilon_{x}, \varepsilon_{\theta}\right)$ Bracketed terms repeated for each fibre integration point.
Not applicable.
Residual stresses at Gauss points.
(1) Resultants (model 29). Nx, N $\theta, \mathrm{Mx}, \mathrm{M} \theta, 0$
(2) Components (all models except 29) $0,0,0,0$, $0,0,0,0,0,0,(\sigma x, \sigma \theta)$ Bracketed terms repeated for each fibre integration point.
Target TSSIE, TSSIA Stress/Strains

Target stresses/strains at nodes/for element. Resultants (for linear material models without cross section integration and material model 29). $\mathrm{Nx}, \mathrm{N} \theta, \mathrm{Mx}, \mathrm{M}_{\theta}, 0$ : axial and circumferential forces, moments/unit width. $\varepsilon_{x}, \varepsilon_{\theta}, \psi x, \psi \theta, 0$, axial and circumferential strains (all models).

|  | TSSIG | Target stresses/strains at Gauss points. <br> (1) Resultants (for linear material models without cross section integration and material model 29). $\mathrm{Nx}, \mathrm{N} \theta, \mathrm{Mx}, \mathrm{M}_{\theta}, 0$ : axial and circumferential forces, moments/unit width. $\varepsilon_{x}, \varepsilon_{\theta}, \psi \mathrm{x}, \psi_{\theta}, 0$ : axial and circumferential strains (all models). <br> (2) Components (for linear material models with cross section integration and all nonlinear material models except 29). $0,0,0,0,0,0,0,0,0,0,(\sigma x$, $\left.\sigma \theta, \varepsilon x, \varepsilon_{\theta}\right)$ Bracketed terms repeated for each fibre integration point. |
| :---: | :---: | :---: |
| Temperatures | TEMP, TMPE | Temperatures at nodes/for element. <br> T, $0, \mathrm{dT} / \mathrm{dy}, 0, \mathrm{To}, 0, \mathrm{dTo} / \mathrm{dy}, 0$ : in local directions. |
| Overburden | Not applicable. |  |
| Phreatic Surface | Applicable. |  |
| Field Loads | Not applicable. |  |
| Temp Dependent | Not applicable. |  |

## LUSAS Output

Solver Force. $\mathrm{Nx}_{\mathrm{x}}, \mathrm{N} \theta, \mathrm{Mx}, \mathrm{M}_{\theta}$ : axial and circumferential forces, moments/unit width in local directions.

Strain. $\varepsilon x, \varepsilon_{\theta}, \gamma_{\mathrm{x}}, \gamma_{\theta}$ : axial and circumferential strains.
Layer stress and strain output is also available when using the nonlinear continuum material models.

Modeller See Results Tables (Appendix K).

## Local Axes

The local x -axis lies along the line of the element in the direction in which the nodes are numbered. The local $y$ and $z$-axes form a right-hand set with the local $x$-axis such that the $y$ axis lies in the global XY-plane with the z -axis parallel to the global Z-axis.

## Sign Convention

Standard shell element. Axial and circumferential moments are positive for tension on element top fibre (the top fibre lies on the positive local y side of the element).

## Formulation

## Geometric Nonlinearity

$$
\begin{aligned}
\text { Total Lagrangian } & \text { For large displacements, rotations up to } 1 \text { radian, and small strains. } \\
\text { Updated } & \text { For large displacements, rotation increments up to } 1 \text { radian and small } \\
\text { Lagrangian } & \text { strains. } \\
\text { Eulerian } & \text { Not applicable. } \\
\text { Co-rotational } & \text { Not applicable. }
\end{aligned}
$$

Integration Schemes

| Stiffness | Default. | 2-point. |
| :---: | :--- | :--- |
|  | Fine (see Options). | 3-point. |
| Mass | Default. | 2-point. |
|  | Fine (see Options). | 3-point. |

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule for element
47 X-axis taken as axis of symmetry
54 Updated Lagrangian geometric nonlinearity.
55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity
105 Lumped mass matrix.
157 Material model 29 (non cross-section elements), see Notes.
170 Suppress transfer of shape function arrays to disk.

## Notes on Use

1. The element formulation is based on a constrained super-parametric approach.
2. The variation of axial force and moment along the length of the element is linear. The variation of displacements is cubic in the local $y$-direction, and quadratic in the local $x$ direction.
3. Temperature dependent properties cannot be used with material model 29.
4. The through-thickness integration is performed explicitly for linear and stress resultant plasticity models and with a 5-point Newton-Cotes rule for all other material models.

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature


## Recommendations on Use

The element can be used for analysing shell structures which are axisymmetric, e.g. pressure vessels or pipes.

## 2D Axisymmetric Thick Shell Elements

## General

Element Name


BXSI2


BXSI3
(s)

Element Group Shells
Element Axisymmetric Shells
Subgroup
Element Straight and curved isoparametric degenerate thick axisymmetric shell
Description elements in 2D for which shearing deformations are included. The element thickness may vary along the length.
Number Of 2 (BXSI2), 3 (BXSI3)
Nodes
End Releases
Freedoms U, V, $\theta \mathrm{z}$ : at end nodes.
Node $\mathrm{X}, \mathrm{Y}$ : at each node.
Coordinates

## Geometric Properties

$\mathbf{t}, \mathbf{t} 2, \mathbf{t} \mathbf{3}$ Thickness at each node.

## Material Properties

Linear Isotropic: MATERIAL PROPERTIES (Elastic: Isotropic) Orthotropic: MATERIAL PROPERTIES ORTHOTROPIC
(Elastic: Orthotropic Plane Stress)
MATERIAL PROPERTIES ORTHOTROPIC
SOLID (Elastic: Orthotropic Thick)
Anisotropic: MATERIAL PROPERTIES ANISOTROPIC 2 (Not supported in LUSAS Modeller)
Rigidities: Not applicable.
Matrix Not applicable.
Joint Not applicable.
Concrete Not applicable.
Elasto-Plastic

## Creep

Stress resultant:
Tresca: MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
Drucker- MATERIAL PROPERTIES NONLINEAR 64
Prager: (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
Mohr- MATERIAL PROPERTIES NONLINEAR 65
Coulomb: (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
Optimised
Implicit Von Mises:
Volumetric
MATERIAL PROPERTIES NONLINEAR 75
(Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic)

Crushing:
Stress Potential STRESS POTENTIAL VON_MISES, HILL,
Not applicable. HOFFMAN (Isotropic: von Mises, Modified von Mises
Orthotropic: Hill, Hoffman)
AASHTO

CEB-FIP

Eurocode
Not applicable.

STRESS POTENTIAL VON_MISES, HILL,

CREEP PROPERTIES (Creep)
MATERIAL PROPERTIES NONLINEAR 86 AASHTO
(Concrete creep model to AASHTO code of Practice)

MATERIAL PROPERTIES NONLINEAR 86 CEBFIP
(Concrete creep model to CEB-FIP Model Code 1990)

Chinese

Eur

MATERIAL PROPERTIES NONLINEAR 86 CHINESE
(Chinese creep model to Chinese Code of Practice)
MATERIAL PROPERTIES NONLINEAR 86 EUROCODE

IRC

## Damage

Viscoelastic Not applicable.

## Shrinkage

Rubber Not applicable.
Generic Polymer Not applicable
Composite Not applicable.
(Concrete creep model to EUROCODE_2)
MATERIAL PROPERTIES NONLINEAR 86 IRC
(Concrete creep model to Indian IRC code of Practice)
DAMAGE PROPERTIES SIMO, OLIVER (Damage)

SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER

## Loading

Prescribed Value PDSP, TPDSP
Concentrated CL Loads
Element Loads ELDS
Prescribed variable. U, V, $\theta$ z: at end nodes.
Concentrated loads. Px, Py, Mx at nodes.
Element loads on nodal line
LTYPE, S1, Px, Py, Mz
LTYPE=11: point loads and moments in local directions.
LTYPE=12: point loads and moments in global directions.
LTYPE, 0, Wx, Wy, Mz
LTYPE=21: uniformly distributed loads in local directions.
LTYPE=22: uniformly distributed loads in global directions.
LTYPE=23: uniformly distributed projected loads in global directions
LTYPE, S1, Wx1, Wy1, Mz1, S2, Wx2, Wy2, Mz2
LTYPE=31: distributed loads in local directions.
LTYPE=32: distributed loads in global directions.
LTYPE=33: distributed projected loads in global directions
LTYPE, S1, Wx, Wy, Mz
LTYPE=41: trapezoidal loads in local directions.
LTYPE=42: trapezoidal loads in global directions.
LTYPE=43: trapezoidal projected loads in global directions

| Distributed Loads | UDL | Uniformly distributed loads. Wx, Wy: forces/unit length/radian in local x , y directions for element. |
| :---: | :---: | :---: |
|  | FLD | Face Loads. Px, Py: local face pressures at nodes. |
|  | FLDG | Not applicable. |
| Body Forces | CBF | Constant body forces for element. Xcbf, Ycbf, $\Omega_{\mathrm{x}}$, $\Omega \mathrm{y}, \Omega_{\mathrm{z}}, \alpha \mathrm{z}$ |
|  | BFP, BFPE | Body force potentials at nodes/for element. $\varphi_{1}, \varphi_{2}$, $0,0, \mathrm{Xcbf}, \mathrm{Ycbf}$ |
| Velocities | VELO | Velocities. Vx, Vy: at nodes. |
| Accelerations | ACCE | Accelerations. Ax, Ay: at nodes. |
| Initial <br> Stress/Strains | SSI, SSIE | Initial stresses/strains at nodes/for element. <br> Components: $0,0,0,0,0,0,0,0,0,0,(\sigma x, \sigma x y$ |
|  |  | $\sigma z, \varepsilon x, \varepsilon x y, \varepsilon z)$ Bracketed terms repeated for each fibre integration point |
|  | SSIG | Initial stresses/strains at Gauss points. These stresses/strains are specified in the same manner as SSI and SSIE. |
| Residual Stresses | SSR, SSRE | Residual stresses at nodes/for element. Components: |
|  |  | $0,0,0,0,0,0,0,0,0,0,(\sigma x, \sigma x y, \sigma z)$ Bracketed terms repeated for each fibre integration point. |
|  | SSRG | Residual stresses at Gauss points for element. |
|  |  | Components: $0,0,0,0,0,0,0,0,0,0,(\sigma x, \sigma x y$, |
|  |  | $\sigma z)$ Bracketed terms repeated for each fibre integration point. |
| Target Stress/Strains | TSSIE, TSSIA | Target stresses/strains at nodes/for element. |
|  |  | Components: $0,0,0,0,0,0,0,0,0,0,(\sigma x, \sigma x y$, |
|  |  | $\sigma z)$ Bracketed terms repeated for each fibre integration point. |
|  | TSSIG | Target stresses/strains at Gauss points. These stresses/strains are specified in the same manner as TSSIE and TSSIA. |
| Temperatures | TEMP, TMPE | Temperatures at nodes/for element. |
|  |  | $\mathrm{T}, 0, \mathrm{dT} / \mathrm{dy}, 0, \mathrm{To}, 0, \mathrm{dTo} / \mathrm{dy}$, 0 : in local directions. |
| Overburden | Not |  |
| Phreatic Surface | Face pressure. | The fluid pressure is applied in the $-y$ direction of the element y axis. |
| Field Loads | Not applicable. |  |
| Temp Dependent | Not |  |

Loads applicable.

## LUSAS Output

Solver Force. Nx, Ne, Mx, Me, Sxy: axial and hoop forces, moments/unit width in local directions, shear force

Strain. $\varepsilon_{x}, \varepsilon_{\square}, \gamma \mathrm{x}, \square \theta$, $\varepsilon_{x y}$ axial, hoop, flexural and shear strains.
Continuum stresses: $\sigma x, \sigma x y, \sigma \theta$ in local directions.
Strain: $\varepsilon_{x}, \varepsilon_{x y}, \varepsilon_{\square}$ : Axial, shear and hoop strains in local directions.
Modeller See Results Tables (Appendix K).

## Local Axes

The local x -axis lies along the line of the element in the direction in which the nodes are numbered. The local y and z -axes form a right-hand set with the local x -axis such that the y axis lies in the global XY-plane with the z -axis parallel to the global Z-axis.

## Sign Convention

Standard shell element. Axial and circumferential moments are positive for tension on element top fibre (the top fibre lies on the positive local y side of the element).

## Formulation

## Geometric Nonlinearity

Total Lagrangian
For large displacements, rotations up to 1 radian, and small strains.
Updated Not applicable. Lagrangian

Eulerian Not applicable.
Co-rotational Not applicable.

## Integration Schemes

Stiffness Default.
Fine (see Options).
Mass Default.

1-point (BXSI2), 2-point (BXSI3).
Same as default.
2-point (BXSI2), 3-point (BXSI3).

Fine (see Options). Same as default.

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule for element
55 Output strains as well as stresses.
87 Total Lagrangian geometric nonlinearity
102 Switch off load correction stiffness matrix due to centripetal acceleration
105 Lumped mass matrix.
134 Gauss to Newton-Cotes in plane (in the local $x$ direction) integration for elements.
139 Output yielded integration points only.

## Notes on Use

1. The element is formulated from the degenerate continuum concept, i.e. enforcing directly the modified Timoshenko hypothesis for thick beams to the continuum theory. Plane cross-sections initially normal to the x axis remain plane and undistorted (the shape of the cross-section remains unchanged) under deformation, but do not necessarily remain normal to the x axis. Shearing deformations are included.
2. The axial force, hoop force, shear force and moments are constant in BXSI2 and vary linearly along the length of the beam in BXSI3.
3. OPTION 36 is only applicable for use with element load types FLD, ELDS, UDL and phreatic surface pressure. Specifying this option makes these element loads follow the element geometry as the analysis progresses.

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature


## Recommendations on Use

The element can be used for analysing linear and nonlinear shell structures which are axisymmetric, e.g. pressure vessels or pipes.

## 3D Flat Thin Shell Elements

## General



TS3


QSI4


Element Group
Element Subgroup

Element Description

A family of flat thin shells in 3D which include a high performance incompatible model. The elements take into account both membrane and flexural deformations. As required by thin plate theory, transverse shearing deformations are excluded. An average thickness value for each element is obtained from the specified nodal thicknesses. Since the elements are formulated in local element axes, directional material properties may be defined relative to the element orientation.

Nodes
Freedoms
Node
Coordinates

3 or 4 numbered anticlockwise.
Shells
Flat Thin Shells

3or
$\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ : at each node.
X, Y, Z: at each node.

## Geometric Properties

Ez, $\mathbf{t} 1 \ldots$ tn Eccentricity and thickness at each node.

## Material Properties

Linear Isotropic:
Orthotropic:

Anisotropic: MATERIAL PROPERTIES ANISOTROPIC 3
MATERIAL PROPERTIES (Elastic: Isotropic) MATERIAL PROPERTIES ORTHOTROPIC (Elastic: Orthotropic Plane Stress) MATERIAL PROPERTIES ORTHOTROPIC SOLID (Elastic: Orthotropic Thick)
(Elastic: Anisotropic Thin Plate)
Rigidities.
Matrix Not applicable Joint Not applicable
Concrete Not applicable Elasto-Plastic Not applicable Creep Not applicable Damage Not applicable Viscoelastic Not applicable

## Shrinkage

Rubber Not applicable
Generic Polymer Not applicable Composite Not applicable

RIGIDITIES 6 (Rigidities: Shell) (D7, D8, D9, D11, D12, D13, D16, D17, D18=0)

## Loading

Prescribed Value PDSP, TPDSP
Concentrated CL
Loads
Element Loads Not applicable.
Distributed Loads UDL
FLD, FLDG
Body Forces CBF
BFP, BFPE

Velocities VELO
Accelerations ACCE
Initial SSI, SSIE
Stress/Strains

Prescribed variable. $\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta_{\mathrm{x}}, \theta_{\mathrm{y}}, \theta_{\mathrm{z}}$ at nodes.
Concentrated loads. Px, Py, Pz, Mx, My, Mz: at nodes.

Uniformly distributed loads. Wx, Wy, Wz: local surface pressures for element (see Notes).
Not applicable.
Constant body forces for element. Xcbf, Ycbf, Zcbf (see Notes).
Body force potentials at nodes/for element. $\varphi_{1}, \varphi_{2}$, $\varphi_{3}$ (see Notes).
Velocities. Vx, Vy, Vz: at nodes.
Accelerations. Ax, Ay, Az: at nodes.
Initial stresses/strains at nodes/for element. Resultants. Nx, Ny, Nxy, Mx, My, Mxy: forces, moments/unit width in local directions. $\varepsilon x, \varepsilon y$, $\gamma \mathrm{xy}, \psi \mathrm{x}, \psi \mathrm{y}, \psi \mathrm{xy}$ : membrane, flexural strains in local directions (see Notes).
Not applicable.
Residual Stresses Not
applicable.
Target TSSIE, TSSIAStress/StrainsResultants. Nx, Ny, Nxy, Mx, My, Mxy: forces,moments/unit width in local directions. $\mathcal{E x}, \mathcal{E}$ y,$\gamma \mathrm{xy}, \psi \mathrm{x}, \psi \mathrm{y}, \psi \mathrm{xy}:$ membrane, flexural strains inlocal directions (see Notes).
TSSIG Not applicable.Temperatures TEMP, TMPETemperatures at nodes/for element. T, $0,0, \mathrm{dT} / \mathrm{dz}$,To, $0,0, \mathrm{dTo} / \mathrm{dz}$ : in local directions. (see Notes)
Overburden Notapplicable.
Phreatic Surface Notapplicable.Field Loads Notapplicable.
Temp Dependent ..... Not
Loads applicable.

## LUSAS Output

Solver Stress resultant: Nx, Ny, Nxy, Mx, My, Mxy: forces, moments/unit width in local directions.

Stress (default): $\sigma \mathrm{x}, \sigma \mathrm{y}, \sigma \mathrm{xy}, \sigma \max , \sigma \mathrm{min}, \beta, \sigma \mathrm{e}$ in local directions (see Notes).

Strain: $\mathcal{E x}, \varepsilon_{y}, \gamma \mathrm{xy}, \psi \mathrm{x}, \psi \mathrm{y}, \psi \mathrm{xy}$ : membrane, flexural strains in local directions.

Modeller See Results Tables (Appendix K).

## Local Axes

$\square$ Standard area element

## Sign Convention

$\square$ Thin shell element

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Stiffness Default. 1-point for the in-plane incompatible modes, (QSI4),
$2 \times 2$ for the in-plane compatible modes, (QSI4), $2 \times 2$ for bending (QSI4).
1-point for in-plane (TS3), 3-point for bending (TS3).
Fine. As default.
Mass Default. 1-point for the in-plane incompatible modes, (QSI4),
$2 \times 2$ for the in-plane compatible modes, (QSI4), $2 \times 2$ for bending (QSI4).
1-point for in-plane (TS3), 3-point for bending (TS3).
Fine. As default.

## Mass Modelling

Lumped mass only.

## Options

32 Suppress stress output but not stress resultants.
34 Outputs stress resultants.
55 Outputs strains as well as stresses.
59 Outputs local direction cosines for elements.
170 Suppresses transfer of shape function arrays to disk.

## Notes on Use

1. The element formulations are based on the standard isoflex approach for the flexural matrices.
2. The variation of membrane stresses within the element can be regarded as constant for TS3 and linear for QSI4. The higher order membrane performance of QSI4 is due to
the addition of four incompatible in-plane displacement modes. The variation of flexural stresses can be regarded as linear for all elements.
3. The stress results are most easily interpreted if the local element axes are all parallel.
4. The elements pass the patch test for mixed triangular and quadrilateral geometry.
5. Stress output to the LUSAS output file is on 4 lines:

- Stresses due to membrane action.
- Top surface stresses due to bending action.
- Top surface stresses due to membrane and bending action.
- Bottom surface stresses due to membrane and bending action.

Gauss point output is not available.
6. All distributed loading will be lumped at the nodes.
7. For effective analysis of curved shell structures, a flat shell element should not extend over more than 15 degrees of arc.
8. Though this element cannot model nonlinear behaviour, it can be mixed with other elements in a nonlinear analysis.
9. A system variable is used to alter the artificial stiffness for in-plane rotations.
10. A fine discretisation will be required to reproduce the correct behavioural response for curved structures. Therefore, the Semiloof shell elements (QSL8,TSL6) or the thick shell elements (QTS8, TTS6) may be more appropriate.
11. The ORTHOTROIC SOLID material model may be used with either composite or non-composite thin shell elements. Using a Solid rather than a Thick orthotropic material means that a local coordinate may be used to orientate the material.
12. Element loading on elements with eccentricity is applied as follows:

- SSI, SSIE, TSSIE, TSSIA, TEMP, TMPE - at the mid-plane of the element.
- UDL, CBF, BFP, BFPE - at the nodal plane.


## Restrictions

A Avoid excessive aspect ratio.
$\square$ Avoid excessive warping.

## Recommendations on Use

- The flat thin shell elements are suitable for modelling both flat and curved thin shell structures which exhibit negligible transverse shear deformations.
- A fine discretisation will be required to reproduce the correct behavioural response for curved structures. Therefore, the Semiloof shell elements (QSL8,TSL6) or the thick shell elements (QTS8, TTS6) may be more appropriate.
- The Semiloof shell elements (QSL8,TSL6) or the thick shell elements (QTS8, TTS6) are more effective for structures containing multiple shell intersections.
- The Semiloof shell elements (QSL8,TSL6) or the thick shell elements (QTS4, QTS8, TTS3, TTS6) may be more effective for eigen-analyses since a consistent mass matrix is available.
- The Semiloof shell elements (QSL8,TSL6) should be utilised for nonlinear analyses.
- The elements can be combined with BMI21 beam elements for analysing ribbed shells with small or no eccentricity. However, the Semiloof shell (QSL8,TSL6) and beam (BSL3,BSL4,BXL4) are more effective for thin ribbed shells with larger eccentricity. For thick ribbed shells with larger eccentricity the thick shell (QTS4, QTS8, TTS3, TTS6) and co-rotational beam (BMI21) are recommended.


## 3D Flat Thin Nonlinear Shell Element

## General

Element Name
TSR6



Element Group Shells
Element
Flat Thin Shells
Subgroup
Element Description

A triangular shell element for the analysis of faceted shell geometries, including multiple branched junctions. The elements can accommodate varying thickness and anisotropic material properties. The element is based on the "Morley shell" formulation and assumes constant membrane and bending strains across the element. As required by thin shell theory, transverse shearing deformations are excluded.
Number Of 6 numbered anticlockwise.
Nodes
Freedoms
$\mathrm{U}, \mathrm{V}, \mathrm{W}:$ at corner nodes. $\theta_{1}$ : (loof rotation) at mid-side nodes (see Notes).
Node X, Y, Z: at each node.
Coordinates

|  | Anisotropic: | MATERIAL PROPERTIES ANISOTROPIC 3 (Elastic: Anisotropic Thin Plate) |
| :---: | :---: | :---: |
|  | Rigidities. | RIGIDITIES 6 (Rigidities: Shell) |
| Matrix | Not applicable |  |
| Joint | Not applicable |  |
| Concrete |  | MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete) |
| Elasto-Plastic | Stress resultant: | MATERIAL PROPERTIES NONLINEAR 29 (Elastic: Isotropic, Plastic: Resultant) (ifcode not required) |
|  | Tresca: | MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain) |
|  | Drucker- <br> Prager: | MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular) |
|  | Mohr- <br> Coulomb: | MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation) |
|  | Volumetric Crushing: | Not applicable. |
|  | Stress <br> Potential | ```STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)``` |
| Creep |  | CREEP PROPERTIES (Creep) |
|  | AASHTO | Not applicable |

CEB-FIP
ChineseNot applicableEurocodeIRC
DamageNot applicableNot applicableNot applicableDAMAGE PROPERTIES SIMO, OLIVER(Damage)
Viscoelastic Not applicable
ShrinkageGENERAL, USER
Rubber Not applicable.
Generic Polymer Not applicable
Composite Not applicable
Loading
Prescribed Value PDSP, TPDSP
Concentrated CL
Loads
Element Loads Notapplicable.
Distributed Loads UDL
FLD, FLDG
Body Forces CBFPrescribed variable. U, V, W: at corner nodes. $\theta_{1}$ : atmid-side nodes.

Prescribed variable. U, V, W: at corner nodes. $\theta_{1}$ : at mid-side nodes.
Concentrated loads. Px, Py, Pz: at corner nodes. M1: at mid-side nodes.

Uniformly distributed loads. Wx, Wy, Wz: midsurface local pressures for element.
Not applicable.
Constant body forces for element. Xcbf, Ycbf, Zcbf,

Phreatic Surface Not applicable.
Field Loads Not applicable.
Temp Dependent Not
Loads applicable.

## LUSAS Output

Solver Stress resultant: Nx, Ny, Nxy, Mx, My, Mxy: forces, moments/unit width in local directions.

Stress (default): $\sigma x, \sigma y, \sigma x y, \sigma \max , \sigma \min , \beta, \sigma e:$ in local directions (see Notes).

Strain: $\mathcal{E x}, \varepsilon_{y}, \gamma x y, \psi x, \psi y, \psi x y$ : membrane, flexural strains in local directions.

Modeller See Results Tables (Appendix K).

## Local Axes

- Standard area element


## Sign Convention

- Thin shell element


## Formulation

## Geometric Nonlinearity

Total Lagrangian Not applicable.
Updated Not applicable.
Lagrangian
Eulerian Not applicable.
Co-rotational For large displacements and rotations

## Integration Schemes

| Stiffness Default. | 1-point |
| :---: | :---: |
| Fine. | 1-point |
| Coarse. | 1-point |
| Mass Default. | 1-point |
| Fine. | 1-point |

## Mass Modelling

$\square$ Consistent mass.

## Options

32 Suppresses stress output but not resultants.
34 Outputs element stress resultants.
55 Outputs strains as well as stresses.
59 Outputs local direction cosines at nodes and Gauss points.
77 Output principal stresses and directions.
139 Output yielded Gauss points only.

## Notes on Use

1. The element formulations are based on a Kirchhoff hypothesis for thin shells.
2. The stresses are constant within the elements.
3. The loof rotations refer to rotations about the element edge at the mid-side nodes. The positive direction of a loof rotation is defined by a right-hand screw rule applied to a vector running in the direction of the lower to higher numbered corner nodes. It should be noted that this direction is enforced on a global level which means that the loof rotations along the adjoining edge of several elements will be consistent in terms of direction and ordering.
4. The element edges must remain straight even though the elements have mid-side nodes.
5. The elements pass the patch test for convergence.
6. Stresse will not be output when using RIGIDITIES or material model 29.
7. The through-thickness integration is performed explicitly for linear analyses and a 5point Newton-Cotes rule is utilised for materially nonlinear analyses with continuum material models. The through-thickness integration rules are as follows:

- Linear models: 3-layers.
- Nonlinear models: 5-layers.


## Restrictions

$\square$ Ensure mid-side node centrality and straight element edges

- Avoid excessive aspect ratio


## Recommendations on Use

- These elements may be utilised for analysing flat and faceted 3D shell structures where the transverse shear effects do not influence the solution. The configuration of the nodal freedoms provides an element suitable for modelling intersecting shells.
- The elements are recommended for geometrically nonlinear problems where large displacements and rotations occur. The single Gauss point integration scheme gives rise to a computationally efficient solution, however, the mesh may need to be refined if there is an unacceptable differentiation in stresses between adjacent elements..


## Semiloof Curved Thin Shell Elements

## General



QSL8

Element
Subgroup
Element Description

Number Of
Nodes
Freedoms

TSL6


Shells
Semiloof Shells . . . . geometries, including multiple branched junctions. The elements can accommodate generally curved geometry with varying thickness and accommodate generally curved geometry with varying thickness and
anisotropic and composite material properties. The element formulation takes account of both membrane and flexural deformations. As required by thin shell theory, transverse shearing deformations are excluded. 6 or 8 numbered anticlockwise.
$\mathrm{U}, \mathrm{V}, \mathrm{W}$ : at corner nodes. $\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta_{1}, \theta_{2}$ : (loof rotations) at mid-side nodes (see Notes).
Node $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.


Semiloof Shell
A family of shell elements for the analysis of arbitrarily curved shell

## Geometric Properties

t1... tn Thickness at each node. Also see Composite Geometry data chapter.

## Material Properties

Linear Isotropic: MATERIAL PROPERTIES (Elastic: Isotropic)

| Orthotropic: | MATERIAL PROPERTIES ORTHOTROPIC <br> (Elastic: Orthotropic Plane Stress) <br> MATERIAL PROPERTIES ORTHOTROPIC |
| :--- | :---: |
|  | SOLID (Elastic: Orthotropic Solid) |
| Anisotropic: | MATERIAL PROPERTIES ANISOTROPIC 3 <br> (Elastic: Anisotropic Thin Plate) |
| Rigidities. | RIGIDITIES 6 (Rigidities: Shell) |
| Not applicable |  |

Joint Not applicable

Concrete

Elasto-Plastic Stress resultant:

Tresca:

Drucker-
Prager:

Mohr-

> Coulomb:

Volumetric Not applicable.
Crushing:

## Creep

Stress Potential STRESS POTENTIAL VON_MISES, HILL, HOFFMAN
(Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
MATERIAL PROPERTIES NONLINEAR 29
(Elastic: Isotropic, Plastic: Resultant) (ifcode not required)

MATERIAL PROPERTIES NONLINEAR 61
(Elastic: Isotropic, Plastic: Tresca, Hardening:
Isotropic Hardening Gradient, Isotropic Plastic
Strain or Isotropic Total Strain)
MATERIAL PROPERTIES NONLINEAR 64
(Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)

MATERIAL PROPERTIES NONLINEAR 65
(Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)

REEP PROPERTIES (Creep)

|  | AASHTO | MATERIAL PROPERTIES NONLINEAR 86 AASHTO <br> (Concrete creep model to AASHTO code of Practice) |
| :---: | :---: | :---: |
|  | CEB-FIP | MATERIAL PROPERTIES NONLINEAR 86 CEBFIP (Concrete creep model to CEB-FIP Model Code 1990) |
|  | Chinese | MATERIAL PROPERTIES NONLINEAR 86 CHINESE <br> (Chinese creep model to Chinese Code of Practice) |
|  | Eurocode | MATERIAL PROPERTIES NONLINEAR 86 EUROCODE <br> (Concrete creep model to EUROCODE_2) |
|  | IRC | MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice) |
| Damage |  | DAMAGE PROPERTIES SIMO, OLIVER (Damage) |
| Viscoelastic | Not applicable |  |
| Shrinkage |  | SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER |
| Rubber | Not applicable. |  |
| Generic Polymer | Not applicable |  |
| Composite | Composite shell: | COMPOSITE PROPERTIES |

## Loading

Prescribed Value PDSP, TPDSP Prescribed variable. U, V, W: at corner nodes. U, V, $\mathrm{W}, \theta_{1}, \theta_{2}$ : at mid-side nodes.
Concentrated CL

Loads
Element Loads Not applicable.
Distributed Loads UDL

FLD, FLDG
Body Forces CBF

BFP, BFPE

## Velocities VELO <br> Accelerations ACCE <br> Initial SSI, SSIE <br> Stress/Strains

SSIG

## Residual Stresses <br> SSR, SSRE <br> SSRG

$\mathrm{Py}, \mathrm{Pz}, \mathrm{M}_{1}, \mathrm{M}_{2}$ : at mid-side nodes.

Uniformly distributed loads. Wx, Wy, Wz: midsurface local pressures for element.
Not applicable.
Constant body forces for element. Xcbf, Ycbf, Zcbf, $\Omega_{\mathrm{x}}, \Omega_{\mathrm{y}}, \Omega_{\mathrm{z}}, \alpha \mathrm{x}, \alpha \mathrm{y}, \alpha_{\mathrm{z}}$
Body force potentials at nodes/for element. $\varphi_{1}, \varphi_{2}$, $\varphi_{3}, 0, \mathrm{Xcbf}, \mathrm{Ycbf}, \mathrm{Zcbf}$, where $\varphi_{1}, \varphi_{2}, \varphi_{3}$ are the face loads in the local coordinate system.
Velocities. Vx, Vy, Vz: at nodes.
Accelerations. Ax, Ay, Az: at nodes.
Not applicable.
Initial stresses/strains at Gauss points.
(1) Resultants (for linear analysis and model 29) Nx, Ny, Nxy, Mx, My, Mxy, $\varepsilon x, \varepsilon_{y}, \gamma x y, \psi x, \psi y$, $\psi x y$ : forces, moments/unit width and membrane/flexural strains in local directions.
(2) Components (for all other nonlinear material models) are: $0,0,0,0,0,0,0,0,0,0,0,0,(\sigma x$, $\sigma y, \sigma x y, \varepsilon x, \varepsilon y, \gamma x y)$ - with the bracketed terms repeated for each of the five layers. (See note 7 in the Notes of Use) section.
Not applicable.
Residual stresses at Gauss points.
(1) Resultants (for model 29) Nx, Ny, Nxy, Mx, My, Mxy: forces, moments/unit width in local directions.
(2) Components (for all other nonlinear material models) are: $0,0,0,0,0,0,0,0,0,0,0,0,(\sigma x, \sigma y$, $\sigma x y)$ - with the bracketed terms repeated for each of the five layers. (See note 7 in the Notes of Use) section.
Target TSSIE, TSSIA Stress/Strains

TSSIG

Not applicable.
Target stresses/strains at Gauss points.
(1) Resultants (for linear analysis and model 29) Nx, Ny, Nxy, Mx, My, Mxy, $\varepsilon x, \varepsilon y, \gamma x y, \psi x, \psi y$, $\psi \mathrm{xy}$ : forces, moments/unit width and
membrane/flexural strains in local directions.
(2) Components (for all other nonlinear material models) are: $0,0,0,0,0,0,0,0,0,0,0,0,(\sigma x$, $\sigma y, \sigma x y, \varepsilon x, \varepsilon y, \gamma x y)$ - with the bracketed terms repeated for each of the five layers. (See note 7 in the Notes of Use) section.

# Temperatures TEMP, TMPE Temperatures at nodes/for element. T, $0,0, \mathrm{dT} / \mathrm{dz}$, To, $0,0, \mathrm{dTo} / \mathrm{dz}$ 

## Overburden Not

 applicable.Phreatic Surface Not applicable.
Field Loads Not applicable.

## Temp Dependent Not

Loads applicable.

## LUSAS Output

Solver Stress resultant: Nx, Ny, Nxy, Mx, My, Mxy: forces, moments/unit width in local directions.
Stress (default): $\sigma x, \sigma y, \sigma x y, \sigma \max , \sigma \min , \beta, \sigma \mathrm{e}$ : in local directions (see Notes).

Strain: $\mathcal{E x}, \varepsilon y, \gamma x y, \psi x, \psi y, \psi x y:$ membrane, flexural strains in local directions.
Modeller See Results Tables (Appendix K).

## Local Axes

- Local y axis The local element $y$-axis at a point coincides with a curvilinear line $\xi=$ constant in the natural coordinate system which lies in the shell mid-surface.
- Local $x$ axis The local $x$-axis at a point is perpendicular to the local $y$-axis in the positive $\eta$ direction and is tangential to the shell mid-surface.
- Local z axis The local z -axis forms a right-hand set with the x and y axes and the direction is given by the ordering of the element nodes according to a right-hand screw rule. The local z -axis + ve direction defines the element top surface.


## TSL6



## QSL8



## Sign Convention

- Thin shell element (seeNotes).


## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements, rotations up to 1 radian and small strains.
Updated For large displacements, rotation increments up to 1 radian and small Lagrangian strains.

Eulerian Not applicable.
Co-rotational Not applicable.

## Integration Schemes

Stiffness Default. 3-point (TSL6), 5-point (QSL8).
Fine (see $3 \times 3$ (QSL8)
Options).
Coarse (see 2x2 (QSL8)
Options).
Mass Default. 3-point (TSL6), 5-point (QSL8).
Fine (see ..... $3 \times 3$ (QSL8)
Options).
Mass Modelling
$\square$ Consistent mass (default).
$\square$ Lumped mass.
Options
18 Invokes fine integration rule.
19 Invokes coarse integration rule.
32 Suppresses stress output but not resultants.
34 Outputs element stress resultants.
54 Updated Lagrangian geometric nonlinearity.
55 Outputs strains as well as stresses
59 Outputs local direction cosines at nodes and Gauss points.
87 Total Lagrangian geometric nonlinearity.
102 Switch off load correction stiffness due to centripetal acceleration.
105 Lumped mass matrix.
138 Output yield flags only.
139 Output yielded Gauss points only.
169 Suppress extrapolation of stresses to nodes.
170 Suppress transfer of shape function arrays to disk.

## Notes on Use

1. The element formulations are based on a Kirchhoff hypothesis for thin shells.
2. The variation of stresses within the elements may be regarded as linear.
3. The loof rotations refer to rotations about the element edge at the loof points. The positive direction of a loof rotation is defined by a right-hand screw rule applied to a vector running in the direction of the lower to higher numbered corner nodes. It should be noted that this direction is enforced on a global level which means that the loof rotations along the adjoining edge of several elements will be consistent in terms of direction and ordering. The ordering is such that loof point 1 is located between the lower numbered node and the appropriate mid-side node. Similarly loof point 2 lies between the mid-side node and the higher numbered node along an element edge. The loof rotations are actually specified at the element mid-side nodes.
4. The elements pass the patch test for convergence for mixed triangular and quadrilateral element geometry.
5. Stress output to the LUSAS output file is on 4 lines:

- Stresses due to membrane action.
- Top surface stresses due to bending action.
- Top surface stresses due to membrane and bending action.
- Bottom surface stresses due to membrane and bending action.

6. Stresses will not be output when using RIGIDITIES or material model 29. Averaged stresses will not be processed when using RIGIDITIES.
7. The through-thickness integration is performed explicitly for linear analyses and a 5point Newton-Cotes rule is utilised for materially nonlinear analyses with continuum material models. The through-thickness integration rules are as follows:

- Linear models: 3-layers.
- Nonlinear models: 5-layers.
- Composite model: Variable.

8. The quadrature points of the 3-point rule are non-standard.
9. The coarse $2 * 2$ quadrature rule provides the most effective element if the mesh is highly constrained. However, the element possesses two mechanisms, the usual inplane hourglass mechanism encountered when reduced integration is utilised with 8noded elements and an out of plane mechanism. The in-plane mechanism is rarely activated but the out-of-plane mechanism may be more troublesome, particularly where elements are regular and have one zero principal curvature, e.g. a cylinder subject to internal pressure. Provided the mechanisms are not activated the element with $2 * 2$ provides the best results.
10. The 5-point quadrature rule provides an element with a performance below that of the element with $2 * 2$ quadrature, but considerably better than the element with $3 * 3$ quadrature. However, the element possesses a 'near' mechanism which may be activated for lightly constrained meshes, particularly if out of plane loads are present.
11. The middle integration point of the 5 point rule is only implemented as a method of reducing the excitation of spurious modes (or mechanisms) which are present with the $2 * 2$ integration rule. The 5 th integration point is actually weighted with an arbitrarily small value which has the effect of stabilising the results. For these reasons, values from the middle integration point are not taken into account for the nodal extrapolation.
12. The $3 * 3$ quadrature rule provides an element that has no mechanisms but tends to provide over-stiff solutions. Therefore, a finer discretisation is required than if the 5point quadrature rule is used.

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature

Avoid excessive aspect ratio

## Recommendations on Use

- These elements may be utilised for analysing flat and curved 3D shell structures where the transverse shear effects do not influence the solution. The configuration of the nodal freedoms provides an element suitable for modelling intersecting shells, e.g. tubular joints and also for use with solid elements (HX20).
- The elements may be combined with the Semiloof beam (BSL3,BSL4,BXL4) for analysing ribbed plates and shells.


## 3D Thick Shell Elements

## General



## TTS3



QTS4


## TTS6



QTS8


## Element Group <br> Element <br> Subgroup <br> Element Description

Shells
Thick Shells

A family of shell elements for the analysis of arbitrarily thick and thin curved shell geometries, including multiple branched junctions. The quadratic elements can accommodate generally curved geometry while all elements account for varying thickness. Anisotropic and composite material properties can be defined. These degenerate continuum elements are also capable of modelling warped configurations. The element formulation takes account of membrane, shear and flexural deformations. The quadrilateral elements use an assumed strain field to define transverse shear which ensures that the element does not lock when it is thin (see Notes).
Number Of 3, 4, 6 or 8 numbered anticlockwise. Nodes
Freedoms Default: 5 degrees of freedom are associated with each node U, V, W, $\theta \alpha, \theta \beta$. To avoid singularities, the rotations $\theta \alpha$ and $\theta \beta$ relate to axes


## Geometric Properties

$\mathbf{e x}_{\text {, }}, \mathbf{t} \ldots$... $\mathrm{tn}^{\text {Eccentricity }}$ and thickness at each node.

## Material Properties

| Linear | Isotropic: | MATERIAL PROPERTIES (Elastic: Isotropic) |
| :---: | :---: | :---: |
|  | Orthotropic: | MATERIAL PROPERTIES ORTHOTROPIC <br> THICK (Elastic: Orthotropic Thick) <br> MATERIAL PROPERTIES ORTHOTROPIC <br> SOLID (Elastic: Orthotropic Thick) |
|  | Anisotropic: | MATERIAL PROPERTIES ANISOTROPIC 5 (Elastic: Anisotropic Thick Plate) |
|  | Rigidities. | Not applicable. |
| Matrix | Not applicable |  |
| Joint | Not applicable |  |
| Concrete |  | MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete) |
| Elasto-Plastic | Stress resultant: | Not applicable. |
|  | Tresca: | MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain) |
|  | Drucker- <br> Prager: | MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular) |
|  | MohrCoulomb: | MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation) |
|  | Volumetric | Not applicable. |



## Loading

Prescribed Value PDSP, TPDSP

Concentrated CL

Prescribed variable. 5 degrees of freedom: U, V, W, $\theta \alpha, \theta \beta$ or 6 degrees of freedom: $\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}$, $\theta z$
Concentrated loads. 5 degrees of freedom: Px, Py,

| Loads |  | $\mathrm{Pz}, \mathrm{M} \alpha, \mathrm{M} \beta$, where $\mathrm{M} \alpha$ and $\mathrm{M} \beta$ relate to axes defined by $\theta \alpha$ and $\theta \beta$ respectively. 6 degrees of freedom: Px, Py, Pz, Mx, My, Mz. |
| :---: | :---: | :---: |
| Element Loads | Not applicable. |  |
| Distributed Loads | UDL | Uniformly distributed loads. Wx, Wy, Wz: midsurface local pressures for element (see Notes). |
|  | FLD, FLDG | Not applicable. |
| Body Forces | CBF | Constant body forces for element. Xcbf, Ycbf, Zcbf, $\Omega_{\mathrm{x}}, \Omega_{\mathrm{y}}, \Omega_{\mathrm{z}}, \alpha_{\mathrm{x}}, \alpha_{\mathrm{y}}, \alpha_{\mathrm{z}}$ (see Notes). |
|  | BFP, BFPE | Body force potentials at nodes/for element. $\varphi_{1}, \varphi_{2}$, $\varphi_{3}, 0, \mathrm{Xcbf}, \mathrm{Ycbf}, \mathrm{Zcbf}$, where $\varphi_{1}, \varphi_{2}, \varphi_{3}$ are the face loads in the local coordinate system (see Notes). |
| Velocities | VELO | Velocities. Vx, Vy, Vz: at nodes. |
| Accelerations | ACCE | Accelerations. Ax, Ay, Az: at nodes. |
| Initial Stress/Strains | SSI, SSIE | Initial stresses/strains at nodes/for element (see Notes). |
|  | SSIG | Initial stresses/strains at Gauss points. Stress/strain components relating to local axes at Gauss points: |
|  |  | $\sigma x, \sigma y, \sigma x y, \sigma y z, \sigma x z, \varepsilon x, \varepsilon y, \gamma x y, \gamma y z, \gamma x z$. All of these 10 terms are repeated for each fibre integration point through the thickness (see Notes). |
| Residual Stresses | SSR, SSRE | Not applicable. |
|  | SSRG | Residual stresses at Gauss points. Stress components relating to local axes at Gauss points: $\sigma x, \sigma y$, |
|  |  | $\sigma x y, \sigma y z, \sigma x z$ all of these 5 terms are repeated for each fibre integration point through the thickness (see Notes). |
| Target Stress/Strains | TSSIE, TSSIA | Target stresses/strains at nodes/for element (see Notes). |
|  | TSSIG | Target stresses/strains at Gauss points. Stress/strain components relating to local axes at Gauss points: |
|  |  | $\sigma x, \sigma y, \sigma x y, \sigma y z, \sigma x z, \varepsilon x, \varepsilon y, \gamma_{x y}, \gamma y z, \gamma x z$. All of these 10 terms are repeated for each fibre integration point through the thickness (see Notes). |
| Temperatures | TEMP, TMPE | Temperatures at nodes/for element. T, $0,0, \mathrm{dT} / \mathrm{dz}$, To, $0,0, \mathrm{dTo} / \mathrm{dz}$ (see Notes). |
| Overburden | Applicable. |  |
| Phreatic Surface | Applicable. |  |
| Field Loads | Not applicable. |  |

## Temp Dependent Not applicable. Loads

## LUSAS Output

Solver Stress resultant: Nx, Ny, Nxy, Mx, My, Mxy, Sx, Sy: forces, moments/unit width in local directions.

Stress (default): $\sigma x, \sigma y, \sigma x y, \sigma y z \sigma x z, \sigma e$ in local directions (see Notes).

Strain: $\varepsilon x, \varepsilon_{y}, \gamma \mathrm{xy}, \gamma \mathrm{yz}, \gamma_{\mathrm{xz}}, \varepsilon_{\mathrm{e}}$ in local directions (see Notes).
Modeller See Results Tables (Appendix K).

## Local Axes

The local element $x$-axis at a point coincides with a curvilinear line $\eta=$ constant in the natural coordinate system which lies in the shell mid-surface. The local z -axis at a point is obtained from the cross product of a curvilinear line $\xi=$ constant in the natural coordinate system and the local x -axis. The local y -axis forms a right-hand set with the x and z axes and the direction is given by the ordering of the element nodes according to a right-hand screw rule. The local z -axis +ve direction defines the element top surface.

## TTSTTS6



QTS8


## Sign Convention

$\square$ Thick shell element (seeNotes).

## Formulation

## Geometric Nonlinearity

Total Lagrangian For large displacements, large rotations and small strains.
Updated Not applicable.
Lagrangian
Eulerian Not applicable.
Co-rotational Not applicable.

## Integration Schemes

| Stiffness | Default. | 1-point (TTS3), 3-point (TTS6), 2x2 (QTS4, QTS8). |
| :---: | :--- | :--- |
|  | Fine (see Options). | 3-point (TTS3), 5-point (QTS8) |
| Mass | Default. | 1-point (TTS3), 3-point (TTS6), 2x2 (QTS4, QTS8). |
|  | Fine (see Options). | 3-point (TTS3), 5 point (QTS8) |

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule.
32 Suppresses stress output but not resultants.
34 Outputs element stress resultants.
55 Outputs strains as well as stresses.
59 Outputs local direction cosines at nodes and Gauss points.
77 Outputs principal stresses.
87 Total Lagrangian geometric nonlinearity.
102 Switch off load correction stiffness due to centripetal acceleration.
105 Lumped mass matrix.
110 Use assumed shear strain field for TTS6 and QTS8 thick shell elements.
139 Output yielded Gauss points only.
169 Suppress extrapolation of stresses to nodes.
171 Switch off assumed strain field for QTS4 elements.
278 Six degrees of freedom.
396 Invokes the improved transverse shear calculation ('on' by default for models created by version 14.4 and above, and 'off' - for models created by previous
versions).
417 Introduce residual bending flexibility correction for 3-node thick shell TTS3.
422 Use assumed transverse shear strain field for TTS3 thick shell element.

## Notes on Use

1. For TTS3 elements all moments and shears are constant for the element. For QTS4 the variations of moments, out of plane shears and in-plane loads is near-constant and the variation of in-plane shear is near-linear. For TTS6 and QTS8 elements the variation of moments and in-plane shear is near-linear while the variation of out of plane shears is near constant.
2. Shear locking is much more of an issue for lower order elements, and hence an assumed shear strain field is always switched on for TTS3/QTS4 elements; if it were switched off, these elements would always lock and perform very badly. Higher order elements are less prone to shear locking, and the situation is not quite so clear cut. It has been found that using an assumed shear strain field with QTS8 elements when transverse shear strain dominates can lead to poor results. The view has therefore been taken that the assumed shear strain field should be switched off by default for the higher order TTS6/QTS8 elements.
3. The QTS8 element fails the shear patch test when the assumed strain field is utilised with $2 * 2$ or 5 point integration rule. When carrying out analyses involving these elements that are dominated by transverse shear effects, e.g. a shear wall, it is recommended, as discussed above, that the assumed strain field is disabled. This is the default setting for QTS8 elements. Option 110 may be used to invoke the assumed strain interpolation but this is not recommended for general use.
4. The assumed strain field is invoked automatically for QTS4 elements. The assumed strain field may be revoked for QTS4 by specifying Option 171.
5. The introduction of assumed transverse shear strains (Option 422) significantly improves the performance of the TTS3 element. The RBF correction (Option 417) further improves the TTS3 element, especially for very thin shells. For elasto-plastic materials, the correction matrix is computed using the linear material properties
6. Continuum stresses (and strains using Option 55) at each fibre integration point are output by default. For linear materials these stresses relate to the top, middle and bottom surfaces of the element. If a nonlinear material is specified then stresses are output at 5 points through the thickness after material yield.
7. Option 55 must be specified if nonlinear state variables are to be written to the LUSAS output file.
8. The through-thickness integration rules are as follows:

- Linear material models: 3-layers.
- Nonlinear material models: 5-layers.
- Composite model: variable.

7. Initial stresses/strains must be specified at 3 layers for a linear material or 5 layers for a nonlinear material. Residual stresses must be specified for 5 layers. In all instances the stresses/strains are specified sequentially from the bottom surface to the top.
8. There are usually 2 rotational degrees of freedom and a common nodal normal associated with each node giving a smooth surface to the shell assembly:


The direction of the axes defining the rotations depends upon the orientation of the normal at a node (see Thick Shell Nodal Rotation). In certain circumstances 3 rotational degrees of freedom relating to global axes will be assigned to a node. This is done automatically:

- When connecting with beam elements, joint elements or other types of shells, eg.QSI4.
- When a Concentrated Load is applied in LUSAS Modeller.
- When a Support is applied in LUSAS Modeller.
- When the angle between adjacent shell normals exceeds the SYSTEM parameter SHLANG (see below).
- When option 278 is specified.

If Option 278 is specified then all nodes for these shell element types will be assigned six global degrees of freedom. To overcome the problems associated with in-plane drilling rotations an artificial stiffness is automatically included for the rotation about the shell normal. The use of Option 278 is not recommended for analyses that involve large displacements or rotations. LUSAS Modeller will automatically specify Option 278 but it can be switched off in Modeller via File > Model Properties > Solution > Element options.
Option 278 should be switched off if QTS4 elements are to be used to model thick curved shells in which membrane action leads to a significant difference between the in-plane strains in the top and bottom surface of the shell. If Option 278 is not disabled under these circumstances the moments associated with this in-plane strain
differential are not accurately accounted for. An alternative approach would be to switch to QTS8 elements as these elements produce more accurate moments under these conditions.

When the maximum angle between adjacent normals at a node is greater than 20 degrees, e.g., branched shell structures. ( 20 degrees is a default value which may be changed using the SYSTEM parameter SHLANG); if the nodal freedom command has not been specified for that node.

9. A system variable (STFINP) is used to alter the artificial stiffness for in-plane rotations. This system parameter can only be used in conjunction with Option 278.
10. The desired number of rotational degrees of freedom for a node may be enforced through the NODAL FREEDOMS data input. Care must be taken if 6 degrees of freedom are specified in this manner as a singularity may occur if appropriate in-plane rotations are not restrained. This facility is provided together with the TRANSFORMED FREEDOMS data chapter to allow more flexibility in the specification of boundary conditions. In these circumstances, the in-plane rotation about the normal of the shell must usually be restrained to avoid singularities. In general, wherever possible, 5 degrees of freedom should be used when the shell surface is smooth.
11. The TTS3 and QTS8 elements possess one out of plane mechanism when using the default integration rules. The 3 noded element is most effective using the one point rule.
12. The through-thickness integration is performed by utilising a 3 point Newton-Cotes rule for linear materials and a 5 point rule for nonlinear materials and creep. In an analysis involving material nonlinearity, a 3 point rule is used until the material yields and then a 5 point rule is invoked.
13. The thick shell formulation assumes constant transverse shear deformation. In the post-processing stage, after the application of the constitutive relationship, this results in a constant transverse shear stress. This result can be improved by taking into
account the true parabolic shear stress distribution while preserving the same shear resultant. Thus, when Option 396 is used, the transverse shear stresses for a nonlayered shell are set to zero at the top and bottom and to 1.5 times the constant value at the middle. For a layered shell, the distribution of the transverse shear depends on the in-plane stiffness of the layers. The output results are for the middle of the layer, thus the top and bottom layers will not have zero transverse shear.
14. The ORTHOTROPIC SOLID material model may be used with either composite or non-composite thick shell elements. Using a Solid rather than a Thick orthotropic material means that a local coordinate may be used to orientate the material.
15. If applying an initial stress/strain or thermal load that varies across an element, a higher order element ( 6 or 8 nodes) should be used. A limitation of the standard isoparametric approach when used for lower order elements ( 3 or 4 nodes) is that only constant stress/strain fields can be imposed correctly.
16. For an element with eccentricity the following load types are applied at the mid-plane of the element (not the nodal plane): UDL, CBF, BFP, BFPE, SSI, SSIE, SSIG, SSRG, TSSIE, TSSIA, TSSIG, TEMP, TMPE.
17. The Smoothed Multi Crack Concrete Model (109) can be used with this element, however, due to the "plane sections remaining plane" hypothesis, crack widths cannot be computed.

## Restrictions

Ensure mid-side node centrality
$\square$ Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio

## Recommendations on Use

- These elements may be utilised for analysing flat and curved 3D shell structures where it is necessary to account for transverse shear. This typically involves thick shell structures where transverse shear deformation can have a considerable influence on the response. The degenerate continuum formulation also allows the low order quadrilateral element (QTS4) to successfully model warped shell configurations.
- The elements may be used for modelling intersecting shells or branched shell junctions. In this instance the nodal rotation freedoms are transformed to relate to the global axes. For modelling stiffened shell structures, the shells may be connected to beam elements BMI21.
- This family of thick shell elements offers a consistent formulation of the tangent stiffness which makes them particularly effective in geometrically nonlinear applications.
- Be aware that when the shell is defined with eccentricity to a reference surface and this reference surface does not pass through the centroid of the cross section,
membrane forces or displacements prescribed/calculated at the nodes will cause bending.


# Chapter 7 : Membrane Elements. 

## 2D Axisymmetric Membrane Elements

## General

## Element Name

BXM2



BXM3



## Geometric Properties

t1... tn Thickness at each node.

## Material Properties

Linear Isotropic:
MATERIAL PROPERTIES (Elastic: Isotropic)
Matrix Not applicable
Joint Not applicable
Concrete Not applicable
Elasto-Plastic Tresca:
MATERIAL PROPERTIES NONLINEAR 61
(Elastic: Isotropic, Plastic: Tresca, Hardening:

Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)<br>Drucker-Prager: MATERIAL PROPERTIES NONLINEAR 64<br>(Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)<br>Mohr-Coulomb: MATERIAL PROPERTIES NONLINEAR 65<br>(Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)<br>Optimised Implicit<br>Von Mises:<br>Volumetric<br>MATERIAL PROPERTIES NONLINEAR 75<br>(Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic \& Kinematic)<br>Not applicable.<br>Crushing:<br>Stress Potential<br>Creep<br>Damage<br>Viscoelastic<br>Not applicable Shrinkage<br>Rubber Ogden:<br>Mooney-Rivlin:<br>Neo-Hookean:<br>Hencky:<br>Generic Polymer Not applicable<br>Composite Not applicable<br>Field Not applicable

## Loading

Prescribed Value PDSP, TPDSP
Concentrated CL Loads
Element Loads Not applicable.

Prescribed variable. U, V: at nodes.
Concentrated loads. Px, Py: at nodes.


## LUSAS Output

Solver
Stress (default): $\sigma x, \sigma_{\theta}$ : axial, circumferential stress.
Strain: $\varepsilon_{x}, \varepsilon_{\theta}$ : axial, circumferential strain.

## Modeller See Results Tables (Appendix K).

Local AxesStandard line element
Sign ConventionStandard membrane element
Formulation
Geometric Nonlinearity
Total Lagrangian For large displacements and small strains.
Updated Not applicable.
Lagrangian
Eulerian Not applicable.
Co-rotational Not applicable.
Integration Schemes
Stiffness Default. 1-point (BXM2), 2-point (BXM3).Fine (see2-point (BXM2).Options).
Mass Default. 1-point (BXM2), 2-point (BXM3).Fine (see2-point (BXM2).
Mass Modelling
Consistent mass (default).
$\square$ Lumped mass.
Options
18 Invokes fine integration rule.
36 Follower loads (see Notes).
47 Use the X-axis as the axis of symmetry.
55 Output strains as well as stresses.

87 Total Lagrangian geometric nonlinearity.
105 Lumped mass matrix.
170 Suppress transfer of shape function arrays to disk

## Notes on Use

1. The element formulation is based on the standard isoparametric approach.
2. The variation of stress along the element is constant for BXM2 and linear for BXM3.
3. To apply a non-conservative (follower) pressure load (load type FLD), Option 36 must be specified. Note that this load should be normal to the face and constant for all the nodes of the element. Follower load can only be used with BXM2 elements.
4. The elements should not be used as 'stand-alone' elements if any bending effects are present. The thin axisymmetric shell element BXS3 should be used for this case.
5. The BXM3 element has a zero energy mode which may be excited if the midside node is free and not connected to any other element.
6. When BXM2 elements are used with either variable nodal thicknesses, temperature dependent material properties or utilised in materially nonlinear analyses the 2-point Gauss rule is most effective.

## Restrictions

$\square$ Ensure mid-side node centrality

- Avoid excessive element curvature

Rubber material models can only be used with element BXM2 and must be used with Total Lagrangian geometric nonlinearity (Option 87).

## Recommendations on Use

The elements may be used alone to model circular plates or pipes, or coupled with axisymmetric solid elements to provide stiffeners, e.g. radial reinforcement.

## 3D Space Membrane Elements

## General



TSM3


SMI4


## Element Group <br> Membranes

Element
Space Membranes
Subgroup
Element
Description
A family of space membrane elements in 3D which include a high performance incompatible model (SMI4 only). The elements are intended for 3D membrane structures (they possess no bending stiffness). The elements are formulated in the local element axes which allows directional material properties to be defined relative to the element orientation. The elements can accommodate varying thickness.
Number Of 3 or 4 numbered anticlockwise.
Nodes
Freedoms
Node
$\mathrm{U}, \mathrm{V}, \mathrm{W}$ : at each node.
$\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.

## Geometric Properties

## t1... tn Thickness at each node.

## Material Properties

| Linear | Isotropic: | MATERIAL PROPERTIES (Elastic: Isotropic) |
| :--- | :--- | :--- |
|  | Orthotropic: | MATERIAL PROPERTIES ORTHOTROPIC |
|  |  | (Elastic: Orthotropic Plane Stress) |
|  | Anisotropic: | MATERIAL PROPERTIES ANISOTROPIC 3 |
|  |  | (Elastic: Anisotropic Thin Plate) |
|  | Rigidities: | RIGIDITIES 3 (Rigidities: Membrane/Thin |
|  |  | Plate) |

Matrix Not applicableJoint Not applicable
Concrete Not applicable
Elasto-Plastic Not applicable
Creep Not applicable
Damage Not applicable
Viscoelastic Not applicable
Shrinkage
Rubber Not applicable
Generic Polymer Not applicable
Composite Not applicable
LoadingPrescribed Value PDSP, TPDSP
Concentrated CL
Loads
Element Loads ..... Notapplicable.
Distributed Loads UDLFLD, FLDGBody Forces CBFBFP, BFPEVelocities VELOAccelerations ACCEInitial SSI, SSIE
Stress/StrainsSSIG
Residual Stresses Notapplicable.Target TSSIE, TSSIAStress/Strains
SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER

Prescribed variable. U, V, W: at nodes.
Concentrated loads. Px, Py, Pz: at nodes.

Uniformly distributed loads. Wx, Wy, Wz: local surface pressures for element.
Not applicable.
Constant body forces for element. Xcbf, Ycbf, Zcbf, $\Omega_{\mathrm{x}}, \Omega_{\mathrm{y}}, \Omega_{\mathrm{z}}, \alpha \mathrm{x}, \alpha \mathrm{y}, \alpha \mathrm{z}$
Body force potentials at nodes/for element. $\varphi_{1}, \varphi_{2}$, ب3
Velocities. Vx, Vy, Vz: at nodes.
Accelerations. Ax, Ay, Az: at nodes.
Initial stresses/strains at nodes/for element. $\mathrm{Nx}, \mathrm{Ny}$, Nxy : forces in local directions. $\varepsilon x, \varepsilon y, \gamma \mathrm{xy}$ : membrane strains in local directions.
Initial stresses/strains at Gauss points. Nx, Ny, Nxy: forces in local directions. $\varepsilon x, \varepsilon y, \gamma x y$ : membrane strains in local directions.
membrane strains in local directions.
TSSIG
Target stresses/strains at Gauss points. Nx, Ny, Nxy: forces in local directions. $\varepsilon x, \varepsilon y, \gamma x y$ : membrane strains in local directions.
Temperatures TEMP, TMPE Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0,0
Overburden Not applicable.
Phreatic Surface Not applicable.
Field Loads Not applicable.
Temp Dependent Not
Loads applicable.

## Output

Solver Stress resultant: $\mathrm{Nx}, \mathrm{Ny}, \mathrm{Nxy}$, Nmax, Nmin, $\beta$ : forces/unit length in local directions.

Stress (default): $\sigma x, \sigma y, \sigma x y, \sigma \max , \sigma \min , \beta$ : membrane stresses in local directions.

Strain: $\varepsilon x, \varepsilon y, \gamma \mathrm{xy}, \varepsilon \max , \varepsilon \min , \beta$ : membrane strains in local directions.
Modeller See Results Tables (Appendix K).

## Local Axes

- Standard area element


## Sign Convention

$\square$ Standard membrane element
Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Stiffness Default. 1-point (TSM3), 2x2 (SMI4).
Fine. As default.
Mass Default. 1-point (TSM3), 2x2 (SMI4).
Fine. As default.

## Mass Modelling

Lumped mass only.

## Options

32 Suppress stress output but not stress resultants.
34 Output stress resultants.
55 Output strains as well as stresses.
59 Output local direction cosines for elements.
77 Output averaged global stresses.

## Notes on Use

1. The element formulations are based on the standard
2. The variation of stresses within an element may be regarded as constant for TSM3 and linear for SMI4.
3. The higher performance of SMI4 is due to the addition of 4 incompatible displacement modes.
4. The elements pass the patch test for mixed triangular and quadrilateral geometry.
5. Distributed loads are lumped at the nodes.
6. The element is formulated so that the material response is evaluated in the local Cartesian system.
7. The SMI4 element is generally the most effective element due to its quadratic displacement accuracy. However, its behaviour tends to deteriorate as the element become distorted.
8. The element matrices are formed using 1-point Gauss quadrature for TSM3. Selective integration is utilised for the evaluation of the element matrices for SMI4. The method used is similar to that proposed by Hughes, with the contribution of the incompatible modes to the strain-displacement matrix being evaluated at the 1-point Gauss rule sampling location and then extrapolated to the $2 * 2$ Gauss rule sampling locations. The element matrices are then formed using the $2 * 2$ Gauss rule.

## Restrictions

A Avoid excessive aspect ratio.
$\square$ Avoid excessive warping.

## Recommendations on Use

- The space membrane elements have limited 'stand-alone' use because of their inability to support any loading except membrane loading. However, they can be utilised with the flat shell elements (QSI4, TS3) to model very thin membranes in structural components.
- If a structure is composed of exactly co-planar flat space membrane elements that are not stiffened by plate or shell elements, singularities may arise since there is no out-of-plane stiffness.
- If there is a possibility of bending behaviour then a thin shell should be utilised for the analysis.


## Chapter 8 : Joint Elements.

## 2D Joint Element for Bars, Plane Stress and Plane Strain

## General

Element Name
JNT3

Element Group ..... Joints
Element 2D Joints
SubgroupElement A 2D joint element which connects two nodes by two springs in the localDescription x and y -directions.
Number Of 3. The 3rd node is used to define the local $x$-direction.
Nodes
Freedoms $\mathrm{U}, \mathrm{V}$ : at nodes 1 and 2 (active nodes).
Node $\mathrm{X}, \mathrm{Y}$ : at each node.
Coordinates

## Geometric Properties

## Not applicable.

## Material Properties

Linear Not applicable
Matrix Stiffness: MATRIX PROPERTIES STIFFNESS 4 K1,..., K10 element stiffness matrix (Not supported in LUSAS Modeller)
Mass: MATRIX PROPERTIES MASS 4 M1,..., M10 element mass matrix (Not supported in LUSAS Modeller)
Damping: MATRIX PROPERTIES DAMPING 4 C1,..., C10 element damping matrix (Not supported in LUSAS Modeller)

Joint Standard:

Dynamic general:
Elasto-plastic:

Elasto-plastic:
Nonlinear contact:
Nonlinear friction:
Viscous damping:
Lead-rubber:
Friction pendulum:
Multi-linear elastic
Multi-linear
hysteresis
Multi-linear compound hysteresis
Axial force dependent multilinear elastic
Concrete Not applicable
Elasto-Plastic Not applicable
Creep Not applicable
Damage Not applicable
Viscoelastic Not applicable
Shrinkage Not applicable
Rubber Not applicable
Generic Polymer Not applicable
Composite Not applicable

JOINT PROPERTIES 2 (Joint: 2/Spring Stiffness Only)
JOINT PROPERTIES GENERAL 2 (Joint: 2/General Properties)
JOINT PROPERTIES NONLINEAR 312
(Joint: 2/Elasto-Plastic (Tension and Compression Equal))
JOINT PROPERTIES NONLINEAR 322 (Joint: 2/Tension and Compression Unequal)
JOINT PROPERTIES NONLINEAR 332 (Joint: 2/Smooth Contact)
JOINT PROPERTIES NONLINEAR 442 (Joint: 2/Frictional Contact)
JOINT PROPERTIES NONLINEAR 352 (Joint: 2/Viscous Damper)
JOINT PROPERTIES NONLINEAR 362 (Joint: 2/Lead Rubber Bearing)
JOINT PROPERTIES NONLINEAR 372 (Joint: 2/Frictional Pendulum System)
JOINT PROPERTIES NONLINEAR 402 (Joint: 2/Multi-Linear Elastic)
JOINT PROPERTIES NONLINEAR 412
(Joint: 2/Multi-Linear Hysteresis)
JOINT PROPERTIES NONLINEAR 422
(Joint: 2/Multi-Linear Compound Hysteresis)
JOINT PROPERTIES NONLINEAR 432
(Joint: 2/Axial Force Dependent Multi-Linear Elastic)

## Loading

Prescribed Value PDSP, TPDSP Prescribed variable. U, V: at active nodes.
Concentrated CL Concentrated loads. Px, Py: at active nodes.
Loads
Element Loads Not
applicable.
Distributed Loads Notapplicable.Body Forces CBF
BFP, BFPE Not applicable.
Velocities VELO
Accelerations ACCEInitial SSI, SSIE
Stress/Strains
SSIG
Residual Stresses Not
applicable.
Target TSSIE, TSSIA Target stresses/strains at nodes/for element. Fx, Fy:
Stress/StrainsTSSIG
Temperatures TEMP, TMPE
Overburden ..... Not applicable.
Phreatic Surface Notapplicable.Field Loads Notapplicable.
Temp Dependent Not
Loads applicable.
LUSAS Output
Solver Force: Fx, Fy: spring forces in local directions.
Strain: $\mathcal{E x}, \varepsilon_{y}$ : spring strains in local directions.
Modeller See Results Tables (Appendix K).

## Local Axes

$\square$ Standard joint element

## Sign Convention

$\square$ Standard joint element

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Stiffness Default. 1-point.
Fine. As default.
Mass Default. 1-point.
Fine. As default.

## Mass Modelling

Lumped mass only. The position of the mass relative to the two active joint nodes is defined in the joint material data. Point mass elements should be used to model lumped masses when no stiffness modelling is required.

## Options

55 Output strains as well as stresses.
119 Invokes temperature input for joints.

## Notes on Use

See Joint Element Compatibility and Notes (Appendix L).

## Restrictions

Not applicable.

## Recommendations on Use

- The joint elements may be used to release degrees of freedom between elements, e.g. a hinged shell, or to provide nonlinear support conditions, e.g. friction-gap condition. Also, point masses may be represented by including a joint at an element node.
- See Joint Element Compatibility (Appendix L)


## 2D Joint Element for Engineering and Kirchhoff Beams

## General

## Element Name

JPH3


## Element Group <br> Joints

## Element <br> 2D Joints

Subgroup
Element Description

A 2D joint element which connects two nodes by two springs in the local x and y -direction and one spring about the local z -direction.
Number Of
3. The 3rd node is used to define the local $x$-direction.

Nodes
Freedoms
Node X, Y: at each node.
Coordinates

## Geometric Properties

ey Eccentricity measured from the joint x axis to the nodal line (i.e. parallel to the joint y axis).
dy Parametric distance factor (between 0.0 and 1.0), which defines the position of the shear spring for the local y direction between nodes 1 and 2 . It is measured from node $1(\mathrm{dy}=0)$ along the local x direction

## Material Properties

## Linear Not applicable <br> Matrix Stiffness: MATRIX PROPERTIES STIFFNESS 6 K1,..., K21 element stiffness matrix (Not supported in LUSAS Modeller) <br> Mass: MATRIX PROPERTIES MASS 6 M1,..., M21 element mass matrix (Not supported in LUSAS

| Damping: | Modeller) <br> MATRI PROPERTIES DAMPING 6 C1,..., C21 <br> element damping matrix (Not supported in LUSAS <br> Modeller) |
| :--- | :--- |
| Joint | Standard: |
| JOINT PROPERTIES 3 (Joint: 3/Spring Stiffness |  |
| Only) |  |

Rubber Not applicable Generic Polymer Not applicable Composite Not applicable

## Loading

Prescribed Value PDSP, TPDSP
Concentrated CL Loads
Element Loads Not applicable
Distributed Loads Not applicable
Body Forces CBF

BFP, BFPE
Velocities VELO
Accelerations ACCE
Initial SSI, SSIE
Stress/Strains

SSIG

## Residual Stresses Not applicable

Target TSSIE, TSSIA Stress/Strains

TSSIG
Temperatures TEMP, TMPE
Overburden Not applicable.
Phreatic Surface Not applicable.
Field Loads Not applicable
Temp Dependent Not applicable Loads

Prescribed variable. U, V, $\theta \mathrm{z}$ : at active nodes. Concentrated loads. Px, Py, Mz: at active nodes.

Constant body forces for element. Xcbf, Ycbf, $\Omega$ x, $\Omega \mathrm{y}, \Omega_{\mathrm{z}}, \alpha \mathrm{z}$
Not applicable.
Velocities. Vx, Vy: at nodes.
Accelerations. Ax, Ay: at nodes.
Initial stresses/strains at nodes/for element.
Resultants. Fx, Fy, Mz: spring forces and moment in local directions. $\varepsilon x, \varepsilon y, \psi z$ : strains at nodes.
Not applicable.
Target stresses/strains at nodes/for element.
Resultants. Fx, Fy, Mz: spring forces and moment in local directions. $\varepsilon x, \varepsilon y, \psi z$ : strains at nodes.
Not applicable.
Temperatures at nodes/for element. $\mathrm{T}_{1}, \mathrm{~T}_{2}, \mathrm{~T}_{3}, \mathrm{~T}_{10}$, T20, T30: actual and initial spring temperatures.

## LUSAS Output

Solver Force: Fx, Fy, Mz: spring forces and moment in local directions.
Strain: $\varepsilon x, \varepsilon y, \psi z$ : spring strains in local directions.
Modeller See Results Tables (Appendix K).

## Local Axes

- Standard joint element


## Sign Convention

- Standard joint element


## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Stiffness Default. 1-point.
Fine. As default.
Mass Default. 1-point.
Fine. As default.

## Mass Modelling

Lumped mass only. The position of the mass relative to the two active joint nodes is defined in the joint material data. Point mass elements should be used to model lumped masses when no stiffness modelling is required.

## Options

55 Output strains as well as stresses.
119 Invokes temperature input for joints.

## Notes on Use

See Joint Element Compatibility and Notes (Appendix L).

## Restrictions

Not applicable.

## Recommendations on Use

- The joint elements may be used to release degrees of freedom between elements, e.g. a hinged shell, or to provide nonlinear support conditions, e.g. friction-gap condition. Also, point masses may be represented by including a joint at an element node.
- See Joint Element Compatibility (Appendix L)


## 2D Joint Element for Grillage Beams and Plates

## General

Element Name
JF3


## Element Group Joints

Element 2D Joints
Subgroup
Element A 2D joint element which connects two nodes by one spring in the local Description z-direction and two springs about the x and y directions.
Number Of 3. The 3rd node is used to define the local $x$-direction.
Nodes
Freedoms
$\mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}$ : at nodes 1 and 2 (active nodes).
Node $\mathrm{X}, \mathrm{Y}$ : at each node.
Coordinates

## Geometric Properties

dz Parametric distance factor (between 0.0 and 1.0), which defines the position of the shear spring for the local z direction between nodes 1 and 2 . It is measured from node $1(\mathrm{dz}=0)$ along the local x direction.

## Material Properties

## Linear Not applicable

Matrix Stiffness:

Mass:

[^0]LUSAS Modeller)Damping: MATRIX PROPERTIES DAMPING 6 C1,...,C21 element damping matrix (Not supportedin LUSAS Modeller)
Joint Standard: JOINT PROPERTIES 3 (Joint: 3/Spring Stiffness Only)
Dynamic general: JOINT PROPERTIES GENERAL 3 (Joint: 3/General Properties)
Elasto-plastic: JOINT PROPERTIES NONLINEAR 313 (Joint: 3/Elasto-Plastic (Tension and Compression Equal))
Elasto-plastic: JOINT PROPERTIES NONLINEAR 323 (Joint: 3/Tension and Compression Unequal)
JOINT PROPERTIES NONLINEAR 333 (Joint: 3/Smooth Contact)
Nonlinear friction: Not applicable
Viscous damping: JOINT PROPERTIES NONLINEAR 353 (Joint: 3/Viscous Damper)
Lead-rubber: Not applicable
Friction pendulum: Not applicable
Multi-linear elastic JOINT PROPERTIES NONLINEAR 403 (Joint: 3/Multi-Linear Elastic)
Multi-linear JOINT PROPERTIES NONLINEAR 413 hysteresis
Multi-linear compound hysteresis
Axial force dependent multilinear elastic
(Joint: 3/Multi-Linear Hysteresis)
JOINT PROPERTIES NONLINEAR 423
(Joint: 3/Multi-Linear Compound Hysteresis)
JOINT PROPERTIES NONLINEAR 433
(Joint: 3/Axial Force Dependent Multi-Linear Elastic)
Concrete Not applicable
Elasto-Plastic Not applicable
Creep Not applicable
Damage Not applicable
Viscoelastic Not applicable.
Shrinkage Not applicable
Rubber Not applicable
Generic Polymer Not applicable
Composite Not applicable

## Loading

Prescribed Value PDSP, TPDSP
Concentrated CL
Loads
Element Loads Not applicable
Distributed Loads Not applicable
Body Forces CBF
BFP, BFPE
Velocities VELO
Accelerations ACCE
Initial SSI, SSIE
Stress/Strains

SSIG
Residual Stresses Not applicable
Target TSSIE, TSSIA Stress/Strains

TSSIG
Temperatures TEMP, TMPE

Prescribed variable. $\omega, \theta \mathrm{x}, \theta \mathrm{y}$ : at active nodes.
Concentrated loads. Pz, Mx, My: at active nodes.

Constant body forces for element. Zcbf Not applicable. Velocities. Vz: at nodes. Accelerations. Az: at nodes. Initial stresses/strains at nodes/for element. Fz, $\mathrm{Mx}, \mathrm{My}$ : at active nodes. $\varepsilon z, \psi \mathrm{x}, \psi \mathrm{y}$ : at active nodes.
Not applicable.
Target stresses/strains at nodes/for element. Fz, $\mathrm{Mx}, \mathrm{My}$ : at active nodes. $\varepsilon z, \psi \mathrm{x}, \psi \mathrm{y}:$ at active nodes.
Not applicable.
Temperatures at nodes/for element. $\mathrm{T}_{1}, \mathrm{~T}_{2}, \mathrm{~T}_{3}$, $\mathrm{T}_{10}, \mathrm{~T}_{20}, \mathrm{~T}_{30}$ : actual and initial spring temperatures.

## LUSAS Output

Solver Force: $\mathrm{Pz}, \mathrm{Mx}, \mathrm{My}$ : spring forces in local directions.
Strain: $\varepsilon z, \psi x, \psi y$ : spring strains in local directions.
Modeller See Results Tables (Appendix K).

## Local Axes

Standard joint element

## Sign Convention

- Standard joint element


## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

| Stiffness | Default. | 1-point. |
| :---: | :--- | :--- |
|  | Fine. | As default. |
| Mass | Default. | 1-point. |
|  | Fine. | As default. |

## Mass Modelling

Lumped mass only. The position of the mass relative to the two active joint nodes is defined in the joint material data. Point mass elements should be used to model lumped masses when no stiffness modelling is required.

## Options

55 Output strains as well as stresses.
119 Invokes temperature input for joints.

## Notes on Use

See Joint Element Compatibility and Notes (Appendix L).

## Restrictions

Not applicable.

## Recommendations on Use

- The joint elements may be used to release degrees of freedom between elements, e.g. a hinged shell, or to provide nonlinear support conditions, e.g. friction-gap condition. Also, point masses may be represented by including a joint at an element node.
- See Joint Element Compatibility (Appendix L)


## 2D Joint Element for Axisymmetric Solids

## General

Element Name


JAX3


Joints
2D Joints
Subgroup
Element An axisymmetric joint element for use with axisymmetric solid elements, Description which connects two nodes by two springs in the local x and y -directions and a 3rd spring in the circumferential direction.
Number Of 3. The 3rd node is used to define the local $x$-direction.
Nodes
Freedoms U, V: at nodes 1 and 2 (active nodes).
Node X, Y: at each node.

## Geometric Properties

Not applicable.

## Material Properties

Linear Not applicable
Matrix Stiffness: MATRIX PROPERTIES STIFFNESS 6 K1,..., K10 element stiffness matrix (Not supported in LUSAS Modeller)
Mass: MATRIX PROPERTIES MASS 6 M1,..., M10
element mass matrix (Not supported in LUSAS Modeller)
Damping: MATRIX PROPERTIES DAMPING 6 C1,..., C10 element damping matrix (Not supported in LUSAS Modeller)
Joint Standard:
Dynamic general:
Elasto-plastic:
Elasto-plastic:
Standard:
Dynamic gener
Elasto-plastic:
Elasto-plastic:
Nonlinear contact:
Nonlinear friction:
Viscous damping:hysteresisMulti-linearcompoundhysteresisAxial forcedependent multi-linear elastic

Concrete Not applicable

Concrete Not applicable

Concrete Not applicable

Concrete Not applicable

Concrete Not applicable

Concrete Not applicable

Concrete Not applicable

Concrete Not applicable

Concrete Not applicable

Elasto-Plastic Not applicable

Elasto-Plastic Not applicable

Elasto-Plastic Not applicable

Elasto-Plastic Not applicable

Elasto-Plastic Not applicable

Elasto-Plastic Not applicable

Elasto-Plastic Not applicable

Elasto-Plastic Not applicable

Elasto-Plastic Not applicable

Creep Not applicable

Creep Not applicable

Creep Not applicable

Creep Not applicable

Creep Not applicable

Creep Not applicable

Creep Not applicable

Creep Not applicable

Creep Not applicable

Damage Not applicable

Damage Not applicable

Damage Not applicable

Damage Not applicable

Damage Not applicable

Damage Not applicable

Damage Not applicable

Damage Not applicable

Damage Not applicable

Viscoelastic Not applicable

Viscoelastic Not applicable

Viscoelastic Not applicable

Viscoelastic Not applicable

Viscoelastic Not applicable

Viscoelastic Not applicable

Viscoelastic Not applicable

Viscoelastic Not applicable

Viscoelastic Not applicable

Shrinkage Not applicable

Shrinkage Not applicable

Shrinkage Not applicable

Shrinkage Not applicable

Shrinkage Not applicable

Shrinkage Not applicable

Shrinkage Not applicable

Shrinkage Not applicable

Shrinkage Not applicable

Rubber Not applicable

Rubber Not applicable

Rubber Not applicable

Rubber Not applicable

Rubber Not applicable

Rubber Not applicable

Rubber Not applicable

Rubber Not applicable

Rubber Not applicable
Generic Polymer Not applicable
Generic Polymer Not applicable
Generic Polymer Not applicable
Generic Polymer Not applicable
Generic Polymer Not applicable
Generic Polymer Not applicable
Generic Polymer Not applicable
Generic Polymer Not applicable
Generic Polymer Not applicable
Composite Not applicable
Composite Not applicable
Composite Not applicable
Composite Not applicable
Composite Not applicable
Composite Not applicable
Composite Not applicable
Composite Not applicable
Composite Not applicableJOINT PROPERTIES 2 (Joint: 2/SpringStiffness Only) (See notes on use)JOINT PROPERTIES GENERAL 2 (Joint:2/General Properties) (See notes on use)
JOINT PROPERTIES NONLINEAR 312 ..... 312
(Joint: 2/Elasto-Plastic (Tension andCompression Equal)) (See notes on use)
JOINT PROPERTIES NONLINEAR 322
(Joint: 2/Tension and Compression Unequal)
(Joint: 2/Tension and Compression Unequal)(See notes on use)
JOINT PROPERTIES NONLINEAR 332
(Joint: 2/Smooth Contact) (See notes on use)
JOINT PROPERTIES NONLINEAR 442
JOINT PROPERTIES NONLINEAR 442
(Joint: 2/Frictional Contact) (See notes on use)
JOINT PROPERTIES NONLINEAR 352
(Joint: 2/Viscous Damper) (See notes on use)
Lead-rubber: JOINT PROPERTIES NONLINEAR 362
(Joint: 2/Lead Rubber Bearing) (See notes on use)
Friction pendulum: JOINT PROPERTIES NONLINEAR ..... 372
(Joint: 2/Frictional Pendulum System) (Seenotes on use)Multi-linear elastic JOINT PROPERTIES NONLINEAR 402(Joint: 2/Multi-Linear Elastic)
Multi-linear

JOINT PROPERTIES 2 (Joint: 2/Spring Stifness Only)(See notes on use) OINT PROPERTIES GENERAL 2 (Joint:use) (See notes on use)

JOINT PROPERTIES NONLINEAR 402 (Joint: 2/Multi-Linear Elastic)(Joint: 2/Multi-Linear Hysteresis)
JOINT PROPERTIES NONLINEAR 422
(Joint: 2/Multi-Linear Compound Hysteresis)
JOINT PROPERTIES NONLINEAR 432(Joint: 2/Axial Force Dependent Multi-LinearElastic)
Loading
Prescribed Value PDSP, TPDSP Prescribed variable. U, V: at active nodes.
Concentrated ..... CLLoads
Element Loads ..... Not
applicable.
Distributed Loads Not
applicable.
Body Forces CBF Constant body forces for element. Xcbf, Ycbf, $\Omega_{\mathrm{x}}$,
BFP, BFPE Not applicable.Velocities VELOAccelerations ACCEInitial SSI, SSIE
Stress/StrainsSSIG
Residual Stresses ..... Notapplicable.Target TSSIE, TSSIA
Stress/Strains
TSSIG
Temperatures TEMP, TMPE Temperatures at nodes/for element. $\mathrm{T}_{1}, \mathrm{~T}_{2}, \mathrm{~T}_{10}, \mathrm{~T}_{20}$ :
Velocities. Vx, Vy: at nodes.
Accelerations. Ax, Ay: at nodes..
Initial stresses/strains at nodes/for element. Fx, Fy:spring forces in local directions. $\mathcal{E x}, \varepsilon_{y}$ : springstrains in local directions.
Not applicable.
Concentrated loads. Px, Py: at active nodes.
$\Omega \mathrm{y}, \Omega \mathrm{z}, \alpha \mathrm{z}$
Target stresses/strains at nodes/for element. Fx, Fy:spring forces in local directions. $\mathcal{E x}, \boldsymbol{\varepsilon y}$ : springstrains in local directions.
Not applicable.actual and initial spring temperatures.
Overburden Notapplicable.Phreatic Surface Notapplicable.
Field Loads Notapplicable.
Temp Dependent NotLoads applicable.

## LUSAS Output

Solver Force: Fx, Fy, Fz: spring forces in local directions.
Strain: $\varepsilon x, \varepsilon y, \varepsilon z$ : spring strains in local directions.

## Modeller See Results Tables (Appendix K).

## Local Axes

$\square$ Standard joint element

## Sign Convention

Standard joint element

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Stiffness Default. 1-point.
Fine. As default.
Mass Default. 1-point.
Fine. As default.

## Mass Modelling

Lumped mass only. The position of the mass relative to the two active joint nodes is defined in the joint material data. Point mass elements should be used to model lumped masses when no stiffness modelling is required.

## Options

$47 \quad$ X-axis taken as axis of symmetry.
55 Output strains as well as stresses.
119 Invokes temperature input for joints.

## Notes on Use

- This joint has only two degrees of freedom but requires 3 inputs. The 3rd input required is the circumferential stiffness.
- For problems where the circumferential forces are to be transmitted by adjacent elements the circumferential stiffness should be input as zero.
- This element cannot be used with axisymmetric Fourier elements.

See Joint Element Compatibility and Notes (Appendix L).

## Restrictions

Not applicable.

## Recommendations on Use

- The joint elements may be used to release degrees of freedom between elements, e.g. a hinged shell, or to provide nonlinear support conditions, e.g. friction-gap condition. Also, point masses may be represented by including a joint at an element node.
- See Joint Element Compatibility (Appendix L)


## 2D Joint Element for Axisymmetric Shells

## General

Element Name
JXS3


## Element Group Joints

Element 2D Joints
Subgroup
Element An axisymmetric joint element for use with axisymmetric shell elements, Description which connects two nodes by two springs in the local x and y -directions, one spring about the local z-direction and a 4th spring in the circumferential direction.
Number Of 3. The 3rd node is used to define the local $x$-direction. Nodes
Freedoms U, V, $\theta$ : at nodes 1 and 2 (active nodes).
Node $\mathrm{X}, \mathrm{Y}$ : at each node.
Coordinates

## Geometric Properties

dy Parametric distance factor (between 0.0 and 1.0), which defines the position of the shear spring for the local y direction between nodes 1 and 2 . It is measured from node $1(\mathrm{dy}=0)$ along the local x direction.

## Material Properties

## Linear Not applicable

Matrix Stiffness: MATRIX PROPERTIES STIFFNESS 8 K1,...,
element mass matrix (Not supported in LUSAS Modeller)
Damping:

Joint Standard:
Dynamic general:
Elasto-plastic:

Elasto-plastic:

Nonlinear contact:
Nonlinear friction:
Viscous damping:
Lead-rubber:

Friction pendulum:

Multi-linear elastic
Multi-linear hysteresis
Multi-linear compound hysteresis
Axial force dependent multilinear elastic
Concrete Not applicable
Elasto-Plastic Not applicable
Creep Not applicable
Damage Not applicable
Viscoelastic Not applicable
Shrinkage Not applicable
Rubber Not applicable

MATRIX PROPERTIES DAMPING 8 C1,..., C21 element damping matrix (Not supported in LUSAS Modeller)
JOINT PROPERTIES 3 (Joint: 3/Spring Stiffness Only) (See notes on use)
JOINT PROPERTIES GENERAL 3 (Joint: 3/General Properties) (See notes on use)
JOINT PROPERTIES NONLINEAR 313 (Joint: 3/Elasto-Plastic (Tension and Compression Equal)) (See notes on use)
JOINT PROPERTIES NONLINEAR 323 (Joint: 3/Tension and Compression Unequal) (See notes on use)
JOINT PROPERTIES NONLINEAR 333 (Joint: 3/Smooth Contact) (See notes on use)
JOINT PROPERTIES NONLINEAR 443 (Joint: 3/Frictional Contact) (See notes on use)
JOINT PROPERTIES NONLINEAR 353 (Joint: 3/Viscous Damper) (See notes on use)
JOINT PROPERTIES NONLINEAR 363 (Joint:3/Lead Rubber Bearing) (See notes on use)
JOINT PROPERTIES NONLINEAR 373 (Joint: 3/Frictional Pendulum System) (See notes on use)
JOINT PROPERTIES NONLINEAR 403 (Joint: 3/Multi-Linear Elastic)
JOINT PROPERTIES NONLINEAR 413 (Joint:
3/Multi-Linear Hysteresis)
JOINT PROPERTIES NONLINEAR 423 (Joint: 3/Multi-Linear Compound Hysteresis)

JOINT PROPERTIES NONLINEAR 433 (Joint: 3/Axial Force Dependent Multi-Linear Elastic)
Generic Polymer Not applicable
Composite Not applicable
Loading
Prescribed Value PDSP, TPDSP
Concentrated CL
Loads
Element Loads ..... Not
applicable.
Distributed Loads Not
applicable.
Body Forces CBF
Constant body forces for element. Xcbf, Ycbf, $\Omega \mathrm{x}$,$\Omega \mathrm{y}, \Omega_{\mathrm{z}}, \alpha_{\mathrm{z}}$
BFP, BFPEVelocities VELOAccelerations ACCE
Initial SSI, SSIE
Stress/StrainsSSIG
Residual Stresses ..... Not
applicable.
Target TSSIE, TSSIA
Stress/StrainsTSSIG
Temperatures TEMP, TMPE Temperatures at nodes/for element. $\mathrm{T}_{1}, \mathrm{~T}_{2}, \mathrm{~T}_{3}, \mathrm{~T}_{10}$,
Target stresses/strains at nodes/for element. Fx, Fy:spring forces in local directions. $\varepsilon x, \varepsilon y$ : springstrains in local directions.
Not applicable.$\mathrm{T}_{20}, \mathrm{~T}_{30}$ : actual and initial spring temperatures.
Overburden Notapplicable.
Phreatic Surface Notapplicable.
Field Loads ..... Notapplicable.
Temp Dependent Not
Loads applicable.

## LUSAS Output

Solver Force: Fx, Fy, Fz,M: spring forces in local directions.
Strain: $\varepsilon x, \varepsilon y, \varepsilon z, \psi z$ : spring strains in local directions.
Modeller See Results Tables (Appendix K).

## Local Axes

Standard joint element

## Sign Convention

$\square$ Standard joint element

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Stiffness Default. 1-point. Fine. As default.
Mass Default. 1-point. Fine. As default.

## Mass Modelling

Lumped mass only. The position of the mass relative to the two active joint nodes is defined in the joint material data. Point mass elements should be used to model lumped masses when no stiffness modelling is required.

## Options

$47 \quad$ X-axis taken as axis of symmetry.
55 Output strains as well as stresses.
119 Invokes temperature input for joints.

## Notes on Use

This joint has only three degrees of freedom but requires 4 inputs. The 4th input required is the circumferential stiffness.
See Joint Element Compatibility and Notes (Appendix L).

## Restrictions

Not applicable.

## Recommendations on Use

- The joint elements may be used to release degrees of freedom between elements, e.g. a hinged shell, or to provide nonlinear support conditions, e.g. friction-gap condition. Also, point masses may be represented by including a joint at an element node.
- See Joint Element Compatibility (Appendix L)


## 3D Joints for Bars, Solids and Space Membranes

## General

Element Name


JNT4


Joints
Element
3D Joints
Subgroup
Element Description

A 3D joint element which connects two nodes by three springs in the
Number Of
Nodes local $\mathrm{x}, \mathrm{y}$ and z -directions.
4. The 3rd and 4th nodes are used to define the local $x$-axis and local $x y$ plane.
Freedoms U, V, W: at nodes 1 and 2 (active nodes).
Node $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.
Coordinates

## Geometric Properties

Not applicable.

## Material Properties

Linear Not applicable
Matrix Stiffness: MATRIX PROPERTIES STIFFNESS 6 K1,..., K21 element stiffness matrix (Not supported in LUSAS Modeller)
Mass: MATRIX PROPERTIES MASS 6 M1,..., M21 element mass matrix (Not supported in LUSAS Modeller)
Damping:
in LUSAS Modeller)
Joint Standard: JOINT PROPERTIES 3 (Joint: 3/SpringStiffness Only)Dynamic general: JOINT PROPERTIES GENERAL 3 (Joint:3/General Properties)Elasto-plastic: JOINT PROPERTIES NONLINEAR 313(Joint: 3/Elasto-Plastic (Tension andCompression Equal))Elasto-plastic: JOINT PROPERTIES NONLINEAR 323(Joint: 3/Tension and Compression Unequal)
Nonlinear contact: JOINT PROPERTIES NONLINEAR ..... 333
(Joint: 3/Smooth Contact)
Nonlinear friction: JOINT PROPERTIES NONLINEAR ..... 443
(Joint: 3/Frictional Contact)
Viscous damping: JOINT PROPERTIES NONLINEAR ..... 353
(Joint: 3/Viscous Damper)
Lead-rubber: JOINT PROPERTIES NONLINEAR ..... 363
(Joint: 3/Lead Rubber Bearing)
Friction pendulum: JOINT PROPERTIES NONLINEAR ..... 373
(Joint: 3/Frictional Pendulum System)
Multi-linear elastic
JOINT PROPERTIES NONLINEAR 403(Joint: 3/Multi-Linear Elastic)Multi-linear
JOINT PROPERTIES NONLINEAR 413
hysteresisMulti-linearcompoundhysteresisAxial forcedependent multi-linear elastic
(Joint: 3/Multi-Linear Hysteresis)
JOINT PROPERTIES NONLINEAR 423
(Joint: 3/Multi-Linear Compound Hysteresis)
JOINT PROPERTIES NONLINEAR ..... 433
(Joint: 3/Axial Force Dependent Multi-LinearElastic)
Concrete Not applicable
Elasto-Plastic Not applicableCreep Not applicable
Damage Not applicable
Viscoelastic Not applicable
Shrinkage Not applicable
Rubber Not applicable
Generic Polymer Not applicable
Composite Not applicable
Loading
Prescribed Value PDSP, TPDSP Prescribed variable. U, V, W: at active nodes.
Concentrated ..... CLLoads
Element Loads ..... Not
applicable.
Distributed Loads Notapplicable.Body Forces CBF Constant body forces for element. Xcbf, Ycbf, Zcbf,$\Omega_{\mathrm{x}}, \Omega_{\mathrm{y}}, \Omega_{\mathrm{z}}, \alpha \mathrm{x}, \alpha \mathrm{y}, \alpha \mathrm{z}$
BFP, BFPE Not applicable.
Velocities VELOAccelerations ACCE
Initial SSI, SSIE
Stress/StrainsSSIG
Velocities. Vx, Vy, Vz: at nodes.
Accelerations. Ax, Ay, Az: at nodes.
Initial stresses/strains at nodes/for element. Fx, Fy,Fz: spring forces in local directions. $\varepsilon x, \varepsilon y, \psi z$ :spring strains in local directions.
Not applicable.Residual Stresses Notapplicable.
Target TSSIE, TSSIA Target initial stresses/strains at nodes/for element.
Stress/Strains
TSSIG
Temperatures TEMP, TMPE Temperatures at nodes/for element. $\mathrm{T}_{1}, \mathrm{~T}_{2}, \mathrm{~T}_{3}, \mathrm{~T}_{1} \mathrm{o}$,Fx, Fy, Fz: spring forces in local directions. Ex,$\varepsilon y, \psi z$ : spring strains in local directions.
Not applicable.$\mathrm{T}_{20}, \mathrm{~T} 30$ : actual and initial spring temperatures.
Overburden Notapplicable.Phreatic Surface Notapplicable.
Field Loads Notapplicable.
Temp Dependent NotLoads applicable.

## LUSAS Output

Solver Force: Fx, Fy, Fz: spring forces in local directions. Strain: $\mathcal{E x}, \varepsilon$ y, $\varepsilon$ z: spring strains in local directions.

# Modeller See Results Tables (Appendix K). 

## Local Axes

$\square$ Standard joint element

## Sign Convention

Standard joint element

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

| Stiffness Default. | 1-point. |
| :---: | :--- |
| Fine. | As default. |
| Mass Default. | 1-point. |
| Fine | As default. |

## Mass Modelling

Lumped mass only. The position of the mass relative to the two active joint nodes is defined in the joint material data. Point mass elements should be used to model lumped masses when no stiffness modelling is required.

## Options

55 Output strains as well as stresses.
119 Invokes temperature input for joints.

## Notes on Use

See Joint Element Compatibility and Notes (Appendix L).

## Restrictions

Not applicable.

## Recommendations on Use

- The joint elements may be used to release degrees of freedom between elements, e.g. a hinged shell, or to provide nonlinear support conditions, e.g. friction-gap condition. Also, point masses may be represented by including a joint at an element node.
- See Joint Element Compatibility (Appendix L)


## 3D Joints for Semiloof Shells

## General

Element Name
JL43


## Element Group Joints

Element
3D Joints
Subgroup
Element
Description
A 3D joint element which connects two nodes by three springs in the
Number Of local $\mathrm{x}, \mathrm{y}$ and z -directions.
4. The 3rd and 4th nodes are used to define the local $x$-axis and local $x y$ -

Nodes plane.
Freedoms U, V, W: at nodes 1 and 2 (active nodes).
Node $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.
Coordinates

## Geometric Properties

Not applicable.

## Material Properties

Linear Not applicable
Matrix Stiffness: MATRIX PROPERTIES STIFFNESS 6 K1,..., K21 element stiffness matrix (Not supported in LUSAS Modeller)
Mass: MATRIX PROPERTIES MASS 6 M1,..., M21
element mass matrix (Not supported in LUSAS Modeller)
Damping:
in LUSAS Modeller)
JOINT PROPERTIES 3 (Joint: 3/SpringStiffness Only)Dynamic general: JOINT PROPERTIES GENERAL 3 (Joint:3/General Properties)
Elasto-plastic: JOINT PROPERTIES NONLINEAR 313(Joint: 3/Elasto-Plastic (Tension andCompression Equal))Elasto-plastic: JOINT PROPERTIES NONLINEAR 323(Joint: 3/Tension and Compression Unequal)
JOINT PROPERTIES NONLINEAR 333
(Joint: 3/Smooth Contact)
Nonlinear friction: JOINT PROPERTIES NONLINEAR ..... 443
(Joint: 3/Frictional Contact)
Viscous damping: JOINT PROPERTIES NONLINEAR ..... 353
(Joint: 3/Viscous Damper)
Lead-rubber: JOINT PROPERTIES NONLINEAR ..... 363
(Joint: 3/Lead Rubber Bearing)
Friction pendulum: JOINT PROPERTIES NONLINEAR ..... 373
(Joint: 3/Frictional Pendulum System)
Multi-linear elastic
JOINT PROPERTIES NONLINEAR 403(Joint: 3/Multi-Linear Elastic)Multi-linear
JOINT PROPERTIES NONLINEAR 413
hysteresisMulti-linearcompoundhysteresisAxial forcedependent multi-linear elastic
(Joint: 3/Multi-Linear Hysteresis)
JOINT PROPERTIES NONLINEAR 423
(Joint: 3/Multi-Linear Compound Hysteresis)
JOINT PROPERTIES NONLINEAR ..... 433
(Joint: 3/Axial Force Dependent Multi-LinearElastic)
Loading
Prescribed Value PDSP, TPDSP Prescribed variable. U, V, W: at active nodes.Concentrated CLLoads
Element Loads ..... Not
applicable.
Distributed Loads Notapplicable.Body Forces CBF Constant body forces for element. Xcbf, Ycbf, Zcbf,$\Omega_{\mathrm{x}}, \Omega_{\mathrm{y}}, \Omega_{\mathrm{z},}, \alpha \mathrm{x}, \alpha \mathrm{y}, \alpha \mathrm{z}$BFP, BFPE Not applicable.

Velocities VELO Accelerations ACCE

Initial SSI, SSIE Stress/StrainsSSIGResidual Stresses Notapplicable.Target TSSIE, TSSIA Target stresses/strains at nodes/for element. Fx, Fy,Stress/StrainsTSSIGTemperatures TEMP, TMPE Temperatures at nodes/for element. $\mathrm{T}_{1}, \mathrm{~T}_{2}, \mathrm{~T}_{3}, \mathrm{~T}_{10}$,$\mathrm{T}_{20}, \mathrm{~T}_{30}$ : actual and initial spring temperatures.
Overburden Notapplicable.Phreatic Surface Notapplicable.Field Loads Notapplicable.
Temp Dependent NotLoads applicable.

## LUSAS Output

Solver Force: Fx, Fy, Fz: spring forces in local directions.
Strain: $\mathcal{E x}, \mathcal{E y}, \varepsilon$ z: spring strains in local directions.

# Modeller See Results Tables (Appendix K). 

## Local Axes

$\square$ Standard joint element

## Sign Convention

Standard joint element

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

| Stiffness | Default. | 1-point. |
| :---: | :--- | :--- |
|  | Fine. | As default. |
| Mass | Default. | 1-point. |
|  | Fine. | As default. |

## Mass Modelling

Lumped mass only. The position of the mass relative to the two active joint nodes is defined in the joint material data. Point mass elements should be used to model lumped masses when no stiffness modelling is required.

## Options

55 Output strains as well as stresses.
119 Invokes temperature input for joints.

## Notes on Use

- When using Modeller to assign this semiloof joint element to interface lines a JL43 joint element will be created at the semiloof shell corner nodes and a JSL4 joint element will be created at the semiloof shell mid-side nodes.

See Joint Element Compatibility and Notes (Appendix L).

## Restrictions

Not applicable.

## Recommendations on Use

- The joint elements may be used to release degrees of freedom between elements, e.g. a hinged shell, or to provide nonlinear support conditions, e.g. friction-gap condition. Also, point masses may be represented by including a joint at an element node.
- See Joint Element Compatibility (Appendix L)


## 3D Joint Elements for Engineering, Kirchhoff and Semiloof Beams

## General

Element Name


JSH4, JL46


## Element Group Joints

## Element <br> 3D Joints

## Subgroup

Element
Description
3D joint elements which connects two nodes by six springs in the local $x$, y and z-directions. Use JL46 for semiloof beam end nodes.
Number Of
Nodes
4. The 3rd and 4th nodes are used to define the local $x$-axis and local $x y$ plane respectively.
Freedoms
Node
Coordinates
$\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ : at nodes 1 and 2 (active nodes).
$\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.

## Geometric Properties

ez Eccentricity measured from the joint xy-plane to the nodal line.
dy Parametric distance factor (between 0.0 and 1.0), which defines the position of the shear spring for the local y direction between nodes 1 and 2 . It is measured from node 1 $(\mathrm{dy}=0)$ along the local x direction.
dz Parametric distance factor (between 0.0 and 1.0), which defines the position of the shear spring for the local z direction between nodes 1 and 2 . It is measured from node 1 $(\mathrm{dz}=0)$ along the local x direction

## Material Properties

Linear Not applicable
Matrix Stiffness:
MATRIX PROPERTIES STIFFNESS 12 K1,..., K78 element stiffness matrix (Not supported in LUSAS Modeller)
Mass: MATRIX PROPERTIES MASS 12 M1,..., M78 element mass matrix (Not supported in LUSAS Modeller)
Damping: MATRIX PROPERTIES DAMPING $12 \mathrm{C} 1, \ldots$, C78 element damping matrix (Not supported in LUSAS Modeller)
Joint Standard: JOINT PROPERTIES 6 (Joint: 6/Spring Stiffness Only)
Dynamic general: JOINT PROPERTIES GENERAL 6 (Joint: 6/General Properties)
Elasto-plastic: JOINT PROPERTIES NONLINEAR 316 (Joint: 6/Elasto-Plastic (Tension and Compression Equal))
Elasto-plastic: JOINT PROPERTIES NONLINEAR 326 (Joint: 6/Tension and Compression Unequal)
Nonlinear contact: JOINT PROPERTIES NONLINEAR 336 (Joint: 6/Smooth Contact)
Nonlinear friction: JOINT PROPERTIES NONLINEAR 446 (Joint: 6/Frictional Contact)
Viscous damping: JOINT PROPERTIES NONLINEAR 356 (Joint: 6/Viscous Damper)
Lead-rubber: JOINT PROPERTIES NONLINEAR 366 (Joint: 6/Lead Rubber Bearing)
Friction pendulum: JOINT PROPERTIES NONLINEAR 376 (Joint: 6/Frictional Pendulum System)
Multi-linear elastic JOINT PROPERTIES NONLINEAR 406 (Joint: 6/Multi-Linear Elastic)
Multi-linear
JOINT PROPERTIES NONLINEAR 416 hysteresis
Multi-linear compound hysteresis
Axial force dependent multilinear elastic
(Joint: 6/Multi-Linear Hysteresis)
JOINT PROPERTIES NONLINEAR 426
(Joint: 6/Multi-Linear Compound Hysteresis)
JOINT PROPERTIES NONLINEAR 436
(Joint: 6/Axial Force Dependent Multi-Linear Elastic)
Damage Not applicable
Viscoelastic Not applicable
Shrinkage Not applicableRubber Not applicable
Generic Polymer Not applicable
Composite Not applicable
Loading
Prescribed Value PDSP, TPDSP
Concentrated CL
Loads
Element LoadsDistributed Loads Not applicable.Body Forces CBFBFP, BFPEVelocities VELOAccelerations ACCEInitial SSI, SSIEStress/Strains
SSIG
Residual Stresses Not applicable.
Target TSSIE, TSSIAStress/Strains
TSSIG
Temperatures TEMP, TMPE
Overburden Not applicable.
Phreatic Surface Not applicable.
Field Loads Not applicable.
Temp Dependent Not applicable.Loads

Prescribed variable. U, V, W, $\theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ : at active nodes.
Concentrated loads. Px, Py, Pz, Mx, My, Mz: at active nodes.

Constant body forces for element. Xcbf, Ycbf, Zcbf, $\Omega_{\mathrm{x}}, \Omega_{\mathrm{y}}, \Omega_{\mathrm{z}}, \alpha \mathrm{x}, \alpha \mathrm{y}, \alpha z_{\mathrm{z}}$ Not applicable.
Velocities. Vx, Vy, Vz: at nodes. Accelerations. Ax, Ay, Az: at nodes. Initial stresses/strains at nodes/for element. Fx, Fy, Fz, Mx, My, Mz: spring forces in local directions. $\varepsilon x, \varepsilon y, \varepsilon z, \psi x, y y, y z:$ spring strains in local directions.
Not applicable.

Target stresses/strains at nodes/for element. Fx, Fy, Fz, Mx, My, Mz: spring forces in local directions. $\varepsilon x, \varepsilon y, \varepsilon z, \psi x, y y, y z$ : spring strains in local directions.
Not applicable.
Temperatures at nodes/for element. $\mathrm{T}_{1}, \mathrm{~T}_{2}, \mathrm{~T}_{3}$, T4, T5, T6, T10, T20, T30, T40, T50, T60: actual and initial spring temperatures.

## LUSAS Output

Solver Force: Fx, Fy, Fz, Mx, My, Mz spring forces in local directions.
Strain: $\varepsilon x, \varepsilon y, \varepsilon z, \psi x, \psi y, \psi z$ : spring strains in local directions.
Modeller See Results Tables (Appendix K).

## Local Axes

- Standard joint element


## Sign Convention

- Standard joint element


## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

| Stiffness Default. | 1-point. |
| :---: | :--- |
| Fine. | As default. |
| Mass Default. | 1-point. |
| Fine | As default. |

## Mass Modelling

Lumped mass only. The position of the mass relative to the two active joint nodes is defined in the joint material data. Point mass elements should be used to model lumped masses when no stiffness modelling is required.

## Options

55 Output strains as well as stresses.
119 Invokes temperature input for joints

## Notes on Use

See Joint Element Compatibility and Notes.

## Restrictions

Not applicable.

## Recommendations on Use

- The joint elements may be used to release degrees of freedom between elements, e.g. a hinged shell, or to provide nonlinear support conditions, e.g. friction-gap condition. Also, point masses may be represented by including a joint at an element node.
- See Joint Element Compatibility (Appendix L)


## 3D Joint Element for Semiloof Beams

## General

JSL4

A 3D joint element which connects two nodes by three springs in the local $\mathrm{x}, \mathrm{y}$ and z -directions and two springs about the local x -direction at

Number Of 4. The 3rd and 4th nodes are used to define the local $x$-axis and local $x y$ -
$\mathrm{U}, \mathrm{V}, \mathrm{W}, \theta_{1}, \theta_{2}$ : at nodes 1 and 2 (active nodes).

Element Name



3D Joints
Subgroup
Element Description

A 3D joint element which co
local $x$, y and z-directions a
the 1st and 2nd loof points.
4. The 3rd and 4th nodes are Nodes plane respectively.
Freedoms
Node $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.
Coordinates

## Element Group Joints

Element
Damping: MATRIX PROPERTIES DAMPING 10 C1,..., C55 element damping matrix (Not supported in LUSAS Modeller)
Joint Standard:
JOINT PROPERTIES 5 (Joint: 5/Spring Stiffness Only)
Dynamic general: JOINT PROPERTIES GENERAL 5 (Joint: 5/General Properties)
Elasto-plastic: JOINT PROPERTIES NONLINEAR 315
(Joint: 5/Elasto-Plastic (Tension and Compression Equal))
Elasto-plastic: JOINT PROPERTIES NONLINEAR 325 (Joint:5/Tension and Compression Unequal)
Nonlinear contact: JOINT PROPERTIES NONLINEAR 335 (Joint: 5/Smooth Contact)
Nonlinear friction: JOINT PROPERTIES NONLINEAR 445 (Joint: 5/Frictional Contact)
Viscous damping: JOINT PROPERTIES NONLINEAR 355 (Joint: 5/Viscous Damper)
Lead-rubber: JOINT PROPERTIES NONLINEAR 365 (Joint: 5/Lead Rubber Bearing)
Friction pendulum: JOINT PROPERTIES NONLINEAR 375 (Joint: 5/Frictional Pendulum System)
Multi-linear elastic JOINT PROPERTIES NONLINEAR 405 (Joint: 5/Multi-Linear Elastic)
Multi-linear
hysteresis
Multi-linear
compound hysteresis
Axial force dependent multilinear elastic
Concrete Not applicable
Elasto-Plastic Not applicable
Creep Not applicable
Damage Not applicable
Viscoelastic Not applicable
Shrinkage Not applicable
Rubber Not applicable
Generic Polymer Not applicable
Composite Not applicable

JOINT PROPERTIES NONLINEAR 415
(Joint: 5/Multi-Linear Hysteresis)
JOINT PROPERTIES NONLINEAR 425
(Joint: 5/Multi-Linear Compound Hysteresis)
JOINT PROPERTIES NONLINEAR 435
(Joint: 5/Axial Force Dependent Multi-Linear Elastic)

## Loading

Prescribed Value PDSP, TPDSP

Concentrated CL
Loads
Element Loads Not applicable.
Distributed Loads Not applicable.
Body Forces CBF

BFP, BFPE
Velocities VELO
Accelerations ACCE
Initial SSI, SSIE
Stress/Strains

SSIG
Residual Stresses Not applicable.
Target TSSIE, TSSIA
Stress/Strains

TSSIG
Temperatures TEMP, TMPE

Overburden Not applicable.
Phreatic Surface Not applicable.
Field Loads Not applicable.
Temp Dependent Not applicable. Loads

Prescribed variable. U, V, W, $\theta_{1}, \theta_{2}$ : at active nodes.
Concentrated loads. Px, Py, Pz, M1, M2: at active nodes.

Constant body forces for element. Xcbf, Ycbf, $Z \mathrm{zbf}, \Omega_{\mathrm{x}}, \Omega_{\mathrm{y}}, \Omega_{\mathrm{z}}, \alpha \mathrm{x}, \alpha \mathrm{y}, \alpha_{\mathrm{z}}$
Not applicable.
Velocities. Vx, Vy, Vz: at nodes.
Accelerations. Ax, Ay, Az: at nodes.
Initial stresses/strains at nodes/for element. Fx, Fy, Fz, Mx, My, Mz: spring forces in local directions. $\varepsilon x, \varepsilon y, \varepsilon z, \psi x, \psi y, \psi z$ : spring strains in local directions.
Not applicable.

Target stresses/strains at nodes/for element. Fx, $\mathrm{Fy}, \mathrm{Fz}, \mathrm{Mx}, \mathrm{My}, \mathrm{Mz}$ : spring forces in local directions. $\varepsilon x, \varepsilon y, \varepsilon z, \psi x, \psi y, \psi z$ : spring strains in local directions.
Not applicable.
Temperatures at nodes/for element. $\mathrm{T}_{1}, \mathrm{~T}_{2}, \mathrm{~T}_{3}$, $\mathrm{T}_{4}, \mathrm{~T}_{5}, \mathrm{~T}_{10}, \mathrm{~T}_{20}, \mathrm{~T}_{30}, \mathrm{~T}_{40}$, T50: actual and initial spring temperatures.

## LUSAS Output

Solver Force: Fx , Fy , $\mathrm{Fz}, \mathrm{M}_{1}, \mathrm{M}_{2}$ : spring forces in local directions.
Strain: $\mathcal{E x}, \varepsilon y, \varepsilon z, \psi_{1}, \psi_{2}$ : spring strains in local directions.
Modeller See Results Tables (Appendix K).

## Local Axes

Standard joint element

## Sign Convention

- Standard joint element


## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Stiffness Default. 1-point. Fine. As default.
Mass Default. 1-point. Fine. As default.

## Mass Modelling

Lumped mass only. The position of the mass relative to the two active joint nodes is defined in the joint material data. Point mass elements should be used to model lumped masses when no stiffness modelling is required.

## Options

55 Output strains as well as stresses.
119 Invokes temperature input for joints.

## Notes on Use

See Joint Element Compatibility and Notes.

## Restrictions

Not applicable.

## Recommendations on Use

- The joint elements may be used to release degrees of freedom between elements, e.g. a hinged shell, or to provide nonlinear support conditions, e.g. friction-gap condition. Also, point masses may be represented by including a joint at an element node.
- See Joint Element Compatibility (Appendix L)


## Chapter 9 : Thermal / Field Elements.

## 2D Bar Field Elements

## General



| Element Group | Field |
| ---: | :--- | :--- |
| Element | Thermal Bars |
| Subgroup |  |
| Element | Straight and curved |
| Description |  |
| Number Of | 2 or 3. |
| Nodes |  |
| Freedoms | $\varphi:$ field value (temperature) at each node |
| Node | X, Y: at each node. |
| Coordinates |  |

## Geometric Properties

A1 ... An Cross-sectional area at each node.

## Material Properties

Matrix Not applicable
Joint Not applicable
Composite Not applicable
Field Isotropic MATERIAL PROPERTIES FIELD

> ISOTROPIC (Field: Isotropic)

MATERIAL PROPERTIES FIELD ISOTROPIC CONCRETE(Field: Isotropic)
Orthotropic:
Not applicable
Linear Not applicable convection/radiation:

Arbitrary convection/radiation:<br>Not applicable

## Loading

Prescribed Value PDSP, TPDSP
Rate of Heat RGN
Inflow at a Point
Element Loads Not applicable.
Distributed Loads UDL
FFL

Rate of Heat RBC Inflow/Unit Volume

RBV, RBVE
Velocities Not applicable.
Accelerations Not applicable.
Initial Not applicable.
Stress/Strains
Residual Stresses Not applicable.
Target Not applicable.
Stress/Strains
Temperatures TEMP, TMPE
Field Loads ENVT

Temp Dependent TDET

RIHG
$\varphi$ : field variable (temperature) at nodes.
Q: field loading at nodes.

Not applicable.
qa: (Q/unit area) at nodes (positive defines heat input) (see FLD Face loading applied to thermal bars).
qv: (Q/unit volume) for element.
qv: (Q/unit volume) at nodes/ for element.

Temperatures at nodes/for element. T, $0,0,0,0$, $0,0,0$ (See Notes.)

Environmental boundary conditions. $\varphi e, h c$, hr : external environmental temperature, convective and radiative heat transfer coefficients. (See Notes)
Temperature dependent environmental boundary conditions. $\varphi \mathrm{e}, \mathrm{hc}, \mathrm{hr}, \mathrm{T}$ : external environmental temperature, convective and radiative heat transfer coefficients and temperature for element. (See Notes)
Internal heat generation rate. $\mathrm{Q}, \mathrm{T}$ : coefficient/unit volume and temperature. (See Notes)

## LUSAS Output

Solver Field variable (temperature). gx, qx: gradient and flow in local axes.
Modeller See Results Tables (Appendix K).

## Local Axes

- Standard line element


## Sign Convention

$\square$ Standard field element

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

| Conductivity | Default. | 1-point (BFD2), 2-point (BFD3). |
| :--- | :--- | :--- |
|  | Fine (see Options). | 2-point (BFD2), 3-point (BFD3). |
| Specific Heat | Default. | 1-point (BFD2), 2-point (BFD3). |
|  | Fine (see Options). | 2-point (BFD2), 3-point (BFD3). |

## Specific Heat Modelling

$\square$ Consistent specific heat (default).
$\square$ Lumped specific heat.

## Options

18 Invokes fine integration rule.
105 Lumped specific heat.

## Notes on Use

1. TEMP/TMPE loading can be used to initialise the temperature field on the first step of a nonlinear field analysis. The temperature will be applied on the first pass of iteration 0 only and the load must be specified as a manual increment.
2. For linear field problems only one load case is allowed if an ENVT load is to be applied.
3. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear solution progresses.
4. Automatic load incrementation under the NONLINEAR CONTROL data chapter cannot be used with TDET or RIHG loading.
5. When using load curves with TDET loading, the environmental temperatures will be factored but the heat coefficients will remain constant. If ENVT loading is used with load curves, any component can be controlled via a load curve.
6. If radiation is to be considered the problem becomes nonlinear and NONLINEAR CONTROL must be specified.

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature


## Recommendations on Use

These elements may be used to analyse heat conduction along bars either individually or in conjunction with continuum field elements, e.g. supporting struts.

## 2D Axisymmetric Membrane Field Elements

## General



## Geometric Properties

tı... tn Thickness at each node.

## Material Properties

Matrix Not applicable.
Composite Not applicable.
Field Isotropic MATERIAL PROPERTIES FIELD ISOTROPIC (Field: Isotropic)
MATERIAL PROPERTIES FIELD ISOTROPIC CONCRETE (Field: Isotropic)
Orthotropic: Not applicable
Linear Not applicable
convection/radiation:
Arbitrary Not applicable
convection/radiation:

## Loading

Prescribed PDSP, TPDSP Value

Rate of Heat
Inflow at a Point
Element Loads Not applicable.
Distributed UDL
Loads
FFL

Rate of Heat RBC
Inflow/Unit
Volume
RBV, RBVE
Velocities Not applicable.
Accelerations Not applicable.
Initial Not applicable.
Stress/Strains
Residual Not applicable.
Stresses
Target Not applicable.
Stress/Strains
Temperatures TEMP, TMPE
Field Loads ENVT

Temp TDET
Dependent
Loads
RGN

RIHG
$\varphi$ : field variable (temperature) at nodes.
Q: field loading at nodes.

Not applicable.
qa: (Q/unit area) at nodes (positive defines heat input) (see FLD Face loading applied to thermal bars).
qv : (Q/unit volume) for element.
qv: (Q/unit volume) at nodes/ for element.

0,0 (See Notes.)

Environmental boundary conditions. $\varphi \mathrm{e}, \mathrm{hc}, \mathrm{hr}$ : external environmental temperature, convective and radiative heat transfer coefficients. (See Notes.)
Temperature dependent environmental boundary conditions. $\varphi \mathrm{e}, \mathrm{hc}, \mathrm{hr}, \mathrm{T}$ : external environmental temperature, convective and radiative heat transfer coefficients and temperature. (See Notes.)
Internal heat generation rate. Q, T: coefficient/unit volume and temperature for element. (See Notes.)

## LUSAS Output

Solver Field variable (temperature). gx, qx: gradient and flow in local axes.
Modeller See Results Tables (Appendix K).

## Local Axes

$\square$ Standard line element

## Sign Convention

$\square$ Standard field element

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

| Conductivity | Default. | 1-point (BFX2), 2-point (BFX3). |
| :--- | :--- | :--- |
|  | Fine (see Options). | 2-point (BFX2), 3-point (BFX3). |
| Specific Heat | Default. | 1-point (BFX2), 2-point (BFX3). |
|  | Fine (see Options). | 2-point (BFX2), 3-point(BFX3). |

## Specific Heat Modelling

Consistent specific heat (default).
$\square$ Lumped specific heat.

## Options

18 Invokes fine integration rule.
$47 \quad \mathrm{X}$-axis taken as axis of symmetry.
105 Lumped specific heat.

## Notes on Use

1. TEMP/TMPE loading can be used to initialise the temperature field on the first step of a nonlinear field analysis. The temperature will be applied on the first pass of iteration 0 only and the load must be specified as a manual increment.
2. For linear field problems only one load case is allowed if an ENVT load is to be applied.
3. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear solution progresses.
4. Automatic load incrementation under the NONLINEAR CONTROL data chapter cannot be used with TDET or RIHG loading.
5. When using load curves with TDET loading, the environmental temperatures will be factored but the heat coefficients will remain constant. If ENVT loading is used with load curves, any component can be controlled via a load curve.
6. If radiation is to be considered the problem becomes nonlinear and NONLINEAR CONTROL must be specified.

## Restrictions

$\square$ Ensure mid-side node centrality
$\square$ Avoid excessive element curvature

## Recommendations on Use

One example of the usage of these elements is the analysis of in-plane temperature flow in a thin circular plate.

## 3D Bar Field Elements

## General



| Element Group | Field |
| ---: | :--- | :--- |
| Element | Thermal Bars |
| Subgroup |  |
| Element | Straight and curved |
| Description |  |
| Number Of | 2 or 3. |
| Nodes |  |
| Freedoms | $\varphi:$ field value (temperature) at each node |
| Node | X, Y, Z: at each node. |
| Coordinates |  |

## Geometric Properties

A1 ... An Cross sectional area at each node.

## Material Properties

Linear Not applicable
Matrix Not applicable
Joint Not applicable
Concrete Not applicable
Elasto-Plastic Not applicable
Creep Not applicable
Damage Not applicable
Viscoelastic Not applicable
Shrinkage Not applicable
Rubber Not applicable.
Generic Polymer Not applicable
Composite Not applicable

Field Isotropic

Orthotropic:
Linear
convection/radiation:
Arbitrary
convection/radiation:
MATERIAL PROPERTIES FIELD
ISOTROPIC (Field: Isotropic)
MATERIAL PROPERTIES FIELD
ISOTROPIC CONCRETE (Field: Isotropic)
Not applicable.
Not applicable.
Not applicable.

## Loading

Prescribed Value PDSP, TPDSP
Rate of Heat RGN
Inflow at a Point
Element Loads Not applicable.
Distributed Loads UDL
FFL

Rate of Heat RBC
Inflow/Unit
Volume
RBV, RBVE
Velocities Not applicable.
Accelerations Not applicable.
Initial Not applicable.
Stress/Strains
Residual Stresses Not applicable.
Target Not applicable.
Stress/Strains
Temperatures TEMP, TMPE

Field Loads ENVT

Not applicable.
qa: (Q/unit area) at nodes (positive defines heat input) (see FLD Face loading applied to thermal bars).
qv : (Q/unit volume) for element.
$\varphi$ : field variable (temperature) at nodes.
Q : field loading at nodes.
$\mathrm{qv}:(\mathrm{Q} /$ unit volume) at nodes/ for element.

Temperatures at nodes/for element. T, $0,0,0,0$, $0,0,0$ (See Notes.)
Environmental boundary conditions. $\varphi \mathrm{e}$, hc, hr: external environmental temperature, convective and radiative heat transfer
Temp Dependent

Loads $\quad$ TDET | coefficients. (See Notes.) |
| :---: |
|  |

## LUSAS Output

Solver Field variable (temperature). gx, qx: gradient and flow in local axes.
Modeller See Results Tables (Appendix K).

## Local Axes

- Standard line element


## Sign Convention

- Standard field element


## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

| Conductivity | Default. | 1-point (BFS2), 2-point (BFS3). |
| :--- | :--- | :--- |
|  | Fine (see Options). | 2-point (BFS2), 3-point (BFS3). |
| Specific Heat | Default. | 1-point (BFS2), 2-point (BFS3). |
|  | Fine (see Options). | 2-point (BFS2), 3-point (BFS3). |

## Specific Heat Modelling

$\square$ Consistent specific heat (default).
$\square$ Lumped specific heat.

## Options

18 Invokes fine integration rule.
105 Lumped specific heat.

## Notes on Use

1. TEMP/TMPE loading can be used to initialise the temperature field on the first step of a nonlinear field analysis. The temperature will be applied on the first pass of iteration 0 only and the load must be specified as a manual increment.
2. For linear field problems only one load case is allowed if an ENVT load is to be applied.
3. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear solution progresses.
4. Automatic load incrementation under the NONLINEAR CONTROL data chapter cannot be used with TDET or RIHG loading.
5. When using load curves with TDET loading, the environmental temperatures will be factored but the heat coefficients will remain constant. If ENVT loading is used with load curves, any component can be controlled via a load curve.
6. If radiation is to be considered the problem becomes nonlinear and NONLINEAR CONTROL must be specified.

## Restrictions

$\square$ Ensure mid-side node centrality

- Avoid excessive element curvature


## 2D Link Field Element

## General



## Element Group <br> Field

Element Thermal Links
Subgroup
Element Straight conductive, convective or radiative thermal link element for 2D
Description field analysis.
Number Of
2.

Nodes
Freedoms
$\varphi$ : field value (temperature) at each node.
Node $\mathrm{X}, \mathrm{Y}$ at each node.
Coordinates

## Geometric Properties

A1 ... An Cross sectional area at each node.

## Material Properties

| Linear | Not applicable |
| ---: | :--- |
| Matrix | Not applicable |
| Joint | Not applicable |
| Concrete | Not applicable |
| Elasto-Plastic | Not applicable |
| Creep | Not applicable |
| Damage | Not applicable |
| Viscoelastic | Not applicable |
| Shrinkage | Not applicable |
| Rubber | Not applicable |

Generic Polymer Not applicable
Composite Not applicable
Field Isotropic: Not applicable.
Orthotropic: Not applicable.
Linear MATERIAL PROPERTIES FIELD LINK 18(Field: Linear Link)
convection/radiation:
ArbitraryMATERIAL PROPERTIES FIELD LINK 19convection/radiation:

## Loading

| Prescribed Value | PDSP, TPDSP | $\varphi$ : field variable (temperature) at nodes. |
| ---: | :--- | :--- |
| Concentrated | Not applicable. |  |
| Loads |  |  |
| Element Loads | Not applicable. |  |
| Distributed Loads | Not applicable. |  |
| Body Forces | Not applicable. |  |
| Velocities | Not applicable. |  |
| Accelerations | Not applicable. |  |
| Initial | Not applicable. |  |
| Stress/Strains |  |  |
| Residual Stresses | Not applicable. |  |
| Target | Not applicable. |  |
| Stress/Strains |  |  |
| Temperatures | Not applicable. |  |
| Field Loads | Not applicable. |  |
| Temp Dependent | Not applicable. |  |

## LUSAS Output

Solver Field variable (temperature). qx: flow at nodes in local directions.
Modeller See Results Tables (Appendix K).

## Local Axes

Standard line element

## Sign Convention

- Standard field element


## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Conduction, Default. 1-point (at element centroid).
Convection,
Radiation

Fine. As default.
Specific Heat Default. Not applicable.
Fine. Not applicable.

## Specific Heat Modelling

Not applicable.

## Options

Not applicable.

## Notes on Use

No notes at present.

## Restrictions

Not applicable.

## Recommendations on Use

An example of the usage of these elements is the analysis of heat conduction at contacting interfaces.

## 3D Link Field Element

## General



## Element Group <br> Field

Element Thermal Links
Subgroup
Element
Straight conductive, convective or radiative thermal link element for 3D
Description field analysis.
Number Of
2.

Nodes
End Releases
Freedoms
Node
Coordinates
$\varphi$ : field value (temperature) at each node.
$\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ at each node.

## Geometric Properties

A1 ... An Cross sectional area at each node.

## Material Properties

Linear Not applicable.
Matrix Not applicable.
Joint Not applicable.
Concrete Not applicable.
Elasto-Plastic Not applicable.
Rubber Not applicable.
Generic Polymer Not applicable
Composite Not applicable.
Field Isotropic: Not applicable.
Orthotropic: Not applicable.
Linear convection/radiation:
Arbitrary convection/radiation:
MATERIAL PROPERTIES FIELD LINK 18 (Field: Linear Link)
MATERIAL PROPERTIES FIELD LINK 19 (Field: Nonlinear Link)
Stress Potential Not applicable.
Creep Not applicable.
Damage Not applicable.
Viscoelastic Not applicable.
Shrinkage Not applicable
Loading
Prescribed Value PDSP, TPDSP
Concentrated Not applicable. Loads
Element Loads Not applicable.
Distributed Loads Not applicable.
Body Forces Not applicable.
Velocities Not applicable.
Accelerations Not applicable.
Initial Not applicable.
Stress/Strains
Residual Stresses Not applicable.
Target Not applicable.
Stress/Strains
Temperatures Not applicable.
Field Loads Not applicable.
Temp Dependent Not applicable.Loads

## LUSAS Output

Solver Field variable (temperature). qx: flow at nodes in local directions.
Modeller See Results Tables (Appendix K).

## Local Axes

Standard line element

## Sign Convention

- Standard field element


## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Conduction, Default. 1-point (at element centroid).
Convection,
Radiation

Fine. As default.
Specific Heat Default. Not applicable.
Fine. Not applicable.

## Specific Heat Modelling

Not applicable.

## Options

Not applicable.

## Notes on Use

No notes at present.

## Restrictions

Not applicable.

## Recommendations on Use

An example of the usage of these elements is the analysis of heat conduction at contacting interfaces.

## 2D Axisymmetric Link Field Element

## General



## Element Group <br> Field

Element Thermal Links
Subgroup
Element Straight conductive, convective or radiative thermal link element for 2D
Description
axisymmetric field analysis.
Number Of
2.

Nodes
End Releases
Freedoms
$\varphi$ : field value (temperature) at each node.
Node X, Y at each node.
Coordinates

## Geometric Properties

tı... tn Thickness at each node.

## Material Properties

Linear Not applicable.
Matrix Not applicable.
Joint Not applicable.
Concrete Not applicable.
Elasto-Plastic Not applicable.
Rubber Not applicable.
Generic Polymer Not applicable
Composite Not applicable.
Field Isotropic: Not applicable.

| Orthotropic: | Not applicable. |
| :--- | :---: |
| Linear | MATERIAL PROPERTIES FIELD LINK 18 |
| convection/radiation: | (Field: Linear Link) |
| Arbitrary MATERIAL PROPERTIES FIELD LINK 19 <br> convection/radiation: (Field: Nonlinear Link) |  |

## Loading

| Prescribed Value | PDSP, TPDSP | $\varphi$ : field variable (temperature) at nodes. |
| ---: | :--- | :--- |
| Concentrated | Not applicable. |  |
| Loads |  |  |
| Element Loads | Not applicable. |  |
| Distributed Loads | Not applicable. |  |
| Body Forces | Not applicable. |  |
| Velocities | Not applicable. |  |
| Accelerations | Not applicable. |  |
| Initial | Not applicable. |  |
| Stress/Strains |  |  |
| Residual Stresses | Not applicable. |  |
| Target | Not applicable. |  |
| Stress/Strains |  |  |
| Temperatures | Not applicable. |  |
| Field Loads | Not applicable. |  |

## LUSAS Output

Solver Field variable (temperature). qx: flow at nodes in local directions.
Modeller See Results Tables (Appendix K).

## Local Axes

Standard line element

## Sign Convention

Standard field element

## Formulation

## Geometric Nonlinearity

## Not applicable.

## Integration Schemes

Conduction, Default. 1-point (at element centroid).
Convection, Radiation

Fine. As default.
Specific Heat Default. Not applicable.
Fine. Not applicable.

## Specific Heat Modelling

Not applicable.

## Options

$47 \quad \mathrm{X}$-axis taken as axis of symmetry.

## Notes on Use

No notes at present.

## Restrictions

Not applicable.

## Recommendations on Use

An example of the usage of these elements is the analysis of heat conduction at contacting interfaces.

## 2D Axisymmetric Field Elements

## General



TXF3


QXF4


TXF6

QXF8


Element Group Field
Element
Plane Field

## Subgroup

Element Description capable of modelling curved boundaries. The elements are applicable to both steady state and transient field problems. The formulations apply over a unit radian segment of the structure and the loading and boundary conditions are axisymmetric. The elements are numerically integrated. Axisymmetry is taken about the Y -axis by default.

Coordinates
$3,4,6$, or 8 numbered anticlockwise.
Nodes
Freedoms
Node X, Y: at each node
Number Of
$\varphi$ : field variable at each node.

## Geometric Properties

Not applicable (a unit radian segment is assumed).

## Material Properties

| Linear | Not applicable. |  |
| ---: | :--- | :--- |
| Matrix | Not applicable. |  |
| Joint | Not applicable. |  |
| Concrete | Not applicable. |  |
| Elasto-Plastic | Not applicable. |  |
| Rubber | Not applicable. |  |
| Generic Polymer | Not applicable |  |
| Composite | Not applicable. | MATERIAL PROPERTIES FIELD |
| Field | Isotropic: | ISOTROPIC (Field: Isotropic) |
|  |  | MATERIAL PROPERTIES FIELD |
|  | Orthotropic: | MATERIAL PROPERTIES FIELD |
|  |  | ORTHOTROPIC (Field: Orthotropic) |
|  |  | ORTERIAL PROPERTIES FIELD |
|  | Linear | Orthotropic) |
|  | convection/radiation: | Not applicable. |
|  | Arbitrary | Not applicable. |

## Loading

Prescribed Value PDSP, TPDSP $\quad \varphi$ : field variable (temperature) at nodes.
Rate of Heat RGN
Q: field loading at nodes.

## Inflow at a Point

## Element Loads Not applicable.

Distributed Loads UDL
FFL
Not applicable.
qa: (Q/unit area) at nodes (see FLD Face loading applied to thermal bars).
Rate of Heat RBC
qv: (Q/unit volume) for element.
Inflow/Unit
Volume
RBV, RBVE qv: (Q/unit volume) at nodes/ for element.
Velocities Not applicable.
Accelerations Not applicable.
Initial Velocities Not applicable.Initial Not applicable.
Stress/Strains
Residual Stresses Not applicable.
Target Not applicable.
Stress/Strains
Temperatures Not applicable.Field Loads ENVT
Environmental boundary conditions. $\varphi \mathrm{e}$, hc,hr : external environmental temperature,convective and radiative heat transfercoefficients. (See Notes.)
Temp Dependent TDET Temperature dependent environmentalLoads
RIHG
boundary conditions. $\varphi \mathrm{e}, \mathrm{hc}, \mathrm{hr}, \mathrm{T}$ : externalenvironmental temperature, convective andradiative heat transfer coefficients andtemperature. (See Notes.)Internal heat generation rate. Q, T:coefficient/unit volume and temperature forelement. (See Notes.)

## LUSAS Output

Solver Field variable (temperature). gx, gy, gz, qx, qy, qz: gradients and flows in global directions.
Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable.

## Sign Convention

$\square$ Standard field element

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

| Conductivity | Default. | $\begin{aligned} & \text { 1-point (TXF3), 3-point (TXF6), 2x2 } \\ & \text { (QXF4, QXF8) } \end{aligned}$ |
| :---: | :---: | :---: |
|  | Fine (see | $3 \times 3$ (QXF8) |
|  | Options). |  |
| Specific Heat | Default. | $\begin{aligned} & \text { 1-point (TXF3), 3-point (TXF6), 2x2 } \\ & \text { (QXF4, QXF8) } \end{aligned}$ |
|  | Fine. | As default. |

## Specific Heat Modelling

$\square$ Consistent specific heat (default)
$\square$ Lumped specific heat.

## Options

18 Invokes fine integration rule for elements.
$47 \quad \mathrm{X}$-axis taken as axis of symmetry.
105 Lumped specific heat.

## Notes on Use

1. The element formulations are based on the standard isoparametric approach. The variation of field variable (temperature) within an element is linear low order (corner node only) elements and quadratic high order (mid-side node) elements.
2. All elements pass the patch test for convergence.
3. For linear field problems only one load case is allowed if an ENVT load is to be applied.
4. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear solution progresses.
5. Automatic load incrementation under the NONLINEAR CONTROL data chapter cannot be used with TDET or RIHG loading.
6. When using load curves with TDET loading, the environmental temperatures will be factored but the heat coefficients will remain constant. If ENVT loading is used with load curves, any component can be controlled via a load curve.
7. If radiation is to be considered the problem becomes nonlinear and NONLINEAR CONTROL must be specified.

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio


## Recommendations on Use

The axisymmetric field elements are suitable for analysing solid field problems which exhibit geometric and loading symmetry about a given axis, e.g. temperature distribution in a pipe or radial groundwater flow into a well.

## 2D Plane Field Elements

## General



## Element Group Field

## Element <br> Plane Field

Subgroup
Element A family of plane field elements in 2D with higher order elements capable Description of modelling curved boundaries. The elements are applicable to both steady state and transient field problems. The elements are numerically integrated.
Number Of 3, 4, 6 or 8 numbered anticlockwise.
Nodes
Freedoms
$\varphi$ : field value (temperature) at each node.
Node $\mathrm{X}, \mathrm{Y}$ : at each node.

## Coordinates

## Geometric Properties

t1... $\mathbf{t n}^{\text {Thickness at each node. }}$

## Material Properties

| Linear | Not applicable |  |
| ---: | :--- | :--- |
| Matrix | Not applicable |  |
| Joint | Not applicable |  |
| Concrete | Not applicable |  |
| Elasto-Plastic | Not applicable |  |
| Creep | Not applicable |  |
| Damage | Not applicable |  |
| Viscoelastic | Not applicable |  |
| Shrinkage | Not applicable |  |
| Rubber | Not applicable. |  |
| Generic Polymer | Not applicable |  |
| Composite | Not applicable. | MATERIAL PROPERTIES FIELD |
| Field | Isotropic: | ISOTROPIC CONCRETE (Field: Isotropic) |
|  |  | ISOTROPIC (Field: Isotropic) |
|  | Orthotropic: | ORTHOTROPIC (Field: Orthotropic) |
|  |  | MATERIAL PROPERTIES FIELD |
|  |  | ORTHOTROPIC CONCRETE (Field: |
|  | Linear | Orthotropic) |
|  | convection/radiation: |  |
|  | Arbitrary | Not applicable. |
|  |  |  |

## Loading

Prescribed Value PDSP, TPDSP
Rate of Heat RGN

## Inflow at a Point

Element Loads Not applicable.
Distributed Loads UDL
FFL
$\varphi$ : field variable (temperature) at nodes.
Q : field loading at nodes.

Not applicable.
qa: (Q/unit area) at nodes (see FLD Face loading applied to thermal bars).
$\left.\begin{array}{rll}\begin{array}{r}\text { Rate of Heat } \\ \text { Inflow/Unit } \\ \text { Volume }\end{array} & \text { RBC } & \text { qv: (Q/unit volume) for element. } \\ \begin{array}{rl}\text { Velocities } \\ \text { RBV, RBVE }\end{array} & \text { Not applicable. }\end{array}\right)$

## LUSAS Output

Solver Field variable (temperature). gx, gy, qx, qy: gradients and flows in global directions.
Modeller See Results Tables (Appendix K).

## Local Axes

- Standard surface element


## Sign Convention

$\square$ Standard field element

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

| Conductivity | Default. | 1-point (TFD3), 3-point (TFD6), 2x2 (QFD4, QFD8). |
| :--- | :--- | :--- |
|  | Fine. | As default. |
| Specific Heat | Default. | 1-point (TFD3), 3-point (TFD6), 2x2 (QFD4, QFD8). |
|  | Fine. | Not applicable. |

## Specific Heat Modelling

$\square$ Consistent specific heat (default).
$\square$ Lumped specific heat.

## Options

18 Invokes fine integration rule for elements.
105 Lumped specific heat.

## Notes on Use

1. The element formulations are based on the standard isoparametric approach. The variation of field variable (temperature) within an element is linear for low order (corner node only) elements and quadratic for high order (mid-side node) elements.
2. All elements pass the patch test for convergence.
3. For linear field problems only one load case is allowed if an ENVT load is to be applied.
4. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear solution progresses.
5. Automatic load incrementation under the NONLINEAR CONTROL data chapter cannot be used with TDET or RIHG loading.
6. When using load curves with TDET loading, the environmental temperatures will be factored but the heat coefficients will remain constant. If ENVT loading is used with load curves, any component can be controlled via a load curve.
7. If radiation is to be considered the problem becomes nonlinear and NONLINEAR CONTROL must be specified.

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio


## Recommendations on Use

The plane field elements may be utilised for analysing continuum field problems whose behaviour is essentially two dimensional, e.g. thermal analysis of a long tunnel . The elements are formulated using the 2D quasi-harmonic equation. See Theory Manuals for details.

## 3D Solid Field Elements

## General

## Element Group

Field

## Element

 SubgroupElement Description


PF6


HF8


TF10

PF12


HF16


PF15

HF20


Solid Field

A family of solid field elements in 3D with higher order elements capable of modelling curved boundaries. The elements are applicable to both
Freedoms
Coordinatessteady state and transient field problems. The elements are numericallyintegrated.
Number Of 4 and 10 (tetrahedra). 6, 12 and 15 (pentahedra). 8, 16 and 20
Nodes (hexahedra). The elements are numbered according to a right-hand screwrule in the local z-direction.$\varphi$ : field variable at each node.Node $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.
Geometric Properties
Not applicable.
Material Properties
Linear Not applicable
Matrix Not applicable
Joint Not applicable
Concrete Not applicable
Elasto-Plastic Not applicable
Creep Not applicable
Damage Not applicable
Viscoelastic Not applicable
Shrinkage Not applicable
Rubber Not applicable
Generic Polymer Not applicable
Composite Not applicable

Field Isotropic:

Orthotropic:

Linear convection/radiation:
Arbitrary Not applicable.

MATERIAL PROPERTIES FIELD ISOTROPIC CONCRETE (Field: Isotropic) MATERIAL PROPERTIES FIELD ISOTROPIC (Field: Isotropic)
MATERIAL PROPERTIES FIELD
ORTHOTROPIC SOLID (Field: OrthotropicSolid)
MATERIAL PROPERTIES FIELD
ORTHOTROPIC SOLID CONCRETE
(Field: Orthotropic Solid)
Not applicable.Not applicable.

## Loading

| Prescribed Value | PDSP, TPDSP |
| ---: | :--- |
| Rate of Heat | RGN |
| Inflow at a Point |  |
| Element Loads | Not applicable. |
| Distributed Loads | UDL |
|  | FFL |
| Rate of Heat | RBC |
| Inflow/Unit |  |
| Volume | RBV, RBVE |
|  | Velocities | Not applicable.

Temp Dependent TDET
Loads

RIHG
$\varphi$ : field variable (temperature) at nodes.
Q : field loading at nodes.

Not applicable.
qa: (Q/unit area) at nodes (see FLD Face loading applied to thermal bars).
qv: (Q/unit volume) for element.
qv: (Q/unit volume) at nodes/ for element.

Environmental boundary conditions. $\varphi \mathrm{e}, \mathrm{hc}$, hr: external environmental temperature, convective and radiative heat transfer coefficients. (See Notes.)
Temperature dependent environmental boundary conditions. $\varphi \mathrm{e}, \mathrm{hc}, \mathrm{hr}, \mathrm{T}$ : external environmental temperature, convective and radiative heat transfer coefficients and temperature. (See Notes.)
Internal heat generation rate. $\mathrm{Q}, \mathrm{T}$ : coefficient/unit volume and temperature for element. (See Notes.)

## LUSAS Output

Solver Field variable (temperature). gx, gy, gz, qx, qy, qz: gradients and flows in global directions.

## Modeller See Results Tables (Appendix K).

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

Standard field element

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Conductivity Default. 1-point (TF4), 4-point (TF10), 3x2 (PF6, PF12, PF15), 2x2x2 (HF8, HF16, HF20)
Fine (see Options). 5-point (TF10)
3x3x2 (HF16), 3×3x3 (HF20)
Coarse (see 1-point (HF20), 14-point (HF20)
Options).
Specific Heat Default. 1-point (TF4), 4-point (TF10), 3x2 (PF6, PF12, PF15), 2x2x2 (HF8, HF16, HF20)
Fine (see Options). 5-point (TF10)
3x3x2 (HF16), $3 \times 3 \times 3$ (HF20)
Coarse (see 13-point (HF20), 14-point (HF20)
Options).

## Specific Heat Modelling

$\square$ Consistent specific heat (default).
$\square$ Lumped specific heat.

## Options

18 Invokes fine integration rule for elements.
105 Lumped specific heat.
155 Use 14-point integration rule for HF20.

156 Use 13-point integration rule for HF20.
398 For HF20 and HF16 with fine integration use all integration points for stress extrapolation.

## Notes on Use

1. The element formulations are based on the standard isoparametric approach. The variation of potential within an element may be regarded as constant for low order (corner node only) elements and linear for high order (mid-side node) elements.
2. For linear field problems only one load case is allowed if an ENVT load is to be applied.
3. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear solution progresses.
4. Automatic load incrementation under the NONLINEAR CONTROL data chapter cannot be used with TDET or RIHG loading.
5. When using load curves with TDET loading, the environmental temperatures will be factored but the heat coefficients will remain constant. If ENVT loading is used with load curves, any component can be controlled via a load curve.
6. If radiation is to be considered the problem becomes nonlinear and NONLINEAR CONTROL must be specified.

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio


## Recommendations on Use

The solid field elements may be used to analyse continuum field problems where the response is fully 3D (i.e. it cannot be approximated using the plane or axisymmetric elements), e.g. temperature distribution in a pipe intersection.

## 3D Solid Composite Field Element (Tetrahedral)

## General



Element Group Field

## Element <br> Solid Field

## Subgroup

Element
3D solid field element capable of modelling curved boundaries. The
Description element is applicable to both steady state and transient field problems. The element is numerically integrated, can be arbitrarily oriented with respect to the laminate, and allows for the fully automatic mesh generation of laminate geometric models imported from CAD packages.
Number Of 10. The element is numbered according to a right-hand screw rule in the Nodes local z-direction.
Freedoms
$\varphi$ : field variable at each node.
Node $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.

## Coordinates

## Geometric Properties

See Composites in the Modeller Reference Manual

## Material Properties

Linear Not applicable
Matrix Not applicable
Joint Not applicable
Concrete Not applicable
Elasto-Plastic Not applicable
Creep Not applicable
Damage Not applicable
Viscoelastic Not applicable
Shrinkage Not applicable
Rubber Not applicable
Generic Polymer ..... Not applicable
CompositeField Isotropic:Orthotropic:
Loading
Prescribed Value PDSP, TPDSP
Rate of Heat ..... RGN
Inflow at a Point
Element Loads Not applicable.
Distributed Loads UDLFFL
Rate of Heat ..... RBC
Inflow/Unit
Volume
RBV, RBVE $\mathrm{qv}:(\mathrm{Q} /$ unit volume $)$ at nodes/ for element.
Velocities Not applicable.
Accelerations Not applicable.
Initial Not applicable.
Stress/Strains
Residual Stresses Not applicable.

Linear convection/radiation: Arbitrary convection/radiation:

COMPOSITE MATERIAL
MATERIAL PROPERTIES FIELD ISOTROPIC (Field: Isotropic) MATERIAL PROPERTIES FIELD ISOTROPIC CONCRETE (Field: Isotropic) MATERIAL PROPERTIES FIELD ORTHOTROPIC SOLID (Field: Orthotropic Solid)
MATERIAL PROPERTIES FIELD ORTHOTROPIC SOLID CONCRETE (Field: Orthotropic Solid)
Not applicable

Not applicable

Target Not applicable.<br>Stress/Strains<br>Temperatures Not applicable.<br>Field Loads ENVT<br>Temp Dependent TDET<br>Loads<br>RIHG<br>Environmental boundary conditions $\varphi \mathrm{e}, \mathrm{hc}$, hr : external environmental temperature, convective and radiative heat transfer coefficients. (See Notes.)<br>Temperature dependent boundary conditions. $\varphi \mathrm{e}, \mathrm{hc}, \mathrm{hr}, \mathrm{T}$ : external environmental temperature, convective and radiative heat transfer coefficients and temperature. (See Notes.)<br>Internal heat generation rate. $\mathrm{Q}, \mathrm{T}$ : coefficient/unit volume and temperature for element. (See Notes.)

## LUSAS Output

Solver Field variable (temperature). gx, gy, gz, qx, qy, qz: gradients and flows. Gauss point values are in local directions. Nodal values are in global directions.
Modeller See Results tables (Appendix K)

## Local Axes

The local axes for each layer are defined by the LAMINAR DIRECTIONS specified for its bottom surface. The three node set in LAMINAR DIRECTIONS define the local Cartesian set origin, the x -axis and the positive quadrant of the xy-plane respectively. The local z -axis forms an orthonormal coordinate system with $x$ and $y$.

## Sign Convention

$\square$ Standard field elements

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Conductivity Default. 1-point for a tetrahedral subdivision (see Notes), 3 -point for a pentahedral/pyramid subdivision, $2 \times 2$ for a hexahedral/wrick subdivision

Fine (see 1-point for a tetrahedral subdivision (see Notes), Options) $3 \times 2$ for a pentahedral/pyramid subdivision, $2 \times 2 \times 2$ for a hexahedral/wrick subdivision

Specific Heat Default. 5-point for the whole element or (see Options) 1point for a tetrahedral subdivision, $3 \times 2$ for a pentahedral/pyramid subdivision, $2 \times 2 \times 2$ for a hexahedral/wrick subdivision
Fine (see 11-point or (see Options) 14 -point for the whole Options) element

## Specific Heat Modelling

- Consistent specific heat (default).
- Lumped specific heat.


## Options

18 Invokes fine integration rule for elements.
91 Formulate element specific heat with fine integration
105 Lumped specific heat.
266 Layer by layer computation of specific heat matrix.
394 Lamina directions supported
395 Use 14-point fine integration rule for specific heat matrix of TH10 family (used together with 91)

## Notes on Use

1. The element formulations are based on the standard isoparametric approach. The variation of field gradients within an element may be regarded as linear.
2. The LAMINAR DIRECTIONS and COMPOSITE MATERIAL data chapters must be used with this element in conjunction with the COMPOSITE ASSIGNMENTS data chapter.
3. If the whole tetrahedral element is embedded in a single lamina, a 4-point integration rule will be used for this tetrahedral subdivision; otherwise a 1-point rule will be used.
4. The specific heat matrix can be computed using a layer by layer integration (OPTION 266), however this should only be used when the thermal properties of the layers vary considerably because the computation time can be greatly increased when this OPTION is specified.
5. Numerical integration through the thickness is performed. The integration points are located in the subdivisions of each layer. Each subdivision forms the shape of a regular 3D solid field element and the integration points are located accordingly within the subdivision as described above.
6. For linear field problems only one load case is allowed if an ENVT load is to be applied.
7. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear solution progresses.
8. Automatic load incrementation under the NONLINEAR CONTROL data chapter cannot be used with TDET or RIHG loading.
9. When using load curves with TDET loading, the environmental temperatures will be factored but the heat coefficients will remain constant. If ENVT loading is used with load curves, any component can be controlled via a load curve.
10. If radiation is to be considered the problem becomes nonlinear and NONLINEAR CONTROL must be specified.
11. Layer 1 is always the bottom layer.

## Restrictions

Ensure mid-side node centrality
$\square$ Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio

## Recommendations on Use

- 3D solid composite field elements should be used for modelling thick composite structures comprising laminae of differing material properties where the computational cost of modelling each lamina with an individual solid element would be prohibitive. This field element can be used to analyse continuum field problems where the response is fully 3D.
- As these elements can be arbitrarily oriented with respect to the laminate, they are particularly aimed at the use of fully automatic mesh generation of laminate geometric models imported from CAD packages.


## 3D Solid Composite Field Elements (Pentahedral and Hexahedral)

## General

Element Name


PF6C


HF8C


PF12C


HF16C


Element Group
Element
Subgroup
Element Description

Number Of
Nodes
Freedoms
Node
Coordinates

Field
Solid Field

3D solid field elements capable of modelling curved boundaries. The elements are applicable to both steady state and transient field problems. The elements are numerically integrated. The composite layers are parallel to the top and bottom faces and the bottom surface of the first layer coincides with the bottom surface of the element. The top and bottom faces of the element are as shown, e.g. nodes $1,2,3,4$ define the bottom face of HF8C
6 or 12 (pentahedra), 8 or 16 (hexahedra). The elements are numbered according to a right-hand screw rule in the local z-direction.
$\varphi$ : field variable at each node.
$\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.

## Geometric Properties

## See Composites in the Modeller Reference Manual

## Material Properties

$$
\begin{array}{rll}
\text { Linear } \\
\text { Matrix } & \text { Not applicable } & \text { Not applicable } \\
\text { Joint } & \text { Not applicable } & \\
\text { Concrete } & \text { Not applicable } & \\
\text { Elasto-Plastic } & \text { Not applicable } & \\
\text { Creep } & \text { Not applicable } & \\
\text { Damage } & \text { Not applicable } & \\
\text { Viscoelastic } & \text { Not applicable } & \\
\text { Shrinkage } & \text { Not applicable } & \\
\text { Rubber } & \text { Not applicable } & \\
\text { Generic Polymer } & \text { Not applicable } & \text { COMPOSITE MATERIAL } \\
\text { Composite } & & \text { MATERIAL PROPERTIES FIELD } \\
\text { Field } & \text { Isotropic: } & \text { ISOTROPIC (Field: Isotropic) } \\
& & \text { MATERIAL PROPERTIES FIELD } \\
& & \text { ISOTROPIC CONCRETE (Field: Isotropic) } \\
& & \text { Orthotropic: } \\
& & \text { ORTHOTRIAL PROPERTIES FIELD } \\
& & \text { MATERIAL PROPERTIES FIELD } \\
& & \text { ORTHOTROPIC SOLID CONCRETE (Field: } \\
& \text { Linear } & \text { Orthotropic Solid) } \\
\text { convection/radiation: } & \\
& \text { Arbitrary } & \text { Not applicable } \\
\text { convection/radiation: } & \\
& &
\end{array}
$$

Inflow/Unit
Volume
RBV, RBVE $\mathrm{qv}:(\mathrm{Q} /$ unit volume) at nodes/ for element.

Velocities Not applicable.
Accelerations Not applicable.
Initial Not applicable. Stress/Strains
Residual Stresses Not applicable.
Target Not applicable.
Stress/Strains
Temperatures Not applicable.
Field Loads ENVT

Temp Dependent TDET
Loads

## 



RIHG

Environmental boundary conditions $\varphi e$, hc, hr: external environmental temperature, convective and radiative heat transfer coefficients. (See Notes.)
Temperature dependent boundary conditions. $\mathrm{Qe}, \mathrm{hc}, \mathrm{hr}, \mathrm{T}$ : external environmental temperature, convective and radiative heat transfer coefficients and temperature. (See Notes.)
Internal heat generation rate. Q, T: coefficient/unit volume and temperature for element. (See Notes.)

## LUSAS Output

Solver Field variable (temperature). gx, gy, gz, qx, qy, qz: gradients and flows. Gauss point values are in local directions. Nodal values are in global directions.
Modeller See Results tables (Appendix K)

## Local Axes

The local axes for each layer are defined using the convention for standard area elements. Local axes are computed at the top and bottom quadratic surfaces (at the Gauss points) and average values are interpolated for the mid-surface. Every layer uses the same averaged values.

## Sign Convention

- Standard field elements


## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Conductivity Default.
1-point for each layer (PF6C), 3-point for each layer (PF12C), $2 \times 2$ for each layer (HF8C, HF16C)
Fine (see 3-point for each layer (PF6C), 3x3 for each layer Options) (HF16C)

Specific Heat Default. 3x2 for the whole element (PF6C, PF12C) or (see Options) 1-point for each layer (PF6C), 3-point for each layer (PF12C), $2 \times 2 \times 2$ for the whole element or $2 \times 2$ for each layer (HF8C, HF16C)
Fine (see $3 \times 2$ for the whole element or 3-point for each Options) layer (PF6C), $3 \times 3 \times 2$ for the whole element or $3 \times 3$ for each layer (HF16C)

## Specific Heat Modelling

- Consistent specific heat (default).
- Lumped specific heat.


## Options

18 Invokes fine integration rule for elements.
105 Lumped specific heat.
266 Layer by layer computation of specific heat matrix.

## Notes on Use

1. The element formulations are based on the standard isoparametric approach.
2. For linear field problems only one load case is allowed if an ENVT load is to be applied.
3. The COMPOSITE GEOMETRY and COMPOSITE MATERIAL data chapters must be used with this element in conjunction with the COMPOSITE ASSIGNMENTS data chapter.
4. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear solution progresses.
5. Automatic load incrementation under the NONLINEAR CONTROL data chapter cannot be used with TDET or RIHG loading.
6. When using load curves with TDET loading, the environmental temperatures will be factored but the heat coefficients will remain constant. If ENVT loading is used with load curves, any component can be controlled via a load curve.
7. If radiation is to be considered the problem becomes nonlinear and NONLINEAR CONTROL must be specified.
8. The through thickness integration is performed assuming a linear variation of the field gradient-variable matrix for each layer.
9. Layer 1 is always the bottom layer.
10. The simplifying assumptions which allow the uncoupling of in-plane and through thickness co-ordinates leads to the restriction that any individual layer should be of a constant thickness. This restriction should be considered when the finite element mesh is created and adhered to as closely as possible. In addition, out of plane lamina curvatures should also be minimised although in-plane curvature (in the $x-y$ plane) is not restricted.

## Restrictions

$\square$ Ensure mid-side node centrality

- Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio
Constant layer thickness for each individual layer


## Recommendations on Use

The 3D solid composite field elements should be used for modelling thick composite structures comprising laminae of differing material properties where the computational cost of modelling each lamina with an individual solid element would be prohibitive. These field elements can be used to analyse continuum field problems where the response is fully 3D.

## Chapter 10 : HygroThermal Elements.

## 2D Plane Hygro-Thermal Elements

## General



Element Group Hygro-Thermal
Element Plane Hygro-Thermal
Subgroup
Element
Description
A family of plane hygro-thermal elements in 2D with higher order elements capable of modelling curved boundaries. The elements can be used in hygro-thermal transient analyses, i.e. heat and moisture flow in porous media, e.g. concrete.
Number Of 3, 4, 6 or 8 numbered anticlockwise.
Nodes
Freedoms T, Pc: Temperature and capillary pressure at each node.
Node X, Y: at each node.
Coordinates

## Geometric Properties

t1... tn Thickness at each node.

## Material Properties

Hygro-Thermal Linear Isotropic

Nonlinear Isotropic

MATERIAL PROPERTIES HYGROTHERMAL LINEAR MATERIAL PROPERTIES HYGROTHERMAL CONCRETE

## Loading

| Initial Conditions | TMPE | Initial temperature $\left(\mathrm{T}_{0}\right)$ and concrete relative humidity ( RH ) per element. |
| :---: | :---: | :---: |
|  | TMP | Initial temperature ( $\mathrm{T}_{0}$ ) and concrete relative humidity ( RH ) per global nodes. |
| Prescribed Values | TDSP | Temperature ( T ) and concrete relative humidity $(\mathrm{RH})$ at nodes. |
|  | RGN | Rates of heat (QT) and/or water inflow (QW) concentrated at nodes. |
|  | RBVE | Rates of heat and/or water inflow per unit volume, per element, can vary across the element. |
|  | RBV | Rates of heat and/or water inflow per unit volume, per global nodes. |
|  | RIHG | Rates of heat and/or water inflow per unit volume, per element at a specific reference nodal temperature (See Notes.) |
| Boundary Conditions | FFL | Rates of heat and/or water inflow per unit area (flux). |
|  | ENVT | Environmental boundary condtions. Tenv, hc, $\mathrm{hr}, \mathrm{RH}, \mathrm{hw}$ : external environmental temperature, convective and radiative heat transfer coefficients, environmental relative humidity, water mass transfer coefficient. (See Notes.) |
|  | TDET | Temperature dependent environmental boundary conditions. Tenv, hc, hr, RH, hw, T: external environmental temperature, convective and radiative heat transfer coefficients, environmental relative humidity, water mass transfer coefficient and reference nodal temperature. (See Notes.) |

## LUSAS Output

Solver | Temperature gradients | $\mathrm{G}_{\mathrm{T}} \mathrm{X}, \mathrm{G}_{\mathrm{T}} \mathrm{Y}$, (in global directions) |
| :--- | :--- |
| Water saturation gradients | $\mathrm{G}_{\mathrm{W}} \mathrm{X}, \mathrm{G}_{\mathrm{W}} \mathrm{Y}$, (in global directions) |
| Temperature fluxes | $\mathrm{qX}, \mathrm{qY}$ (in global directions) |
| Water fluxes | $\mathrm{J}_{\mathrm{w}} \mathrm{X}, \mathrm{J}_{\mathrm{w}} \mathrm{Y}$, (in global directions) |
| Vapour fluxes | $\mathrm{J}_{\mathrm{V}} \mathrm{X}, \mathrm{J}_{\mathrm{v}} \mathrm{Y}$, (in global directions) |
| Modeller | See Results Tables (Appendix K). |.

## Local Axes

$\square$ Standard surface element

## Sign Convention

$\square$ Standard field element

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

1-point (THT3), 3-point (THT6), 2x2 (QHT4), 3x3 (QHT8).

## Options

55 Output all element Gauss point derivatives and state variables

## Notes on Use

1. The element formulations are based on the standard isoparametric approach. The variation of temperature and capillary pressure within an element is linear for the low order triangle and bi-linear for the low order quadrilateral; similarly it is quadratic for the higher order triangle and bi-quadratic for the higher order quadrilateral.
2. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear transient solution progresses.
3. Decreasing permeability and increasing water vapour convection coefficient in ENVT may result in divergence and an unstable solution. A rough estimate for the latter may be obtained by dividing the heat convection coefficient by a factor of 104 (obtained by the Chilton-Colburn analogy and scaled by an average porosity).
4. Variable thickness results in a heat and moisture transfer that is not in the plane of the element, this effect is neglected. The variable thickness influences only the amount of heat and moisture stored in the element's volume.
5. Heat of hydration loading is defined via the hygro-thermal concrete material properties.
6. Concrete relative humidity RH in TMPE, TMP and TPDSP is internally converted to capillary pressure (Pc).
7. ENVT load over the area of the element cannot be modelled.

## Restrictions

Ensure mid-side node centrality
$\square$ Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio
$\square$ Certain combinations of permeability and convection boundary water vapour transfer coefficient may result in problems that do not converge.

## Recommendations on Use

The plane hygro-thermal elements may be utilised for analysing continuum problems involving the heat of hydration of concrete, when behaviour is essentially two dimensional. These elements are normally used in a hygro-thermal-structural coupled analysis. They can be coupled with plane strain structural elements (since the heat/moisture exchange over the area of the element would have effect only near both ends of the 'infinite' thickness), or with thin, plane stress elements, when they are ideally isolated on both sides of their area.

## 2D Axisymmetric Solid Hygro-Thermal Elements

## General



Element Group Hygro-Thermal
Element Axisymmetric Solid Hygro-Thermal
Subgroup
Element
Description
A family of axi-symmetric solid hygro-thermal elements in 2D with higher order elements capable of modelling curved boundaries. The elements can be used in hygro-thermal transient analyses, i.e. heat and moisture flow in porous media, e.g. concrete.
$3,4,6$, or 8 numbered anticlockwise.
Number Of
Nodes
Freedoms
T, Pc: Temperature and capillary pressure at each node.
Node X, Y: at each node
Coordinates

## Geometric Properties

Not applicable (a unit radian segment is assumed).
Material Properties

| Hygro-Thermal | Linear Isotropic | MATERIAL PROPERTIES HYGRO- |
| :--- | :--- | :--- |
|  |  | THERMAL LINEAR |

## Loading

Initial Conditions TMPE

TMP

Prescribed Values TDSP

RGN

RBVE

RBV

RIHG

Boundary FFL
Conditions
ENVT

TDET

Initial temperature $\left(\mathrm{T}_{0}\right)$ and concrete relative humidity ( RH ) per element.
Initial temperature ( $\mathrm{T}_{0}$ ) and concrete relative humidity (RH) per global nodes.
Temperature ( T ) and concrete relative humidity (RH) at nodes.
Rates of heat (QT) and/or water inflow (QW) concentrated at nodes.
Rates of heat and/or water inflow per unit volume, per element, can vary across the element.
Rates of heat and/or water inflow per unit volume, per global nodes.
Rates of heat and/or water inflow per unit volume, per element at a specific reference nodal temperature (See Notes.)
Rates of heat and/or water inflow per unit area (flux).
Environmental boundary condtions. Tenv, hc, hr, RH, hw: external environmental temperature, convective and radiative heat transfer coefficients, environmental relative humidity, water mass transfer coefficient. (See Notes.)
Temperature dependent environmental boundary conditions. Tenv, hc, hr, RH, hw, T: external environmental temperature, convective and radiative heat transfer coefficients, environmental relative humidity, water mass transfer coefficient and reference nodal temperature. (See Notes.)

## LUSAS Output

| Solver | Temperature gradients | $\mathrm{G}_{\mathrm{T}} \mathrm{X}, \mathrm{G}_{\mathrm{T}} \mathrm{Y}$, (in global directions) |
| :---: | :---: | :---: |
|  | Water saturation gradients | $\mathrm{G}_{\mathrm{W}} \mathrm{X}, \mathrm{G}_{\mathrm{W}} \mathrm{Y}$, (in global directions) |
|  | Temperature fluxes | $\mathrm{qX}, \mathrm{qY}$ (in global directions) |
|  | Water fluxes | $\mathrm{J}_{\mathrm{w}} \mathrm{X}, \mathrm{J}_{\mathrm{w}} \mathrm{Y}$, (in global directions) |
|  | Vapour fluxes | $\mathrm{J}_{\mathrm{v}} \mathrm{X}, \mathrm{J}_{\mathrm{v}} \mathrm{Y}$, (in global directions) |
| Modeller |  | See Results Tables (Appendix K) |

## Local Axes

- Standard surface element


## Sign Convention

$\square$ Standard field element

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

1-point (TXHT3), 3-point (TXHT6), 2x2 (QXHT4), 3x3 (QXHT8).

## Options

47 Axisymmetry about the global X-axis
55 Output all element Gauss point derivatives and state variables

## Notes on Use

1. The element formulations are based on the standard isoparametric approach. The variation of temperature and capillary pressure within an element is linear for the low order triangle and bi-linear for the low order quadrilateral; similarly it is quadratic for the higher order triangle and bi-quadratic for the higher order quadrilateral.
2. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear transient solution progresses.
3. Decreasing permeability and increasing water vapour convection coefficient in ENVT may result in divergence and an unstable solution. A rough estimate for the latter may be obtained by dividing the heat convection coefficient by a factor of 104 (obtained by the Chilton-Colburn analogy and scaled by an average porosity).
4. Variable thickness results in a heat and moisture transfer that is not in the plane of the element, this effect is neglected. The variable thickness influences only the amount of heat and moisture stored in the element's volume.
5. Heat of hydration loading is defined via the hygro-thermal concrete material properties.
6. Concrete relative humidity RH in TMPE, TMP and TPDSP is internally converted to capillary pressure (Pc).

## Restrictions

Ensure mid-side node centrality
$\square$ Avoid excessive element curvature

- Avoid excessive aspect ratio

Certain combinations of permeability and convection boundary water vapour transfer coefficient may result in problems that do not converge.

## Recommendations on Use

The axi-symmetric solid hygro-thermal elements may be utilised for analysing continuum problems involving the heat of hydration of concrete, which exhibit geometric and loading symmetry about a given axis. These elements are normally used in a hygro-thermal-structural coupled analysis.

## 3D Solid Hygro-Thermal Elements

## General



PHT6


## HHT8



THT10


PHT12


HHT16


## PHT15



HHT20


## Element Group

Hygro-Thermal

## Element

Solid Hygro-Thermal
Subgroup
Element
A family of solid hygro-thermal elements in 3D with higher order
Description
elements capable of modelling curved boundaries. The elements can be
used in hygro-thermal transient analyses, i.e. heat and moisture flow in porous media, e.g. concrete
Number Of 4 and 10 (tetrahedra). 6, 12 and 15 (pentahedra). 8,16 and 20

## Nodes

 (hexahedra). The elements are numbered according to a right-hand screw rule in the local z-direction.Freedoms
Node
T, Pc: Temperature and capillary pressure at each node.
$\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.
Coordinates

## Geometric Properties

Not applicable.

## Material Properties

Hygro-Thermal Linear Isotropic

Nonlinear Isotropic

MATERIAL PROPERTIES HYGROTHERMAL LINEAR MATERIAL PROPERTIES HYGROTHERMAL CONCRETE

## Loading

Initial Conditions TMPE
TMP

Prescribed Values TDSP

RGN

RBVE

RBV

RIHG

Boundary FFL
Conditions
ENVT

Initial temperature $\left(\mathrm{T}_{0}\right)$ and concrete relative humidity ( RH ) per element.
Initial temperature ( $\mathrm{T}_{0}$ ) and concrete relative humidity ( RH ) per global nodes.
Temperature ( T ) and concrete relative humidity (RH) at nodes.
Rates of heat (QT) and/or water inflow (QW) concentrated at nodes.
Rates of heat and/or water inflow per unit volume, per element, can vary across the element.
Rates of heat and/or water inflow per unit volume, per global nodes.
Rates of heat and/or water inflow per unit volume, per element at a specific reference nodal temperature (See Notes.)
Rates of heat and/or water inflow per unit area (flux).
Environmental boundary condtions. Tenv, hc, hr , RH, hw: external environmental temperature,
convective and radiative heat transfer coefficients, environmental relative humidity, water mass transfer coefficient. (See Notes.)
Temperature dependent environmental boundary conditions. Tenv, hc, hr, RH, hw, T: external environmental temperature, convective and radiative heat transfer coefficients, environmental relative humidity, water mass transfer coefficient and reference nodal temperature. (See Notes.)

## LUSAS Output

| SolverTemperature gradients | $\mathrm{G}_{\mathrm{T}} \mathrm{X}, \mathrm{G}_{\mathrm{T}} \mathrm{Y}, \mathrm{G}_{\mathrm{T}} \mathrm{Z}$ (in global directions) |
| :--- | :--- |
| Water saturation <br> gradients | $\mathrm{G}_{\mathrm{W}} \mathrm{X}, \mathrm{G}_{\mathrm{W}} \mathrm{Y}, \mathrm{G}_{\mathrm{W}} \mathrm{Z}$ (in global directions) |
| Temperature fluxes | $\mathrm{qX}, \mathrm{qY}, \mathrm{qZ}$ (in global directions) |
| Water fluxes | $\mathrm{J}_{\mathrm{w}} \mathrm{X}, \mathrm{J}_{\mathrm{w}} \mathrm{Y}, \mathrm{J}_{\mathrm{w}} \mathrm{Z}$ (in global directions) |
| Vapour fluxes | $\mathrm{J}_{\mathrm{v}} \mathrm{X}, \mathrm{J}_{\mathrm{v}} \mathrm{Y}, \mathrm{J}_{\mathrm{w}} \mathrm{Z}$ (in global directions) |
| Modeller | See Results Tables (Appendix K).. |

## Local Axes

Not applicable (global axes are the reference).

## Sign Convention

$\square$ Standard field element

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

1-point (THT4), 5-point (THT10), $3 \times 2$ (PHT6, PHT12, PHT15), $2 \times 2 \times 2$ (HHT8), $3 \times 3 \times 2$ (HHT16), 3x3x3 (HHT20)

## Options

55 Output all element Gauss point derivatives and state variables

## Notes on Use

1. The element formulations are based on the standard isoparametric approach. The distribution of temperature and capillary pressure within an element may be regarded as linear or bilinear for low order elements and quadratic or bi-qudratic for higher order elements.
2. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear solution progresses.
3. Decreasing permeability and increasing water vapour convection coefficient in ENVT may result in divergence and an unstable solution. A rough estimate for the latter may be obtained by dividing the heat convection coefficient by a factor of 104 (obtained by the Chilton-Colburn analogy and scaled by an average porosity).
4. Heat of hydration loading is defined via the hygro-thermal concrete material properties.
5. Concrete relative humidity RH in TMPE, TMP and TPDSP is internally converted to capillary pressure (Pc).

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio
$\square$ Certain combinations of permeability and convection boundary water vapour transfer coefficient may result in problems that do not converge.


## Recommendations on Use

The solid hygro-thermal elements may be used to analyse continuum problems where the response is fully 3D (i.e. it cannot be approximated using the plane or axisymmetric elements). These elements are generally used for problems involving the heat of hydration of concrete, and are normally used in a hygro-thermal-structural coupled analysis.

## Chapter 11: Interface Elements.

## 2D Interface Element

## General



Element Group Interface

## Element <br> 2D Interface

Subgroup
Element A family of 2D interface elements used for modelling standard Mohr-
Description
Coulomb friction contact as well as delamination for plane stress, plane strain and axisymmetric crack propagation. An initial gap is allowed for Mohr-Coulomb friction contact but not for delamination.
Number Of
4,6
Nodes
Freedoms
Node X, Y: at each node.
Coordinates

## Geometric Properties

Not applicable to plane strain and axisymmetric elements.
For plane stress t1..tn for each node

## Material Properties

## Linear Not applicable

Matrix Not applicable
Joint Not applicable
Concrete Not applicable
Elasto-Plastic Not applicable
Creep Not applicable
Damage Not applicable
Viscoelastic Not applicable
Shrinkage Not applicableInterface Interface MATERIAL PROPERTIES NONLINEAR25
MATERIAL PROPERTIES INTERFACE Interface
Rubber Not applicable
Generic Polymer Not applicable
Composite Not applicable
Loading
Prescribed ValueConcentratedPDSP, TPDSPCL
Loads
Element Loads Not applicable.
Distributed Loads Not applicable.
Body Forces Not applicable.VelocitiesAccelerationsVELOACCE
Initial Not applicable.
Stress/Strains
Residual Stresses Not applicable.
Target Not applicable.
Stress/Strains
Temperatures TEMP, TMPEVelocities. Vx, Vy: at nodes.Acceleration Ax, Ay: at nodes.
Prescribed variable. U, V: at each node.Concentrated loads. Px, Py: at each node.
Temperatures at nodes/for element. T, $0,0,0$, To, $0,0,0$
Overburden Not applicable.
Phreatic Surface Not applicable.Field Loads Not applicable.
Temp Dependent Not applicable.

## LUSAS Output

Solver Stress (default): shear and direct tractions. Strain: shear and direct relative displacements Modeller See Results Tables (Appendix K).

## Local Axes



## Sign Convention

A positive traction occurs if the local relative displacement (with respect to the first line of the element) is a positive value, i.e. for the quadratic elements at nodes $3>6$ the local relative displacement, Ez, would be positive if (DZ3 - DZ6) $>0$, where DZi is the local displacement at node i.

## Formulation

## Geometric Nonlinearity

| Total Lagrangian | Not applicable. |
| ---: | :--- |
| Updated <br> Lagrangian | Not applicable. |
| Eulerian | Not applicable. |
| Co-rotational | Applicable to IPN4 and IAX4 elements. |

## Integration Schemes

Stiffness Default. 2 (Newton Cotes) (IPN4, IPM4, IAX4) 3 (Newton-Cotes) (IPN6, IPM6, IAX6)
Fine. As default

## Mass Modelling

Not applicable.

## Options

62 Continue solution if more than one negative pivot occurs
64 Non-symmetric solver
229 Co-rotational geometric non-linearity.
252 Suppress pivot warning messages.
261 Select the root with the lowest residual norm with arc-length.

## Notes on use in delamination analyses

1. When defining the transient analysis control the arc-length procedure should be adopted with the option to select the root with the lowest residual norm [option 261].
2. It is recommended that fine integration [option 18] is selected for the parent elements.
3. The nonlinear convergence criteria should be selected to converge on the residual norm.
4. Option 62, Continue solution if more than one negative pivot occurs, should be selected to continue if more than one negative pivot is encountered and option 252 should be used to suppress pivot warning messages from the solution process.
5. The non-symmetric solver is selected automatically when mixed mode delamination is specified.
6. Although the solution is largely independent of the mesh discretisation, to avoid convergence difficulties it is recommended that at least 2 elements are placed in the process zone.

## Restrictions

None.

## Recommendations on Use

These elements may be used to model contact between two bodies. For delamination problems they should be placed at sites of potential delamination between 2D plane and axisymmetric continuum elements. The non-symmetric solver should be used.

## 2D Two Phase Interface Element

## General

Element Name
IPN6P, IAX6P


Element Group Interface
Element 2D Two-phase Interface
Subgroup
Element A family of 2D interface elements used for modelling standard Mohr-
Description Coulomb friction contact in soil/structure interactions.
Number Of 6
6
Nodes
Freedoms U, V, P: at end nodes, U,V at middle nodes.
Node X, Y: at each node.
Coordinates

## Geometric Properties

Not applicable to plane strain and axisymmetric elements.
For plane stress t 1 ..tn for each node

## Material Properties

Linear Not applicable
Matrix Not applicable
Joint Not applicable
Concrete Not applicable
Elasto-Plastic Not applicable
Creep Not applicable
Damage Not applicable
Viscoelastic Not applicable
Shrinkage Not applicable Interface Interface
Interface
Rubber Not applicable
Generic Polymer Not applicable
Composite Not applicable
Two-Phase Interface

## Loading

Prescribed Value PDSP, TPDSP

Concentrated CL
Loads
Element Loads Not applicable.
Distributed Loads Not applicable.
Body Forces Not applicable.
Velocities VELO
Accelerations ACCE
Initial Not applicable.
Stress/Strains
Residual Stresses Not applicable.
Target Not applicable.
Stress/Strains
Temperatures TEMP, TMPE

Overburden Not applicable.
Phreatic Surface Not applicable.
Field Loads Not applicable.
Temp Dependent Not applicable.

TWO PHASE MATERIAL INTERFACE
MATERIAL PROPERTIES NONLINEAR 25
MATERIAL PROPERTIES INTERFACE


## LUSAS Output

Solver Stress (default): shear and direct tractions.
Strain: shear and direct relative displacements
Modeller See Results Tables (Appendix K).

## Local Axes

Element Name IPN6P, IAX6P
Evaluated at each node.


## Sign Convention

A positive traction occurs if the local relative displacement (with respect to the first line of the element) is a positive value, i.e. for the quadratic elements at nodes $3>6$ the local relative displacement, Ez, would be positive if (DZ3 - DZ6) $>0$, where DZi is the local displacement at node i.

## Formulation

## Geometric Nonlinearity

Total Lagrangian
Updated
Lagrangian
Eulerian
Co-rotational

Not applicable.
Not applicable.

Not applicable.
Not applicable.

## Integration Schemes

## Stiffness Default. 3 (Newton-Cotes)

Fine. As default

## Mass Modelling

Not applicable.

## Options

64 Non-symmetric solver

## Restrictions

None.

## Recommendations on Use

These elements should be used to model soil/structure and soil/soil interactions. The nonsymmetric solver should be used.

## 3D Interface Element

## General



IS6


> IS12


## IS8



IS16


Element Group
Interface
Element
3D Interface
Subgroup
Element
Description
Number Of
6,8,12,16
Nodes
Freedoms
Node
Coordinates crack propagation.

A family of 3D interface elements used for modelling delamination and

U, V, W: at each node.
$\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.

## Geometric Properties

Not applicable (a zero thickness is assumed).

## Material Properties

$$
\begin{aligned}
\text { Linear } & \text { Not applicable } \\
\text { Matrix } & \text { Not applicable } \\
\text { Joint } & \text { Not applicable }
\end{aligned}
$$

Concrete Not applicable Elasto-Plastic Not applicable Creep Not applicable
Damage Not applicable Viscoelastic Not applicable Shrinkage Not applicable Interface Interface Interface
Rubber Not applicable Generic Polymer Not applicable Composite Not applicable

MATERIAL PROPERTIES NONLINEAR 25

MATERIAL PROPERTIES INTERFACE

## Loading

| Prescribed Value Concentrated Loads | PDSP, TPDSP CL | Prescribed variable. U, V, W: at each node. Concentrated loads. Px, Py, Pz: at each node. |
| :---: | :---: | :---: |
| Element Loads | Not applicable. |  |
| Distributed Loads | Not applicable. |  |
| Body Forces | Not applicable. |  |
| Velocities | VELO | Velocities. Vx, Vy, Vz: at nodes. |
| Accelerations | ACCE | Acceleration Ax, Ay, Az: at nodes. |
| Initial Stress/Strains | Not applicable. |  |
| Residual Stresses | Not applicable. |  |
| Target Stress/Strains | Not applicable. |  |
| Temperatures | TEMP, TMPE | Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}$, $0,0,0$ |
| Overburden | Not applicable. |  |
| Phreatic Surface | Not applicable. |  |
| Field Loads | Not applicable. |  |

## Temp Dependent Not

Loads applicable.

## LUSAS Output

Solver Stress (default): shear tractions in X and Y , and direct tractions. Strain: relative displacements in $\mathrm{X}, \mathrm{Y}$ and Z directions.
Modeller See Results Tables (Appendix K).

## Local Axes

## Element Name

IS6
Evaluated at each node.


IS12
Evaluated at each node.


IS8


IS16


## Sign Convention

A positive traction occurs if the local relative displacement (with respect to the first surface of the element) is a positive value, i.e. for the IS16 element at nodes $3>11$ the local relative displacement, EZ, would be positive if $(\mathrm{DZ} 11-\mathrm{DZ3})>0$, where DZi is the local displacement at node i.

## Formulation

## Geometric Nonlinearity

## Total Lagrangian Not applicable.

Updated Not applicable.
Lagrangian
Eulerian Not applicable.
Co-rotational Applicable to IS6 and IS8 elements.

## Integration Schemes

Stiffness Default. $3 \times 3$ (Newton-Cotes) (IS16), $2 \times 2$ (Newton Cotes) (IS8), 7-point cubic (IS12), 3-point (IS6)
Fine. As default

## Mass Modelling

Not applicable.

## Options

62 Continue solution if more than one negative pivot occurs.
64 Non-symmetric solver.
229 Co-rotational geometric non-linearity.
252 Suppress pivot warning messages
261 Select the root with the lowest residual norm with arc-length.

## Notes on Use

1. When defining the transient analysis control the arc-length procedure should be adopted with the option to select the root with the lowest residual norm [option 261].
2. It is recommended that fine integration [option 18] is selected for the parent elements.
3. The nonlinear convergence criteria should be selected to converge on the residual norm.
4. Option 62, Continue solution if more than one negative pivot occurs, should be selected to continue if more than one negative pivot is encountered and option 252 should be used to suppress pivot warning messages from the solution process.
5. The non-symmetric solver is selected automatically when mixed mode delamination is specified.
6. Although the solution is largely independent of the mesh discretisation, to avoid convergence difficulties it is recommended that at least 2 elements are placed in the process zone.

## Restrictions

None.

## Recommendations on Use

These elements should be used at places of potential delamination between 3D continuum elements. The non-symmetric solver should be used.

## 3D Two Phase Interface Element

## General



## Geometric Properties

Not applicable (a zero thickness is assumed).

## Material Properties

| Linear | Not applicable |  |
| ---: | :--- | :--- |
| Matrix | Not applicable |  |
| Joint | Not applicable |  |
| Concrete | Not applicable |  |
| Elasto-Plastic | Not applicable |  |
| Creep | Not applicable |  |
| Damage | Not applicable |  |
| Viscoelastic | Not applicable |  |
| Shrinkage | Not applicable |  |
| Interface | Interface | MATERIAL PROPERTIES NONLINEAR |
|  |  | 25 |

Interface
Two-phase Interface
Rubber Not applicable Generic Polymer Not applicable Composite Not applicable

## Loading

| Prescribed Value | PDSP, TPDSP | Prescribed variable. U, V, W, Q: at corner nodes $\mathrm{U}, \mathrm{V}, \mathrm{W}$ at midside nodes. |
| :---: | :---: | :---: |
| Concentrated Loads | CL | Concentrated loads. Px, Py, Pz, Q: at corner nodes, $\mathrm{Px}, \mathrm{Py}, \mathrm{Pz}$ at midside nodes. |
| Element Loads | Not applicable. |  |
| Distributed Loads | Not applicable. |  |
| Body Forces | Not applicable. |  |
| Velocities | VELO | Velocities. Vx, Vy, Vz: at nodes. |
| Accelerations | ACCE | Acceleration Ax, Ay, Az: at nodes. |
| Initial Stress/Strains | Not applicable. |  |
| Residual Stresses | Not applicable. |  |
| Target Stress/Strains | Not applicable. |  |
| Temperatures | TEMP, TMPE | Temperatures at nodes/for element. T, $0,0,0, \mathrm{To}$, $0,0,0$ |
| Overburden | Not applicable. |  |
| Phreatic Surface | Not applicable. |  |
| Field Loads | Not applicable. |  |
| Temp Dependent Loads | Not applicable. |  |

## LUSAS Output

Solver Stress (default): shear tractions in X and Y, and direct tractions. Strain: relative displacements in $\mathrm{X}, \mathrm{Y}$ and Z directions.
Modeller See Results Tables (Appendix K).

## Local Axes

## Element Name

IS6
Evaluated at each node.


IS12
Evaluated at each node.


IS8


IS16


## Sign Convention

A positive traction occurs if the local relative displacement (with respect to the first surface of the element) is a positive value, i.e. for the IS16 element at nodes $3>11$ the local relative displacement, Ez, would be positive if (DZ11-DZ3) $>0$, where DZi is the local displacement at node i.

## Formulation

## Geometric Nonlinearity

## Total Lagrangian <br> Not applicable.

Updated
Not applicable.
Lagrangian
Eulerian Not applicable.
Co-rotational Applicable to IS6 and IS8 elements.

## Integration Schemes

$$
\begin{array}{ccl}
\text { Stiffness } & \text { Default. } & \begin{array}{l}
3 \times 3(\underline{\text { Newton-Cotes }}) \\
\\
\\
\text { (IS12), 3-point (IS16), } 2 \times 2 \text { (Newton Cotes) (IS8), 7-point cubic }
\end{array} \\
\text { Fine. } & \text { As default }
\end{array}
$$

## Mass Modelling

Not applicable.

## Options

64 Non-symmetric solver.

## Restrictions

None.

## Recommendations on Use

These elements should be used to model soil/structure and soil/soil interactions. The nonsymmetric solver should be used.

## Chapter 12 : NonStructural Mass Elements

## 2D Point Mass Element



## Geometric Properties

Not applicable.

## Material Properties

## Linear Not applicable

Matrix Not applicable
Joint Not applicable
Mass 2D
MATERIAL PROPERTIES MASS 21
Concrete Not applicable
Elasto-Plastic Not applicable
Creep Not applicable
Damage Not applicable
Viscoelastic Not applicable

# Shrinkage Not applicable <br> Rubber Not applicable <br> Generic Polymer Not applicable <br> Composite Not applicable <br> Field Not applicable 

## Loading

| Prescribed |  |
| ---: | :--- |
| Value | CBF | | Constant body forces for element. Xcbf, Ycbf, |
| :--- |
| Zcbf (applied as accelerations) |

## LUSAS Output

None

## Local Axes

The 2 nd node is used to define the local x -axis.

## Sign Convention

$\square$ Not applicable.
Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Not applicable.

## Mass Modelling

Consistent mass (default).
$\square$ Lumped mass.

## Options

105 Lumped mass matrix.

## Notes on Use

1. Use to model point mass in a structure.

## Restrictions

None.

## Recommendations on Use

The 2D point mass element can be used to model point masses occur in a 2D structure.

## 3D Point Mass Element



## Geometric Properties

Not applicable.

## Material Properties

Linear Not applicable
Matrix Not applicable
Joint Not applicable
Mass 3D.
MATERIAL PROPERTIES MASS 31

Concrete Not applicable
Elasto-Plastic Not applicable
Creep Not applicable

# Damage Not applicable <br> Viscoelastic Not applicable <br> Shrinkage Not applicable <br> Rubber Not applicable <br> Generic Polymer Not applicable <br> Composite Not applicable 

## Loading

Prescribed Value CBF Constant body forces for element. Xcbf, Ycbf, Zcbf (applied as accelerations)

## Output

None

## Local Axes

The $2^{\text {nd }}$ node is used to define the local $x$-axis. The $2^{\text {nd }}$ and $3^{\text {rd }}$ node define the local $x-y$ plane.

## Sign Convention

$\square$ Not applicable.

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Not applicable.

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

105 Lumped mass matrix.

## Notes on Use

1. Use to model point mass in a structure.

## Restrictions

None.

## Recommendations on Use

The 3D point mass element can be used to model point masses occur in a 3D structure.

## 3D Line Mass Elements

## General



LMS3


LMS4


## Element Group Non-Structural Mass

Element 3D Line
Subgroup
Element
Description
3D straight (LMS3) and curved (LMS4) line mass elements to model
mass along an edge. The elements can accommodate varying mass along the length.
Number Of 3 (LMS3). The $3^{\text {rd }}$ node is used to define the local $x-y$ plane.
Nodes 4 (LMS4). The $4^{\text {th }}$ node is used to define the local $x-y$ plane.
End Releases
Freedoms U, V, W, $\theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$ : at each active node (see Notes).
Node $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ : at each node.
Coordinates

## Geometric Properties

Not applicable.

## Material Properties

Linear Not applicable
Matrix Not applicable
Joint Not applicable.
Mass 3D.
MATERIAL PROPERTIES MASS 32 ( or 3)
Concrete Not applicable
Elasto-Plastic Not applicable
Creep Not applicable
Damage Not applicable

# Viscoelastic Not applicable <br> Shrinkage Not applicable <br> Rubber Not applicable <br> Generic Polymer Not applicable <br> Composite Not applicable 

## Loading

## Prescribed Value CBF Constant body forces for element. Xcbf, Ycbf, Zcbf (applied as accelerations)

## Output

None

## Local Axes

Standard Line Element

## Sign Convention

$\square$ Not applicable.

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Mass Default. 2-point
Fine 2-point (LMS2), 3-point (LMS3)

## Mass Modelling

Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule.
105 Lumped mass matrix.

## Notes on Use

1. Use to model mass on an edge in a structure.
2. There is no mass associated with the rotational degrees of freedom $\theta \mathrm{x}, \theta \mathrm{y}, \theta \mathrm{z}$; these freedoms are used purely to orientate the directions of the local element axes. If the LMS3/LMS4 elements are connected to an element that does not possess the same rotational degrees of freedom (e.g. the edge of a continuum element), then the rotational degrees of freedom will automatically be restrained

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature


## Recommendations on Use

3D line mass elements can be used to model masses along an edge in a 3D structure.

## 2D Line Mass Elements

## General



LM3


## Element Group Non-Structural Mass

> Element 2D Line

Subgroup
Element 2D straight (LM2) and curved (LM3) line mass elements to model mass
Description along an edge. The elements can accommodate varying mass along the length.
Number Of 2 (LM2). 3 (LM3). Nodes
End Releases
Freedoms U, V: at each node.
Node X, Y: at each node.
Coordinates

## Geometric Properties

Not applicable.

## Material Properties

Linear Not applicable
Matrix Not applicable
Joint Not applicable
Mass 2D.
MATERIAL PROPERTIES MASS 22 ( or 3)
Concrete Not applicable
Elasto-Plastic Not applicable
Creep Not applicable
Damage Not applicable

# Viscoelastic Not applicable <br> Shrinkage Not applicable <br> Rubber Not applicable <br> Generic Polymer Not applicable <br> Composite Not applicable 

## Loading

Prescribed Value CBF Constant body forces for element. Xcbf, Ycbf, Zcbf (applied as accelerations)

## Output

None

## Local Axes

Standard Line Element

## Sign Convention

$\square$ Not applicable.

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Mass Default. 2-point
Fine 2-point (LM2), 3-point (LM3)

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule.
105 Lumped mass matrix.

## Notes on Use

1. Use to model mass on an edge in a structure.

## Restrictions

$\square$ Ensure mid-side node centrality
$\square$ Avoid excessive element curvature

## Recommendations on Use

2D line mass elements can be used to model masses along an edge in a 2 D structure.

## Surface Mass Elements

## General



## Geometric Properties

Not applicable.

## Material Properties

Linear Not applicable<br>Matrix Not applicable<br>Joint Not applicable<br>Mass 3D MATERIAL PROPERTIES MASS 3 (3,4,6 or 8)<br>Concrete Not applicable.<br>Elasto-Plastic Not applicable.<br>Creep Not applicable<br>Damage Not applicable<br>Viscoelastic Not applicable<br>Shrinkage Not applicable<br>Rubber Not applicable<br>Generic Polymer Not applicable<br>Composite Not applicable.

## Loading

Prescribed Value CBF Constant body forces for element. Xcbf, Ycbf, Zcbf (applied as accelerations)

## Output

None

## Local Axes

- Standard Surface Element


## Sign Convention

Not applicable.

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Mass Default. 1-point (TM3), 3-point (TM6), 4-point (QM4,QM8)
Fine $\quad 3$-point (TM3, TM6), 4-point (QM4), 9-point (QM8)

## Mass Modelling

$\square$ Consistent mass (default).
$\square$ Lumped mass.

## Options

18 Invokes fine integration rule.
105 Lumped mass matrix.

## Notes on Use

1. Use to model mass on a surface in a structure.

## Restrictions

Ensure mid-side node centrality

- Avoid excessive element curvature
$\square$ Avoid excessive aspect ratio


## Recommendations on Use

The surface mass elements can be used to model masses on a surface 3D structures.

# Chapter 13 : Rigid Slideline Elements 

## Rigid Slideline Surface 2D Elements

## General

## Element Name R2D2



## Element Group Rigid

Element 2D Rigid Slideline Surface
Subgroup
Element 2D Rigid Slideline Surface elements capable of modelling non-
Description deformable surfaces in a contact analysis.
Number Of 2

Nodes
Freedoms U, V at each node
Node X, Y at each node.
Coordinates

## Geometric Properties

Not applicable.

## Material Properties

Linear Isotropic:
MATERIAL PROPERTIES (Elastic: Isotropic)

## Loading

| Prescribed Value | PDSP, TPDSP | Prescribed variable. U, V at each node. |
| ---: | :--- | :--- |
| Concentrated | Not applicable. |  |
| Loads |  |  |
| Element Loads | Not applicable. |  |
| Distributed Loads | Not applicable. |  |
| Body Forces | Not applicable. | Velocities. Vx, Vy at nodes. |


| Accelerations | ACCE | Acceleration Ax, Ay at nodes. |
| ---: | :--- | :--- |
| Initial | Not applicable. |  |
| Stress/Strains |  |  |
| Residual Stresses | Not applicable. |  |
| Temperatures | Not applicable. |  |
| Field Loads | Not applicable. |  |
| Temp Dependent | Not applicable. |  |
| Loads |  |  |

## LUSAS Output

Solver Displacements \& Reactions only.
Modeller Displacements \& Reactions only.

## Formulation

## Geometric Nonlinearity

$$
\begin{aligned}
\text { Total Lagrangian } & \begin{array}{l}
\text { Depends on the other surface (deformable surface) which is in contact } \\
\text { with the rigid surface. See the related section for the deformable } \\
\text { surface elements. }
\end{array} \\
\text { Updated } & \text { As above. } \\
\text { Lagrangian } & \\
\text { Eulerian } & \text { As above. } \\
\text { Co-rotational } & \text { As above. }
\end{aligned}
$$

## Integration Schemes

Not applicable.

## Mass Modelling

Not applicable.

## Restrictions

- A rigid slideline surface cannot contact another rigid slideline surface.
- Rigid slideline surface elements do not accept external applied forces.


## Notes on use

1. All the rigid slideline surface element nodes must be fully restrained.
2. There is no stress and strain calculation for these elements.
3. If rigid slideline surfaces are defined there is no need to assign geometric and material properties to these elements. However, when using automatic contact surfaces, linear elastic isotropic material properties need to be assigned.
4. For saving analysis time a one pass contact algorithm can be used. In this case only the penetration of the deformable surface into the rigid slideline surface is checked. To avoid the penetration of the rigid surface into the deformable surface use either the default two pass algorithm or a finer mesh on the deformable surface.

## Recommendations on Use

These elements should be used when one of the surfaces which come into contact is nondeformable. Using these elements will make the analysis faster.

## Rigid Slideline Surface 3D Elements

## General

Element R3D3
Name

R3D4

Element Group Rigid
Element 3D Rigid Slideline Surface
Subgroup
Element 3D Rigid Slideline Surface elements capable of modelling non-
Descriptiondeformable surfaces in a contact analysis.
Number Of ..... 3/4
Nodes
Freedoms U, V, W at each node.
Node $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ at each node.
Coordinates

## Geometric Properties

## Not applicable.

## Material Properties

## Linear Isotropic:

## Loading

| Prescribed Value | PDSP, TPDSP |
| ---: | :--- |
| Loads | Prescribed variable. U, V, W at each node. |
| Concentrated |  |
| Element Loads | Not applicable. |
| Distributed Loads | Not applicable. |
| Body Forces | Not applicable. |


| Velocities | VELO | Velocities. Vx, Vy, Vz at nodes. |
| ---: | :--- | :--- |
| Accelerations | ACCE | Acceleration Ax, Ay, Az at nodes. |
| Initial | Not applicable. |  |
| Stress/Strains |  |  |
| Residual Stresses | Not applicable. |  |
| Temperatures | Not applicable. |  |
| Field Loads | Not applicable. |  |
| Temp Dependent | Not applicable. |  |
| Loads |  |  |

## LUSAS Output

Solver Displacements \& Reactions only.
Modeller Displacements \& Reactions only.

## Formulation

## Geometric Nonlinearity

Total Lagrangian Depends on the other surface (deformable surface) which is in contact with the rigid surface. See the related section for the deformable surface elements.
Updated As above.
Lagrangian
Eulerian As above.
Co-rotational As above.

## Integration Schemes

Not applicable.

## Mass Modelling

Not applicable.

## Restrictions

- A rigid slideline surface cannot contact another rigid surface.
- Rigid slideline surface elements do not accept external applied forces.


## Notes on use

1. All the rigid slideline surface element nodes must be fully restrained.
2. There is no stress and strain calculation for these elements.
3. If rigid slideline surfaces are defined there is no need to assign geometric and material properties to these elements. However, when using automatic contact surfaces, linear elastic isotropic material properties need to be assigned.
4. For saving analysis time a one pass contact algorithm can be used. In this case only the penetration of the deformable surface into the rigid slideline surface is checked. To avoid the penetration of the rigid surface into the deformable surface use either the default two pass algorithm or a finer mesh on the deformable surface.

## Recommendations on Use

These elements should be used when one of the surfaces which come into contact is nondeformable. Using these elements will make the analysis faster.

## Chapter 14 : <br> Phreatic Elements

## Phreatic Surface 2D Elements

## General

## Element Name PHS2 <br> 

| Element Group | Phreatic surface |
| ---: | :--- |
| Element | 2D Phreatic Surface |
| Subgroup |  |
| Element | 2D Phreatic surface elements for defiing phreatic surface |
| Description |  |
| Number Of | 2 |
| Nodes |  |
| Freedoms | U, V at each node |
| Node | X, Y at each node. |
| Coordinates |  |

## Geometric Properties

Not applicable.

## Material Properties

Not applicable.

## Loading

| Prescribed Value | PDSP, TPDSP | Prescribed variable. U, V at each node. |
| ---: | :--- | :--- |
| Concentrated | Not applicable. |  |
| Loads |  |  |
| Element Loads | Not applicable. |  |
| Distributed Loads | Not applicable. |  |
| Body Forces | Not applicable. | Velocities. Vx, Vy at nodes. |
| Velocities | VELO |  |Initial Not applicable.Stress/Strains

Residual Stresses Not applicable.
Temperatures Not applicable.
Field Loads Not applicable.
Temp Dependent Not applicable.

Not applicable.
Accelerations ACCE Acceleration Ax, Ay at nodes.

Acceleration Ax, Ay at nodes.

Not applicable.

Loads

## LUSAS Output

Not applicable.

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Not applicable.

## Mass Modelling

Not applicable.

## Restrictions

Not applicable.

## Notes on use

1. All the phreatic surface element nodes must be fully restrained.
2. There are no stress or strain calculations.
3. There is no need to assign geometric and material properties.
4. The phreatic surface elements are used with the Phreatic Surface load type and are used to define the location and extent of a phreatic surface.

## Recommendations on Use

These elements are for use in geotechnical problems for the definition of the nodal pore-water pressures and hydrostatic loads.

## Phreatic Surface 3D Elements

## General



PHS4


## Element Group

Phreatic Surface
Element
3D Phreatic Surface
Subgroup
Element 3D Phreatic surface elements for defiing phreatic surface.
Description
Number Of
3/4
Nodes
Freedoms U, V, W at each node.
Node $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$ at each node.
Coordinates

## Geometric Properties

Not applicable.

## Material Properties

Not applicable.

## Loading

Prescribed Value Concentrated

Loads
Element Loads Not applicable.
Distributed Loads Not applicable.
Body Forces Not applicable.
PDSP, TPDSP Not applicable.

Prescribed variable. U, V, W at each node.

| Velocities | VELO | Velocities. Vx, Vy, Vz at nodes. |
| ---: | :--- | :--- |
| Accelerations | ACCE | Acceleration Ax, Ay, Az at nodes. |
| Initial | Not applicable. |  |
| Stress/Strains |  |  |
| Residual Stresses | Not applicable. |  |
| Temperatures | Not applicable. |  |
| Field Loads | Not applicable. |  |
| Temp Dependent | Not applicable. |  |

## LUSAS Output

Not applicable.

## Formulation

## Geometric Nonlinearity

Not applicable.

## Integration Schemes

Not applicable.

## Mass Modelling

Not applicable.

## Restrictions

Not applicable.

## Notes on use

1. All the phreatic surface element nodes must be fully restrained.
2. There are no stress or strain calculations.
3. There is no need to assign geometric and material properties.
4. The phreatic surface elements are used with the Phreatic Surface load type and are used to define the location and extent of a phreatic surface.

## Recommendations on Use

These elements are for use in geotechnical problems for the definition of the nodal pore-water pressures and hydrostatic loads.

# Appendix A: Element and <br> <br> Pressure Loads. 

 <br> <br> Pressure Loads.}

## ELDS Element Loads

These are referred to as Internal Beam Point Loads and Internal Beam Distributed Loads within LUSAS Modeller.

| Parameter | Description |
| :---: | :---: |
| Itype | Element load type |
| S1, S2 | Distances to specified loads |
| Px, Py, Pz | Point loads in local/global directions |
| Mx, My, Mz | Point moments in local/global directions |
| Wx, Wy, Wz | Distributed loads in local/global directions |

Itype 11
Point loads and moments in local directions


Itype 21
Uniformly distributed loads in local directions


Itype 12
Point loads and moments in global directions


Itype 22
Uniformly distributed loads in global directions


Itype 31
Distributed loads in local directions. Multiple load sets supported.


Itype 23
Uniformly distributed projected loads in global directions

1
Itype 32


Distributed loads in global directions. Multiple load sets supported.


Global
Itype 41
Trapezoidal loads in local directions
Definition only supported in LUSAS Solver. In LUSAS Modeller trapezoidal beam loads are defined in accordance with Itype 31.
Wx, Wy, Wz


Local

Distributed projected loads in global directions. Multiple load sets supported.


## Itype 42

Trapezoidal loads in global directions
Definition only supported in LUSAS Solver. In LUSAS Modeller trapezoidal beam loads are defined in accordance with Itype 32.
Wx, Wy, Wz


Global

Itype 43
Trapezoidal projected loads in global directions Definition only supported in LUSAS Solver. In LUSAS Modeller trapezoidal beam loads are defined in accordance with Itype 33.


## ENVT/TDET Environmental Boundary Conditions

Contains some or all of:

| Parameter | Description |
| :---: | :---: |
| Tenv | External environmental temperature. |
| hc | Convective heat transfer coefficient. |
| RH | Radiative heat transfer coefficient. |
| hv | Vapour mass transfer coefficient. |
| T | Temperature for element. |



Face Numbering Convention for Thermal Bars

## Note

The environmental temperature loading for node 2 cannot be specified for a 3 noded bar.

## FLD Face loading applied to thermal bars



Face number $=$ local node number

## Face Numbering Convention for Thermal Bars

## Face Loads On 2D Continuum Elements

| Parameter |  |
| :--- | :--- |
| Px, Py |  |
| Face pressures defined at nodes in local $x, y$ <br> directions |  |

2-Noded Element Faces


3-Noded Element Faces


## Notes

- In structural analysis note that the direction of the normal face load is not consistent between 2D and 3D continuum elements. For 2D continuum elements it is from the
face towards the interior of the element. For 3D elements it is in the opposite direction - from the face of the element outwards.
- Face loads for explicit dynamics elements are constant, i.e. the average of the input nodal pressures


## Face Numbering Convention

## 3 Noded Elements 4 Noded Elements 6 Noded Elements 8 Noded Elements



## Face Loads On 3D Continuum Elements

$\frac{\text { Parameter }}{\text { Px, Py, Pz }} \frac{\text { Description }}{$|  Face pressures defined at nodes in local $x, y \text { directions acting positively in the local }$ |
| :--- |
|  coordinate directions  |}

## Note

- In structural analysis note that the direction of the normal face load is not consistent between 2D and 3D continuum elements. For 2D continuum elements it is from the face towards the interior of the element. For 3D elements it is in the opposite direction - from the face of the element outwards.
- Face loads for explicit dynamics elements are constant, i.e. the average of the input nodal pressures.+


## Local Face Coordinates



## Face Numbering Convention

The following diagrams show exploded view of the various 3D elements. The grey faces show the element external faces that can be seen from a single perspective point, the white faces depict the internal faces from the same view point.

## Notes

- The views of the internal faces show the x -axis direction from the inside. Take care when converting this to a view from the outside of the element.




## UDL Loads on Shells



## Appendix B: Element Restrictions.

## Mid-side Node Centrality

The mid-length node must be equidistant from the end nodes. Mid-side nodes may be automatically corrected for elements with global translational mid-side node freedoms using Option 49. The mid-side node is moved along the existing element edge until it is positioned centrally.

## Excessive Element Curvature

Elements must not be excessively curved. A warning will be invoked (but the analysis will continue) if the element curvature is not in accordance with the following inequalities:
i) $\mathrm{ABS}(\mathrm{S} 1-\mathrm{S} 2) /(\mathrm{S} 1+\mathrm{S} 2)<0.05$
ii) $(S 1+S 2) / S 3<1.02$


Where the function ABS returns the absolute value of the arguments.

## Excessive Aspect Ratios

An aspect ratio can be defined as the ratio of the longest to shortest element side lengths, such that:

R $\quad$ max ( $\mathrm{a} / \mathrm{b}, \mathrm{b} / \mathrm{a}$ ) for surface elements (e.g. 2D continuum, plates and shells)
$\square R=\max (\mathrm{a} / \mathrm{b}, \mathrm{b} / \mathrm{a}, \mathrm{c} / \mathrm{a}, \mathrm{c} / \mathrm{b}, \ldots)$ for three dimensional solid elements


Elements must not have an excessive aspect ratio. A warning will be invoked (but the analysis will continue) if the element aspect ratio is greater than 10.
In general, severe distortion of an element will affect the accuracy of the stress distribution through an element. The type of stress field being imposed is also of importance, since a badly shaped element will still yield a good distribution in the presence of a constant uniaxial stress field, but not when subjected to a full stress field in which any of the components have a significant variation across the element.
The force equilibrium for the element will always be satisfied.

## Excessive Warping

The four nodal points defining quadrilateral surface elements should be coplanar. However a small out of plane tolerance is permitted to allow a slightly warped shape according to

$$
\mathrm{z}<0.01(\mathrm{~L} 12)
$$

where $\mathbf{z}$ is the out of plane distance of a node, and L12 is the length between the first and second nodes.
If the above inequality is exceeded a warning will be issued but the analysis will proceed.

# Appendix C : Local Element Axes. 

## Standard Joint Element

Local x-axis The local x-axis is defined by the vector between the first and the third nodes of the element topology.

## Note.

The third node must be different from nodes 1 and 2 of the topology.

## Standard Line Element

Local x axis The local x -axis lies along the element in the direction in which the element nodes are defined. For curved elements the local x -axis is the tangent to the curve.
Local y axis The local xy plane is either defined by a dummy node and the two end nodes, or (in the absence of a dummy node), defined by the two end nodes and the central node. For the latter case, the local $y$-axis is perpendicular to the x -axis and on the positive convex side.
Local z axis The local z -axis forms a right-handed set with the local xy plane.
For cross-section beams the top surface is defined by the local +ve z direction.

## Note

Default line axes are defined in Modeller with the local x axis of the element following the line direction. The element local z is then defined in the XZ plane unless the local x axis is aligned to the global Z axis in which case the element local z axis is aligned with the global Y axis.

## Standard Surface Element

Local $\mathbf{x}$ axis For 3 or 4 noded elements the local x -axis is defined by a line joining the first and second element nodes. For 6 and 8 noded elements the local $x$-axis is the tangent to the curve between the first 3 nodes.
Local $y$ axis The local $x y$-plane is defined by the remaining nodes, the local $y$-axis being perpendicular to the x -axis and forming a right-handed set with the x -axis and the xy plane.

## Element Reference Manual

Local z-axis The local z -axis forms a right-handed set with the local x and y -axes. For shell elements the top surface is defined by the local +ve z direction.

## Appendix D: Sign Conventions.

The sign convention for forces, moments, stresses, rotations, eccentricities and potentials for different element types is documented in the following section headings.

## Standard Bar Element

## Axial force

(+ve) Axial tension
(-ve) Axial compression


## Standard Beam Element

## Numerically Integrated Beam Elements

## Axial force

(+ve) Axial tension
(-ve) Axial compression

## Bending Moment

(+ve) Hogging moment (Top of beam in tension)
(-ve) Sagging moment (Bottom of beam in tension)
Note: The top/bottom of the beam is determined by the element axes.

## Torsion

(+ve) Rotation at 1st node greater than rotation at other end node
(-ve) Rotation at 1st node smaller than rotation at other end node

## Grillage Elements

## End Forces and Rotations

Positive end forces and rotations for grillage elements are those acting on the element nodes in local directions, and are as follows:


Note that when a reference path has been specified, additional force/moment components are available, and for this situation the $\mathrm{x}, \mathrm{y}$, and z element axes relate to longitudinal, transverse and vertical terms respectively. For instance My will relate to MF (longitudinal) - the flexural moment in longitudinal members that are following the path and MF (transverse) - the flexural moment in the transverse members that are orthogonal or skewed in relation to the reference path. Similarly, Fz will relate to FV (longitudinal) - the force in the vertical direction for longitudinal members that are following the path and FV (transverse) - the vertical direction for transverse members that are orthogonal or skewed in relation to the reference path.

## Internal forces

These forces follow the sign convention for numerically integrated beams.

Axial force
Not applicable

Bending Moment
(+ve) Sagging moment
(-ve) Hogging moment

## Torsion

(+ve) Rotation at 1st node greater than rotation at other end node
(-ve) Rotation at 1st node smaller than rotation at other end node

## Sign convention in Modeller for bending moment

(+ve) Top of beam in tension
(-ve) Bottom of beam in tension
Where the top/bottom of the beam are determined by the element axes
See numerically integrated beam sign convention.

## 2D Engineering Beam Elements

## End Forces and Rotations

Positive end forces and rotations for 2D engineering beams are those


## Internal forces

These forces follow the sign convention for numerically integrated beams.

| Axial force |  |
| :--- | :--- |
| (+ve) Axial tension  <br> (-ve) Axial compression Moment  <br> (+ve) Hogging moment  <br>   <br> (-ve) Sagging moment  |  |

## Sign convention in Modeller for bending moment

(+ve) Top of beam in tension
(-ve) Bottom of beam in tension
Where the top/bottom of the beam are determined by the element axes See numerically integrated beam sign convention.

## 3D Engineering Beam Elements

## End Forces and Rotations

Positive end forces and rotations for 3D engineering beams are those acting on the element nodes in local directions, and are as follows:


## Internal forces

These forces follow the sign convention for numerically integrated beams.

Axial force
(+ve) Axial tension
(-ve) Axial
compression

Bending Moment
(+ve) Hogging moment
(-ve) Sagging moment

Torsion (+ve) Rotation at 1st node greater than rotation at other end node (-ve) Rotation at 1st node smaller than rotation at other end node

## Sign convention in Modeller for bending moment

(+ve) Top of beam in tension
(-ve) Bottom of beam in tension
Where the top/bottom of the beam are determined by the element axes
See numerically integrated beam sign convention.

## Standard Beam Eccentricities

Eccentricities are optional geometric properties for some elements and may be specified if the nodal line of the element does not lie along the required bending line/plane for the structural component being modelled.
Measurement of Ez (see diagram) is from the required bending plane (the beam xy plane) to the nodal line in the local element axis z-direction. If a beam xy plane is required such that it has negative local z coordinates relative to
 the nodal line, the eccentricity is positive.
Similarly, measurement of Ey is from the required bending plane (the beam xz plane) to the nodal line in the local element axis $y$-direction. If a beam $x z$ plane is required such that it has negative local y coordinates relative to the nodal line, the eccentricity is positive.

## Standard 2D Continuum Element

## Direct stress

(+ve) Tension
(-ve) Compression

## Shear stress

(+ve) Shear into XY quadrant
(-ve) Shear into XY quadrant


Note. Positive stress values are shown.

## Standard 3D Continuum Element

## Direct stress

(+ve) Tension
(-ve) Compression

## Shear stress

(+ve) Shear into XY, YZ and XZ quadrants
(-ve) Shear into $\mathrm{XY}, \mathrm{YZ}$ and XZ quadrants




Note. Positive stress values shown.

## Standard Plate Element

## Flexural stress

(+ve) Hogging moment (producing +ve stresses on the element top surface)
(-ve) Sagging moment (producing -ve stresses on the element top surface)



The +ve local z-direction defines the top surface.

## Thin Shell Element

## Membrane stress

| $(+\mathrm{ve})$ | Direct tension |
| :--- | :--- |
| $(-\mathrm{ve})$ | Direct compression |
| $(+\mathrm{ve})$ | In-plane shear into xy quadrant |
| $(-\mathrm{ve})$ | In-plane shear into xy quadrant |

## Flexural stress

(+ve) Hogging moment (producing +ve stresses on the element top surface)
(-ve) Sagging moment (producing -ve stresses on the element top surface)



## Notes

- Positive stress values shown.
- The +ve local z-direction defines the top surface.


## Thin Shell Eccentricity

Eccentricity is an optional geometric property for this element type and may be specified if the nodal plane of the element does not lie along the required bending plane for the structural component being modelled.


Measurement of $e_{z}$ is from the required bending plane to the nodal plane in the local element axis z -direction.

## Thick Shell Element

## Thick shell stress



## Stress Resultant

| Membrane stress | $(+\mathrm{ve})$ <br> $(-\mathrm{ve})$ | Direct tension <br> Direct compression |
| :--- | :--- | :--- |
|  | $(+\mathrm{ve})$ | In-plane shear into xy quadrant |
| $(-\mathrm{ve})$ | In-plane shear into xy quadrant |  |





The + ve local z-direction defines the top surface.

## Thick Shell Eccentricity

Eccentricity is an optional geometric property for this element type and may be specified if the nodal plane of the element does not lie along the required bending plane for the structural component being modelled.


Measurement of ez is from the required bending plane to the nodal plane in the local element axis z -direction.

## Standard Membrane Element

| Direct stress | $(+\mathrm{ve})$ <br> $(-\mathrm{ve})$ | Tension <br> Compression |
| :--- | :--- | :--- |

Shear stress (+ve) Shear into xy quadrant
(-ve) Shear into xy quadrant


## Standard Field Element

## Potential

(+ve) +ve field value, $\mathrm{dT} / \mathrm{dx}$ rate of change of field in x direction

## Standard Joint Element

Direct force : (+ve) Tension and (-ve) Compression
Spring Moment : (+ve) for positive rotational spring strain and (-ve) for negative rotational spring strain
The sign of joint results is dependent upon both the element direction(that is which geometry is the master, and which is the slave) and the orientation of the local coordinate axes chosen.


Coincident Master and Slave nodes, $M=$ Master, $S=$ Slave

## Element Reference Manual

| Compression | Tension | Negative Moment | Positive Moment |
| :---: | :---: | :---: | :---: |
| $\mathrm{Mu}>\mathrm{Su}$ | $\mathrm{Su}>\mathrm{Mu}$ | $\mathrm{M}_{6 \mathrm{x}}>S_{\text {ex }}$ | $\mathrm{S}_{\theta \mathrm{x}}>\mathrm{M}_{\theta \mathrm{x}}$ |
| $\mathrm{Mv}>\mathrm{Sv}$ | Sv > Mv | $\mathrm{M}_{\theta \mathrm{y}}>\mathrm{S}_{\theta \mathrm{\theta}}$ | $\mathrm{S}_{\theta \mathrm{y}}>\mathrm{M}_{\theta \mathrm{y}}$ |
| $\mathrm{Mw}>\mathrm{Sw}$ | $\mathrm{Sw}>\mathrm{Mw}$ | $\mathrm{M}_{\theta \mathrm{z}}>\mathrm{S}_{\theta \mathrm{z}}$ | $S_{\theta z}>M_{\theta z}$ |

# Appendix E: Thick Shell Notation. 

## Thick Shell Nodal Rotation

## Problems with Singularities

In general, five degrees of freedom will be associated with each shell node: three translations and two rotations. The first axis of rotation will be defined by one of the global axes. The second axis of rotation is defined by the vector product of the selected global axis and the nodal normal.
Choosing one global axis to define the first rotation is not possible for all cases as singularities can occur depending on the orientation of the shell. As the topology of the shell cannot be known a means of choosing suitable rotations after the shell orientation has been defined must be provided.

## How the Nodal Systems are Defined

The axis defining the $\theta \alpha$ rotation is chosen by examining the global components of the nodal normal. The smallest (absolute) component of the normal vector defines the global axis to be chosen as the first axis of rotation. The vector product of this axis and the nodal normal defines the axis for the second rotation $\theta \beta$. If the nodal normal coincides with the global Z axis, the global X axis will be chosen to define $\theta \alpha$. In this instance, the X and Y components will both be
 minimum values. When two components define the same minimum value the order of priority for selection of the axis is $\mathrm{X}, \mathrm{Y}, \mathrm{Z}$. Note that, in general, the axes of rotation and the nodal normal will form a non-orthogonal left-handed set. The rotations are indicated in the following figure where the global x axis has been used to define $\theta \alpha$ :

## Five or Six Degrees of Freedom at a Node

LUSAS Solver will automatically select five degrees of freedom at a node, with rotations defined as above, unless:
$\square$ The maximum angle between the normals of adjacent elements meeting at the node is greater than 20 degrees. The value of 20 degrees is selected by default and may be changed using the SYSTEM parameter SHLANG.

- Beam, joint or other shell element types are connected to the node

Concentrated loads or support conditions have been specified at the node using LUSAS Modeller

- Option 278 has been specified

Six degrees of freedom have been selected for the node within the NODAL FREEDOMS data chapter If six degrees of freedom are used at a node the rotations will relate to the global axes, $\theta \mathrm{X}, \theta \mathrm{Y}$ and $\theta \mathrm{Z}$ unless TRANSFORMED FREEDOMS have been specified. It is recommended that the default value for SHLANG is retained wherever possible.

## When are Six Degrees of Freedom Necessary?

Rotations relating to global axes will be required in the following circumstances:
$\square$ When a branched shell connection exists in the structure to be analysed. LUSAS Solver will automatically detect this and assign six degrees of freedom to nodes along the branch connection.
$\square$ When connecting with other element types. Six degrees of freedom will automatically be assigned to shell nodes connected to beams, joints or other shell element types.
$\square$ When boundary conditions or loading cannot be easily specified using the above definition of rotations, e.g. when applying moments or using symmetry.
If the rotations $\theta \alpha, \theta \beta$ will not allow the required loading or symmetry conditions to be applied, rotations about global axes may be enforced using NODAL FREEDOMS. The use of TRANSFORMED FREEDOMS will then allow the rotations to be related to a more convenient local orthogonal set if necessary. If six degrees of freedom at a node are enforced using NODAL FREEDOMS (i.e. not set automatically by LUSAS Solver) singularities may occur if the in-plane rotation (about the normal) is not restrained.

# Appendix F: Newton Coates Integration. 

## Newton-Cotes Integration Points

For beam elements BMX3, BSX4 and BXL4 the rigidity is computed by integration of the cross section. The default integration employs a $3 \times 3$ Newton Cotes rule for linear materials and a $5 \times 5$ rule for nonlinear materials. These may be altered by the user within the GEOMETRIC PROPERTIES definition. The locations of the default integration points are shown in the accompanying diagram, together with the local axes for the beam cross section (note the different corner numbering). The integration points are equally spaced along a particular natural ordinate for the section. The integration point numbers shown correspond with those given in the stress output for the element. More information on the cross sectional integration for these elements is available in the LUSAS Theory Manual.


## Newton-Cotes Integration Points for 3D Elements



Newton-Cotes Integration Points for 2D Elements

# Appendix G: Shear Area and Torsional <br> <br> Constant. 

 <br> <br> Constant.}

## Shear Areas

In beams of small span to depth ratio, the shear stresses are likely to be high and the resulting deflection due to shear may not be negligible. The shear area is used to control the amount of shear deformation which will occur (Asz, Asy). For various sections, approximate values are as follows:

Rectangular beams $=5 \mathrm{~A} / 6$
I-beams (along web direction) = Area of web
I-beams (along flange direction) $=$ Area of flanges
Thin walled, hollow circular section $=\mathrm{A} / 2$

- Solid circular section $=9 \mathrm{~A} / 10$
$\square$ No shear deformation $=1000 \mathrm{~A}$


## Note

- If Asz or Asy equal zero, mechanisms may occur.
- For elements which support this geometric input, shear deformation effects may be removed by assigning an artificially large value.
- The section property calculator in Modeller can be used to accurately compute shear areas


## Torsional Constant

The torsional constant provides a measure of the torsional rigidity of a line member. Approximate values are as follows:

## Solid circle

(equivalent to the polar moment of inertia)

$$
\frac{\pi \cdot r^{4}}{2}
$$

where $\mathbf{r}$ is the radius of the circle

## Hollow circle

$$
\frac{\pi}{2}\left(r_{2}^{4}-r_{1}^{4}\right)
$$

where $r 2$ is the outer radius and r 1 is the inner radius

Solid square $=0.1406 \mathrm{a}^{4}$
where $a$ is the side length

## Solid rectangle $=$

$$
a b^{3}\left[\frac{16}{3}-3.36 \frac{b}{a}\left(1-\frac{b^{4}}{12 a^{4}}\right)\right]
$$

where $\mathbf{2 a}$ is the length of the longest side and $\mathbf{2 b}$ is the length of the shortest side

## Equilateral triangle

$$
\frac{a^{4} \sqrt{3}}{80}
$$

where $\mathbf{a}$ is the side length

## Rectangular tube

$$
\frac{2 \cdot t_{1} \cdot t_{2} \cdot\left(a-t_{2}\right)^{2}\left(b-t_{1}\right)^{2}}{a t_{2}+b t_{1}-t^{2}{ }_{2}-t^{2}{ }_{1}}
$$

where
$\mathbf{a}$ is the length of the longest side
$\mathbf{t} \mathbf{1}$ is the thickness of the longest side
$\mathbf{b}$ is the length of the shortest side
$\mathbf{t 2}$ is the thickness of the shortest side

## Thin rectangle

$$
\frac{1}{3} b t^{3}
$$

where $\mathbf{b}$ is the rectangle length and $\mathbf{t}$ is the rectangle length thickness

## Any section consisting of thin rectangles

$$
\frac{1}{3} \sum b t^{3}
$$

## Solid ellipse

$$
\frac{\pi a^{3} b^{3}}{a^{2}+b^{2}}
$$

where $\mathbf{2 a}$ is the longest dimension
and $\mathbf{2 b}$ is the shortest dimension

## Note

- The section property calculator in Modeller can be used to accurately compute torsional constants


## Appendix H: Principal Stress Output.

## Output Notation for Principal Stresses

For a bi-axial stress state, the Mohr's circle representation of a stress field is:

where:
Smax is the maximum principal stress.
$\mathbf{S m i n}$ is the minimum principal stress
Ss is the maximum shear stress
$\boldsymbol{\beta}$ defines the orientation of the principal axis (the plane on which the principal stresses act).
$\mathbf{S x}, \sigma \mathbf{y}, \sigma \mathbf{x y}$ represent an arbitrary two dimensional stress state.

## Appendix I: Mass Lumping.

## Mass Lumping in LUSAS

Non-Structural mass elements are used to define a lumped mass at a point, or a distributed mass along a line and over a surface.
See Non-Structural Mass Elements in the Modeller Reference Manual for more details.

## Appendix J: Moments of Inertia.

## Moments of Inertia Definitions

Second moment of area about line yy

$$
I_{W}=\int z^{2} d A
$$

Second moment of area about line $\mathbf{z z}$

$$
I_{Z Z}=\int y^{2} d A
$$

Product moment of inertia of section

$$
I_{y z}=\int y z d A
$$

( $=0$ for sections symmetric about either yy or zz )
First moment of area about yy

$$
I_{y}=\int z d A
$$

(=0 for sections symmetric about yy)
First moment of area about $\mathbf{z z}$

$$
I_{z}=\int y d A
$$

(=0 for sections symmetric about zz)


## Note

- The above definitions are for a section defined in the two dimensional yz plane. Similar expressions apply for a section in the three dimensional space.
- For a beam with eccentricity e from the nodal line, then:

$$
I_{z z}=A e^{2}+I_{n a} \text { and } I_{z}=e A
$$

where $I_{\mathrm{na}}$ is the second moment of area about the centroidal axis.

- For the purpose of the moment inertia definitions above only, the eccentricity is measured from the nodal line to the required bending plane (the beam's xy plane in the figure above). For example, if a beam xy plane is required such that it has negative local $z$ coordinates relative to the nodal line, the eccentricity to be used above is negative.


# Appendix K: Results Tables. 

## Key to Element Results Tables

This section contains the notation for the results in the Results Tables. Some results are available in local and global directions depending on the element type. The case of the direction indicator associated for each term in the table will indicate its default direction for that element. Lower case indicates local element directions and upper case indicates that results are available in global directions by default.

## Displacements

DX Displacement in X
direction

DY Displacement in Y
direction

DZ Displacement in Z direction
RSLT Resultant displacement
THX Rotation about X
THY Rotation about Y
THZ Rotation about Z

THL1 First loof rotation

THL2 Second loof rotation
DU Hierarchical disp. at mid-node
DTHX Hierarchical rotation at mid-node
PRES Pore Pressure
THw Rate of change of twisting angle (warping beams)

Note: Rotations are output in radians.

## Velocities and Accelerations

## VX Velocity in X direction

VY Velocity in Y direction
VZ Velocity in Z direction
RSLT Resultant velocity

AX Acceleration in X direction
AY Acceleration in Y direction
$\mathbf{A Z}$ Acceleration in Z direction
RSLT Resultant acceleration

VC Results calculator values

## Strains

EX Direct strain in X direction
EY Direct strain in Y direction
EZ Direct strain in Z direction

EXY Shear strain in XY plane

EYZ Shear strain in YZ plane
EZX Shear strain in XZ plane
EMa Maximum principal strain
x
EMin Minimum principal strain
E1 Major principal strain
E2 Intermediate principal strain
E3 Minor principal strain
Eabs Signed largest value of principal strain
Bx Bending strain (curvature) about $x$
axis

By Bending strain (curvature) about y axis
Bz Bending strain (curvature) about z axis
Bxy Bending or torsional strain into $x y$ plane
Byz Bending or torsional strain into yz plane
Bxz Bending or torsional strain into $x z$ plane
BMax Maximum principal bending strain
BMin Minimum principal bending strain
$\boldsymbol{\beta}$ Angle between E1 and X axis
EE Equivalent strain (von Mises)
EI Maximum shear strain
EV Volumetric strain

## Strains: Top/Middle/Bottom (TMB)

EX Direct strain in X direction
EY Direct strain in Y direction
EZ Direct strain in $Z$ direction
EXY Shear strain in XY plane
EYZ Shear strain in YZ plane
EXZ Shear strain in XZ plane

## Plastic Strains

EPX Plastic direct strain in X direction
EPY Plastic direct strain in Y direction
EPZ Plastic direct strain in Z

E1 Major principal strain
E2 Intermediate principal strain
E3 Minor principal strain
Eabs Signed largest value of principal strain
$\boldsymbol{\beta}$ Angle between E1 and X axis
EE Equivalent strain (von Mises)
EI Maximum shear strain

EP1 Major principal strain
EP2 Intermediate principal plastic strain
EP3 Minor principal plastic strain
direction
EPXY Plastic shear strain in XY plane
EPYZ Plastic shear strain in YZ plane
EPZX Plastic shear strain in ZX plane
EPMax Maximum principal plastic strain
EPMin Minimum principal plastic strain

## Creep Strains

## ECX Creep direct strain in X direction

ECY Creep direct strain in Y direction
ECZ Creep direct strain in Z direction
ECXY Creep shear strain in XY plane
ECYZ Creep shear strain in YZ plane
ECZX Creep shear strain in ZX plane
ECMax Maximum principal creep strain
ECMin Minimum principal creep strain

## Rubber Stretches

StchX $\begin{aligned} & \text { Direct stretch tensor in X } \\ & \text { direction }\end{aligned}$
StchY Direct stretch tensor in Y direction
StchZ Direct stretch tensor in Z direction
StchXY Shear stretch tensor in XY plane
StchYZ Shear stretch tensor in YZ plane
StchXZ Shear stretch tensor in XZ

EPabs Signed largest value of principal plastic strain
$\boldsymbol{\beta}$ Angle between EP1 and X axis
EPE Equivalent plastic strain (von Mises)
EPI Maximum shear strain
CWMax Maximum crack width
EFSMax Maximum equivalent fracture strain

EC1 Major principal creep strain
EC2 Intermediate principal creep strain
EC3 Minor principal creep strain
Ecabs Signed largest value of principal creep strain
$\boldsymbol{\beta}$ Angle between EC 1 and X axis
ECE Equivalent creep strain (von Mises)
ECI Maximum shear creep strain

Stch1 Major principal stretch
Stch2 Intermediate principal stretch
Stch3 Minor principal stretch
StchAbs Signed largest value of principal stretch
$\boldsymbol{\beta}$ Angle between Stch1 and X axis
StchE Equivalent stretch
plane
StchMax Maximum principal stretch
StchI Maximum shear stretch
StchMin Minimum principal stretch
Strains: Interface Elements
Ex Shear relative displacement in local $x$ direction

Ey Shear relative displacement in local y
direction

Ez Direct relative displacement in the
thickness direction
dP Pressure difference
Stresses: Continuum Elements
SX Direct stress in global X direction
SY Direct stress in global Y direction
SZ Direct stress in global $Z$ direction
SXY Shear stress in Y-direction on a planenormal to X
SYZ Shear stress in yz plane
SXZ Shear stress in xz plane
SMax Maximum principal stress
SMin Minimum principal stress
S1 Major principal stress
S2 Intermediate principal stress
S3 Minor principal stress
Sabs Signed largest value of principal stress
$\boldsymbol{\beta}$ Angle between E1 and x axis
SI Maximum shear stress
SE Equivalent stress (von Mises)
Pres Pore pressure

## Force/Moment: Bar and Beam Elements

Fx Force in local x direction
Fy Force in local y direction
Fz Force in local z direction
Fb Bi-shear or torque (warping)

Mx Moment about local x direction
My Moment about local y direction
Mz Moment about local z direction
Mb Bi-moment (warping)

## Stresses: Bar and Beam Elements

$\mathbf{S x}(\mathbf{F x})$ Stress due to axial force in $x$
$\mathbf{S x}(\mathbf{M y})$ Stress due to bending about y
$\mathbf{S x}(\mathbf{M z})$ Stress due to bending about z
$\mathbf{S x}(\mathbf{M y}, \mathbf{M z})$ Stress due to bending about y and z
$\mathbf{S x}(\mathbf{F x}, \mathbf{M y})$ Stress due to axial force and bending about y
$\mathbf{S x}(\mathbf{F x}, \mathbf{M z})$ Stress due to axial force and bending about $y$
$\mathbf{S x}(\mathbf{F x}, \mathbf{M y}, \mathbf{M z}) \quad$ Stress due to axial force and bending about y and z

## Force/Moment: Plate Elements (per unit width)

SX Shear force in global YZ plane
SY Shear force in global XZ plane

MX Moment in global X
MY Moment in global Y
MXY Twisting moment in global XY plane
Mmax Major principal moment
Mmin Minor principal moment
$\boldsymbol{\beta}$ Angle between MMax and X axis
MI Maximum shear moment
Mabs Signed largest value of moment
ME Equivalent moment

## Force/Moment: Membrane and Shell Elements (per unit width)

Nx In-plane force in local $x$ direction
Ny In-plane force in local y direction
Nxy In-plane shear force
NMax Major principal in-plane force
NMin Minor principal in-plane force
$\mathrm{N} \beta \varepsilon \tau \boldsymbol{\alpha}$ Angle between NMax and x axis
NI Maximum in-plane shear force
NE Equiv stress resultant (von Mises)
Nabs Signed largest value of in-plane force
Sx Shear force in local yz plane
Sy Shear force in local xz plane
Mx Moment in local $x$ direction
My Moment in local y direction
Mxy Twisting moment in local xy plane
Mmax Major principal moment
Mmin Minor principal moment
M $\beta \boldsymbol{\varepsilon} \boldsymbol{\tau} \boldsymbol{\alpha}$ Angle between MMax and Xaxis
MI Maximum shear moment
ME Equivalent moment
Mabs Signed largest value of moment
Stresses: Top/Middle/Bottom (TMB)SX Direct stress in global X direction
SY Direct stress in global Y direction
SZ Direct stress in global Z direction
SXY Shear stress in XY plane
$\mathbf{S Y Z}$ Shear stress in YZ plane
$\mathbf{S X Z}$ Shear stress in XZ plane

S1 Major principal stress
S2 Intermediate principal stress
S3 Minor principal stress
Sabs Signed largest value of principal stress
SI Maximum shear stress
SE Equivalent stress (von Mises)

## Stresses: Interface Elements

Sx Shear traction in local $x$ direction
Sz Direct traction in thickness direction

Sy Shear traction in local y direction
Q Flow

## Force/Moment: Wood-Armer (per unit width for Shells)

$\mathbf{M x}(\mathbf{T})$ Top surface local $x$ moment
$\mathbf{M y}(\mathbf{T})$ Top surface local y moment
$\mathbf{M x}(\mathbf{B})$ Bottom surface local x moment
$\mathbf{M y}(\mathbf{B})$ Bottom surface local y moment
Util(T) Top surface utilisation factor
Util(B) Bottom surface utilisation factor
MUtil(T) Top surface utilisation factor for bending only
MUtil(B) Bottom surface utilisation factor for bending only
$\mathbf{N x}(\mathbf{T})$ Top surface local x force
$\mathbf{N y}(\mathbf{T})$ Top surface local $y$ force
$\mathbf{N x}(\mathbf{B})$ Bottom surface local x force
$\mathbf{N y}(B)$ Bottom surface local y force
$\mathbf{F c}(\mathbf{T})$ Top surface concrete force
$\mathbf{F c}(\mathbf{B})$ Bottom surface concrete force

## Force/Moment: Wood-Armer (per unit width for Plates and Grillages)

MX(T) Top surface global X moment
MY(T) Top surface global Y moment
MX(B) Bottom surface global X moment
MY(B) Bottom surface global Y moment

MUtil(T) Top surface utilisation factor for bending only
MUtil(B) Bottom surface utilisation factor for bending only

## Additional Force/Moment Components

Note for influence analysis when a reference path has been specified, additional force/moment components are available for selection when transforming results. These are not listed for relevant elements in the Results tables.

FV Force in Vertical direction for
(longitudinal) longitudinal members that are following the reference path

FV Force in Vertical direction for (transverse) transverse members that are

MF Flexural Moment in
(longitudinal) longitudinal members that are following the reference path
MF Flexural Moment in (transverse) transverse members that are
orthogonal or skewed in relation to the reference path

## Stresses: Interface Elements

orthogonal or skewed in relation to the reference path

Sx Shear traction in local $x$ direction
Sz Direct traction in the thickness direction

## Concrete Results

## CWmax Max Crack width

EPshk Shrinkage strain
Temp Temperature
Ftens tensile strength
ECX Creep strain in global X
ECZ Creep strain in global Z

## Potential

PHI Field variable
T Temperature

## Gradients

GX Field gradient in X direction
GY Field gradient in Y direction
GY Field gradient in Z direction

## Hygro-Thermal Results

SW Water saturation
PV Vapour pressure
Por Porosity
TC Thermal conductivity
HR Relative humidity of concrete

Sy Shear traction in local y direction

ESFmax Max fracture strain EPthm Thermal strain
Fcomp Compressive strength
Young Young's modulus
ECY Creep strain in global Y

PHIC Results calculator values

Fluxes
qX Field flux in X direction
qY Field flux in Y direction
qZ Field flux in Z direction

## Reactions / Residual Forces

FX Force in X direction $\quad \mathbf{M Z}$ Moment about Z axis

FY Force in Y direction
FZ Force in Z direction
RSLT Resultant force
MX Moment about X axis
MY Moment about $Y$ axis

FDU Force due to hierarchical displacement
MDX Moment due to hierarchical rotation

QC Flow at a point (field problems)
VFLW Velocity of Flow

## Reaction Stress

PX Stress due to reaction in X direction
PZ Stress due to reaction in Z direction
PY Stress due to reaction in Y direction

## Fatigue Parameters

Damage A measure of damage
LogLife Log repeats to failure
Note. The fatigue facility uses Miner's rule, that is:

$$
\mathrm{n} 1 / \mathrm{N} 1+\mathrm{n} 2 / \mathrm{N} 2+\cdots+\mathrm{ni} / \mathrm{Ni}=\text { Damage }
$$

where Damage is the damage variable and is usually taken as unity (experiment usually gives values between 0.7 and 2.2). ni is the number of cycles of stress applied to the structure and Ni is the life corresponding to the stress. Loglife is the log (base 10) of the life expectancy of the structure according to the loading and the number of cycles specified. Life is measured in terms of cycles.

## Damage Parameters

DDAMA Damage variable DAMAM Damage consistency parameter
CCURD Damage threshold DFUNC Damage function
Note. Damage parameters are only available when a damage model is in use.

## Strain Energy and Plastic Work

SED Strain energy density (StEngD) PWD Plastic work density
Note. Strain energy density and plastic work density values can be accessed if turned on by selecting Calculate Strain Energy and Plastic Work Densities from the Results > Options dialog or by using the command: SET RESULTS ENERGY.

## Adaptive Error

## Eadp Adaptive error.

Note. Adaptive error results are only available when an adaptive results column is set. See the LUSAS User Manual for more details.

## State Variables

State variables can be accessed with the command:

## SET RESULTS STATE_VARIABLES istvb nsvcmp isvloc

Where istvb is the type of state variable required, nsvcmp is the number of state variables required, and isvloc is the start location of the first state variable required.
The results columns for these state variables vary according to the results type set. The column descriptors have the following prefixes:

- PL Plastic, Rubber
- CR Creep
- DM Damage
- followed by the number of the state variable required. For example, if four creep state variables are required, the column descriptors will be CR1, CR2, CR3 and CR4.


## Key to Slideline Results Components

This section contains the notation for slideline results. Note that slideline results components are not listed in the results tables.

| TanGapFrcx | Tangential gap force in local <br> x direction | NrmPen | Penetration normal to contact <br> surface |
| ---: | :--- | ---: | :--- |
| TanGapFrcy | Tangential gap force in local <br> y direction | ContStatus | In-contact/out-of-contact <br> status |
| RsitTanGFc | Resultant tangential gap <br> force | ContacArea | Nodal contact area |
| NrmGapForc | Gap force normal to contact <br> surface | ContactIn-contact/out-of-contact <br> status |  |
| ForceX | Contact force in system x <br> direction | Zone | Zonal contact parameter |

## Transforming Results Directions

Important: Some results entities can be transformed. The results components will use alternative suffixes if results are calculated relative to a system other than the global axis set. The element results tables show the default results directions for all elements with lower case subscripts being used for local results.
See the Local and Global Results in the LUSAS Modeller User Manual for details of results transformation procedures.

## 2D Structural Bars BAR2, BAR3

| Entity | Component |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | RSLT |  |  |  |  |  |  |  |  |
| Force/Moment | FX | Fabs | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |
| Strain | EX | Eabs | DDAMA | CURRD | damam | DFUNC | SED | PWD | Eadp |  |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |
| Loading | FX | FY | RSLT |  |  |  |  |  |  |  |  |
| Reaction | FX | FY | RSLT |  |  |  |  |  |  |  |  |
| Residual Force | FX | FY | RSLT |  |  |  |  |  |  |  |  |
| Reaction Stress |  |  |  |  |  |  |  |  |  |  |  |
| Velocity | vx | VY | RSLT |  |  |  |  |  |  |  |  |
| Acceleration | AX | AY | RSLT |  |  |  |  |  |  |  |  |
| Plastic Strain | EPX | EPabs | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |
| Creep Strain | ECX | ECabs | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |  |  |

## 3D Structural Bars BRS2, BRS3

| Entity | Component |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | DZ | RSLT |  |  |  |  |  |  |  |
| Force/Moment | FX | Fabs | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |
| Strain | EX | Eabs | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |
| Loading | FX | FY | FZ | RSLT |  |  |  |  |  |  |  |
| Reaction | FX | FY | FZ | RSLT |  |  |  |  |  |  |  |
| Residual Force | FX | FY | FZ | RSLT |  |  |  |  |  |  |  |
| Reaction Stress |  |  |  |  |  |  |  |  |  |  |  |
| Velocity | VX | VY | VZ | RSLT |  |  |  |  |  |  |  |
| Acceleration | AX | AY | AZ | RSLT |  |  |  |  |  |  |  |
| Plastic Strain | EPX | EPabs | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |
| Creep Strain | ECX | ECabs | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |  |  |

## 2D Engineering Grillage Thick Beam GRIL

| Entity | Component |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DZ | RSLT | THX | THY |  |  |  |  |  |  |  |  |  |
| Force/Moment | Fz | Mx | My | Mx( ) $^{\text {( }}$ | My( ) $^{\text {( }}$ | Mx(B) | My(B) | Util( $T$ ) | Util(B) | Damage | LogLife | SED | Eadp |
| Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Loading | FZ | RSLT | MX | MY |  |  |  |  |  |  |  |  |  |
| Reaction | FZ | RSLT | MX | MY |  |  |  |  |  |  |  |  |  |
| Residual Force |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Reaction Stress |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Velocity | VZ | RSLT |  |  |  |  |  |  |  |  |  |  |  |
| Acceleration | AZ | RSLT |  |  |  |  |  |  |  |  |  |  |  |
| Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Creep Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |

Note: Wood-Armer results are only available for plotting /printing at nodes. They are not available unaveraged at nodes within elements or at Gauss points.

## 2D Thick Beam Elements BMI2, BMI3, BMI2X, BMI3X

| Entity | Component |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX DY | RSLT | THZ |  |  |  |  |  |  |  |  |
| Force/Moment | Fx My | Mz | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |
| Strain | Ex Exy | Bz | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |
| Loading | FX FY | RSLT | MZ |  |  |  |  |  |  |  |  |
| Reaction | FX FY | RSLT | MZ |  |  |  |  |  |  |  |  |
| Residual Force | FX FY | RSLT | MZ |  |  |  |  |  |  |  |  |
| Reaction Stress |  |  |  |  |  |  |  |  |  |  |  |
| Velocity | VX VY | RSLT |  |  |  |  |  |  |  |  |  |
| Acceleration | AX AY | RSLT |  |  |  |  |  |  |  |  |  |
| Plastic Strain | EPx EPxy | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |
| Creep Strain | ECx ECxy | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |
| Rubber Stretches | Sx Sy |  |  |  |  |  |  |  |  |  |  |
| TMB Stress | Ex Exy |  |  |  |  |  |  |  |  |  |  |
| TMB Strain | EPx EPxy |  |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain | ECx ECxy |  |  |  |  |  |  |  |  |  |  |

Note: Plastic and creep strains are only available for BMI2X and BMI3X elements with the appropriate material models.

## 3D Thick Beam Elements BMI21, BMI22, BMI31, BMI33, BMX21, BMX22, BMX31, BMX33



Note: Plastic and creep strains are only available for BMX21, BMX31, BMX22, BMX33 elements with the appropriate material models.

## 3D Thick Beam Elements with Torsional Warping BMI21W, BMI22W, BMI31W, BMI33W, BMX21W, BMX22W, BMX31W, BMX33W

| Entity | Component |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | DZ | RSLT | THX | THY | THY | THw |  |  |  |  |  |  |  |
| Force/Moment | Fx | My | Mz | Mx | My | Mz | Fb | Mb | Damage | LogLife | DDAMA | $\begin{aligned} & \text { CURR } \\ & \text { D } \end{aligned}$ | $\begin{gathered} \text { DAMA } \\ \mathrm{M} \end{gathered}$ | $\begin{aligned} & \text { DFUN } \\ & \text { C } \end{aligned}$ | SED PWD Eadp |
| Strain | Ex | By | Bz | Bx | By | Bz | Efb | Emb | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |
| Loading | FX | FY | FZ | RSLT | MX | MY | MZ |  |  |  |  |  |  |  |  |
| Reaction | FX | FY | FZ | RSLT | MX | MY | MZ | Mw |  |  |  |  |  |  |  |
| Residual Force | FX | FY | FZ | RSLT | MX | MY | MZ |  |  |  |  |  |  |  |  |
| Reaction Stress |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Velocity | vx | VY | VZ | RSLT |  |  |  |  |  |  |  |  |  |  |  |
| Acceleration | AX | AY | AZ | RSLT |  |  |  |  |  |  |  |  |  |  |  |
| Plastic Strain | EPx | EPxy | EPzx | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |
| Creep Strain | ECx | ECxy | ECzx | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Note: Plastic and creep strains are only available for BMX21W, BMX31W, BMX22W, BMX33W elements with the appropriate material models.

## 2D Kirchhoff Thin Beams BM3, BMX3

| Entity | Component |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | RSLT | THZ | DU |  |  |  |  |  |  |  |
| Force/Moment | Fx | Fy | Mz | Damage | LogLife | DDAMA | CURRD | damam | DFUNC | SED | PWD | Eadp |
| Strain | Ex | Ey | Bz | DDAMA | CURRD | damam | DFUNC | SED | PWD | Eadp |  |  |
| Loading | FX | FY | RSLT | MZ | FDU |  |  |  |  |  |  |  |
| Reaction | FX | FY | RSLT | MZ | FDU |  |  |  |  |  |  |  |
| Residual Force | FX | FY | RSLT | MZ | FDU |  |  |  |  |  |  |  |
| Reaction Stress |  |  |  |  |  |  |  |  |  |  |  |  |
| Velocity | vx | VY | RSLT |  |  |  |  |  |  |  |  |  |
| Acceleration | AX | AY | RSLT |  |  |  |  |  |  |  |  |  |
| Plastic Strain | EPx | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |
| Creep Strain | ECx | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |  |  |  |

Note: Plastic and creep strains are only available for BMX3 elements with the appropriate material models.

## 3D Kirchhoff Thin Beams BS3, BS4, BSX4



## 3D Semilloof Thin Beams BSL3, BSL4, BXL4

| Entity | Component |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | DZ | RSLT | THX | THY | THZ | THL1 | THL2 |  |  |  |  |  |
| Force.Moment |  | My | Mz | Tzx | Txy | Fy | Fz | Damage | LogLife | DDAMA | CURRD | AMA | FUNC | SED |
| (continued) | Eadp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Strain |  | By | Bz | Bzx | Bxy | Ey | Ez | DDAMA | CURRD | DAMAN | DFUNC | SED | PWD | Ead |
| Loading |  | FY | FZ | RSLT | MX | MY | MZ | ML1 | ML2 |  |  |  |  |  |
| Reaction | FX | FY | FZ | RSLT | MX | MY | MZ | ML1 | ML2 |  |  |  |  |  |
| Residual Force | FX | FY | FZ | RSLT | MX | MY | MZ | ML1 | ML2 |  |  |  |  |  |
| Reaction Stress |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Velocity |  | VY | VZ | RSLT |  |  |  |  |  |  |  |  |  |  |
| Acceleration | AX | AY | AZ | RSLT |  |  |  |  |  |  |  |  |  |  |
| Plastic Strain | EPx |  | EPyz | EPzx | $\begin{gathered} \text { DDAM } \\ \text { A } \end{gathered}$ | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |
| Creep Strain | ECx |  | ECyz | ECzx | $\begin{gathered} \text { DDAM } \\ \text { A } \end{gathered}$ | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Note: Plastic and creep strains are only available for BXL4 elements with the appropriate material models.

## Plane Strain Beam Elements BMI2N, BMI3N

| Entity | Component |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | RSLT | THZ |  |  |  |  |  |  |
| Stress | Nx | Nz | Mx | Mz | Nxy | NMax | NMin | Ns | $\beta$ | Nabs Ne |
| (continued) | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |
| Strain | Ex | Ez | Bx | Bz | Exy | EMax | EMin | EI | $\beta$ | Eabs EE |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |
| Loading | FX | FY | RSLT | MZ |  |  |  |  |  |  |
| Reaction | FX | FY | RSLT | MZ |  |  |  |  |  |  |
| Residual Force | FX | FY | RSLT | MZ |  |  |  |  |  |  |
| Reaction Stress | PX | PY |  |  |  |  |  |  |  |  |
| Velocity | vx | VY | RSLT |  |  |  |  |  |  |  |
| Acceleration | AX | AY |  |  |  |  |  |  |  |  |
| Plastic Strain |  |  |  |  |  |  |  |  |  |  |
| Creep Strain |  |  |  |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |
| TMB Stress | Sx | Sz | Sxy | SMax | Smin | SI | $\beta$ | Sabs | SE |  |
| (continued) | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |
| TMB Strain | Ex | Ez | Exy | EPmax | EMin | El | $\beta$ | Eabs | ECE |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |
| TMB Plastic Strain | EPx | EPz | EPxy | EPMax | EPMin | EPI | $\beta$ | EPabs | ECE |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |
| TMB Creep Strain | ECx | ECz | ECxy | ECMax | ECMin | ECI | $\beta$ | ECabs | ECE |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |

## 2D Continuum (Plane Stress) TPM3/6, QPM4/8, QPM4M, TPK6, QPK8



## Notes:

Rubber stretches are only available for QPM4M elements with rubber material models. Strains are not available for this element when using rubber materials.
Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Models (105 and 109) are used.

## 2D Continuum Plane Stress (Explicit Dynamics) TPM3E, QPM4E

| Entity | Component |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | RSLT |  |  |  |  |  |  |
| Stress | SX | SY | SXY | SMax | SMin | SI | $\beta$ | Sabs | SE |
| (continued) | Damage | LogLife | DDAMA | CURRD | damam | DFUNC | SED | PWD | Eadp |
| Strain | EX | EY | EXY | EMax | EMin | El | $\beta$ | Eabs | EE |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |
| Loading | FX | FY | RSLT |  |  |  |  |  |  |
| Reaction | FX | FY | RSLT |  |  |  |  |  |  |
| Residual Force | FX | FY | RSLT |  |  |  |  |  |  |
| Reaction Stress | PX | PY |  |  |  |  |  |  |  |
| Velocity | vx | VY | RSLT |  |  |  |  |  |  |
| Acceleration | AX | AY | RSLT |  |  |  |  |  |  |
| Plastic Strain | EPX | EPY | EPXY | EPMax | EPMin | EPI | $\beta$ | EPabs | EPE |
| (continued) | DDAMA | CURRD | damam | DFUNC | SED | PWD | Eadp |  |  |
| Creep Strain | ECX | ECY | ECXY | ECMax | ECMin | ECI | $\beta$ | ECabs | ECE |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |

## 2D Continuum (Plane Strain) TPN3/6, QPN4/8, TNK6, QNK8, QPN4M

| Entity | Component |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | RSLT |  |  |  |  |  |  |  |  |  |
| Stress | SX | SY | SXY | Sz | S1 | S2 | S3 | SI | Sabs | SE |  |  |
| (continued) | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |
| Strain | EX | EY | EXY | EZ | E1 | E2 | E3 | El | Eabs | EE |  |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |
| Loading | FX | FY | RSLT |  |  |  |  |  |  |  |  |  |
| Reaction | FX | FY | RSLT |  |  |  |  |  |  |  |  |  |
| Residual Force | FX | FY | RSLT |  |  |  |  |  |  |  |  |  |
| Reaction Stress | PX | PY |  |  |  |  |  |  |  |  |  |  |
| Velocity | vX | VY | RSLT |  |  |  |  |  |  |  |  |  |
| Acceleration | AX | AY | RSLT |  |  |  |  |  |  |  |  |  |
| Plastic Strain | EPX | EPY | EPXY | EPZ | EP1 | EP2 | EP3 | EPI | EPabs | EPE | CWMax | EFSMax |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |
| Creep Strain | ECX | ECY | ECXY | ECZ | EC1 | EP2 | EC3 | ECI | ECabs | ECE |  |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |
| Rubber Stretches | Stch $X$ | StchY | StchXY | StchZ | Stch1 | Stch2 | Stch3 | Stchl | StchAbs | StchE |  |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |  |  |  |

## Notes:

Rubber stretches are only available for QPN4M elements with rubber material models. Strains are not available for this element when using rubber materials.
Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Models (105 and 109) are used.

## 2D Continuum (Plane Strain) QPN4L

| Entity |  |  |  |  | Component |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | RSLT |  |  |  |  |  |  |
| Stress | SX | SY | SXY | SZ | S1 | S2 | S3 | SI | SE |
| Strain | StchX | StchY | StchXY | StchZ | Stch1 | Stch2 | Stch3 | Stchl | StchE |
| Loading | FX | FY | RSLT |  |  |  |  |  |  |
| Reaction | FX | FY | RSLT |  |  |  |  |  |  |
| Residual Force | FX | FY | RSLT |  |  |  |  |  |  |
| Reaction Stress | PX | PY |  |  |  |  |  |  |  |
| Velocity | VX | VY | RSLT |  |  |  |  |  |  |
| Acceleration | AX | AY | RSLT |  |  |  |  |  |  |
| Plastic Strain | EPX | EPY | EPXY | EPZ | EP1 | EP2 | EP3 | EPI | EPE |
| Creep Strain |  |  |  |  |  |  |  |  |  |
| Rubber Stretches | StchX | StchY | StchXY | StchZ | Stch1 | Stch2 | Stch3 | Stchl | StchE |
| TMB Stress |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |

## 2D Plane Strain Two Phase Continuum TPN6P, QPN8P

| Entity | Component |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | RSLT | Pres |  |  |  |  |  |  |  |  |
| Stress | SX | SY | SXY | Sz | PRES | S1 | S2 | S3 | SI | Sabs | SE |  |
| (continued) | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |
| Strain | EX | EY | EXY | EZ | EV | E1 | E2 | E3 | El | Eabs | EE |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |
| Loading | FX | FY | RSLT | Q |  |  |  |  |  |  |  |  |
| Reaction | FX | FY | RSLT | Q |  |  |  |  |  |  |  |  |
| Residual Force | FX | FY | RSLT |  |  |  |  |  |  |  |  |  |
| Reaction Stress | PX | PY |  |  |  |  |  |  |  |  |  |  |
| Velocity | vx | VY | RSLT |  |  |  |  |  |  |  |  |  |
| Acceleration | AX | AY | RSLT |  |  |  |  |  |  |  |  |  |
| Plastic Strain | EPX | EPY | EPXY | EPZ | EP1 | EP2 | EP3 | EPI | EPabs | EPE | CWMax | EFSMax |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |
| Creep Strain | ECX | ECY | ECXY | ECZ | EC1 | EP2 | EC3 | ECI | ECabs | ECE |  |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |  |  |  |

## Notes

Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Model (Model 109) is used.

## 2D Continuum Plane Strain (Explicit Dynamics) TPN3E, QPN4E



## 2D Continuum Axisymmetric Solid (Explicit Dynamics) TAX3E, QAX4E



## 2D Axisymmetric Solid Two Phase Continuum TAX6P, QAX8P

| Entity | Component |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | RSLT | Pres |  |  |  |  |  |  |  |  |
| Stress | SX | SY | SXY | Sz | PRES | S1 | S2 | S3 | SI | Sabs | SE |  |
| (continued) | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |
| Strain | EX | EY | EXY | EZ | EV | E1 | E2 | E3 | EI | Eabs | EE |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |
| Loading | FX | FY | RSLT | Q |  |  |  |  |  |  |  |  |
| Reaction | FX | FY | RSLT | Q |  |  |  |  |  |  |  |  |
| Residual Force | FX | FY | RSLT |  |  |  |  |  |  |  |  |  |
| Reaction Stress | PX | PY |  |  |  |  |  |  |  |  |  |  |
| Velocity | vx | VY | RSLT |  |  |  |  |  |  |  |  |  |
| Acceleration | AX | AY | RSLT |  |  |  |  |  |  |  |  |  |
| Plastic Strain | EPX | EPY | EPXY | EPZ | EP1 | EP2 | EP3 | EPI | EPabs | EPE | CWMax | EFSMax |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |
| Creep Strain | ECX | ECY | ECXY | ECZ | EC1 | EP2 | EC3 | ECl | ECabs | ECE |  |  |
| (continued) | DDAMA | CURRD | damam | DFUNC | SED | PWD | Eadp |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |  |  |  |

## Notes

Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Model (Model 109) is used.

## 2D Continuum Axisymmetric Solid Fourier TAX3/6F, QAX4/8F

| Entity | Component |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | DZ | RSLT |  |  |  |  |  |  |
| Stress | SX | SY | SXY | SZ | S1 | S2 | S3 | SI | Sabs | SE |
| (continued) | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | Eadp |  |  |
| Strain | EX | EY | EXY | EZ | E1 | E2 | E3 | El | Eabs | EE |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | Eadp |  |  |  |  |
| Loading | FX | FY | FZ | RSLT |  |  |  |  |  |  |
| Reaction | FX | FY | FZ | RSLT |  |  |  |  |  |  |
| Residual Force |  |  |  |  |  |  |  |  |  |  |
| Reaction Stress | PX | PY |  |  |  |  |  |  |  |  |
| Velocity | VX | VY | VZ | RSLT |  |  |  |  |  |  |
| Acceleration | AX | AY | AZ | RSLT |  |  |  |  |  |  |
| Plastic Strain |  |  |  |  |  |  |  |  |  |  |
| Creep Strain |  |  |  |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |  |

## Axisymmetric Solid TAX3/6, QAX4/8, QAX4M, TXK6, QXK8



## Notes

Rubber stretches are only available for QAX4M elements with rubber material models. Strains are not available for this element when using rubber materials
Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Models (105 and 109) are used.

## Axisymmetric Solid Large Strain QAX4L

| Entity | Component |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | RSLT | Pres |  |  |  |  |  |  |
| Stress | SX | SY | SXY | SZ | S1 | S2 | S3 | SI | Sabs | SE |
| (continued) | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |
| Strain | Stch $X$ | StchY | StchXY | StchZ | Stch1 | Stch2 | Stch3 | Stchl | StchE |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |
| Loading | FX | FY | RSLT |  |  |  |  |  |  |  |
| Reaction | FX | FY | RSLT |  |  |  |  |  |  |  |
| Residual Force | FX | FY | RSLT |  |  |  |  |  |  |  |
| Reaction Stress | PX | PY |  |  |  |  |  |  |  |  |
| Velocity | VX | VY | RSLT |  |  |  |  |  |  |  |
| Acceleration | AX | AY | RSLT |  |  |  |  |  |  |  |
| Plastic Strain | EPX | EPY | EPXY | EPZ | EP1 | EP2 | EP3 | EPI | EPE |  |
| Creep Strain |  |  |  |  |  |  |  |  |  |  |
| Rubber Stretches | Stch X | StchY | StchXY | StchZ | Stch1 | Stch2 | Stch3 | Stchl | StchE |  |
| TMB Stress |  |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |  |

## 3D Solid Continuum TH4/10, TH10S, PN6/12/15, PN6L/12L, HX8/16/20, HX8M, HX8L/16L, TH10K, PN15K, HX20K

| Entity | Component |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | DZ | RSLT |  |  |  |  |  |  |  |  |  |
| Stress | SX | SY | Sz | SXY | SYZ | SZX | PRES | S1 | S2 | S3 | SI | Sabs | SE |
| (continued) | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |
| Strain | EX | EY | EZ | EXY | EYZ | EZX | EV | E1 | E2 | E3 | El | Eabs | EE |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |  |
| Loading | FX | FY | FZ | RSLT |  |  |  |  |  |  |  |  |  |
| Reaction | FX | FY | FZ | RSLT |  |  |  |  |  |  |  |  |  |
| Residual Force | FX | FY | FZ | RSLT |  |  |  |  |  |  |  |  |  |
| Reaction Stress | PX | PY | PZ |  |  |  |  |  |  |  |  |  |  |
| Velocity | vx | VY | VZ | RSLT |  |  |  |  |  |  |  |  |  |
| Acceleration | AX | AY | AZ | RSLT |  |  |  |  |  |  |  |  |  |
| Plastic Strain | EPX | EPY | EPZ | EPXY | EPYZ | EPZX | EP1 | EP2 | EP3 | EPI | EPabs | EPE |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp | CWMax | EFSMax |  |  |  |  |
| Creep Strain | ECX | ECY | ECZ | ECXY | ECYZ | ECZX | EC1 | EC2 | EC3 | ECl | ECabs | ECE |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |  |
| Rubber Stretches | StchX | StchY | StchZ | StchXY | StchYZ | StchZX | Stch1 | Stch2 | Stch3 | Stchl | StchAbs | StchE |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Notes:

Rubber stretches are only available for HX8M elements with rubber material models. Strains are not available for this element when using rubber materials.
Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Models (105 and 109) are used.

## 3D Solid Continuum Two Phase TH10P, PN12P, PN15P, HX16P, HX20P

| Entity | Component |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | DZ | RSLT | Pres |  |  |  |  |  |  |  |
| Stress | SX | SY | SZ | SXY | SYZ | SZX | S1 | S2 | S3 | SI | Sabs | SE |
| (continued) | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |
| Strain | EX | EY | EZ | EXY | EYZ | EZX | E1 | E2 | E3 | El | Eabs | EE |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |
| Loading | FX | FY | FZ | RSLT | Q |  |  |  |  |  |  |  |
| Reaction | FX | FY | FZ | RSLT | Q |  |  |  |  |  |  |  |
| Residual Force | FX | FY | FZ | RSLT |  |  |  |  |  |  |  |  |
| Reaction Stress | PX | PY | PZ |  |  |  |  |  |  |  |  |  |
| Velocity | vx | VY | VZ | RSLT |  |  |  |  |  |  |  |  |
| Acceleration | AX | AY | AZ | RSLT |  |  |  |  |  |  |  |  |
| Plastic Strain | EPX | EPY | EPZ | EPXY | EPYZ | EPZX | EP1 | EP2 | EP3 | EPI | EPabs | EPE |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp | CWMax | EFSMax |  |  |  |
| Creep Strain | ECX | ECY | ECZ | ECXY | ECYZ | ECZX | EC1 | EC2 | EC3 | ECI | ECabs | ECE |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |  |  |  |

## Notes

Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Model (Model 109) is used.

## 3D Solid Continuum Explicit Dynamics TH4E, PN6E, HX8E

| Entity | Component |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | DZ | RSLT | Pres |  |  |  |  |  |  |
| Stress | SX | SY | SZ | SXY | SYZ | SZX | S1 | S2 | S3 | SI Sabs |  |
| (continued) | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |
| Strain |  |  |  |  |  |  |  |  |  |  |  |
| Loading | FX | FY | FZ | RSLT |  |  |  |  |  |  |  |
| Reaction | FX | FY | FZ | RSLT |  |  |  |  |  |  |  |
| Residual Force | FX | FY | FZ | RSLT |  |  |  |  |  |  |  |
| Reaction Stress | PX | PY | PZ |  |  |  |  |  |  |  |  |
| Velocity | VX | VY | VZ | RSLT |  |  |  |  |  |  |  |
| Acceleration | AX | AY | AZ | RSLT |  |  |  |  |  |  |  |
| Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |
| Creep Strain |  |  |  |  |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |  |  |

## Isoflex Thin Plates TF3, QF4

| Entity |  |  |  |  |  | Component |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DZ | RSLT | THX | THY |  |  |  |  |  |  |  |  |  |
| Stress | MX | MY | MXY | MMax | MMin Ml | $\beta$ | Nabs ME | Mx( T $^{\text {a }}$ | My( T $^{\text {) }}$ |  |  |  | Util(B) |
| (continued) | Damage | LogLife | SED | PWD | Eadp |  |  |  |  |  |  |  |  |
| Strain | BX | BY | BXY | BMax | BMin Bl | $\beta$ | Eabs BE | SED | PWD | Eadp |  |  |  |
| Loading | FZ | RSLT | MX | MY |  |  |  |  |  |  |  |  |  |
| Reaction | FZ | RSLT | MX | MY |  |  |  |  |  |  |  |  |  |
| Residual Force | FZ | RSLT | MX | MY |  |  |  |  |  |  |  |  |  |
| Reaction Stress | PZ |  |  |  |  |  |  |  |  |  |  |  |  |
| Velocity | VZ | RSLT |  |  |  |  |  |  |  |  |  |  |  |
| Acceleration | AZ | RSLT |  |  |  |  |  |  |  |  |  |  |  |
| Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Creep Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress | SX | SY | SXY | SMax | SMin SI | $\beta$ | Sabs SE | Damage | LogLife | SED | PWD | Ead |  |
| TMB Strain | EX | EY | EXY | EMax | EMin El | $\beta$ | Eabs EE | SED | PWD | Eadp |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Isoflex Thick Plates QSC4

| Entity | Component |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DZ | RSLT | THX | THY |  |  |  |  |  |  |  |  |  |  |  |
| Stress | MX | MY | MXY | Sx | Sy | MMax | MMin | MI | $\beta$ | Nabs | ME | Mx(T) | My( ) $^{\text {( }}$ | Mx(B) | My(B) |
| (continued) | Util( T) $^{\text {a }}$ | Util(B) | Damage | LogLife | SED | PWD | Eadp |  |  |  |  |  |  |  |  |
| Strain | BX | BY | BXY | EZX | EYZ | BMax | BMin | BI | $\beta$ | Eabs | BE | SED | PWD | Eadp |  |
| Loading | FZ | RSLT | MX | MY |  |  |  |  |  |  |  |  |  |  |  |
| Reaction | FZ | RSLT | MX | MY |  |  |  |  |  |  |  |  |  |  |  |
| Residual Force | FZ | RSLT | MX | MY |  |  |  |  |  |  |  |  |  |  |  |
| Reaction Stress | PZ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Velocity | VZ | RSLT |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Acceleration | AZ | RSLT |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Creep Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress | SX | SY | SXY | SMax | SMin | SI | $\beta$ | Sabs | SE | Damage | LogLife | SED | PWD | Eadp |  |
| TMB Strain | EX | EY | EXY | EMax | EMin | El | $\beta$ | Eabs | EE | SED | PWD | Eadp |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Mindlin Thick Plates TTF6, QTF8

| Entity | Component |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DZ | RSLT | THX | THY |  |  |  |  |  |  |  |  |  |  |  |
| Stress | MX | MY | MXY | Sx | Sy | MMax | MMin | MI | $\beta$ | Nabs | ME | Mx( T $^{\text {) }}$ | My( T $^{\text {( }}$ | Mx(B) | My(B) |
| (continued) | Util (T) | Util(B) | Damage | LogLife | SED | PWD | Eadp |  |  |  |  |  |  |  |  |
| Strain | BX | BY | BXY | EZX | EYZ | BMax | BMin | BI | $\beta$ | Eabs | BE | SED | PWD | Eadp |  |
| Loading | FZ | RSLT | MX | MY |  |  |  |  |  |  |  |  |  |  |  |
| Reaction | FZ | RSLT | MX | MY |  |  |  |  |  |  |  |  |  |  |  |
| Residual Force | FZ | RSLT | MX | MY |  |  |  |  |  |  |  |  |  |  |  |
| Reaction Stress | PZ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Velocity | VZ | RSLT |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Acceleration | AZ | RSLT |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Creep Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress | SX | SY | SXY | SMax | SMin | SI | $\beta$ | Sabs | SE | Damage | LogLife | SED | PWD | Eadp |  |
| TMB Strain | EX | EY | EXY | EMax | EMin | El | $\beta$ | Eabs | EE | SED | PWD | Eadp |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## 2D Axisymmetric Membranes BXM2, BXM3

| Entity | Component |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | RSLT |  |  |  |  |  |  |
| Stress | Sx | Sz | SMax | SMin | SI | $\beta$ | Sabs | SE |  |
| (continued) | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |
| Strain | Ex | Ez | EMax | EMin | EI | $\beta$ | Eabs | EE |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |
| Loading | FX | FY | RSLT |  |  |  |  |  |  |
| Reaction | FX | FY | RSLT |  |  |  |  |  |  |
| Residual Force | FX | FY | RSLT |  |  |  |  |  |  |
| Reaction Stress | PX | PY |  |  |  |  |  |  |  |
| Velocity | vX | VY | RSLT |  |  |  |  |  |  |
| Acceleration | AX | AY | RSLT |  |  |  |  |  |  |
| Plastic Strain | EPx | EPz | EPMax | EPMin | EPI | $\beta$ | EPabs | EPE |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |
| Creep Strain | ECx | ECz | ECMax | ECMin | ECI | $\beta$ | ECabs | ECE |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |

Note: Rubber models are available for use with the BXM2 element, however strains are output and rubber stretches are not available.

## 3D Space Membranes TSM3, SMI4

| Entity | Component |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | DZ | RSLT |  |  |  |  |  |  |  |
| Stress | Nx | Ny | Nxy | NMax | NMin | Ns | $\beta$ | Nabs | Ne |  |  |
| (continued) | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |
| Strain | Ex | Ey | Exy | EMax | EMin | El | $\beta$ | Eabs | EE |  |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |
| Loading | FX | FY | FZ | RSLT |  |  |  |  |  |  |  |
| Reaction | FX | FY | FZ | RSLT |  |  |  |  |  |  |  |
| Residual Force | FX | FY | FZ | RSLT |  |  |  |  |  |  |  |
| Reaction Stress | PX | PY | PZ |  |  |  |  |  |  |  |  |
| Velocity | vX | VY | VZ | RSLT |  |  |  |  |  |  |  |
| Acceleration | AX | AY | AZ | RSLT |  |  |  |  |  |  |  |
| Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |
| Creep Strain |  |  |  |  |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress | SX | SY | Sz | SXY | SYZ | SZX | S1 | S2 | S3 | SI Sabs | SE |
| (continued) | DDAMA | CURRD | damam | DFUNC | SED | PWD | Eadp |  |  |  |  |
| TMB Strain | EX | EY | EZ | EXY | EYZ | EZX | E1 | E2 | E3 | El Eabs | EE |
| (continued) | DDAMA | CURRD | damam | DFUNC | SED | PWD | Eadp |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |  |  |

## Element Reference Manual

## 2D Thin Axisymmetric Shells BXS3

| Entity | Component |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | RSLT | THZ | DU |  |  |  |  |  |  |
| Stress | Nx | Nz | Mx | Mz | Ny | NMax | NMin | Ns | $\beta$ | Nabs | Ne |
| (continued) | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |
| Strain | Ex | Ez | Bx | Bz | Ey | EMax | EMin | El | $\beta$ | Eabs | EE |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |
| Loading | FX | FY | RSLT | MZ | FDU |  |  |  |  |  |  |
| Reaction | FX | FY | RSLT | MZ | FDU |  |  |  |  |  |  |
| Residual Force | FX | FY | RSLT | MZ | FDU |  |  |  |  |  |  |
| Reaction Stress | PX | PY |  |  |  |  |  |  |  |  |  |
| Velocity | vX | VY | RSLT |  |  |  |  |  |  |  |  |
| Acceleration | AX | AY |  |  |  |  |  |  |  |  |  |
| Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |
| Creep Strain |  |  |  |  |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress | Sx | Sz | SMax | SMin | SI | $\beta$ | Sabs | SE |  |  |  |
| (continued) | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |
| TMB Strain | Ex | Ez | EPMax | EMin | El | $\beta$ | Eabs | EE |  |  |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |
| TMB Plastic Strain | EPx | EPz | EPMax | EPMin | EPI | $\beta$ | EPabs | EPE |  |  |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |
| TMB Creep Strain | ECx | ECz | ECMax | ECMin | ECI | $\beta$ | ECabs | ECE |  |  |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |

## 2D Thick Axisymmetric Shells BXSI2, BXSI3

| Entity | Component |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | RSLT | THZ |  |  |  |  |  |  |  |
| Stress | Nx | Nz | Mx | Mz | Nxy | NMax | NMin | Ns | $\beta$ | Nabs | Ne |
| (continued) | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |
| Strain | Ex | Ez | Bx | Bz | Exy | EMax | EMin | El | $\beta$ | Eabs | EE |
| (continued) | DDAMA | CURRD | damam | DFUNC | SED | PWD | Eadp |  |  |  |  |
| Loading | FX | FY | RSLT | MZ |  |  |  |  |  |  |  |
| Reaction | FX | FY | RSLT | MZ |  |  |  |  |  |  |  |
| Residual Force | FX | FY | RSLT | MZ |  |  |  |  |  |  |  |
| Reaction Stress | PX | PY |  |  |  |  |  |  |  |  |  |
| Velocity | vX | VY | RSLT |  |  |  |  |  |  |  |  |
| Acceleration | AX | AY |  |  |  |  |  |  |  |  |  |
| Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |
| Creep Strain |  |  |  |  |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress | Sx | Sz | Sxy | SMax | SMin | SI | $\beta$ | Sabs | SE |  |  |
| (continued) | Damage | LogLife | DDAMA | CURRD | damam | DFUNC | SED | PWD | Eadp |  |  |
| TMB Strain | Ex | Ez | Exy | EPMax | EMin | El | $\beta$ | Eabs | EE |  |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |
| TMB Plastic Strain | EPx | EPz | EPxy | EPMax | EPMin | EPI | $\beta$ | EPabs | EPE |  |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |
| TMB Creep Strain | ECx | ECz | ECxy | ECMax | ECMin | ECI | $\beta$ | ECabs | ECE |  |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |

## Element Reference Manual

## 3D Flat Thin Shells TS3, QSI4



## 3D Flat Thin Nonlinear Shell TSR6

| Entity | Component |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | DZ | RSLT | THL1 |  |  |  |  |  |  |  |  |  |  |
| Stress | Nx | Ny | Nxy | Mx | My | Mxy | NMax | NMin | Ns | $\beta$ | Nabs | Ne | $\begin{aligned} & \mathrm{Nx}(\mathrm{~T}) / \\ & \mathrm{Mx}(\mathrm{~T}) \end{aligned}$ | $\begin{aligned} & \mathrm{Ny}(\mathrm{~T}) / \\ & \mathrm{Ny}(\mathrm{~T}) \end{aligned}$ | $\begin{aligned} & \mathrm{Nx}(\mathrm{~B}) / \\ & \mathrm{Mx}(\mathrm{~B}) \end{aligned}$ |
| (continued) | $\begin{aligned} & \mathrm{Ny}(\mathrm{~B}) / \\ & \mathrm{My}(\mathrm{~B}) \end{aligned}$ | Util(T) | Util(B) | MUtil(T) | MUtil(B) | Damage | Loglife | $\begin{gathered} \text { DDAM } \\ \text { A } \end{gathered}$ | $\begin{gathered} \text { CURR } \\ \mathrm{D} \end{gathered}$ | $\begin{gathered} \text { DAMA } \\ \mathrm{M} \end{gathered}$ | $\begin{gathered} \text { DFUN } \\ \mathrm{C} \end{gathered}$ | SED | PWD | $\mathrm{Fc}(\mathrm{T})$ | Fc (B) |
| Eadp |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Strain | Ex | Ey | Exy | Bx | By | Bxy | EMax | EMin | El | $\beta$ | Eabs | EE |  |  |  |
| (continued) | DDAMA | CURRD | damam | DFUNC | SED | PWD | Eadp |  |  |  |  |  |  |  |  |
| Loading | FX | FY | FZ | RSLT | ML1 |  |  |  |  |  |  |  |  |  |  |
| Reaction | FX | FY | FZ | RSLT | ML1 |  |  |  |  |  |  |  |  |  |  |
| Residual Force | FX | FY | FZ | RSLT | ML1 |  |  |  |  |  |  |  |  |  |  |
| Reaction Stress | PX | PY | PZ |  |  |  |  |  |  |  |  |  |  |  |  |
| Velocity | vx | VY | VZ | RSLT |  |  |  |  |  |  |  |  |  |  |  |
| Acceleration | AX | AY | AZ | RSLT |  |  |  |  |  |  |  |  |  |  |  |
| Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Creep Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress | sx | SY | sz | SXY | SYZ | szx | S1 | S2 | S3 | SI | Sabs | SE |  |  |  |
| (continued) | Damage | LogLife | DDAMA | CURRD | damam | DFUNC | SED | Eadp |  |  |  |  |  |  |  |
| TMB Strain | EX | EY | EZ | EXY | EYZ | EZX | E1 | E2 | E3 | EI | Eabs | EE |  |  |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |  |  |  |
| TMB Plastic Strain | EPX | EPY | EPZ | EPXY | EPYZ | EPLX | EP1 | EP2 | EP3 | EPI | EPabs | EPE | $\underset{\mathrm{x}}{\text { CWMa }}$ | $\begin{gathered} \text { EFSMa } \\ \mathrm{x} \end{gathered}$ |  |
| (continued) | DDAMA | CURRD | damam | DFUNC | SED | PWD | Eadp |  |  |  |  |  |  |  |  |
| TMB Creep Strain | ECX | ECY | ECZ | ECXY | ECYZ | ECZX | EC1 | EC2 | EC3 | ECI | ECabs | ECE |  |  |  |
| (continued) | DDAMA | CURRD | damam | DFUNC | SED | PWD | Eadp |  |  |  |  |  |  |  |  |
|  | TMB Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Model (Model 109) is used. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Element Reference Manual

## Semilloof Shells TSL6, QSL8

| Entity | Component |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | DZ | RSLT | THL1 | THL2 |  |  |  |  |  |  |  |  |
| Stress | Nx | Ny | Nxy | Mx | My | Mxy | NMax | NMin | Ns | $\beta$ | Nabs |  | $\begin{aligned} & \mathrm{Nx}(\mathrm{~T}) / \\ & \mathrm{Mx}(\mathrm{~T}) \end{aligned}$ | $\begin{array}{ll} \mathrm{Ny}(\mathrm{~T}) / & \mathrm{Nx}( \\ \mathrm{My}(\mathrm{~T}) & \mathrm{B}) / \\ & \mathrm{Mx} \\ & \text { (B) } \end{array}$ |
| (continued) | $\begin{aligned} & \mathrm{Ny}(\mathrm{~B}) / \\ & \mathrm{My}(\mathrm{~B}) \end{aligned}$ | Util( $\mathrm{T}^{\text {( }}$ | Util(B) | MUtil(T) | MUtil(B) | Damage | LogLife | DDAMA | $\begin{aligned} & \text { CURR } \\ & \text { D } \end{aligned}$ | DAMAM | DFUNC | SED | PWD | $\mathrm{Fc}(\mathrm{T}) \mathrm{Fc}$ <br> B) |
| (continued) | Eadp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Strain | Ex | Ey | Exy | Bx | By | Bxy | EMax | EMin | El | $\beta$ | Eabs | EE |  |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |  |  |
| Loading | FX | FY | FZ | RSLT | ML1 | ML2 |  |  |  |  |  |  |  |  |
| Reaction | FX | FY | FZ | RSLT | ML1 | ML2 |  |  |  |  |  |  |  |  |
| Residual Force | FX | FY | FZ | RSLT | ML1 | ML2 |  |  |  |  |  |  |  |  |
| Reaction Stress | PX | PY | PZ |  |  |  |  |  |  |  |  |  |  |  |
| Velocity | VX | VY | VZ | RSLT |  |  |  |  |  |  |  |  |  |  |
| Acceleration | AX | AY | AZ | RSLT |  |  |  |  |  |  |  |  |  |  |
| Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Creep Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress | SX | SY | SZ | SXY | SYZ | SZX | S1 | S2 | S3 | SI | Sabs | SE |  |  |
| (continued) | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |
| TMB Strain | EX | EY | EZ | EXY | EYZ | EZX | E1 | E2 | E3 | El | Eabs | EE |  |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |  |  |
| TMB Plastic Strain | EPX | EPY | EPZ | EPXY | EPYZ | EPZX | EP1 | EP2 | EP3 | EPI | EPabs |  | CWMax | $\begin{gathered} \text { EFSMa } \\ \mathrm{x} \end{gathered}$ |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |  |  |
| TMB Creep Strain | ECX | ECY | ECZ | ECXY | ECYZ | ECZX | EC1 | EC2 | EC3 | ECI | ECabs | ECE |  |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |  |  |

## Notes

TMB Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Model (Model 109) is used.

## 3D Thick Shells TTS3, TTS6, QTS4, QTS8

| Entity | Component |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | DZ | RSLT | THX | THY | THZ |  |  |  |  |  |  |  |  |
| Stress | Nx | Ny | Nxy | Mx | My | Mxy | Sx | Sy | NMax | NMin | $\beta$ | $\begin{gathered} \mathrm{Nab} \\ \mathrm{~s} \end{gathered}$ | NE | $\begin{aligned} & \mathrm{Nx}(\mathrm{~T}) / \\ & \mathrm{Mx}(\mathrm{~T}) \end{aligned}$ | $\begin{aligned} & \mathrm{Ny}(\mathrm{~T}) / \\ & M y(T) \end{aligned}$ |
| (continued) | $N x(B) / M x($ <br> B) | $\begin{aligned} & \mathrm{Ny}(\mathrm{~B}) / \\ & \mathrm{My}(\mathrm{~B}) \end{aligned}$ | Util( ${ }^{\text {( }}$ | Util(B) | MUtil( T ) | MUtil(B) | Damage | LogLife | DDAMA | CURRD | DAMAM | $\begin{aligned} & \text { DFU } \\ & \text { NC } \end{aligned}$ | SED | PWD | $\mathrm{Fc}(\mathrm{T})$ |
| (continued) | Fc (B) | Eadp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Loading | FX | FY | FZ | RSLT | MX | MY | MZ |  |  |  |  |  |  |  |  |
| Reaction | FX | FY | FZ | RSLT | MX | MY | MZ |  |  |  |  |  |  |  |  |
| Residual Force | FX | FY | FZ | RSLT | MX | MY | MZ |  |  |  |  |  |  |  |  |
| Reaction Stress | PX | PY | PZ |  |  |  |  |  |  |  |  |  |  |  |  |
| Velocity | VX | VY | VZ | RSLT |  |  |  |  |  |  |  |  |  |  |  |
| Acceleration | AX | AY | AZ | RSLT |  |  |  |  |  |  |  |  |  |  |  |
| Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Creep Strain |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress | SX | SY | SZ | SXY | SYZ | SZX | S1 | S2 | S3 | SI | Nabs | SE |  |  |  |
| (continued) | Damage | LogLife | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |  |
| TMB Strain | EX | EY | EZ | EXY | EYZ | EZX | E1 | E2 | E3 | El | Eabs | EE |  |  |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |  |  |  |
| TMB Plastic Strain | EPX | EPY | EPZ | EPXY | EPYZ | EPZX | EP1 | EP2 | EP3 | EPI | EPabs |  | $\begin{gathered} \text { CWMa } \\ \text { x } \end{gathered}$ | $\begin{gathered} \text { EFSMa } \\ \mathrm{x} \end{gathered}$ |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |  |  |  |
| TMB Creep Strain | ECX | ECY | ECZ | ECXY | ECYZ | ECZX | EC1 | EC2 | EC3 | ECI | ECabs | ECE |  |  |  |
| (continued) | DDAMA | CURRD | DAMAM | DFUNC | SED | PWD | Eadp |  |  |  |  |  |  |  |  |

Notes
TMB Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Model (Model 109) is used.

## Element Reference Manual

## 2D Joints (for Bars, Plane Stress and Plane Strain) JNT3

| Entity | Component |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | RSLT |  |  |  |  |
| Stress | Fx | Fy | Damage | LogLife | SED | PWD | Eadp |
| Strain | Ex | Ey | SED | PWD | Eadp |  |  |
| Loading | FX | FY | RSLT |  |  |  |  |
| Reaction | FX | FY | RSLT |  |  |  |  |
| Residual Force | FX | FY | RSLT |  |  |  |  |
| Reaction Stress |  |  |  |  |  |  |  |
| Velocity | VX | VY | RSLT |  |  |  |  |
| Acceleration | AX | AY | RSLT |  |  |  |  |
| Plastic Strain | EPx | EPy | SED | PWD | Eadp |  |  |
| Creep Strain |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |

## 2D Joints (for Engineering and Kirchhoff Beams) JPH3

| Entity | Component |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | RSLT | THZ |  |  |  |  |
| Stress | Fx | Fy | Mz | Damage | LogLife | SED | PWD | Eadp |
| Strain | Ex | Ey | Bz | SED | PWD | Eadp |  |  |
| Loading | FX | FY | RSLT | MZ |  |  |  |  |
| Reaction | FX | FY | RSLT | MZ |  |  |  |  |
| Residual Force | FX | FY | RSLT | MZ |  |  |  |  |
| Reaction Stress |  |  |  |  |  |  |  |  |
| Velocity | vx | VY | RSLT |  |  |  |  |  |
| Acceleration | AX | AY | RSLT |  |  |  |  |  |
| Plastic Strain | EPx | EPy | BPz | SED | PWD | Eadp |  |  |
| Creep Strain |  |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |

## 2D Joints (for Grillage Beams and Plates) JF3

| Entity | Component |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DZ | RSLT | THXZ | THY |  |  |  |  |  |
| Stress | Fz | Mx | My | Damage | LogLife | SED | PWD | Eadp |  |
| Strain | Ez | Bx | By | SED | PWD | Eadp |  |  |  |
| Loading | FZ | RSLT | MX | MY |  |  |  |  |  |
| Reaction | FZ | RSLT | MX | MY |  |  |  |  |  |
| Residual Force | FZ | RSLT | MX | MY |  |  |  |  |  |
| Reaction Stress |  |  |  |  |  |  |  |  |  |
| Velocity | VZ | RSLT |  |  |  |  |  |  |  |
| Acceleration | AZ | RSLT |  |  |  |  |  |  |  |
| Plastic Strain | EPx | EPy | BPz | SED | PWD | Eadp |  |  |  |
| Creep Strain |  |  |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |

## 2D Joints (for Axisymmetric Solids) JAX3

| Entity | Component |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | RSLT |  |  |  |  |
| Stress | Fx | Fy | Damage | LogLife | SED | PWD | Eadp |
| Strain | Ex | Ey | SED | PWD | Eadp |  |  |
| Loading | FX | FY | RSLT | MZ |  |  |  |
| Reaction | FX | FY | RSLT | MZ |  |  |  |
| Residual Force | FX | FY | RSLT | MZ |  |  |  |
| Reaction Stress |  |  |  |  |  |  |  |
| Velocity | vx | VY | RSLT |  |  |  |  |
| Acceleration | AX | AY | RSLT |  |  |  |  |
| Plastic Strain | EPx | EPy | SED | PWD | Eadp |  |  |
| Creep Strain |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |

## 2D Joints (for Axisymmetric Shells) JXS3

| Entity | Component |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | RSLT | THZ |  |  |  |  |
| Stress | Fx | Fy | Mz | Damage | LogLife | SED | PWD | Eadp |
| Strain | Ex | Ey | Bz | SED | PWD | Eadp |  |  |
| Loading | FX | FY | RSLT | MZ |  |  |  |  |
| Reaction | FX | FY | RSLT | MZ |  |  |  |  |
| Residual Force | FX | FY | RSLT | MZ |  |  |  |  |
| Reaction Stress |  |  |  |  |  |  |  |  |
| Velocity | vx | VY | RSLT |  |  |  |  |  |
| Acceleration | AX | AY | RSLT |  |  |  |  |  |
| Plastic Strain | EPx | EPy | BPz | SED | PWD | Eadp |  |  |
| Creep Strain |  |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |

## 3D Joints (for generall 3 dof connection) JNT4, JL43

(for Bars, Solids, Space Membranes and Semiloof Shell Corners)

| Entity | Component |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | DZ | RSLT |  |  |  |  |
| Stress | Fx | Fy | Fz | Damage | LogLife | SED | PWD | Eadp |
| Strain | Ex | Ey | Ez | SED | PWD | Eadp |  |  |
| Loading | FX | FY | FZ | RSLT |  |  |  |  |
| Reaction | FX | FY | FZ | RSLT |  |  |  |  |
| Residual Force | FX | FY | FZ | RSLT |  |  |  |  |
| Reaction Stress |  |  |  |  |  |  |  |  |
| Velocity | VX | VY | VZ | RSLT |  |  |  |  |
| Acceleration | AX | AY | AZ | RSLT |  |  |  |  |
| Plastic Strain | EPx | EPy | EPz | SED | PWD | Eadp |  |  |
| Creep Strain |  |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |

## 3D Joints (for generall 6 dof connection) JSH4, JL46

(for Engineering, Kirchhoff and Semiloof Beam End Nodes)

| Entity | Component |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | DZ | RSLT | THX | THY | THZ |  |  |  |  |
| Stress | Fx | Fy | Fz | Mx | My | Mz | Damage | LogLife | SED | PWD | Eadp |
| Strain | Ex | Ey | Ez | Bx | By | Bz | SED | PWD | Eadp |  |  |
| Loading | FX | FY | FZ | RSLT | MX | MY | MZ |  |  |  |  |
| Reaction | FX | FY | FZ | RSLT | MX | MY | MZ |  |  |  |  |
| Residual Force | FX | FY | FZ | RSLT | MX | MY | MZ |  |  |  |  |
| Reaction Stress |  |  |  |  |  |  |  |  |  |  |  |
| Velocity | VX | VY | VZ | RSLT |  |  |  |  |  |  |  |
| Acceleration | AX | AY | AZ | RSLT |  |  |  |  |  |  |  |
| Plastic Strain | EPx | EPy | EPz | BPx | BPy | BPz | SED | PWD | Eadp |  |  |
| Creep Strain |  |  |  |  |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |  |  |

## 3D Joints (for Semilloof Element Mid-side Nodes) JSL4

| Entity | Component |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | DX | DY | DZ | RSLT | THL1 | THL2 |  |  |  |  |
| Stress | Fx | Fy | Fz | M1 | M2 | Damage | LogLife | SED | PWD | Eadp |
| Strain | Ex | Ey | Ez | B1 | B2 | SED | PWD | Eadp |  |  |
| Loading | FX | FY | FZ | RSLT | ML1 | ML2 |  |  |  |  |
| Reaction | FX | FY | FZ | RSLT | ML1 | ML2 |  |  |  |  |
| Residual Force | FX | FY | FZ | RSLT | ML1 | ML2 |  |  |  |  |
| Reaction Stress |  |  |  |  |  |  |  |  |  |  |
| Velocity | vx | VY | VZ | RSLT |  |  |  |  |  |  |
| Acceleration | AX | AY | AZ | RSLT |  |  |  |  |  |  |
| Plastic Strain | EPx | EPy | EPz | BP1 | BP2 | SED | PWD | Eadp |  |  |
| Creep Strain |  |  |  |  |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |  |  |  |  |

## Thermal Bars BFD2/3, BFS2/3, BFX2/3

| Entity |  | Component |
| :---: | :---: | :--- |
| Potential | PHI |  |
| Gradient | Gx | Eadp |
| Flux | qx | Eadp |
| Reaction | Q |  |

## Thermal Links LFD2, LFS2, LFX2

| Entity |  | Component |
| :---: | :---: | :--- |
| Potential | PHI |  |
| Gradient | n.a. | Eadp |
| Flux | qx | Eadp |
| Reaction | Q |  |

## Plane and Axisymmetric Field TFD3/6, QFD4/8, TXF3/6, QXF4/8

| Entity |  |  | Component |  |
| :---: | :---: | :---: | :---: | :---: |
| Potential | PHI |  |  |  |
| Gradient | Gx | Gy | Eadp |  |
| Flux | qx | qy | Eadp |  |
| Reaction | Q |  |  |  |

## Solid Field TF4/10, PF6/12/15, HF8/16/20, TF10S, PF6C/12C, HF8C/16C

| Entity |  |  |  | Component |
| :---: | :---: | :---: | :---: | :---: |
| Potential | PHI |  |  |  |
| Gradient | Gx | Gy | Gz | Eadp |
| Flux | qx | qy | qz | Eadp |
| Reaction | Q |  |  |  |

## Plane and Axisymmetric Hygro-Thermal THT3/6, QHT4/8, TXHT3/6, QXHT4/8

| Entity | Component |  |  |  |  |  |  |
| :---: | :---: | :--- | :--- | :--- | :--- | :--- | :--- |
| Nodal variable | T |  |  |  |  |  |  |
| Temperature flux | qX | qY | qZ | RSLT |  |  |  |
| Water vapour flux | JVX | JyY | JVZ | RSLT |  |  |  |
| Liquid water flux | JWX | JWY | JWZ | RSLT |  |  |  |
| Temperature gradient | GTX | GTY | GTZ | RSLT |  |  |  |
| Water saturation <br> gradient | GWX | GWY | GWZ | RSLT |  |  |  |
| Other hygro-thermal <br> results | SW | ROWC | PV | DH | TEFH | POR | TC |

## Hygro-thermal results components:

SW = Water saturation
ROWC = Liquid water content
$P V=$ Water vapour pressure
DH $=$ Degree of hydration
TEFH = Effective time of hydration
POR = Porosity
$T C=$ Thermal conductivity
PMD = Water permeability
$\mathrm{Hr}=$ Relative humidity

## Solid Hygro-Thermal THT4/10, PHT6/12/16, HHT8/16/20



Hygro-thermal results components:
SW = Water saturation
ROWC = Liquid water content
$P V=$ Water vapour pressure
DH $=$ Degree of hydration
TEFH $=$ Effective time of hydration
$P O R=$ Porosity
$T C=$ Thermal conductivity
PMD = Water permeability
$\mathrm{Hr}=$ Relative humidity

## 2D Interface Element IPN4, IPN6, IAX4, IAX6

| Entity |  |  | Component |  |  |
| :---: | :--- | :--- | :---: | :--- | :--- |
| Displacement | Dx | Dy | RSLT |  |  |
| Stress | Sx | Sy | Damage | LogLife | Eadp |
| Strain | Ex | Ey | Eadp |  |  |
| Loading | Fx | Fy | RSLT | MZ |  |
| Reaction | Fx | Fy | RSLT | MZ |  |
| Residual Force | Fx | Fy | RSLT |  |  |
| Reaction Stress |  |  |  |  |  |
| Velocity | Vx | Vy | RSLT |  |  |
| Acceleration | Ax | Ay | RSLT |  |  |
| Plastic Strain |  |  |  |  |  |
| Creep Strain |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |

## 2D Two Phase Interface Elements IPN6P, IPN8P

| Entity | Component |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | Dx | Dy | RSLT | Press |  |  |
| Stress | Sx | Sy | Q | Damage | LogLife | Eadp |
| Strain | Ex | Ey | dP | Eadp |  |  |
| Loading | Fx | Fy | RSLT |  |  |  |
| Reaction | Fx | Fy | RSLT | Q |  |  |
| Residual Force | Fx | Fy | RSLT | Q |  |  |
| Reaction Stress |  |  |  |  |  |  |
| Velocity | Vx | Vy | RSLT |  |  |  |
| Acceleration | Ax | Ay | RSLT |  |  |  |
| Plastic Strain |  |  |  |  |  |  |
| Creep Strain |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |

## 3D Interface Element IS6 IS8 IS12 IS16

| Entity |  |  |  | Component |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | Dx | Dy | RSLT |  |  |
| Stress | Sx | Sy | Sz | Ez | Eadp |
| Strain | Ex | Ey | Eadp |  |  |
| Loading | Fx | Fy | RSLT |  |  |
| Reaction | Fx | Fy | RSLT |  |  |
| Residual Force | Fx | Fy | RSLT |  |  |
| Reaction Stress |  |  |  |  |  |
| Velocity | Vx | Vy | RSLT |  |  |
| Acceleration | Ax | Ay | RSLT |  |  |
| Plastic Strain |  |  |  |  |  |
| Creep Strain |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |

## 3D Two Phase Interface Element IS12P, IS16P

| Entity |  |  | Component |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement | Dx | Dy | Dz | RSLT | Press |  |
| Stress | Sx | Sy | Q | Damage | LogLife | Eadp |
| Strain | Ex | Ey | Ez | dP | Eadp |  |
| Loading | Fx | Fy | Fz | RSLT |  |  |
| Reaction | Fx | Fy | Fz | RSLT | Q |  |
| Residual Force | Fx | Fy | Fz | RSLT | Q |  |
| Reaction Stress |  |  |  |  |  |  |
| Velocity | Vx | Vy | Vz | RSLT |  |  |
| Acceleration | Ax | Ay | Az | RSLT |  |  |
| Plastic Strain |  |  |  |  |  |  |
| Creep Strain |  |  |  |  |  |  |
| Rubber Stretches |  |  |  |  |  |  |
| TMB Stress |  |  |  |  |  |  |
| TMB Strain |  |  |  |  |  |  |
| TMB Plastic Strain |  |  |  |  |  |  |
| TMB Creep Strain |  |  |  |  |  |  |

## Appendix L: Joint Element

## Compatibility.

## Joint Element Compatibility and Notes

Joint elements are compatible with the following elements:

| Joint Element | Compatible Finite Elements |  |
| :---: | :---: | :---: |
| JNT3 | Bars | BAR2, BAR3 |
|  | 2D Plane Stress | $\begin{aligned} & \text { TPM3, TPM6, QPM4, QPM8, TPK6, QPK8, QPM4M, } \\ & \text { TPM3E, QPM4E, } \end{aligned}$ |
|  | 2D Plane Strain | TPN3, TPN6, QPN4, QPN8, TNK6, QNK8, TPN6P, QPN8P, QPN4M, QPN4L |
| JPH3 | 2D Beams | BMI2, BMI21, BMI2N, BMI3N, BMI3, BMI3N, BMI2X, BMI3X, BM3, BMX3 |
| JF3 | 2D Grillage | GRIL |
|  | 2D Plates | TF3, QF4, TF6, QSC4, TTF6, QTF8 |
| JNT4 | 3D Bars | BRS2, BRS3, |
|  | 3D Solids | TH4, TH10, PN6, PN12, PN15, HX8, HX16, HX20, TH10P, PN12P, PN15P, HX16P, HX20P, HX8M, PN6L, PN12L, HX8L, HX16L, TH10S |
|  | Space | TSM3, SMI4 |


| Joint Element | Compatible Finite Elements |  |
| :---: | :---: | :---: |
|  | Membranes |  |
|  | 3D Shell | TSR6 (corner nodes) |
| JL43 | Semiloof Shells | TSL6, QSL8 (corner nodes) |
| JSH4 | 3D Beams | BS3, BS4, BSX4, BMI21, BMI31, BMI22, BMI33, <br> BMX21, BMX31, BMX22, BMX33, BMI21W, BMI22W, <br> BMI31W, BMI33W, BMX21W, BMX22W, BMX31W, BMX33W |
|  | 3D Shells | TS3, QSI4, TTS3, TTS6, QTS4, QTS8 |
| JL46 | Semiloof Beams | BSL3, BSL4, BXL4 (corner nodes) |
| JSL4 | Semiloof Beams | BSL3, BSL4, BXL4 (mid-side nodes) |
|  | Semiloof Shells | QSL8, TSL6 (mid-side nodes) |
| JAX3 | Axisymmetric Solids | TAX3, TAX6, QAX4, QAX8, TAX6P, QAX8P, TAX3E, QAX4E, TAX6P, TXK6, QXK8, QAX4M, QAX4L |
| JXS3 | Axisymmetric Shells | BXS3, BXSI2, BXSI3, |

## Notes on the use of Joints

1. The nodes of a joint element need not be coincident, but for correct response the distance between them should be as small as possible. This is particularly important with joint elements which contain rotational degrees of freedom, since the stiffness matrix is not formulated using engineering beam theory. This means that a joint moment is independent of both shear force and its length. For instance, the moment calculated with a joint length of zero will remain the same magnitude at any other joint length. These effects can be exacerbated significantly in dynamic analyses (e.g. eigenvalue extraction or Hilber dynamics). Non-coincident nodes will lead to additional forces in the solution which are not in equilibrium (usually small and swamped, but could be significant sometimes). It is not recommend to have joints "hanging off" the side of a modelled structure, having a large stiffness associated.
2. If eccentricity is defined for a joint element (JPH3/JSH4/JL46), the joint will behave in the same manner as an infinitesimally short eccentric beam.
3. Joints do not support any geometric nonlinearity. They may be used, however, in geometrically nonlinear analyses but will themselves remain geometrically linear (that is, infinitesimal strain is assumed and large deformation effects are ignored).
4. The strain for a joint element is measured as follows:

- $\quad$ Strain measure $=($ displacement for 2 nd node $)-($ displacement for 1 st node $)$
- This strain being measured in the local axis system. Therefore, if node 1 is restrained, node 2 would need to be displaced in the negative local ( $\mathrm{x} / \mathrm{y} / \mathrm{z}$ ) direction to generate compressive contact forces.

4. The rotation output for a joint element is measured in radians.

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[^0]:    MATRIX PROPERTIES STIFFNESS 6 K1
    K21 element stiffness matrix (Not supported in LUSAS Modeller)
    MATRIX PROPERTIES MASS 6 M1,..., M21 element mass matrix (Not supported in

