LUSAS

Element Reference Manual

Element Reference Manual

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LUSAS Forge House, 66 High Street, Kingston upon Thames, Surrey, KT1 1HN, United Kingdom

> Tel: +44 (0)20 8541 1999 Fax +44 (0)20 8549 9399 Email: info@lusas.com http://www.lusas.com

Distributors Worldwide

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Notation.

Α	Cross sectional area	
Ар	Plastic area	
As, Asy, Asz	Effective shear area	
$\mathbf{A}_1 \dots \mathbf{A}_n$	Nodal cross sectional areas	
ar	Mass Rayleigh damping constant	
α	Coefficient of thermal expansion	
αs	Softening parameter	
α x , α y , α z , α xy , α xz , α yz	Orthotropic thermal expansion coefficients	
αχ, αγ, αζ	Angular accelerations	
br	Stiffness Rayleigh damping parameter	
β	Shear retention factor/parameter	
β	Principal stresses direction	
С	Specific heat capacity	
Ci	(i)th hardening stiffness	
\mathbf{C}_0	Neo-Hookean rubber model constant	
C_1, C_2	Mooney-Rivlin rubber model constants	
c	Cohesion	
со	Initial cohesion	
Dij	Rigidity coefficients	
	8	
du, dq	Relative displacement, rotation	

Ер	Elasto-plastic modulus		
Ex, Ey, Ez	Orthotropic moduli of elasticity		
ер	Strain at peak compressive strength		
ey, ez	Eccentricity		
εχ, εγ, εΖ	Direct strains (local or global)		
ES	Maximum shear strain		
ε	Von Mises equivalent strain		
εc	Creep strains		
ε p	Equivalent plastic strain		
Fx, Fy, Fz	Forces (local or global)		
Fyld	Yield force		
F	Deformation gradient		
fc'	Compressive strength of concrete		
ft'	Tensile strength of concrete		
ψ x , ψ y , ψ z	Flexural (bending) strain resultants		
ψ xy , ψ xz , ψ yz	Torsional strain resultants		
G	Shear modulus		
Gf	Fracture energy		
Gxy, Gxz, Gyz	Orthotropic shear moduli		
$\gamma \mathbf{x}, \gamma \mathbf{y}, \gamma \mathbf{z}$	Membrane strain resultants		
$\gamma \mathbf{x}, \gamma \mathbf{y}, \gamma \mathbf{z}$	Field gradients (local or global)		
Н	Enthalpy		
Hiı	Isotropic hardening parameter		
Hk1	Kinematic hardening parameter		
hc	Convective heat transfer coefficient		
hf	Heat fraction		
hr	Radiative heat transfer coefficient		

$\theta \mathbf{x}, \theta \mathbf{y}, \theta \mathbf{z}$	Rotations (local or global)		
θ_1, θ_2	Loof node rotations (local)		
θα, θβ	Nodal rotations for thick shells		
θλ	Angle defining principal directions of λ_1, λ_2		
Iy, Iz	1st moments of inertia		
Iyy, Izz	2nd moments of inertia		
Iyz	Product moment of inertia		
J	Volume ratio (determinant of F)		
K	Spring stiffness		
Kc	Contact stiffness		
Kl	Lift-off stiffness		
Ко	Original gap conductance		
Kt	Torsional constant		
k	Thermal conductivity		
kx, ky, kz	Orthotropic thermal conductivities		
kr	Bulk modulus		
к	Hardening stiffness		
Li	Limit of (i)th hardening stiffness		
$\lambda_1, \lambda_2, \lambda_3$	Principal stretches		
Μ	Mass		
Mx, My, Mz	Concentrated moments (local or global)		
$Mx, My, Mz, M\theta$	Flexural moments (local or global)		
Mxy, Mxz, Myz	Torsional moments (local or global)		
$\mathbf{M}_1, \mathbf{M}_2$	Concentrated loof moments (local or global)		
$\mathbf{m}_{\mathrm{x}}, \mathbf{m}_{\mathrm{y}}, \mathbf{m}_{\mathrm{z}}$	Mass in element local directions		
μ	Coulomb friction coefficient		
μ ri, α ri	Ogden rubber model constants		

Nx, Ny, Nz, No Membran	e resultants (local or global)
------------------------	--------------------------------

Nx, Ny, Nxy Stress resultants

- Nmax, Nmin Principal stress resultants
 - Ns Maximum shear stress resultant
 - Ne Von Mises equivalent stress resultant
 - υ Poisson's ratio
- υxy, υxz, υyz Orthotropic Poisson's ratio
 - Px, Py, Pz Concentrated loads (global)
 - ρ Mass density
 - Q Field loading
 - qa Field face loading flux/unit area
 - qv Field volume loading flux/unit volume
 - qx, qy, qz Field fluxes (local or global)
 - \mathbf{Q}_{H} Rate of internal heat generation per unit volume Rate of internal mass (liquid+vapour) generation per unit volume Heat flux
 - \mathbf{Q}_{w} Rate of internal heat generation per unit volume Rate of internal mass (liquid+vapour) generation per unit volume Heat flux
 - \mathbf{q}_{H} Rate of internal heat generation per unit volume Rate of internal mass (liquid+vapour) generation per unit volume Heat flux
 - qs Stress potential parameters
 - \mathbf{q}_{w} Mass (liquid+vapour) flux Relative humidity Initial relative humidity
 - **RH** Mass (liquid+vapour) flux Relative humidity Initial relative humidity
 - **RH**₀ Mass (liquid+vapour) flux Relative humidity Initial relative humidity
 - Sp Plastic shear area
 - σy Yield stress
 - σy_0 Initial uniaxial yield stress
 - $\sigma x, \sigma y, \sigma z$ Direct stresses (local or global)

σ max. σmin	Principal stresses
,	Shear stresses (local or global)
••••••	Maximum shear stress
	Von Mises equivalent stress
Т	Temperature
	Final, initial temperatures
	Nodal thicknesses
	Displacements (global)
	Field variable
_	External environmental temperature
	Frictional angle
· ·	Initial frictional angle
φ	Body force potential
Vx, Vy, Vz	Nodal velocities (global)
V11, V12 V33	Left stretch tensor components
Wx, Wy, Wz	Uniformly distributed intensities
X, Y, Z	Nodal coordinates (global)
Xcbf, Ycbf, Zcbf	Constant body forces (global)
Xo, Yo, Zo	Offsets of finite element model coordinate system from point about which global angular acceleration and velocities are applied
$y_1, z_1 y_4, z_4$	Cross sectional coordinates (local)
Zyp, Zzp	Torsional plastic moduli
Zyy _p , Zzz _p	Flexural plastic moduli
ω	Frequency of vibration
$\Omega \mathbf{x}, \Omega \mathbf{y}, \Omega \mathbf{z}$	Angular velocities (global)

Introduction.

Overview

The LUSAS *Element Reference Manual* describes the elements currently available in LUSAS Solver. It has been designed to be used in conjunction with the *Solver Reference Manual* and provides input/output information which is specific to each element type. If you require:

- General theoretical information refer to Theory Manual Volume 1
- <u>Element related</u> theoretical / formulation information refer to *Theory Manual Volume 2*

Element selection

Details of typical <u>element uses</u> are provided and, to assist you with choosing an element for a particular modelling task, three alternative selection methods are available for selecting by:

- **Element type** listing just element group, sub-group and element name
- Element index showing element name, geometry, nodal freedoms and element availability
- □ Element summary showing element names, material property, loading, nonlinear, integration, and mass modelling capabilities

Of these three methods, the element summary tables provide the most detail to enable correct element selection for a particular modelling task.

Element uses

The following brief descriptions of each element group are provided to assist you with element selection for a particular modelling task.

Additional more detailed and element-specific recommendations on use can be found by viewing the Recommendations on Use section provided within each element's listing. For an example see <u>3D Isoparametric Thick Beam Elements</u>

Bar Elements

Bar elements are used to model plane and space truss structures, cables in cable-stayed structures, and stiffening reinforcement.

- LUSAS incorporates 2 and 3-dimensional bar elements which may either be straight or curved.
- Bar elements model *axial force* only.

Beam Elements

Beam elements are used to model plane frames, space frame structures, and cables in cable-stayed structures.

- LUSAS incorporates a variety of thin and thick beams in both 2 and 3-dimensions. In addition, specialised beam elements for modelling grillage or eccentrically ribbed plate structures are available.
- LUSAS beam elements may be either straight or curved and may model *axial force*, *bending* and *torsional behaviour*.

2D Continuum Elements

2D continuum elements are used to model solid structures whose behaviour *may reasonably be assumed to be 2-dimensional*.

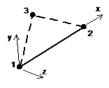
- 2D continuum elements may be applied to plane stress, plane strain and axisymmetric solid problems.
- Triangular and quadrilateral elements are available.
- Fourier elements, which allow non-axisymmetric loading to be applied to axisymmetric models, are considered a special case of the 2D continuum elements since the mesh is defined entirely in the xy-plane, but the resulting displacements, strains and stresses are fully three-dimensional.
- Special crack tip elements are available to model the singularities encountered at crack opening
- Explicit elements are available to model high speed dynamics problems efficiently.

3D Continuum Elements

3D continuum elements are used to model *fully3-dimensional structures*.

• Tetrahedral, pentahedral and hexahedral solid elements are available to model full 3-dimensional stress fields.









- Composites elements are available to model laminates.
- Special crack tip elements are available to model the singularities encountered at crack opening

Plate Elements

Plate elements are used to model flat structures whose deformation can be assumed to be predominantly flexural

- LUSAS incorporates both thin and thick plate elements.
- Triangular and quadrilateral flexural plate elements are available.

Shell Elements

Shell elements are used to model 3-dimensional structures whose behaviour is dependent upon both *flexural and membrane effects*.

- LUSAS incorporates both flat and curved shell elements.
- Triangular and quadrilateral elements are available
- Both thin and thick shell elements are available.

Membrane Elements

Membrane elements are used to model 2 and 3-dimensional structures whose behaviour is dominated by in-plane membrane effects.

- LUSAS incorporates both axisymmetric and space (3dimensional) membrane elements.
- Membrane elements incorporate *in-plane (membrane) behaviour only* (they include no bending behaviour).

Joint Elements

Joint elements are used to model *flexible joints* between other LUSAS elements.

- LUSAS incorporates a variety of joint elements which are designed to match the nodal freedoms of their associated elements.
- Joint elements may also be used to model point masses, elastoplastic hinges, or smooth and frictional element contacts.

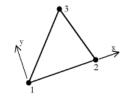
Non-Structural Mass Elements

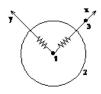
Non-Structural Mass elements are used to model translational *mass* at a point, along an edge or on a surface.

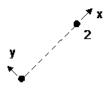
• Non-Structural Mass elements must be used with other structural











elements.

Thermal / Field Elements

Thermal / Field elements are used to model quasi-harmonic equation problems such as *thermal conduction* or potential distribution.

- LUSAS incorporates bar, plane, axisymmetric solid and 3dimensional solid field elements.
- Thermal link elements are also available.

Hygro-Thermal Elements

Hygro-thermal elements are used in *hygro-thermal* transient analyses, i.e. to model heat and moisture flow in porous media. The elements are generally used for problems involving the heat of hydration of concrete, and are normally used in a hygro-thermal-structural coupled analysis.

- LUSAS incorporates plane, axisymmetric solid and 3dimensional solid hygro-thermal elements
- Thermal link elements can also be used in a hygro-thermal analysis.

Interface Elements

Mohr-Coulomb interface elements are used to model the *contact behaviour* between two bodies.

Delamination interface elements model *delamination* and *crack propagation* in composites. They are positioned at places of potential delamination between continuum elements

Rigid Elements

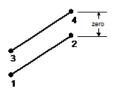
Rigid elements are used to define the shape of a rigid surface which is not part of the analysis model.

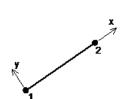
Phreatic Surface Elements

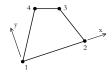
Phreatic surface elements are used to define the shape of a phreatic surface. They may be used with 2D and 3D continuum and two-phase elements.











Element Groups

The LUSAS Element Library is arranged into the following element groups:

- **Bars**
- Beams
- **D** 2D Continuum elements
- **3D** Continuum elements
- **Plates**
- **Shells**
- **Membranes**
- **Joints**
- Non-structural mass elements
- **Thermal/Field elements**
- Hygro-thermal elements
- □ Interface elements
- <u>Rigid elements</u>
- <u>Phreatic surface elements</u>

Element Sub-Groups

Each element group is also sub-divided into element sub-groups according to the type of element formulation as shown in the following <u>table</u>. For example, the **Beam** element group contains the element sub-groups: Engineering beams, Thick beams, Kirchhoff beams and Semiloof beams.

Within each sub-group elements vary according to the geometry, the number of nodes, and the properties required by each element. The individual elements are referred to by their LUSAS name, for example: BMI21 or QTS4.

Note

The dimensional classification of LUSAS elements is on the basis of the number of dimensions required for input of the nodal coordinates. For example, an engineering grillage element, (GRIL) requires X, Y coordinates and is hence classed as being 2-dimensional (despite having an out of plane displacement freedom).

Element Types and Availability

Element Group	Element Subgroup	Element Name and Software Product Version Availability			
			Standard (S)	Plus (+)	
Bars	Structural bars	<u>BAR2</u> , <u>BRS2</u>	<u>BAR3, BRS3</u>		
<u>Beams</u>	Engineering beams	<u>GRIL</u>			
	Plain strain beams		<u>BMI2N, BMI3N</u>		
	Thick beams	<u>BMI2,</u> <u>BMI21</u>		<u>BMI3, BMI2X,</u> <u>BMI3X, BMI22,</u> <u>BMI31, BMI33,</u> <u>BMX21, BMX22,</u> <u>BMX31, BMX33</u>	
	Thick cross- section beams			<u>BMI3, BMI2X,</u> <u>BMI3X, BMI22,</u> <u>BMI31, BMI33,</u> <u>BMX21, BMX22,</u> <u>BMX31, BMX33</u>	
	Warping beams			BMI21W, BMI22W, BMI31W, BMI33W, BMX21W, BMX22W, BMX31W, BMX33W	
	Thin (Kirchhoff) beams		<u>BM3, BMX3</u>	<u>BS3, BS4, BSX4</u>	
	Semiloof beams			<u>BSL3, BSL4, BXL4</u>	
2D Continuum	Plane stress continuum		<u>TPM3, TPM6,</u> <u>QPM4, QPM8,</u> <u>QPM4M, TPK6,</u> <u>QPK8</u>	<u>TPM3E, OPM4E</u>	
	Plane strain continuum		TPN3, TPN6, OPN4, OPN8, OPN4M,	<u>TPN3E, OPN4E</u>	

Element Group	Element Subgroup	Elemer	Product Version	
		LT	Standard (S)	Plus (+)
			<u>QPN4L</u> , <u>TNK6</u> , <u>QNK8</u>	
	Plain strain two phase		<u>TPN6P</u> , <u>QPN8P</u>	
	Axisymmetric solid continuum		<u>TAX3, TAX6, QAX4,</u> <u>QAX8, QAX4M,</u> <u>QAX4L, TXK6,</u> <u>QXK8, TAX3F,</u> <u>TAX6F, QAX4F,</u> <u>QAX8F</u>	<u>TAX3E, QAX4E</u>
	Axisymmetric solid two-phase			TAX6P, QAX8P
	Fourier ring			<u>TAX3F, TAX6F, QAX4F, QAX4F, QAX8F</u>
<u>3D Continuum</u>	Solid continuum		<u>TH4, PN6, HX8,</u> <u>HX8M</u>	<u>TH10, PN12, PN15,</u> <u>HX16, HX20,</u> <u>TH108, PN6L</u> <u>PN12L, HX8L,</u> <u>HX16L, TH4E,</u> <u>PN6E, HX8E</u>
	Solid continuum crack tip			<u>TH10K, PN15K,</u> <u>HX20K</u>
	Solid continuum two phase			<u>TH10P, PN12P,</u> <u>PN15P, HX16P,</u> <u>HX20P</u>
<u>Plates</u>	Isoflex plates		<u>TF3, QF4, QSC4</u>	
	Mindlin plates		<u>TTF6, QTF8</u>	
<u>Shells</u>	Axisymmetric thin shells		BXS3	
	Axisymmetric thick shells		<u>BXSI2, BXSI3</u>	
	Flat thin shells		<u>TS3, QSI4</u>	<u>TSR6</u> ,

Element Group	Subgroup				Element Name and Software Product Version Availability		
		LT	Standard (S)	Plus (+)			
	Semiloof shells			<u>TSL6, QSL8</u>			
	Thick shells		<u>TTS3, OTS4</u>	<u>TTS6, QTS8</u>			
<u>Membranes</u>	Axisymmetric membranes		<u>BXM2, BXM3</u>				
	Space membranes		<u>TSM3</u> , <u>SMI4</u>				
<u>Joints</u>	2D joints		JNT3, JPH3, JF3, JAX3, JXS3				
	3D joints		<u>JNT4, JL43, JSH4, JL46</u>	JSL4			
<u>Field</u>	Thermal bars		BFD2, BFD3, BFX2, BFX3, BFS2, BFS3				
	Thermal links		<u>LFD2, LFX2, LFS2</u>				
	Plane field		TFD3, TFD6, QFD4, QFD8				
	Axisymmetric field		TXF3, TXF6, QXF4, QXF8				
	Solid field		<u>TF4, TF10, PF6,</u> <u>PF12, PF15, HF8</u>	<u>HF16, HF20, PF6C, PF12C, HF8C, HF16C, TF10S</u>			
<u>Hygro-Thermal</u>	Plane hygro- thermal			<u>THT3, THT6,</u> <u>QHT4</u> , <u>QHT8</u>			
	Axisymmetric hygro-thermal			<u>TXHT3, TXHT6,</u> QXHT4, QXHT8			
	Solid hygro- thermal			<u>THT4, THT10,</u> <u>PHT6, PHT12,</u> <u>PHT15, HHT8,</u> <u>HHT16, HHT20</u>			
Interface	2D Interface			<u>IPN4, IPN6, IPM4, IPM6, IAX4, IAX6</u>			
	2D Two-phase interface			<u>IPN6P, IAX6P</u>			

Element Group	Element Subgroup	Element Name and Software Product Version Availability		
		LT	Standard (S)	Plus (+)
	3D Interface			<u>IS6, IS8, IS12, IS16</u>
	3D Two-phase interface			<u>IS12P, IS16P</u>
<u>Mass</u>	Point Mass			<u>PM2</u> , <u>PM3</u>
	Line Mass			<u>LM2, LM3, LM83, LM83, LM84</u>
	Surface Mass			<u>TM3, TM6, QM4, QM8</u>
Rigid Surface	2D Rigid			<u>R2D2</u>
	3D Rigid			<u>R3D3</u> , <u>R3D4</u>
<u>Phreatic</u> Surface	2D		<u>PHS2</u>	
	3D		<u>PHS3, PHS4</u>	

For details of the compatibility of joint elements with other elements see Appendix L : <u>Joint</u> <u>Element Compatibility</u>

Element Index

The following element index tables provide a diagrammatic index for each element with a description of the element, the nodal freedoms, and the software product version in which it is available.

The tables are listed in the following order:

- **Bar elements**
- Beam elements
- **<u>D</u> <u>2D</u>** Continuum elements
- **<u>3D Continuum elements</u>**
- Plate elements
- □ <u>Shell elements</u>
- Membrane elements
- **Joint elements**
- **Thermal / Field elements**
- Hygro-Thermal elements
- □ Interface elements
- Non-Structural Mass elements
- □ <u>Rigid elements</u>
- <u>Phreatic elements</u>

Bar Elements

Name	Geometry	Title	Freedoms	Product Version
BAR2	2	BAR element in 2D	U, V	LT
BAR3	2 3	BAR element in 2D	U, V	Standard

<u>BRS2</u>	• 2 1	BAR element in 3D	U, V, W	LT
BRS3	2 3	BAR element in 3D	U, V, W	Standard

Beam Elements

Name	Geometry	Title	Freedoms	Product Version
<u>GRIL</u>	x 2 1	ENGINEERING grillage thick beam element in 2D	W, qx, qy	LT
BMI2	y 1 1	THICK beam element in 2D (co-rotational)	U, V, qz	LT
BMI3	y 2 3	THICK beam element in 2D (co-rotational)	U, V, qz	Plus
BMI2X	у 1 1	THICK beam element in 2D with quadrilateral cross-section (co-rotational)	U, V, qz	Plus
<u>BMI3X</u>	y 3 3	THICK beam element in 2D with quadrilateral cross-section (co-rotational)	U, V, qz	Plus

<u>BMI21</u>	y y y 3 y y 1 1 z z 2	THICK linear thick beam element in 3D	U, V, W, qx, qy, qz	LT
BMI21W	y 1 3 2 y 1 x 2 1 2	THICK linear thick beam element with torsional warping in 3D	U, V, W, qx, qy, qz, α	Plus
<u>BMX21</u>	y 3 y 1 1 x 1 z	THICK linear thick beam element in 3D with quadrilateral cross-section		Standard
BMX21W	y 3 y 1 1 z	THICK linear thick beam element with torsional warping in 3D with quadrilateral cross- section	U, V, W, qx, qy, qz, α	Plus
<u>BMI31</u>	y y 1 z y y y z z z z z z z z z z	THICK quadratic thick beam element in 3D	U, V, W, qx, qy, qz	Plus
BMI31W	y y 1 z z z z z z z z z z z z z z z z z	THICK quadratic thick beam element with torsional warping in 3D	U, V, W, qx, qy, qz, α	Plus

<u>BMX31</u>	y y y y y y y y y y	THICK quadratic thick beam element in 3D with quadrilateral cross-section	U, V, W, qx, qy, qz	Plus
BMX31W	y y 1 z z z z z z z z z z z z z z z z z	THICK quadratic thick beam element with torsional warping in 3D with quadrilateral cross- section	U, V, W, qx, qy, qz, α	Plus
<u>BMI22</u>	y 1 4 y 2 y y 1 4 y 1 4	THICK twisted linear thick beam element in 3D	U, V, W, qx, qy, qz	Plus
BMI22W	y 1 3 y 1 x 1 z	THICK twisted linear thick beam element with torsional warping in 3D	U, V, W, qx, qy, qz, α	Plus
BMX22	y y y y y y y y y y y y y y y y y y y	THICK twisted linear thick beam element in 3D with quadrilateral cross-section	U, V, W, qx, qy, qz	Plus
BMX22W	y y y y y y y y y y y y y y y y y y y	THICK twisted linear thick beam element with torsional warping in 3D with quadrilateral cross-section	U, V, W, qx, qy, qz, α	Plus

<u>BMI33</u>	y 4 y 1 1 z y 6 x 3 z z y 6 x z y 6 x z y 1 y 2 y 1 z 3 z z y 1 z z y 1 z z y 1 z z y 1 z z y 1 z z z z y 1 z z z z	THICK twisted quadratic thick beam element in 3D	U, V, W, qx, qy, qz	Plus
BMI33W	y 1 z y 6 z 3 z z y 6 z	THICK twisted quadratic thick beam element with torsional warping in 3D	U, V, W, qx, qy, qz, α	Plus
<u>BMX33</u>	y + y + z = y + y + y + y + y + y + y + y + y + y	THICK twisted quadratic beam element in 3D with quadrilateral cross-section	U, V, W, qx, qy, qz	Plus
BMX33W	$y + \frac{4}{1 + 2} + \frac{4}{2} + \frac{1}{2} + \frac{4}{2} + \frac{1}{2} + \frac{4}{2} + \frac{1}{2} + \frac{1}{2$	THICK twisted quadratic beam element with torsional warping in 3D with quadrilateral cross- section	U, V, W, qx, qy, qz, α	Plus
<u>BM3</u>	3	KIRCHHOFF thin beam element in 2D	end nodes: U, V, qz mid-node: dU	Standard
BMX3	y 3 2 1	KIRCHHOFF thin beam element in 2D with quadrilateral cross-section	end nodes: U, V, qz mid-node: dU	Standard
<u>BS3</u>	2 1	KIRCHHOFF thin beam element in 3D	end nodes: U, V, W, qx, qy, qz mid-node: dU, dqx	Plus

<u>BS4</u>	y 1 x 2 1 z z z 3	KIRCHHOFF thin beam element in 3D	end nodes: U, V, W, qx, qy, qz mid-node: dU, dqx	Plus
<u>BSX4</u>	y y 1 2 3 3 3	KIRCHHOFF thin beam element in 3D with quadrilateral cross-section	end nodes:	Plus
BSL3	y 1 x 2 1 z z 3	SEMILOOF thin beam element in 3D for use with TSL6	end nodes: U, V, W, qx, qy, qz mid-node: U, V, W, q1, q2	Plus
BSL4		SEMILOOF thin beam element in 3D for use with QSL8	end nodes: U, V, W, qx, qy, qz mid-node: U, V, W, q1, q2	Plus
BXL4	y y 1 y 1 y 3 x 3 x 3 x 3 x 3 x 3 x 3 x 1 1 1 1 2 1 1 1 2 1 1 1 1 2 1 1 1 1 1 1 1 1 2 1 1 1 1 1 1 1 1 1 1	SEMILOOF thin beam element in 3D with quadrilateral cross- section	end nodes: U, V, W, qx, qy, qz mid-node: U, V, W, q1, q2	Plus
<u>BMI2N</u>	$ \begin{array}{c} $	Plane strain beam (co-rotational)	U, V, qz,	Standard
<u>BMI3N</u>	1 2 3 4 y	Plane strain beam (co-rotational)	U, V, qz,	Standard

2D Co	2D Continuum Elements					
Name	Geometry	Title	Freedoms	Product Version		

<u>TPM3</u>		PLANE STRESS continuum element in 2D	U, V	Standard
TPM6	5 1 2 3	PLANE STRESS continuum element in 2D	U, V	Standard
<u>OPM4</u>		PLANE STRESS continuum element in 2D	U, V	Standard
<u> QPM8</u>		PLANE STRESS continuum element in 2D	U, V	Standard
<u>QPM4M</u>		PLANE STRESS continuum element in 2D with enhanced strains	U, V	Standard
<u>TPK6</u>	5 1 6 2 3	PLANE STRESS continuum crack tip element in 2D	U, V	Standard
<u>OPK8</u>		PLANE STRESS continuum crack tip element in 2D	U, V	Standard
TPM3E	2	PLANE STRESS explicit dynamics element in 2D	U, V	Plus
<u>QPM4E</u>		PLANE STRESS explicit dynamics element in 2D	U, V	Plus
TPN3	3	PLANE STRAIN continuum element in 2D	U, V	Standard

<u>TPN6</u>	6 1 2 3	PLANE STRAIN continuum element in 2D	U, V	Standard
<u>OPN4</u>		PLANE STRAIN continuum element in 2D	U, V	Standard
<u>OPN8</u>		PLANE STRAIN continuum element in 2D	U, V	Standard
<u>OPN4M</u>	4 3 2	PLANE STRAIN continuum element in 2D with enhanced strains	U, V	Standard
<u>QPN4L</u>		PLANE STRAIN continuum element in 2D for large strains	U, V	Standard
<u>TNK6</u>	5 6 2 3	PLANE STRAIN continuum crack tip element in 2D	U, V	Standard
<u>ONK8</u>		PLANE STRAIN continuum crack tip element in 2D	U, V	Standard
TPN3E	2	PLANE STRAIN explicit dynamics element in 2D	U, V	Plus
<u>QPN4E</u>		PLANE STRAIN explicit dynamics element in 2D	U, V	Plus
TPN6P	6 1 2 3	PLANE STRAIN continuum two phase element in 2D	U, V P: corner nodes U, V: Midside nodes	Standard

<u>OPN8P</u>		PLANE STRAIN continuum two phase element in 2D	U, V P: corner nodes U, V: Midside nodes	Standard
<u>TAX3</u>	3	AXISYMMETRIC solid continuum element in 2D	U, V	Standard
<u>TAX6</u>	6 6 1 2 3	AXISYMMETRIC solid continuum element in 2D	U, V	Standard
<u>OAX4</u>	4 3	AXISYMMETRIC solid continuum element in 2D	U, V	Standard
<u>QAX8</u>		AXISYMMETRIC solid continuum element in 2D	U, V	Standard
<u>OAX4M</u>		AXISYMMETRIC solid continuum element in 2D with enhanced strains	U, V	Standard
<u>QAX4L</u>		AXISYMMETRIC solid continuum element in 2D for large strains	U, V	Standard
<u>TXK6</u>	5 1 2 3	AXISYMMETRIC solid continuum crack tip element in 2D	U, V	Standard
<u>OXK8</u>		AXISYMMETRIC solid continuum crack tip element in 2D	U, V	Standard
TAX3E		AXISYMMETRIC solid explicit dynamics element in 2D	U, V	Plus

<u>OAX4E</u>		AXISYMMETRIC solid explicit dynamics element in 2D	U, V	Plus
TAX6P	6 6 4 4 2 3	AXISYMMETRIC solid two phase continuum element in 2D	U, V P: corner nodes U, V: Midside nodes	Plus
<u>QAX8P</u>		AXISYMMETRIC solid two phase continuum element in 2D	U, V P: corner nodes U, V: Midside nodes	Plus
TAX3F	3	AXISYMMETRIC Fourier ring element in 2D	U, V, W	Plus
TAX6F	6 1 2 3	AXISYMMETRIC Fourier ring element in 2D	U, V, W	Plus
QAX4F		AXISYMMETRIC Fourier ring element in 2D	U, V, W	Plus
<u>QAX8F</u>		AXISYMMETRIC Fourier ring element in 2D	U, V, W	Plus

3D Continuum Elements

Name	Geometry	Title	Freedo ms	Product Version
<u>TH4</u>	4	SOLID CONTINUUM element in 3D	U, V, W	Standard

<u>TH10</u>	10 7 8 6 4 5 3	SOLID CONTINUUM element in 3D	U, V, W	Plus
<u>PN6</u>	a 5	SOLID CONTINUUM element in 3D	U, V, W	Standard
<u>PN12</u>	7 12 10 10 10 10 10 10 10 10	SOLID CONTINUUM element in 3D	U, V, W	Plus
<u>PN15</u>	$10 \\ 11 \\ 11 \\ 12 \\ 11 \\ 12 \\ 12 \\ 12 \\ $	SOLID CONTINUUM element in 3D	U, V, W	Plus
<u>HX8</u>	5 6 44 3	SOLID CONTINUUM element in 3D	U, V, W	Standard
<u>HX16</u>	$\begin{array}{c} 16 \\ 9 \\ 10 \\ 11 \\ 12 \\ 18 \\ 7 \\ 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 3 \\ 4 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5$	SOLID CONTINUUM element in 3D	U, V, W	Plus
<u>HX20</u>	$\begin{array}{c} 20 \\ 13 \\ 14 \\ 15 \\ 16 \\ 12 \\ 10 \\ 1 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 1 \\ 4 \\ 5 \\ 1 \\ 1 \\ 2 \\ 3 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1$	SOLID CONTINUUM element in 3D	U, V, W	Plus
HX8M	5 0 44 3	SOLID CONTINUUM element in 3D with enhanced strains	U, V, W	Standard
<u>TH108</u>	10 7 8 6 4 5 3	SOLID CONTINUUM composite element in 3D	U, V, W	Plus
PN6L		SOLID CONTINUUM composite element in 3D	<u>U, V, W</u>	Plus

<u>PN12L</u>	7 12 10 10 10 10 10 10 10 10	SOLID CONTINUUM composite element in 3D	U, V, W	Plus
HX8L	5 0 44 3	SOLID CONTINUUM composite element in 3D	U, V, W	Plus
<u>HX16L</u>	$\begin{array}{c} 16 \\ 9 \\ 10 \\ 11 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12 \\ 3 \\ 4 \\ 5 \\ 3 \\ 3 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5$	SOLID CONTINUUM composite element in 3D	U, V, W	Plus
<u>TH10K</u>	10 7 8 6 4 5 3	SOLID CONTINUUM crack tip element in 3D	U, V, W	Plus
<u>PN15K</u>	$10 \\ 11 \\ 12 \\ 7 \\ 1 \\ 2 \\ 3 \\ 3 \\ 3 \\ 4 \\ 4 \\ 3 \\ 3 \\ 1 \\ 2 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3$	SOLID CONTINUUM crack tip element in 3D	U, V, W	Plus
<u>HX20K</u>	$\begin{array}{c} 20 \\ 13 \\ 14 \\ 15 \\ 16 \\ 16 \\ 17 \\ 6 \\ 12 \\ 3 \\ 10 \\ 4 \\ 5 \\ 10 \\ 4 \\ 5 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 $	SOLID CONTINUUM crack tip element in 3D	U, V, W	Plus
<u>TH4E</u>	1 2	SOLID CONTINUUM explicit dynamics element in 3D	U, V, W	Plus
PN6E	4	SOLID CONTINUUM explicit dynamics element in 3D	U, V, W	Plus
HX8E	5 6 44 5	SOLID CONTINUUM explicit dynamics element in 3D	U, V, W	Plus
<u>TH10P</u>	10 7 8 6 4 3	SOLID CONTINUUM two phase element in 3D	U, V, W	Plus

<u>PN12P</u>		SOLID CONTINUUM two phase element in 3D	U, V, W	Plus
<u>PN15P</u>	$15 \\ 10 \\ 11 \\ 12 \\ 6 \\ 1 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 1 \\ 1 \\ 2 \\ 3 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1$	SOLID CONTINUUM two phase element in 3D	U, V, W	Plus
<u>HX16P</u>	$\begin{array}{c} 16 \\ 9 \\ 10 \\ 11 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12$	SOLID CONTINUUM two phase element in 3D	U, V, W	Plus
<u>HX20P</u>	$\begin{array}{c} 20 \\ 13 \\ 14 \\ 15 \\ 16 \\ 12 \\ 10 \\ 4 \\ 3 \\ 1 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1$	SOLID CONTINUUM two phase element in 3D	U, V, W	Plus

Plate Elements

Name	Geometry	Title	Freedoms	Product Version
<u>TF3</u>		ISOFLEX thin plate flexure element in 2D	W, qx, qy	Standard
QF4		ISOFLEX thin plate flexure element in 2D	W, qx, qy	Standard
<u>QSC4</u>		ISOFLEX thick plate flexure element in 2D	W, qx, qy	Standard
TTF6	6 6 1 2 3	MINDLIN thick plate flexure element in 2D	W, qx, qy	Standard
QTF8		MINDLIN thick plate flexure element in 2D	W, qx, qy	Standard

Shell Element	ts
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Name	Geometry	Title	Freedoms	Product Version
BXS3		AXISYMMETRIC thin shell element in 2D	end nodes: U, V, qz	Standard
BXSI2		AXISYMMETRIC thick shell element in 2D	end nodes: U, V, qz	Standard
<u>BXSI3</u>	2 2 3 4 4	AXISYMMETRIC thick shell element in 2D	end nodes: U, V, qz mid-node: dU	Standard
<u>TS3</u>		FLAT thin shell element in 3D	U, V, W, qx, qy, qz	Standard
<u>OSI4</u>	x 1 2	FLAT thin shell element in 3D	U, V, W, qx, qy, qz	Standard
<u>TSR6</u>	x 1 2 3	FLAT thin nonlinear shell element in 3D	corner nodes: U, V, W mid-side nodes: q1	Plus
<u>TSL6</u>	6 1 2 3	SEMILOOF curved thin shell element in 3D	corner nodes: U, V, W mid-side nodes: U, V, W, q1, q2	Plus
QSL8		SEMILOOF curved thin shell element in 3D	corner nodes: U, V, W mid-side nodes: U, V, W, q1, q2	Plus

<u>TTS3</u>	THICK SHELL flat element in 3D	U, V, W, qa, qbor U, V, W, qx, qy, qz	Standard
<u>TTS6</u>	THICK SHELL curved element in 3D	U, V, W, qa, qbor U, V, W, qx, qy, qz	Plus
<u>QTS4</u>	THICK SHELL flat element in 3D	U, V, W, qa, qbor U, V, W, qx, qy, qz	Standard
<u>QTS8</u>	THICK SHELL curved element in 3D	U, V, W, qa, qbor U, V, W, qx, qy, qz	Plus

Membrane Elements

Name	Geometry	Title	Freedom s	Product Version
BXM2	2	AXISYMMETRIC membrane element in 2D	U, V	Standard
BXM3	3	AXISYMMETRIC membrane element in 2D	U, V	Standard
TSM3		SPACE membrane element in 3D	U, V, W	Standard
<u>SMI4</u>	x y 1 2 x	SPACE membrane element in 3D	U, V, W	Standard

Joint Elements

Name	Geometry	Title	Freedoms	Product

		I		Version
JNT3	y the with a	JOINT ELEMENT in 2D for bars, plane stress and plane strain	U, V	Standard
JPH3	y the num 3	JOINT ELEMENT in 2D for engineering and Kirchhoff beams	U, V, qz	Standard
JF3	y y y y y y y y y y y y y y y y y y y	JOINT ELEMENT in 2D for grillage beams and plates	W, qx, qy	Standard
JAX3	y the with a	JOINT ELEMENT in 2D for axisymmetric solids	U, V	Standard
JXS3	y the unit of the second secon	JOINT ELEMENT in 2D for axisymmetric shells	U, V, qz	Standard
JNT4	the num	JOINT ELEMENT in 3D for bars, solids and space membranes	U, V, W	Standard
<u>JL43</u>	Mar Hull	JOINT ELEMENT in 3D for corner nodes of semiloof elements	U, V, W	Standard
<u>JSH4</u> <u>JL46</u>	y the second sec	JOINT ELEMENT in 3D for engineering and Kirchhoff beams and the end/corner nodes of semiloof elements	U, V, W, qx, qy, qz	Standard
JSL4	the mark a	JOINT ELEMENT in 3D for mid-side nodes of semiloof elements	U, V, W, q1, q2	Plus

Name	Geometry	Title	Freedoms	Product Version
BFD2	2	THERMAL BAR element in 2D	F	Standard
<u>3FD3</u>	3	THERMAL BAR element in 2D	F	Standard
BFX2	1 2	Axisymmetric THERMAL MEMBRANE element in 2D	F	Standard
BFX3	3	Axisymmetric THERMAL MEMBRANE element in 2D	F	Standard
BFS2	2	THERMAL BAR element in 3D	F	Standard
BFS3	3	THERMAL BAR element in 3D	F	Standard
LFD2	•	THERMAL LINK element in 2D	F	Standard
LFX2	• ····································	Axisymmetric THERMAL LINK element in 2D	F	Standard
LFS2	••.•.•• 2	THERMAL LINK element in 3D	F	Standard
TFD3		PLANE FIELD element in 2D	F	Standard
<u>TFD6</u>	6 4	PLANE FIELD element in 2D	F	Standard

QFD4	4 • • 3	PLANE FIELD element in 2D	F	Standard
	2			
QFD8	7.	PLANE FIELD element in 2D	F	Standard
<u>TF4</u>	1 2	SOLID FIELD element in 3D	F	Standard
<u>TF10</u>	10 7 8 6 4 5	SOLID FIELD element in 3D	F	Plus
<u>PF6</u>	4 5	SOLID FIELD element in 3D	F	Standard
<u>PF12</u>	7 12 10 11 10 10 10 10 10 10	SOLID FIELD element in 3D	F	Plus
<u>PF15</u>	$10 \\ 11 \\ 12 \\ 11 \\ 12 \\ 12 \\ 12 \\ 12 \\ $	SOLID FIELD element in 3D	F	Plus
<u>HF8</u>	5 0 1 2 2	SOLID FIELD element in 3D	F	Standard
<u>HF16</u>	$\begin{array}{c} 16 & 15 \\ 14 & 13 \\ 9 & 10 & 11 \\ 18 & 7 & 6 \\ 1 & 2 & 4 \\ 3 & 4 & 5 \end{array}$	SOLID FIELD element in 3D	F	Plus
<u>HF20</u>	$\begin{array}{c} 20 \\ 13 \\ 14 \\ 15 \\ 12 \\ 10 \\ 1 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 1 \\ 1 \\ 2 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1$	SOLID FIELD element in 3D	F	Plus

<u>TF10S</u>	10 7 8 6 5 1 2 4	SOLID FIELD composite element in 3D	F	Plus
<u>PF6C</u>	4 1 1 1 1 1 3	SOLID FIELD composite element in 3D	F	Plus
<u>PF12C</u>		SOLID FIELD composite element in 3D	F	Plus
HF8C	5	SOLID FIELD composite element in 3D	F	Plus
<u>HF16C</u>	$\begin{array}{c} 16 \\ 9 \\ 10 \\ 11 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12 \\ 3 \\ 3 \\ 4 \\ 5 \\ 5 \\ 3 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5$	SOLID FIELD composite element in 3D	F	Plus
<u>TXF3</u>		AXISYMMETRIC FIELD element in 2D	F	Standard
<u>TXF6</u>	5 6 1 2 3	AXISYMMETRIC FIELD element in 2D	F	Standard
<u>QXF4</u>		AXISYMMETRIC FIELD element in 2D	F	Standard
<u>QXF8</u>		AXISYMMETRIC FIELD element in 2D	F	Standard

Hygro	o-Thermal	Elements		
Name	Geometry	Title	Freedo	Product
	-		ms	Version

<u>THT3</u>	3	PLANE HYGRO-THERMAL element in 2D	T, Pc	Plus
<u>THT6</u>	6 4 3 1 2 3	PLANE HYGRO-THERMAL element in 2D	T, Pc	Plus
<u>QHT4</u>		PLANE HYGRO-THERMAL element in 2D	T, Pc	Plus
<u>OHT8</u>		PLANE HYGRO-THERMAL element in 2D	T, Pc	Plus
<u>TXHT3</u>	3	AXISYMMETRIC HYGRO-THERMAL element in 2D	T, Pc	Plus
<u>TXHT6</u>	6 1 2 3	AXISYMMETRIC HYGRO-THERMAL element in 2D	T, Pc	Plus
<u>QXHT4</u>	4 3 2	AXISYMMETRIC HYGRO-THERMAL element in 2D	T, Pc	Plus
<u>OXHT8</u>		AXISYMMETRIC HYGRO-THERMAL element in 2D		Plus
<u>THT4</u>	1 2	3D	T, Pc	Plus
<u>THT10</u>	10 7 8 6 4 5 3	SOLID HYGRO-THERMAL element in 3D	T, Pc	Plus

<u>PHT6</u>	4 1 1 2	SOLID HYGRO-THERMAL element in 3D	T, Pc	Plus
<u>PHT12</u>	7 12 10 11 10 10 10 10 10 10	SOLID HYGRO-THERMAL element in 3D	T, Pc	Plus
<u>PHT15</u>	$\begin{array}{c} 15 \\ 10 \\ 11 \\ 12 \\ 7 \\ 1 \\ 2 \\ 3 \\ 3 \\ 3 \\ 4 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3$	SOLID HYGRO-THERMAL element in 3D	T, Pc	Plus
<u>HHT8</u>	5 0 44 3	SOLID HYGRO-THERMAL element in 3D	T, Pc	Plus
<u>HHT16</u>	$\begin{array}{c} 15 \\ 9 \\ 10 \\ 1 \\ 2 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 5 \\ 5 \\ 5 \\ 5$	SOLID HYGRO-THERMAL element in 3D	T, Pc	Plus
<u>HHT20</u>	$\begin{array}{c} 20 \\ 13 \\ 14 \\ 15 \\ 12 \\ 10 \\ 12 \\ 3 \\ 10 \\ 4 \\ 3 \\ 3 \\ 10 \\ 4 \\ 5 \\ 10 \\ 4 \\ 5 \\ 10 \\ 4 \\ 5 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 $	SOLID HYGRO-THERMAL element in 3D	T, Pc	Plus

Interface Elements

Name	Geometry	Title	Freedoms	Product Version
IPN4	4 2 3 1	PLANE STRAIN INTERFACE ELEMENT in 2D (Initial gap allowed for Mohr-Coulomb variant)	U, V	Plus
IPM4		PLANE STRESS INTERFACE ELEMENT in 2D (Initial gap allowed for Mohr-Coulomb variant)	U, V	Plus

IAX4		AXISYMMETRIC INTERFACE ELEMENT in 2D (Initial gap allowed for Mohr-Coulomb variant)	U, V	Plus
IPN6	5 3 4 2 1	PLANE STRAIN INTERFACE ELEMENT in 2D (Initial gap allowed for Mohr-Coulomb variant)	U, V, P corner nodes; U,V midside nodes	Plus
IPM6		PLANE STRESS INTERFACE ELEMENT in 2D (Initial gap allowed for Mohr-Coulomb variant)	U, V, P corner nodes; U,V midside nodes	Plus
IAX6		AXISYMMETRIC INTERFACE ELEMENT in 2D (Initial gap allowed for Mohr-Coulomb variant)	U, V	Plus
IPN6P		PLANE STRAIN TWO PHASE INTERFACE ELEMENT in 2D (Initial gap allowed for Mohr- Coulomb variant)	U, V	Plus
IAX6P		AXISYMMETRIC TWO PHASE INTERFACE ELEMENT in 2D (Initial gap allowed for Mohr- Coulomb variant)	U, V	Plus
<u>186</u>		INTERFACE ELEMENT in 3D (Initial gap allowed for Mohr- Coulomb variant)	U, V, W	Plus
<u>158</u>		INTERFACE ELEMENT in 3D (Initial gap allowed for Mohr- Coulomb variant)	U, V, W	Plus
<u>IS12</u>	7 - 6 = 8 - 4 - 9 - 2 = 7 -	INTERFACE ELEMENT in 3D (Initial gap allowed for Mohr- Coulomb variant)	U, V, W	Plus

<u>IS16</u>	$\begin{array}{c}15 & 14 & 13\\16 & 7 & & 6 & 12\\2 & & & & & \\0 & & & & & 10\\1 & & & & & & \\1 & & & & & & 3\end{array}$	INTERFACE ELEMENT in 3D (Initial gap allowed for Mohr- Coulomb variant)	U, V, W	Plus
<u>IS12P</u>	11 7 7 8 6 8 4 9 2 2 3 2 2 7 2 2 7 2 2 7 2 2 7 0	TWO PHASE INTERFACE ELEMENT in 3D	U, V, W, P corner nodes; U,V, W midside nodes	Plus
<u>IS16P</u>	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	TWO PHASE INTERFACE ELEMENT in 3D	U, V, W, P corner nodes; U,V, W midside nodes	Plus

Non-Structural Mass Elements

Name	Geometry	Title	Freedo ms	Product Version
<u>PM2</u>	y 2 2	NON-STRUCTURAL MASS ELEMENT in 2D to model mass at a point	U, V	Plus
<u>PM3</u>	2 * x 2 * 1 * y	NON-STRUCTURAL MASS ELEMENT in 3D to model mass at a point	U, V, W	Plus
LMS3	3 y y 1 z z	NON-STRUCTURAL MASS ELEMENT in 3D to model mass along an edge	U, V, W, qx, qy, qz	Plus
LMS4	y 4 y 1 x 2 1 y z	NON-STRUCTURAL MASS ELEMENT in 3D to model mass along an edge	U, V, W, qx, qy, qz	Plus
<u>LM2</u>	2	NON-STRUCTURAL MASS ELEMENT in 2D to model mass along an edge	U, V	Plus
<u>LM3</u>	2 3	NON-STRUCTURAL MASS ELEMENT in 2D to model mass along an edge	U, V	Plus

<u>TM3</u>		NON-STRUCTURAL MASS ELEMENT in 3D to model mass on a surface.	U,V,W	Plus
<u>TM6</u>	6 6 4 1 2 3	NON-STRUCTURAL MASS ELEMENT in 3D to model mass on a surface.	U,V,W	Plus
<u>QM4</u>		NON-STRUCTURAL MASS ELEMENT in 3D to model mass on a surface.	U,V,W	Plus
<u>QM8</u>		NON-STRUCTURAL MASS ELEMENT in 3D to model mass on a surface.	U,V,W	Plus

Rigid Slideline Elements

				-
Name	Geometry	Title	Freedo	Product
			ms	Version
<u>R2D2</u>	×	RIGID SLIDELINE SURFACE ELEMENT in	U, V	Plus
	¥ 2	2D for modelling non-deformable surfaces in a contact analysis		
<u>R3D3</u>		RIGID SLIDELINE SURFACE ELEMENT in 3D for modelling non-deformable surfaces in a contact analysis	U, V, W	Plus
<u>R3D4</u>	y 1 x x x	RIGID SLIDELINE SURFACE ELEMENT in 3D for modelling non-deformable surfaces in a contact analysis	U, V, W	Plus

Phreatic Elements

Name	Geometry	Title	Freedo ms	Product Version
PHS2	~	PHREATIC SURFACE ELEMENT in 2D for modelling phreatic surface.	U, V	Plus

PHS3	PHREATIC SURFACE ELEMENT in 3D for modelling phreatic surface.	U, V, W	Plus
PHS4	PHREATIC SURFACE ELEMENT in 3D for modelling phreatic surface.	U, V, W	Plus

Element Summary Tables

The following element summary tables list element facilities arranged by LUSAS element group:

- **Bar and Beam elements**
- **<u>D</u> <u>2D</u> Continuum elements**
- **3D** Continuum elements
- **Plate, Shell and Membrane elements**
- **Joint elements**
- **Thermal/Field elements**
- Hygro-Thermal elements
- □ Interface, Non-Structural Mass, Rigid, Interface and Phreatic elements

		Ba	rs			Γ	Γ			I	Beam	s	I	I		I		
Bar and Elemen	l Beam It Summary	<u>BAR2, BAR3</u>	BRS2, BRS3	<u>GRIL</u>	BMI21	<u>BMI2, BMI3</u>	BMI2N, BMI3N	<u>BMI2X, BMI3X</u>	<u>BMI22, BMI31, BMI33</u>	<u>BMI21W, BMI22W,</u> BMI31W, BMI33W	<u>BMX21, BMX22,</u> BMX31, BMX32	<u>BMX21W, BMX22W,</u> BMX31W, BMX33W	BM3	BMX3	BS3, BS4	BSX4	BSL3, BSL4	BXL4
Product version	LT, Standard (S) or Plus (+)	LT	LT	LT	LT	LT	s	+	+	+	+	+	s	s	+	+	+	+
Nodal freedoms	U, V	✓																
	U, V, W		\checkmark															
(mid-side)	U, V, qz					✓	✓	✓										
, ,	U, V, qz (dU)												✓	\checkmark				
	W, qx, qy			✓														
	U, V, W, qx, qy, qz (dU, dqx)														✓	~		
	U, V, W, qx, qy, qz (U, V, W,q1, q2)																~	~
	Ū, V, W, qx, qy																	
	U, V, W, qx, qy, qz				✓				✓		~	~						
Material properties	Linear (Isotropic)	✓	✓	✓	✓	✓	✓	✓	✓	~	~	~	✓	~	✓	✓	✓	✓
	Linear (Orthotropic)																	
	Linear (Anisotropic)																	
	Linear (Rigidities)				✓	✓			✓	✓			✓		✓	✓	✓	
	Matrix																	
	Joint																	
	Concrete Multi- crack							~			~	~						
	Stress Resultant				✓	✓			>	✓			✓		>		✓	
	Tresca	\checkmark	✓				✓	\checkmark			✓	✓		\checkmark		✓		\checkmark
	Drucker-Prager	✓	✓				✓	\checkmark			✓	\checkmark		✓		✓		\checkmark

	Mohr-Coulomb	✓	\checkmark				✓	\checkmark			✓	✓		\checkmark		✓		\checkmark
	Optimised Implicit	✓	✓				✓	✓			✓	✓		✓		✓		✓
	Von Mises																	
	Volumetric																	
	Crushing/Foam																	
	Stress	\checkmark	✓				✓	✓			✓	✓	✓	✓	✓	✓	✓	✓
	Potential(Von																	
	Mises, Modified																	
	Von Mises)																	
	Creep (General)	✓	\checkmark				✓	✓		-	✓	✓	✓	✓	✓	✓	✓	✓
	Creep (AASHTO)				✓	✓	✓	✓	✓	~	✓	✓	✓	✓	✓	✓	✓	✓
	Creep (CEB-FIP)				✓	✓	✓	✓	\checkmark	✓	✓	✓	✓	✓	✓	✓	✓	✓
	Creep (Chinese)				✓	✓	✓	✓	✓	~	✓	✓	✓	✓	✓	✓	✓	✓
	Creep (Eurocode)				✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	~	✓	✓	✓
	Creep (IRC)				✓	✓	✓	✓	✓	>	✓	✓	✓	✓	✓	✓	✓	<
	Damage (Simo, Oliver)	✓	✓				✓	√			1	1		✓		1		~
	Viscoelastic	✓																
	Shrinkage	✓			✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓
	(CEB-FIP_90,																	
	Eurocode_2,																	
	General, User)																	
	Rubber																	
	Generic Polymer																	
	Multi-linear	✓	✓															
	Composite																	
	Field																	
Loading types	Prescribed Value (PDSP,TPDSP)	✓	~	✓	✓	✓	✓	✓	✓	✓	1	~	✓	✓	✓	✓	✓	<
	Concentrated Loads (CL)	✓	✓	✓	✓	✓	~	✓	~	~	~	✓	~	✓	~	✓	✓	✓
	Element Load			\checkmark	\checkmark	\checkmark	✓	✓	✓	✓	✓	✓	✓	✓				\checkmark
	(ELDS)																	
	Distributed Load (UDL)			~	✓	•	~	~	~	✓	~	~	~	~	~	1	~	~
	Distributed Load																	
	(FLD)																	
	Body Force	✓	✓	✓	✓	✓	√	✓	✓	✓	1	~	√	✓	✓	1	✓	✓
	(CBF)																	
	Body Force (BFP,BFPE)	✓	✓	✓	✓	✓	✓	✓	✓	~	~	~	✓	~	✓	✓	~	~
	Velocity (VELO)	✓	✓	✓	✓	✓	✓	✓	✓	~	✓	✓	✓	✓	✓	✓	✓	\checkmark
	Acceleration (ACCE)	✓	✓	✓	✓	✓	✓	✓	✓	~	✓	✓	✓	✓	✓	✓	✓	✓

	Initial	✓	✓		✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓
	Stress/Strain																	
	(SSI,SSIE)																	
	Initial	✓	\checkmark		\checkmark	✓	✓	✓	\checkmark	✓	✓	✓	✓	✓	✓	✓	\checkmark	\checkmark
	Stress/Strain																	
	(SSIG)																	
	Residual Stress				✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓
	(SSR,SSRE)																	
	Residual Stress	\checkmark	\checkmark		\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	✓	✓	✓	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark
	(SSRG)																	
	Target	✓	✓		✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓
	Stress/Strain																	
	(TSSIE,TSSIA)																	
	Target	✓	\checkmark		✓	✓	✓	✓	\checkmark	✓	✓	✓	\checkmark	✓	✓	✓	✓	\checkmark
	Stress/Strain																	
	(TSSIG)																	
	Temperature	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓
	(TEMP,TMPE)																	
	Field Loads																	
	Temperature																	
	Dependent Loads																	
Nonlinear	Total Lagrangian	\checkmark	\checkmark	✓	✓	✓	✓	✓	✓	✓	✓	✓	\checkmark	✓	✓	✓	~	✓
geometry																		
	Updated							✓					\checkmark	✓	✓	✓		
	Lagrangian																	
	Eulerian																	
	Co-rotational	✓	✓	✓	✓	✓			\checkmark	~	✓	✓						
Integration	Explicitly			✓														
schemes	Integrated																	
	Numerically	✓	✓		✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓
	Integrated																	
Mass	Consistent Mass	✓	\checkmark	✓	✓	\checkmark	✓	✓	✓	✓	✓	✓	✓	✓	\checkmark	✓	✓	\checkmark
modelling	(default)																	
	Lumped Mass	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	\checkmark

									21) C	onti	nuu	m	1			•	
2D Continuı Summary	ım Element	TPM3/6, OPM4/8	<u>OPM4M</u>	TPK6, QPK8	TPM3E, QPM4E	TPN3/6, OPN4/8	<u>OPN4M</u>	OPN4L	TNK6, QNK8	TPN3E, QPN4E	TPN6P, QPN8P	TAX3/6, OAX4/8	<u>OAX4M</u>	<u>OAX4L</u>	TXK6, QXK8	TAX3E, QAX4E	TAX6P, QAX8P	<u>TAX3F/6F,</u> <u>OAX4F/8F</u>
Product Version	LT, Standard (S) or Plus (+)	s	s	s	+	s	s	s	s	+	+	s	S	s	s	+	+	+
Nodal freedoms	U, V	✓	✓	✓	✓	✓	✓	✓	✓	✓		✓	✓	✓	✓	✓		
	U, V, W																	✓
(corner)	U, V, (P)										✓						✓	
Material properties	Linear (Isotropic)	~	✓	✓	✓	✓	✓		~	✓	~	1	~		1	~	~	~
	Linear (Orthotropic)	•	✓	✓	✓	✓	✓		~	✓	~	✓	~		✓	✓	✓	~
	Linear (Anisotropic)	✓	~	~		✓	√ *		√ *		√ *	~	√ *		√ *		√ *	
	Linear (Rigidities)	\checkmark	✓	✓		✓	√ *		√ *		√ *						√ *	
	Matrix																	
	Joint																	
	Concrete Multi- crack	✓	✓	✓		✓	✓		✓		✓	✓	~		✓		~	
	Concrete Multi- crack(Transient)	1	✓	✓		~	✓					✓	~					
	Stress Resultant																	
	Tresca	✓	✓	✓	✓	✓	✓		✓	✓	✓	>	>		✓	>	~	
	Optimised Implicit Von Mises	✓	✓	✓	✓	✓	✓		✓	✓	~	~	~		~	~	~	
	Mohr-Coulomb	✓	✓	✓	✓	✓	✓		✓	✓	✓	✓	✓		✓	✓	✓	
	Modified Mohr-Coulomb					~	✓		~	✓	✓	✓	~		~	~	~	
	Drucker-Prager	✓	✓	✓	✓	✓	✓		✓	✓	✓	✓	✓		✓	✓	✓	
	Modified Cam-clay					~	✓		~		✓	✓	~		~		~	
	Volumetric Crushing/Foam					~	✓		~	✓	~	✓	~		✓	~	~	
	Stress Potential (Von Mises, Modified Von Mises)	✓	•	•	•	~	•		✓	~	•	✓	•		✓ 	~	•	

	Interface (2D)	✓		[[[[1			
	Creep (General)	✓	✓	✓		✓	✓		✓	✓	\checkmark	✓	✓		✓	✓	✓	
	Creep (AASHTO)	✓	✓	✓		✓	✓		✓			✓	✓		✓			
	Creep (CEB-FIP)	✓	✓	✓		\checkmark	✓		✓			✓	✓		\checkmark			
	Creep (Chinese)	✓	✓	✓		✓	✓		✓			✓	✓		 ✓ 			
	Creep (Eurocode)	✓	\checkmark	✓		\checkmark	✓		✓			\checkmark	✓		\checkmark			
	Creep (IRC)	✓	✓	✓		\checkmark	✓		✓			✓	✓		✓			
	Damage (Simo, Oliver)	~	✓	✓		~	✓		✓	✓	~	✓	~		~	~	~	
	Viscoelastic					\checkmark	✓			✓	✓	✓	✓		✓	✓	✓	
	Shrinkage (CEB- FIP, Eurocode. General, User)	✓		✓		✓	✓		✓		✓	~	✓	~	 ✓ 		✓	
	Ko Initialisation					✓	✓		✓			✓	✓		✓	✓	✓	
	Rubber (Ogden, Mooney-Rivlen, Neo-Hookean, Hencky)		~				~	~						~				
	Generic Polymer		✓	✓		✓	✓		✓		✓	✓	✓		\checkmark		✓	
	Composite																	
	Field																	
Loading types	Prescribed Value (PDSP,TPDSP)	✓	✓	~	✓	✓	~	✓	✓	~	~	✓	~	~	~	~	~	~
	Concentrated Loads (CL)	✓	✓	✓	✓	✓	✓	✓	✓	✓	~	✓	~	~	~	~	~	~
	Element Load																	
	Distributed Load (UDL)																	
	Distributed Load (FLD)	✓	✓	✓	✓	~	✓	✓	✓	✓	~	✓	~	~	~	~	~	~
	Body Force (CBF,BFP,BFPE)	~	~	~	~	~	~	✓	~	~	~	✓	~	~	~	~	~	~
	Velocity (VELO)	✓	✓		✓	\checkmark		✓	✓			✓	~	✓	✓	✓	\checkmark	\checkmark
	Acceleration (ACCE)	✓	✓	✓	✓	✓	✓	✓	✓	✓	~	✓	~	~	~	~	~	~
	Initial Stress/Strain (SSI,SSIE)	~	✓	✓	✓	~	✓	✓	✓	✓	✓	✓	~	✓	~	✓	~	~
	Initial Stress/Strain (SSIG)	✓	✓	~	✓	~	~	~	~	~	~	✓	~	1		~	~	~
	Residual Stress (SSR)	✓	✓	✓	✓	✓	~	✓	✓	✓	✓	✓	~	✓	✓	~	~	
	Residual Stress (SSRE,SSRG)	✓	✓	~	✓	~	✓	✓	✓	~	~	1	~	~	1	~	~	
	Target Stress/Strain	✓	✓	✓	✓	\checkmark	✓	✓	✓	✓	\checkmark	✓	✓	✓	✓	✓	✓	✓

	(TSSIE,TSSIA)																	
	Target Stress/Strain	\checkmark		\checkmark	\checkmark	✓												
	(TSSIG)																	
	Temperature	\checkmark	✓	\checkmark	\checkmark													
	(TEMP,TMPE)							-										
	, , ,																	
	Field Load																	
	Temp Dependent																	
	Load																	
	Overburden	✓	✓	✓		✓	✓	✓	✓		✓	✓	✓	✓	✓		✓	
	Phreatic Surface	\checkmark	✓	✓		✓	\checkmark	\checkmark			\checkmark	✓	✓	\checkmark	\checkmark		✓	
Nonlinear	Total Lagrangian	✓	✓	✓		✓	✓		✓		✓	✓	✓		✓		✓	
geometry																		
	Updated	\checkmark	✓	✓		\checkmark	✓		\checkmark		\checkmark	✓	✓		\checkmark		✓	
	Lagrangian																	
	Eulerian	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	
	Co-rotational	\checkmark	✓	✓		✓	\checkmark		\checkmark		\checkmark							
Integration	Explicitly																	
schemes	Integrated																	
	Numerically	\checkmark	✓	✓	\checkmark	✓	✓	\checkmark	\checkmark	✓	\checkmark	\checkmark						
	Integrated																	
Mass modelling	Consistent Mass	✓	✓	✓		✓	✓	✓	✓		✓	✓	✓	✓	✓		✓	\checkmark
8	(default)																	
	Lumped Mass	\checkmark	\checkmark	\checkmark	✓	\checkmark	✓	✓	\checkmark	\checkmark	\checkmark	\checkmark	✓	✓	✓	✓	✓	✓

* Linear anisotropic and rigidities material properties for elements marked are supported in LUSAS Solver but not supported in LUSAS Modeller.

							31) Con	tinuu	m				
3D Con Elemen	tinuum t Summary	<u>TH4</u>	<u>TH10</u>	PN6	PN12/15	HX8	<u>HX16/20</u>	HX8M	TH10K, PN15K, HX20K	TH10S	PN6L, PN12L	<u>HX8L, HX16L</u>	TH4E, PN6E, HX8E	<u>TH10P, PN12P, PN15P,</u> <u>HX16P, HX20P</u>
	LT, Standard (S)	S	+	s	+	s	+	S	+	+	+	+	+	+
Version	or Plus (+)		-											
Nodal	U, V													
freedoms		✓	✓	✓	✓	\checkmark	✓	✓	✓	✓	✓	✓	✓	
(00,000)	U, V, W U, V, W (P)	v	v	v	•	v	•	v	v	v	v	•	v	 ✓
(corner) Material	Linear (Isotropic)	✓	✓	✓	~	✓	✓	 ✓ 	~	✓	~	1	✓	•
properties			-				•		•	•		•		•
	Linear (Orthotropic)	✓	✓	✓	√	✓	√	 ✓ 	√	✓	✓	✓	✓	 ✓
	Linear (Anisotropic)	✓	✓	\checkmark	✓	✓	√	✓	✓	✓	✓	✓		✓
	Linear (Rigidities)													
	Matrix		-											
	Joint				,									
	Concrete (Multi-crack)	✓	✓	✓	✓	✓	√	✓	✓	✓	✓	✓		✓
	Concrete (Multi- crack)Transient	~	>	~	~	✓	~	~						
	Stress Resultant													
	Tresca	<	✓	\checkmark	✓	\checkmark	✓	✓	~	✓	>	✓	✓	✓
	Optimised Implicit Von Mises	~	~	~	~	~	~	~	~	~	~	~	~	~
	Mohr-Coulomb	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓
	Modified Mohr-Coulomb	✓	~	~	~	~	~	~	~					~
	Drucker-Prager	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	 Image: A start of the start of
	Modified Cam-clay	\checkmark	✓	✓	✓	✓	✓	✓	✓					✓
	Volumetric Crushing/Foam	✓	✓	~	~	~	✓		~	1	✓	~	~	~
	Stress Potential(Von Mises, Modified Von Mises	✓	•	•	•	*	✓	*	1	✓	✓	✓	✓	√

	Hill, Hoffman)													
	Creep (General)	✓	✓	✓	✓	\checkmark	✓		✓				✓	✓
	Creep (AASHTO)	\checkmark	✓	\checkmark	✓	✓	√	✓	✓	✓	✓	✓		
	Creep (CEB-FIP)	✓	 ✓ 	✓	✓	 ✓ 	✓	✓	✓	✓	✓	✓		
	Creep (Chinese)	\checkmark	✓	✓	✓	\checkmark	✓	✓	✓	✓	✓	✓		
	Creep (Eurocode)	✓	 ✓ 	✓	✓	✓	✓	✓	✓	✓	✓	✓		
	Creep (IRC)	✓	✓	\checkmark	✓	✓	√	✓	✓	✓	✓	✓		
	Damage	✓	✓	✓	✓	 Image: A start of the start of	✓	 ✓ 	✓	 ✓ 	✓	✓	✓	✓
	Viscoelastic	\checkmark	✓	\checkmark	✓	\checkmark	√	✓	✓	✓	✓	✓		✓
	Shrinkage (CEB-FIP,	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓		✓
	Eurocode, General,													
	User)													
	Ko Initialisation	✓	✓	✓	✓	\checkmark	✓	✓	✓					✓
	Elasto-plastic interface	✓	✓	✓	✓	✓	✓		✓					✓
	Rubber (Ogden,							✓						
	Mooney-Rivlin,													
	Neo- Hookean,													
	Hencky													
	Generic Polymer	✓	✓	✓	✓	✓	✓	✓	✓	 ✓ 	 ✓ 	 ✓ 		✓
	Resin Cure Model								•	✓	✓	✓		
	Composite (Composite								•	✓	~	~		
	Solid)													
	Composite (Composite													
	Shell) Field													
T	Prescribed Value	✓	✓	✓	./	✓				✓	✓			
Loading	(PDSP,TPDSP)	v	•	•	v	v	v	•	×	•	•	v	v	¥
types	Concentrated Loads	✓	✓	✓	✓	~	1	 ✓ 	 ✓ 	 ✓ 	√	 ✓ 	 Image: A start of the start of	1
	(CL)	•	•		•		•	•	•	•	•	•		•
	Element Loads													
	Distributed Load													
	(UDL)													
	Distributed Load (FLD)	~	~	<	~	~	~	~	✓	✓	✓	1	~	~
	Body Force	✓	✓	✓	✓	\checkmark	✓	✓	✓	✓	✓	✓	✓	✓
	(CBF,BFP,BFPE)													
	Velocity (VELO)	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓
	Acceleration (ACCE)	✓	✓	✓	✓	 ✓ 	✓	 ✓ 	✓	 ✓ 	✓	✓	✓	✓
	Initial Stress/Strain	✓	✓	✓	~	✓	✓	✓	✓	✓	✓	✓	✓	✓
	(SSI,SSIE)													
	Initial Stress/Strain (SSIG)	~	~	~	~	1	~	~	~	~	~	-		~
	Residual Stress (SSR,SSRE)	✓	~	✓	✓	~	~	~	~	~	~	~	~	~

	Residual Stress (SSRG)	✓	~	~	~	1	~	1	~	1	✓	1	✓	~
	Target Stress/Strain (TSSIE,TSSIA)	✓	~	✓	1	~	*	~	*	~	~	1	~	~
	Target Stress/Strain (TSSIG)	✓	~	~	~	1	~	1	~	1	1	1	•	~
	Temperature (TEMP,TMPE)	~	~	~	~	~	~	✓	~	1	*	~	~	~
	Field Load													
	Temp Dependent Load													
	Overburden	✓	~	✓	✓	✓	✓	✓	√	✓	✓	✓		✓
	Phreatic Surface	>	~	✓	✓	✓	1	✓	1	~	~	~		✓
Nonlinear	Total Lagrangian	~	~	<	✓	~	~	~	~					~
geometry	Updated Lagrangian	\checkmark	✓	\checkmark	~	✓	~	1	~					~
	Eulerian	✓	√	✓	✓	√	√	✓	√				✓	✓
	Co-rotational	\checkmark	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓		✓
Integration schemes	Explicitly Integrated													
	Numerically Integrated	\checkmark	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓
Mass modelling	Consistent Mass (default)	✓	~	✓	1	~	~	✓	~	✓	✓	✓		~
8	Lumped Mass	\checkmark	✓	\checkmark	✓	\checkmark	✓	✓	✓	✓	✓	✓	✓	✓

		Plates						S	hells	-				Memb s	
Plate, Sl Membra Summar	ne Element	TF3, QF4	<u>QSC4</u>	TTF6, QTF8	BXS3	BXSI2, BXSI3	<u>TS3, OSI4</u>	TSR6	TSL6, OSL8	TTS3	TTS6	OTS4	OTS8	<u>BXM2/3</u>	TSM3, SM14
Product	LT, Standard (S)	s	s	s	s	S	s	+	+	s	+	s	+	s	s
Version	or Plus (+)														
Nodal	U, V													✓	
Freedoms	U, V, W														✓
(mid-side)	W, qx, qy		✓	✓											
	W, qx, qy (dq)	\checkmark													
	U, V, W, qx, qy														
	U, V, qz					✓									
	U, V, qz (dU)				✓										
	U, V, W, qx, qy,						✓								
	qz														
	U, V, W (U, V, W,								✓						
	q1, q2)														
	U, V, W (q1,)							✓							
	U, V, W, qa, qb (U, V, W, qx, qy, qz)									~	~	~	~		
Material	Linear (Isotropic)	\checkmark	\checkmark	✓	\checkmark	\checkmark	\checkmark	✓	\checkmark	✓	\checkmark	✓	✓	✓	\checkmark
properties	Linear (isouropie)														
F F	Linear	✓	✓	✓	✓		✓	✓	✓	√	✓	✓	 ✓ 		✓
	(Orthotropic)														
	Linear	\checkmark	✓	✓	✓		\checkmark	✓	✓	✓	✓	✓	✓		✓
	(Anisotropic)														
	Linear (Rigidities)	✓	✓	✓			✓	✓	✓						✓
	Matrix														
	Joint														
	Concrete (Multi-							✓	✓	✓	✓	✓	✓		
	crack)														
	Stress Resultant				✓			✓	✓						
	Tresca				✓	✓		✓	✓	\checkmark	✓	✓	✓	✓	
	Optimised				✓	✓		✓	✓	✓	✓	✓	✓	✓	
	Implicit Von Mises														
	Mohr-Coulomb				✓	✓		✓	✓	✓	✓	✓	✓	✓	

	Drucker-Prager				√	✓		✓	✓	✓	✓	✓	✓	✓	
	Volumetric														
	Crushing/Foam														
	Stress Potential				✓	✓		✓	✓	✓	✓	✓	✓	✓	
	(Von-Mises,														
	Modified Von														
	Mises)														
	Stress				✓	✓		✓	✓	\checkmark	✓	✓	✓		
	Potential(Hill,														
	Hoffman)					-		_			-	-		-	
	Creep (General)				✓	✓		✓	✓	✓	✓	✓	✓	~	
	Creep (AASHTO)				✓	✓			✓	✓	✓	✓	✓		
	Creep				✓	✓			✓	\checkmark	✓	✓	✓		
	(CEB_FIP_90)									<u> </u>					
	Creep (Chinese)				✓	✓			✓	✓	✓	✓	✓		
	Creep (Eurocode)				✓	✓			✓	✓	✓	✓	✓		
	Creep (IRC)				✓	✓			✓	✓	✓	✓	✓		
	Damage				✓	✓		✓	✓	✓	✓	✓	✓	~	
	Viscoelastic														
	Shrinkage (CEB-				✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓
	FIP_90,														
	Eurocode_2,														
	General, User)														
	Ko Initialisation	•	•	•	•	•	•	•	•	•	•	•	•	•	•
	Rubber (Ogden,													~	
	Mooney-Rivlin,														
	Neo-Hookean,														
	Hencky)														
	Generic Polymer									\checkmark					
	Composite								✓	v	✓	✓	~		
	(Composite Shell) Field														
T and the state		√	✓	✓	 ✓ 	✓	 ✓ 	 ✓ 	✓	√	 ✓ 	 ✓ 	✓	✓	\checkmark
Loading types	Prescribed Value (PDSP,TPDSP)		•	*	*	•		•	•	•	•	•	•	•	×
	Concentrated	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	\checkmark
	Loads (CL)														
	Element Load				✓	✓									
	(ELDS)														
	Distributed Load	✓	~	✓	✓	~	✓	✓	~	\checkmark	✓	~	✓	✓	\checkmark
	(UDL)														
	Distributed Load				✓	✓								~	
	(FLD)		L .												
	Body Force	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	~	~	~	\checkmark
	(CBF,BFP,BFPE)														

	Velocity (VELO)	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓
	Acceleration (ACCE)	1	~	~	~	~	~	~	~	~	~	~	~	~	~
	Initial Stress/Strain (SSI,SSIE)	•	~	1	~	~	 ✓ 	•						~	~
	Initial Stress/Strain (SSIG)				✓	✓		~	~	✓	✓	~	~	~	~
	Residual Stress (SSR,SSRE)							~							
	Residual Stress (SSRG)				✓	~		~	✓	~	✓	~	>	>	
	Target Stress/Strain (TSSIE,TSSIA)	√	~	~	~	✓	√	~						~	~
	Target Stress/Strain (TSSIG)				~	•		✓	~	~	✓	~	~	~	~
	Temperature (TEMP,TMPE)	✓	~	~	✓	~	✓	~	✓	~	~	✓	~	~	~
	Field Load Temp Dependent Loads														
	Overburden									\checkmark	✓	✓	✓		
	Phreatic surface			✓	✓	✓				✓	✓	✓	✓		
Nonlinear geometry	Total Lagrangian				1	1			~	~	~	~	~	~	
	Updated Lagrangian				✓				~						
	Eulerian														
-	Co-rotational							✓							
Integration schemes	Explicitly Integrated														
	Numerically Integrated	~	✓	1	1	1	~	✓	~	~	~	~	~	~	~
Mass modelling	Consistent Mass (default)	~	~	~	~	~		~	•	~	~	~	~	~	
	Lumped Mass	✓	✓	✓	✓	✓	✓		✓	✓	✓	✓	✓	✓	✓

						Joints	5		
Joint El	ement Summary	<u>JNT3</u>	JPH3	JF3	<u>JAX3</u>	JXS3	<u>JNT4, JL43</u>	<u>JSH4, JL46</u>	JSL4
Product version	LT, Standard (S) or Plus (+)	s	s	s	S	s	s	s	+
Nodal freedoms	U, V	1			✓				
	U, V, W						✓		
	U, V, qz		✓			✓			
	W, qx, qy			\checkmark					
	U, V, W, qx, qy								
	U, V, W, qx, qy, qz							✓	
	U, V, W, q1, q2								✓
Material properties	Linear								
	Matrix (Stiffness, Mass, Damping)*	~	~	~	✓	~	√	√	~
	Joint (Stiffness, General)	✓	✓	\checkmark	✓	✓	✓	✓	\checkmark
	Joint (Dynamic, General)	√	✓	✓	✓	✓	✓	✓	✓
	Joint (Elasto-Plastic)	✓	✓	\checkmark	✓	✓	✓	✓	✓
	Joint (Nonlinear Contact)	√	✓	✓	✓	✓	✓	✓	✓
	Joint (Nonlinear Friction)	✓	✓	✓	✓	✓	✓	✓	\checkmark
	Viscous damping	√	✓	✓	✓	✓	✓	✓	✓
	Lead-Rubber	✓	✓	\checkmark	✓	✓	✓	✓	\checkmark
	Friction Pendulum	✓	✓	✓	✓	✓	✓	✓	✓
	Multilinear elastic	✓	✓	\checkmark	✓	✓	√	✓	\checkmark
	Axial force dependent multilinear elastic	 ✓ 	~	1	~	~	~	~	~
	Concrete Elasto-Plastic								
	Creep								
	Damage								
	Viscoelastic								
	Shrinkage								
	Volumetric Crushing/Foam								
	Rubber								
	Composite								

	Field								
Loading types	Prescribed value (PDSP,TPDSP)	~	~	✓	~	~	1	4	~
	Concentrated Load (CL)	✓	✓	✓	✓	✓	√	✓	✓
	Element Load								
	Distributed Load								
	Body Force(CBF)	\checkmark	\checkmark	\checkmark	✓	\checkmark	✓	✓	\checkmark
	Body Force (BFP,BFPE)								
	Velocities (VELO)	✓	✓	\checkmark	>	\checkmark	✓	~	\checkmark
	Acceleration (ACCE)	\checkmark	✓	\checkmark	✓	✓	✓	✓	\checkmark
	Initial Stress/Strain (SSI,SSIE)	✓	✓	\checkmark	>	✓	✓	~	\checkmark
	Initial Stress/Strain (SSIG)								
	Residual Stress								
	Target Stress/Strain (TSSIE,TSSIA)	1	✓	~	~	~	√	~	<
	Target Stress/Strain (TSSIG)								
	Temperature (TEMP,TMPE)	✓	✓	✓	✓	✓	✓	✓	✓
	Field Load								
	Temp Dependent Load								
Nonlinear geometry	Total Lagrangian								
	Updated Lagrangian								
	Eulerian								
	Co-rotational								
Integration schemes	Explicitly Integrated								
	Numerically Integrated	✓	✓	✓	✓	✓	✓	✓	✓
Mass modelling	Consistent Mass (default)								
	Lumped Mass	✓	✓	\checkmark	✓	\checkmark	✓	✓	\checkmark

* Supported in LUSAS Solver but not supported in LUSAS Modeller for all joints listed.

										F	ield	ł								
Thermal / Field Element Summary		BFD2/3	BFX2/3	BFS2/3	LFD2	LFX2	LFS2	TFD3/6, OFD4/8	TFX3/6, QFX4/8	TF4	TF10	PF6	PF12/15	HF8	<u>HF16/20</u>	TF10S	PF6C, HF8C	PF12C, HF16C	TXF3, OXF4	<u>TXF6, QXF8</u>
Product version	LT, Standard (S) or Plus (+)	s	s	s	s	s	s	s	s	s	s	s	s	s	+	+	+	+	s	s
Freedoms	F	✓	✓	✓	✓	✓	✓	✓	✓	√	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓
Material properties	Composite															✓	•	1		
	Field (Isotropic)	✓	✓	✓				✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓
	Field (Isotropic Concrete)	~	~	~				~	~	~	~	✓	~	✓	~	~	✓	~	~	~
	Field (Orthotropic)							~	~	<	✓	<	~	<	√	~	~	~	~	✓
	Field (Orthotropic Concrete)							>	~	~	✓	~	1	✓	~	✓	✓	✓	✓	~
	Field (Linear Conv/Rad)				✓	✓	✓													
	Field (Arbitary Conv/Rad)				✓	~	✓													
Loading types	Prescribed (TPDSP)	~	~	~	✓	✓	<	~	~	✓	✓	<	✓	<	✓	~	✓	~	~	~
	Rate of heat inflow, concentrated (RGN)	~	√	✓ 				~	•	~	~	<	•	<	•	✓	~	•	✓ 	•
	Face heat and water fluxes (FFL)	~	~	~				~	~	~	~	~	✓	~	1	~	~	~	~	~
	Rate of heat inflow, per unit volume (RBC, RBV, RBVE)	✓	•	✓ 				~	•	~	~	✓	•	~	•	~	•	~	~	✓
	Temperature (TEMP, TMPE)	✓	~	~																
	Environmental conditions (ENVT)	~	~	✓				~	~	~	✓	✓	~	✓	~	✓	✓	✓	✓	~
	Temp Dep Load (TDET/RIHG)	✓	✓	✓				~	~	✓	✓	✓	✓	✓	~	✓	✓	1	✓	✓

Schemes	Numerically Integrated	~	✓	✓	✓	~	~	~	~	✓	✓	~	~	~	~	✓	✓	~	✓	✓
Specific	Consistent	~	~	~				~	✓	√	✓	<	~	<	~	✓	<	✓	<	\checkmark
heat	(default)																			
	Lumped	✓	✓	✓				✓	✓	√	✓	✓	✓	<	✓	~	✓	\checkmark	\checkmark	\checkmark

				H	ygro-7	Thern	nal		
	Thermal nt Summary	THT3/6, OHT4/8	<u>TXHT3/6, QXHT4/8</u>	THT4	THT10	PHT6	<u>PHT12/15</u>	HHT8	HHT16/20
Product	LT, Standard (S)	+	+	+	+	+	+	+	+
version	or Plus (+)								
Freedoms Material properties	Hygro-thermal concrete	✓ ✓	✓ ✓	✓ ✓	✓ ✓	✓ ✓	✓ ✓	✓ ✓	✓ ✓
properties	Hygro-thermal linear	✓	✓	✓	✓	✓	✓	✓	✓
Loading types	Prescribed temperature and relative humidity (TPDSP)	•	1	✓	1	~	1	~	✓
	Environmental conditions (ENVT)	1	~	1	~	~	1	~	~
	Rate of heat and/or water inflow (concentrated) (RGN)	4	~	•	•	~	•	~	~
	Rate of heat and/or water inflow per unit area - flux, (FFL)	√	•	√	1	~	✓	1	•
	Rate of heat and/or water inflow per unit volume (RBC, RBV, RBVE)	•	~	•	~	~	•	~	~
	Temperature dependent environmental conditions (TDET)	•	~	✓	~	~	~	~	~
	Temperature dependent rate of heat and/or water inflow per unit volume (RIHG)	✓	•	✓	✓	✓	•	 ✓ 	•
	Initial conditions (TMPE, TMP)	✓	1	✓	~	~	1	~	~
Integratio n schemes	Numerically Integrated	4	~	✓	~	~	~	~	~

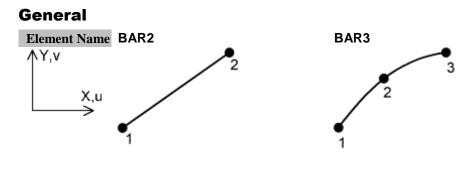
]	Inte	erfao	ce	I			Mas	SS			gid eline	Phreati c	
Structu Slidelin	ce, Non- Iral Mass, Rigid le and Phreatic It Summary	IPN4, IAX4, IPM4	IPN6, IAX6, IPM6	<u>IS6, IS8</u>	<u>IS12, IS16</u>	IPN6P, IAX6P	<u>IS12P, IS16P</u>	PM2	PM3	LMS3, LMS4	<u>LM2, LM3</u>	<u>TM3/6, QM4/8</u>	<u>R2D2</u>	<u>R3D3, R4D3</u>	PHS2	PHS3, PHS4
Product version	LT, Standard (S) or Plus (+)	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
version Nodal freedoms	U, V	~	~					~			~		1			
	U, V, P					✓										
	U, V, W			 ✓ 	✓				✓	✓		✓		✓		
	U,V,W, P						✓				_					
	U, V, qz															
	W, qx, qy															
	U, V, W, qx, qy															
	U, V, W, qx, qy, qz									>						
	U, V, W, q1, q2															
Material properties	Linear												~	~		
	Matrix															
	Joint															
	Mass							✓	✓	✓	✓	✓				
	Concrete															
	Elasto-Plastic															
	Creep															
	Damage															
	Shrinkage															
	Interface	✓	✓	✓	✓	✓	✓									
	Rubber															
	Generic Polymer															
	Stress Potential															
	Composite Field															
Loading types	Prescribed value (PDSP,TPDSP)	~	~	√	~	~	~						~	✓		
	Concentrated Loads	✓	✓	\checkmark	✓	✓	✓									

	(CL)														
	Element Load														
	Distributed Load														
	Body Force (CBF)							✓	✓	✓	✓	✓			
	Body Force (BFP,BFPE)														
	Velocity (VELO)	✓	✓	\checkmark	✓								✓	✓	
	Acceleration (ACCE)	>	✓	\checkmark	>								~	✓	
	Initial Stress/Strain (SSI,SSIE)														
	Initial Stress/Strain (SSIG)														
	Residual Stress														
	Target Stress/Strain (TSSIE,TSSIA)														
	Target Stress/Strain (TSSIG)														
	Temperature (TEMP,TMPE)	~	~	~	✓	~	✓								
	Field Load														
	Temp Dependent Load														
Nonlinear geometry	Total Lagrangian												√ *	√ *	
	Updated Lagrangian												√ *	√ *	
	Eulerian												√ *	√ *	
	Co-rotational	✓		✓									√ *	√ *	
Integration schemes	Explicitly Integrated														
	Numerically Integrated	✓	✓	✓	✓	✓	✓	✓	>	✓	✓	✓			
Mass modelling	Consistent Mass (default)							✓	✓	~	~	✓			
	Lumped Mass							\checkmark	✓	✓	\checkmark	✓			

* Dependent upon the other surface (deformable surface) that the element is in contact with.

Chapter 1 : Bar Elements.

2D Structural Bar Elements



Element Group	Bars
Element	Structural Bars
Subgroup	
Element	Straight and curved <i>isoparametric</i> bar elements in 2D which can
Description	accommodate varying cross sectional area.
Number Of	2 or 3.
Nodes	
Freedoms	U, V at each node
Node	X, Y at each node
Coordinates	

Geometric Properties

- A1 ... An Cross sectional area at each node.
- **SF1, MF1** Optional scale factor applied to the areas in the calculation of the stiffness and mass matrices

Material Properties

Linear	Isotropic
Matrix	Not applicable
Joint	Not applicable
Concrete	Not applicable
Elasto-Plastic	Stress resultant
	Tresca:

MATERIAL PROPERTIES (Elastic: Isotropic)

Not applicable MATERIAL PROPERTIES NONLINEAR 61

		(Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker-Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr-Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Optimised Implicit Von Mises:	MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic)
	Volumetric Crushing:	Not applicable
	Stress Potential	STRESS POTENTIAL VON_MISES (Isotropic: von Mises, Modified von Mises)
Creep		CREEP PROPERTIES (Creep)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic		VISCO ELASTIC PROPERTIES
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Rubber	Not applicable	
Multi-linear		MATERIAL PROPERTIES NONLINEAR 104
Composite	Not applicable	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V at each node.
Concentrated	CL	Concentrated loads. Px, Py at each node.
Loads		
Element Loads	Not applicable.	
Distributed Loads	Not applicable.	
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Ωx ,
		Ωy, Ωz, αz
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0, 0, Xcbf, Ycbf
Velocities	VELO	Velocities. Vx, Vy at nodes.
Accelerations	ACCE	Acceleration Ax, Ay at nodes.
	SSI, SSIE	Initial stresses/strains at nodes/for element. Fx, &x,
Stress/Strains		σx, εx

	SSIG	Initial stresses/strains at Gauss points. F , ϵx , σx ,
Residual Stresses	SSR, SSRE SSRG	Ex Not applicable. Residual stresses at Gauss points.
Target Stress/Strains	TSSIE, TSSIA	Components (nonlinear material models): 0, 0, σx Target stresses/strains at nodes/for element. Fx, ϵx ,
50 (55) 50 ams	TSSIG	σx , ϵx Target stresses/strains at nodes/for element. F, $\epsilon x,$
Temperatures	TEMP, TMPE	σx , εxTemperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0 in local directions.
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent Loads	Not applicable.	

LUSAS Output

Solver	Force (default): Fx	
	Strain: Ex	
Modeller	See <u>Results Tables (Appendix K)</u>	

Local Axes

□ Standard line element

Sign Convention

□ Standard bar element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and small strains
Updated	Not applicable.
Lagrangian	

EulerianNot applicable.Co-rotationalFor large displacements and small strains.

Integration Schemes

Stiffness	Default.	1-point (BAR2), 2-point (BAR3).
	Fine (see <i>Options</i>).	2-point (BAR2).
Mass	Default. Fine (see	2-point (BAR2), 3-point (BAR3). As default.
	Options).	As default.

Mass Modelling

- □ Consistent mass (default).
- Lumped mass.

Options

- **18** Invokes fine integration rule for element.
- **55** Outputs strains as well as stresses
- 87 Total Lagrangian geometric nonlinearity.
- 105 Lumped mass matrix.
- 229 Co-rotational geometric nonlinearity.

Notes on Use

- 1. The bar formulation is based on the standard **isoparametric** approach. The variation of axial force is constant for BAR2, and linear for BAR3.
- 2. Since the 3-noded element has no bending stiffness mechanisms may occur when used as 'stand alone' elements if the central node is not constrained in some way.
- 3. When the BAR2 element is used with either varying cross-sectional area or temperature dependent material properties, the 2-point Gauss rule should be utilised. This provides an improved representation of the variation of the material properties along the length of the element.
- 4. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties

and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command.

Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature

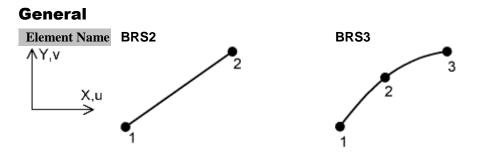
Recommendations on Use

- The 2-node elements are the most effective bar elements for modelling 'stand-aloneelements' such as members of trusses or bars connecting two discrete structures.
- They can be used to model cables in cable-stayed structures.
- Both the 2-noded and 3-noded elements are suitable for modelling reinforcement with continuum elements e.g. BAR3 may be used with QPM8 for analysis of reinforced concrete structures, or for modelling rock bolts surrounding an excavation

Theory

For additional information see the LUSAS Theory Manual

3D Structural Bar Elements



Element Group	Bars
Element	Structural Bars
Subgroup	
Element	Straight and curved isoparametric bar elements in 3D which can
Description	accommodate varying cross-sectional area.
Number Of	2 or 3.
Nodes	
Freedoms	U, V, W at each node
Node	X, Y, Z at each node.
Coordinates	

Geometric Properties

- A1 ... An Cross sectional area at each node.
- **SF1, MF1** Optional scale factor applied to the areas in the calculation of the stiffness and mass matrices

Material Properties

Isotropic
Not applicable
Not applicable
Not applicable
Stress resultant
Tresca:

MATERIAL PROPERTIES (Elastic: Isotropic)

Not applicable MATERIAL PROPERTIES NONLINEAR 61

		(Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic
		Strain or Isotropic Total Strain)
	Drucker-	MATERIAL PROPERTIES NONLINEAR 64
	Prager:	(Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr-	MATERIAL PROPERTIES NONLINEAR 65
	Coulomb:	(Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Optimised	MATERIAL PROPERTIES NONLINEAR 75
	Implicit Von	(Elastic: Isotropic, Plastic: Von Mises, Hardening:
	Mises:	Isotropic & Kinematic)
	Volumetric	Not applicable
	Crushing:	
	Stress	STRESS POTENTIAL VON_MISES
	Potential	(Isotropic: von Mises, Modified von Mises)
Creep		CREEP PROPERTIES (Creep)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic		VISCO ELASTIC PROPERTIES
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Multi-linear		MATERIAL PROPERTIES NONLINEAR 104
Rubber	Not applicable	
Composite	Not applicable	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, W at each node.
Concentrated	CL	Concentrated loads. Px, Py, Pz at each node.
Loads		
Element Loads	Not applicable	
Distributed Loads	Not applicable	
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf,
		Zcbf, Ωx , Ωy , Ωz , αx , αy , αz
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0

Velocities	VELO
Accelerations	ACCE
Initial	SSI, SSIE
Stress/Strains	

 $\begin{array}{l} \text{Zcbf, } \Omega x, \, \Omega y, \, \Omega z, \, \alpha x, \, \alpha y, \, \alpha z \\ \text{Body force potentials at nodes/for element. 0, 0, \\ 0, 0, \, Xcbf, \, Ycbf, \, Zcbf \\ \text{Velocities. Vx, Vy, Vz at nodes.} \\ \text{Acceleration Ax, Ay, Az at nodes.} \\ \text{Initial stresses/strains at nodes/for element. Fx,} \\ \epsilon x, \, \sigma x \, , \, \epsilon x \\ \end{array}$

Residual Stresses	SSIG SSR, SSRE SSRG	Initial stresses/strains at Gauss points. F, εx , σx , εx Not applicable Residual stresses at Gauss points. Components (nonlinear material models): 0, 0,
Target Stress/Strains	TSSI, TSSIA TSSIG	σ_x Target stresses/strains at nodes/for element. Fx, ε_x , σ_x , ε_x Target stresses/strains at nodes/for element. F,
Temperatures		 εx, σx, εx Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0 in local directions.
Overburden	Not applicable.	
Phreatic Surface	••	
Field Loads	Not applicable	
Temp Dependent Loads	Not applicable	

LUSAS Output

Solver	Force (default): Fx	
	Strain: Ex	
Modeller	See <u>Results Tables (Appendix K)</u>	

Local Axes

□ Standard line element

Sign Convention

□ Standard bar element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and small strains
Updated	Not applicable.
Lagrangian	

EulerianNot applicable.Co-rotationalFor large displacements and small strains.

Integration Schemes

Stiffness	Default.	1-point (BRS2), 2-point (BRS3).
	Fine (see Options).	2-point (BRS2).
Mass	Default.	2-point (BRS2), 3-point (BRS3).
	Fine (see Options).	As default.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- 18 Invokes fine integration rule for element.
- 55 Outputs strains as well as stresses
- 87 Total Lagrangian geometric nonlinearity.
- 105 Lumped mass matrix.
- 229 Co-rotational geometric nonlinearity.

Notes on Use

- 1. The bar formulation is based on the standard
- 2. Since the 3-noded element has no bending stiffness, mechanisms may occur, when used as 'stand alone' elements, if the central node is not constrained in some way.
- 3. When the BRS2 element is used with either varying cross-sectional area or temperature dependent material properties, the 2-point Gauss rule should be utilised. This provides an improved representation of the variation of the material properties along the length of the element.
- 4. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command.

Restrictions

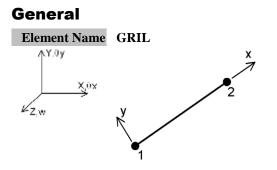
- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature

Recommendations on Use

- The 2-node elements are the most effective bar elements for modelling 'stand-aloneelements' such as members of trusses or bars connecting two discrete structures.
- They can be used to model cables in cable-stayed structures.
- Both the 2-noded and 3-noded elements are suitable for modelling reinforcement with continuum elements e.g. BRS3 may be used with HX20 for analysis of reinforced concrete structures, or for modelling rock bolts surrounding an excavation.

Chapter 2 : Beam Elements.

2D Engineering Grillage Thick Beam Element



Element Group	Beams
Element	Engineering Beams
Subgroup	
Element	A straight grillage element for which shear deformations are included.
Description	The geometric properties are constant along the length.
Number Of	2 with moment release end conditions
Nodes	
End Releases	The element node numbers should be followed by: R restrained (default),
	F free defined in the order θ y at node 1 and then θ y at node 2 related to
	local element axes
Freedoms	W, θx , θy : at each node.
Node	X, Y: at each node.
Coordinates	

Geometric Properties

A, Iyy, Izz, Jxx, Asz, EFW	for element
	Optional scale factors applied to the geometric properties in the calculation of the stiffness and mass matrices
Α	Cross sectional area
Iyy, Izz	2nd moments of area about local y, z axes (see
	Definition and <i>Notes</i>)
Jxx	Torsional constant
Asz	Effective shear area on local yz plane in local z

directions EFW Equivalent plate width

Material Properties

Isotropic:	M
Not applicable	
Not applicable.	
	Not applicable Not applicable Not applicable Not applicable Not applicable Not applicable Not applicable Not applicable Not applicable Not applicable

MATERIAL PROPERTIES (Elastic: Isotropic)

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. W, θx , θy : at nodes.
Concentrated Loads	CL	Concentrated loads. Pz, Mx, My: at nodes (global).
Element Loads	ELDS	Element loads LTYPE, S1, Pz, Mx, My LTYPE=11: point loads and moments in local directions. LTYPE=12: point loads and moments in global directions.

LTYPE, 0, Wz, Mx, 0

		LTYPE=21: uniformly distributed loads in local directions. LTYPE, S1, Wz1, Mx1, 0, S2, Wz2, Mx2, 0 LTYPE=31: distributed loads in local directions.
		LTYPE, S1, Wz, Mx, 0 LTYPE=41: trapezoidal loads in local directions.
Distributed Loads	UDL	Uniformly distributed loads. Wz: Force/unit length in local directions for element (Local z and global Z are coincident).
	FLD, FLDG	Not applicable.
Body Forces	CBF	Constant body forces for element. Zcbf
-	BFP, BFPE	Not applicable.
Velocities	VELO	Velocities. Vz: at nodes.
Accelerations	ACCE	Acceleration Az: at nodes.
Initial	Not	
Stress/Strains	applicable.	
Residual Stresses	Not	
	applicable.	
Target		
Stress/Strains	11	
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. 0, 0, 0, dT/dz, 0, 0, 0, dTo/dz: in local directions.
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	
Field Loads	applicable.	
Temp Dependent Loads		

Output

Solver	Force (default): Fz, Mx, My: in local directions (see <i>Notes</i>).
	Element output is with respect to the beam centre line.
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

□ Standard line element

Sign Convention

□ 2D engineering grillage thick beam element. Positive external forces and moments acting on the element nodes are in the direction of the local element axes.

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Explicitly integrated.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

105 Lumped mass matrix

Notes on Use

- 1. The element formulation is based on the standard grillage element formulation. The force variations along the element are linear shear force, constant torsion and quadratic bending moment.
- 2. The displacement variations along the element are linear torsional rotations and cubic transverse flexural displacements.
- Internal forces and moments are output at intervals of 1/10th of the element length by specifying the Gauss point option from the Output button on the File > LUSAS datafile dialog.
- 4. The <u>second moment of area</u> about local z, (Izz), is only required when assembling the mass matrix.
- 5. Strains are not available for GRIL elements.

- 6. Though this element cannot model nonlinear behaviour it can be mixed with other elements in a nonlinear analysis.
- 7. For restrictions on the use of <u>Wood-Armer</u> with grillages refer to the LUSAS User Guide and Theory Manual.
- 8. The element has constant material properties along its length. For analyses utilising temperature dependent material properties, the temperature used is the average of the nodal values.
- 9. A moment release option permits modelling of internal hinges (torsional rotations cannot be released). See <u>Number of Nodes</u> section.
- 10. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command.

Restrictions

The element does not model material or geometric nonlinear effects.

Recommendations on Use

The element can be used to model two dimensional grillage type structures. Linear, eigen, and dynamic analysis procedures can be used with GRIL elements.

2D Thick Beam Elements

General	
Element Name	BMI2 BMI3
∧Y,v X,u	$\begin{array}{c} Y \\ 1 \\ r_1 \end{array}$
Element Group	Beams
Element	
Subgroup	
Element Description	
Description	accommodate varying geometric properties along the length.
Number Of	
Nodes	
Freedoms	0, v, 02. at cach hode.
End Releases	3
	F free defined in the order U, V, θz for node 1 and then U, V, θz for the other end node (node 2 for BMI2, node 3 for BMI3). The releases relate to the local element axes (see Notes, Assumptions and Limitations).
Partial fixity	Partial fixity at each end node can be defined for all freedoms; this can
	take the form of a fixity reduction factor or an explicitly defined stiffness
	value. Partial fixities are defined with respect to the local element axes (see Notes, Assumptions and Limitations).
Rigid ends	
	these elements. If these lengths are non zero then any end release or
	partial fixity is applied at the inner point defining the rigid end. A rigidity factor $(1.0>\lambda>0.0)$ can be specified to make the ends semi-rigid, and
	options to include/exclude the masses of the rigid ends are also provided
	(see Notes, Assumptions and Limitations).
Node	
Coordinates	

Geometric Properties

A, Izz, Asy, ey for element

SF1,SF2,SF3,SF4, Optional scale factors applied to the geometric properties in the MF1,MF2,MF3,MF4 calculation of the stiffness and mass matrices

- A Cross sectional area
- Izz 2nd moment of area about local z-axis (see <u>Definition</u>)
- Asy Effective shear area on local yz plane in local y directions
 - ey <u>Eccentricity</u> from beam xz-plane to nodal line (+ve in +ve local ydirection)

Note: For MATERIAL MODEL 29 additional geometric properties are appended to the previous 8 (BMI2) or 12 (BMI3) geometric properties (see Notes, Assumptions and Limitations).

Material Properties

Matrix	Isotropic: Not applicable Not applicable Not applicable	MATERIAL PROPERTIES (Elastic: Isotropic)
Elasto-Plastic	Stress resultant	MATERIAL PROPERTIES NONLINEAR 29 (Elastic: Isotropic, Plastic: Resultant) (ifcode=1 or 2, see Assumptions and Limitations)
Сгеер	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB-FIP (Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)

Damage	Not applicable
Viscoelastic	Not applicable
Shrinkage	

RubberNot applicableGeneric PolymerNot applicableCompositeNot applicable

SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, θz : at nodes.
Concentrated Loads	CL	Concentrated loads. Px, Py, Mz: at nodes (global).
Element Loads	ELDS	Element loads on nodal line (load type number LTYPE *10 defines the corresponding element load type on beam axis, see Notes) LTYPE, S1, Px, Py, Mz LTYPE=11: point loads and moments in local directions. LTYPE=12: point loads and moments in global directions. LTYPE, 0, Wx, Wy, 0 LTYPE=21: uniformly distributed loads in local directions. LTYPE=22: uniformly distributed loads in global directions. LTYPE=23: uniformly distributed projected loads in global directions LTYPE, S1, Wx1, Wy1, 0, S2, Wx2, Wy2, 0 LTYPE=31: distributed loads in local directions. LTYPE=32: distributed loads in global directions. LTYPE=32: distributed loads in global directions. LTYPE=33: distributed projected loads in global directions LTYPE, S1, Wx, Wy, 0 LTYPE=41: trapezoidal loads in local directions. LTYPE=42: trapezoidal loads in global directions. LTYPE=43: trapezoidal projected loads in global directions
		directions. LTYPE, 0, Wx, Wy, 0 LTYPE=21: uniformly distributed loads in local directions. LTYPE=22: uniformly distributed loads in global directions. LTYPE=23: uniformly distributed projected loads in global directions LTYPE, S1, Wx1, Wy1, 0, S2, Wx2, Wy2, 0 LTYPE=31: distributed loads in local directions. LTYPE=32: distributed loads in global directions. LTYPE=33: distributed projected loads in global directions LTYPE, S1, Wx, Wy, 0 LTYPE=41: trapezoidal loads in local directions. LTYPE=42: trapezoidal loads in global directions. LTYPE=43: trapezoidal projected loads in

Distributed Loads	UDL	Uniformly distributed loads. Wx, Wy: forces/unit length for element in local directions.
	FLD	Not applicable.
Body Forces	CBF	Constant body forces for element.
		Xcbf, Ycbf, Ωx , Ωy , Ωz , αz
	BFP, BFPE	Not applicable.
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Acceleration. Ax, Ay: at nodes.
Initial Stress/Strains	SSI, SSIE	Residual stresses at nodes/for element. Resultants (for material model 29). Fx, Fy, Mz: axial force, shear force and moment in local directions.
Residual Stresses	SSR, SSRE, SSRG	Residual stresses at Gauss points. These stresses are specified in the same manner as SSR and SSRE.
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. Fx, Fy, Mz: axial force, shear force and moment in local directions. ε_x , ε_y , ψ_z : axial, shear and flexural strains in local directions.
		Target stresses/strains at Gauss points. These stresses/strains are specified in the same manner as TSSIE and TSSIA.
Temperatures	TEMP, TMPE	Temperatures at nodes/for elements. T, 0, dT/dy, 0, To, 0, dTo/dy, 0
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not	
Loads	applicable.	

LUSAS Output

Solver Stress resultants (default): Fx, Fy, Mz: axial force, shear force and moment in local directions.
 Strain: εx, εy, ψz: Axial, shear and flexural strains in local directions.
 By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal

axes.

Modeller See Results Tables (Appendix K).

Local Axes

□ Standard line element

Sign Convention

□ 2D engineering beam element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and large rotations (see Notes)
Updated	Not applicable.
Lagrangian	
Eulerian	Not applicable.
Co-rotational	For large displacements and large rotations
P-Delta	Displacements and rotations should be small (see Notes)

Integration Schemes

Stiffness	Default.	1-point (BMI2), 2-point (BMI3).
	Fine.	Same as default.
Mass	Default.	2-point (BMI2), 3-point (BMI3).
	Fine.	Same as default.

Note: A 3-point <u>Newton-Cotes integration</u> rule is also available for BMI3 using OPTION 134. This may be more applicable for infinitesimal strain, elasto-plastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory Manual.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- **36** Follower loads
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity. (see Notes)
- **102** Switch off load correction stiffness matrix due to centripetal acceleration
- **105** Lumped mass matrix.
- **134** Gauss to <u>Newton-Cotes</u> in plane (in the local x direction) integration for elements
- 157 Material model 29 (non cross-section elements), see Notes.
- 229 Co-rotational geometric nonlinearity.
- **403** Introduce residual bending flexibility correction for 2-node thick beam BMI21, see Assumptions and Limitations (on by default).
- **404** Compute equivalent nodal loading from equilibrium considerations for 2-node thick beam BMI21, see Assumptions and Limitations (on by default).
- **405** Specify geometric properties along beam centroidal axes
- 406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
- 418 Output stress resultants relative to beam centroidal axes for eccentric elements
- 421 P-Delta analysis, see Notes
- 432 Use P-Delta geometric stiffness matrix of thick beams for linear buckling analysis

Notes, Assumptions and Limitations

- 1. The element is formulated from the degenerate continuum concept, i.e. enforcing directly the modified Timoshenko hypothesis for thick beams to the continuum theory. Plane cross-sections initially normal to the beam axis remain plane and undistorted (the shape of the cross-section remains unchanged) under deformation, but do not necessarily remain normal to the beam axis. Shearing deformations are included.
- 2. Input of geometric properties (OPTION 405) and loads (OPTION 406), and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axes. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line.
- 3. When OPTION 403 is specified to introduce residual bending flexibility correction (on by default), for BMI2, the axial force is constant, while the shear force and moment vary linearly along the length of the beam. For BMI3 the axial force, shear force and moment all vary linearly along the length.
- 4. When BMI2 is used together with OPTION 403 to introduce residual bending flexibility correction, its stiffness matrix is enhanced to the order of a cubic. Note that if OPTION 403 is used with eccentrically stacked elements, slippage can occur.

- 5. When BMI2 is used together with OPTION 404, loading that varies along the element length is accounted for in the force diagrams (i.e. for a beam under CBF or internal element loading). A post-processing technique has been introduced to obtain accurate quadratic bending moments for BMI3. For BMI2 (with OPTION 404) and BMI3, internal forces and moments are output at intervals of 1/10th of the element length by specifying the Gauss point option from the Output button of the LUSAS Datafile dialog.
- 6. The end releases for this element allow a joint to be modelled between adjacent elements. These joints allow rotation and translation of one beam with respect to another without load transferral. The rotations and translations remain in the local directions of the beam elements and support large deformations.
- 7. For nonlinear material model 29 the following geometric properties are appended to those already specified (see Geometric Properties).
 - Ap, Zzzp, Sp at each node
 - Ap Plastic area (=elastic area)
 - Zzzp Plastic modulus for bending about z axes
 - Sp Plastic area for shear (Sp=0).

Note that if eccentricity has been specified the plastic properties must be defined with reference to the nodal line and not the beam axes, i.e. the eccentricity is not used to automatically modify the plastic properties, they must be defined via modified geometry.

For nonlinear material model 29 the following ifcode parameters are applicable: ifcode=1 for circular hollow sections and ifcode=2 for solid rectangular sections.

- 8. Temperature dependent properties cannot be used with material model 29.
- 9. The <u>rigidity matrix</u> is evaluated explicitly from the geometric properties for both linear and nonlinear materials.
- 10. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command.
- 11. OPTION 36 is only applicable for use with element load types ELDS and UDL. Specifying this option makes these element loads follow the element geometry as the analysis progresses.
- 12. When a nonlinear material is used with this element the transverse shear stresses are excluded from the plasticity computations i.e. the transverse shear stresses are assumed to remain elastic. This means that if a nonlinear material is used in

applications where transverse shear tends to dominate the stress field the equivalent von Mises and maximum principal stresses can exceed the uniaxial yield stress.

- 13. When a step by step dynamic analysis is carried out using BMI elements with distributed loading, the "free body force diagrams" pertaining to applied loading, are not superimposed on the nodal values, to do so would lead to erroneous results until a steady state is reached. It should therefore be noted that different force diagrams will be obtained for BMI elements if static and dynamic analyses are directly compared.
- 14. OPTION 229 considers large displacements and large rotations using a co-rotational formulation. When both options 87 and 229 are true, a local Total Lagrangian formulation will be used within a global co-rotational framework. Note that OPTION 87 has no effect when specified without OPTION 229.
- 15. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command.
- 16. The P-Delta formulation is only applicable to lower order (2-noded) beams, higher order beams used in a P-Delta analysis will default to co-rotational GNL.
- 17. Partial fixities and rigid ends are defined via the ELEMENT TOPOLOGY data and follow on the same line after the end releases, for example:

1 1 2 3 RFFRRR
$$K \hat{k}_{12} \hat{k}_{13} [r_1 r_2 \lambda m_1 m_2]$$

or
1 1 2 3 RFFRRR $N n_{12} n_{13} [r_1 r_2 \lambda m_1 m_2]$

The character K is used to identify that the partial fixity stiffnesses $\hat{k}_{12} \hat{k}_{13}$ are being explicitly defined, while the character N signifies that fixity factors, $n_{12} n_{13}$ are being defined. The fixity factors are used as follows:

$$\hat{k}_{ij} = \frac{n_{ij}}{1 - n_{ij}} \, \tilde{k}_{ij}$$

The value of the factor n_{ij} ranges from zero for a pinned connection to 1.0 for a fully fixed connection.

The values r_1 and r_2 are the rigid end lengths at nodes 1 and 2 and λ is the rigidity factor (1.0 = fully rigid, the default). The factors m1 and m2 dictate how much mass to include for the rigid ends, full mass = 1.0 (default $m_1=m_2=0.0$).

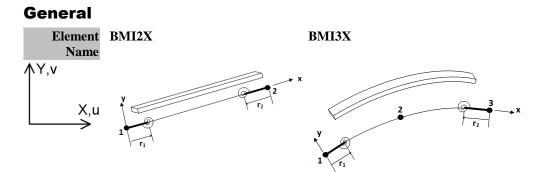
Restrictions

- Ensure mid-side node centrality
- □ Avoid excessive element curvature

Recommendations on Use

• The element may be used for linear and nonlinear analysis of two dimensional beam, frame and arch structures.

2D Thick Beam Element with Quadrilateral Cross-Section

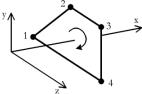


Element Group	Beams
Element	2D Thick Beams
Subgroup	
Element	Straight and curved isoparametric degenerate thick beam elements in 2D
Description	for which shearing deformations are included. The elements have a quadrilateral cross section which may vary along its length.
Number Of	2 (BMI2X) 3 (BMI3X)
Nodes	
Freedoms	U, V, θz : at end nodes.
End Releases	The element node numbers should be followed by: R restrained (default) F free defined in the order U, V, θz for node 1 and then U, V, θz for the other end node (node 2 for BMI2X, node 3 for BMI3X). The releases relate to the local element axes (see Notes, Assumptions and Limitations).
Partial fixity	Partial fixity at each end node can be defined for all freedoms; this can take the form of a fixity reduction factor or an explicitly defined stiffness value. Partial fixities are defined with respect to the local element axes (see Notes, Assumptions and Limitations).
Rigid ends	Rigid lengths r_1 and r_2 measured from each end node can be specified for these elements. If these lengths are non zero then any end release or partial fixity is applied at the inner point defining the rigid end. A rigidity factor (1.0> λ >0.0) can be specified to make the ends semi-rigid, and options to include/exclude the masses of the rigid ends are also provided (see Notes, Assumptions and Limitations).
Node	X, Y: at each node.
Coordinates	

Geometric Properties

y1, z1, y2, z2, y3, z3, y4, z4: local cross section coordinate pairs at each node; followed by nt12, nt14: specifying the number of <u>Newton-Cotes integration</u> points in the direction defined by the local cross-section points 1-2 and 1-4 (zero indicates default values). See *Notes*. Multiple quadrilateral cross-sections can be used to build up complex beam cross-sections.

Note. The coordinates of the cross section are numbered clockwise about the local x-axis (the beam nodal line). That is, a right-hand screw rule in the direction of increasing x.



Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
Matrix	Not applicable	
Joint	Not applicable	
Concrete		MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi Crack Concrete)
Elasto-Plastic	Stress resultant:	Not applicable
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker- Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr- Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Optimised Implicit Von Mises:	MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic)
	Volumetric Crushing:	Not applicable
	Stress Potential	STRESS POTENTIAL VON_MISES (Isotropic: von Mises, Modified von Mises)
Creep		CREEP PROPERTIES (Creep)

	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP (Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic	Not applicable	
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Rubber	Not applicable	
Generic Polymer	Not applicable	
Composite	Not applicable	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, θz : at end nodes. dU at mid-side node.
Concentrated Loads	CL	Concentrated loads. Px, Py, Mz: at end nodes (global). dPx: at mid-side node (local).
Element Loads	ELDS	Element loads on nodal line (load type number LTYPE *10 defines the corresponding element load type on beam axis). LTYPE, S1, Px, Py, Mz LTYPE=11: point loads and moments in local directions. LTYPE=12: point loads and moments in global directions.

		LTYPE, 0, Wx, Wy, Mz
		LTYPE=21: uniformly distributed loads in local
		directions.
		LTYPE=22: uniformly distributed loads in global directions.
		LTYPE=23: uniformly distributed projected loads
		in global directions
		LTYPE, S1, Wx1, Wy1, Mz1, S2, Wx2, Wy2, Mz2
		LTYPE=31: distributed loads in local directions.
		LTYPE=32: distributed loads in global directions.
		LTYPE=33: distributed projected loads in global
		directions
		LTYPE, S1, Wx, Wy, Mz
		LTYPE=41: trapezoidal loads in local directions.
		LTYPE=42: trapezoidal loads in global directions. LTYPE=43: trapezoidal projected loads in global
		directions
Distributed Loads	UDL	Uniformly distributed loads. Wx, Wy: force/unit length in local directions.
	FLD	Not applicable.
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Ωx ,
·		$\Omega_{\rm V}, \Omega_{\rm Z}, \alpha_{\rm Z}$
	BFP, BFPE	
	DIT, DITL	Body force potentials at nodes/for element. φ1, φ2, 0, 0, Xcbf, Ycbf
	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay: at nodes
Initial	SSI, SSIE	Target stresses/strains at nodes/for element.
Stress/Strains		Components: Fx, Fy, Mz, εx , εy , ψz , (σx , σxy ,
		Ex, Exy) Bracketed terms repeated for each fibre integration point.
	SSIG	Initial stresses/strains at Gauss points. These stresses/strains are specified in the same manner as SSI and SSIE.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element.
		Components: $0, 0, 0, 0, 0, 0, 0, (\sigma x, \sigma xy)$ Bracketed
		terms repeated for each fibre integration point.
	SSRG	Residual stresses at Gauss points. These stresses are specified in the same manner as SSR and SSRE.
Target	TSSIE, TSSIA	Target stresses/strains at nodes/for element.
Stress/Strains		Components: Fx, Fy, Mz, εx , εy , ψz , (σx , σxy , εx ,
		Exy) Bracketed terms repeated for each fibre integration point.

	TSSIG	Target stresses/strains at Gauss points. These stresses/strains are specified in the same manner as TSSIE and TSSIA.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element T, 0, dT/dy, 0, To, 0, dTo/dy, 0: in local directions.
Phreatic surface	Face_Pressure	The fluid pressure is applied in the –y direction of the element y axis.
Field Loads	Not applicable.	
Temp Dependent Loads	Not applicable.	

LUSAS Output

Solver	Stress resultants (default): Fx, Fy, Mz: axial force, shear forces and moment in local directions.
	Continuum stresses: σx , σxy , in local directions.
	Strain: εx , εy , ψz : Axial, shear and flexural strains in local directions.
	Continuum strains: Ex, Exy in local directions. By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal axes.
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

□ Standard line element

Sign Convention

□ Standard beam element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements, small rotations and small strains (see Notes).
Updated	For large displacements, large rotations and small strains.
Lagrangian	
Eulerian	Not applicable.
Co-rotational	For large displacements and large rotations

P-Delta Displacements and rotations should be small (see *Notes*)

Integration Schemes

Stiffness	Default.	1-point (BMI2X), 2-point (BMI3X).
	Fine (see Options).	Same as default.
Mass	Default.	2-point (BMI2X), 3-point (BMI3X).
	Fine (see Options).	Same as default.

A 3-point <u>Newton-Cotes integration</u> rule is also available for BMI3X using OPTION 134. This may be more applicable for infinitesimal strain, elasto-plastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory Manual

Mass Modelling

- □ Consistent mass (default).
- Lumped mass.

Options

- 36 Follower loads
- 55 Output strains as well as stresses
- 87 Total Lagrangian geometric nonlinearity (see *Notes*).
- 102 Switch off load correction stiffness matrix due to centripetal acceleration
- **105** Lumped mass matrix
- **134** Gauss to <u>Newton-Cotes</u> in plane (in the local x direction) integration for elements.
- 139 Output yielded integration points only
- 229 Co-rotational geometric nonlinearity
- **403** Introduce residual bending flexibility correction for 2-node thick beam BMI21, see Assumptions and Limitations (on by default).
- **404** Compute equivalent nodal loading from equilibrium considerations for 2-node thick beam BMI2X, see Notes (on by default).
- 406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
- 418 Output stress resultants relative to beam centroidal axes for eccentric elements
- 421 P-Delta analysis, see Notes
- **432** Use P-Delta geometric stiffness matrix of thick beams for linear buckling analysis

Notes on Use

- 1. The element is formulated from the degenerate continuum concept, i.e. enforcing directly the modified Timoshenko hypothesis for thick beams to the continuum theory. Plane cross-sections initially normal to the beam axis remain plane and undistorted (the shape of the cross-section remains unchanged) under deformation, but do not necessarily remain normal to the beam axis. Shearing deformations are included.
- 2. Input of loads (OPTION 406) and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axis. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line. Fiber stress/strain results are output at the actual location.
- 3. When OPTION 403 is specified to introduce residual bending flexibility correction (on by default), for BMI2X, the axial force is constant, while the shear force and moment vary linearly along the length of the beam. For BMI3X the axial force, shear force and moment all vary linearly along the length.
- 4. When BMI2X is used together with OPTION 403 to introduce residual bending flexibility correction, its stiffness matrix is enhanced to the order of a cubic. Note that if OPTION 403 is used with eccentrically stacked elements, slippage can occur.
- 5. When BMI2X is used together with OPTION 404, loading that varies along the element length is accounted for in the force diagrams (i.e. for a beam under CBF or internal element loading). Internal forces and moments are output at intervals of 1/10th of the element length by specifying the Gauss point option from the Output button of the LUSAS Datafile dialog.
- 6. The end releases for this element allow a joint to be modelled between adjacent elements. These joints allow rotation and translation of one beam with respect to another without load transferral. The rotations and translations remain in the local directions of the beam elements and support large deformations
- OPTION 36 is only applicable for use with element load types ELDS and UDL. Specifying this option makes these element loads follow the element geometry as the analysis progresses.
- 8. OPTION 229 considers large displacements and large rotations using a co-rotational formulation. When both options 87 and 229 are true, a local Total Lagrangian formulation will be used within a global co-rotational framework. Note that OPTION 87 has no effect when specified without OPTION 229.
- 9. The P-Delta formulation is only applicable to lower order (2-noded) beams, higher order beams used in a P-Delta analysis will default to co-rotational GNL.
- 10. The Smoothed Multi Crack Concrete Model (109) can be used with this element, however, due to the "plane sections remaining plane" hypothesis, crack widths cannot be computed.

11. Partial fixities and rigid ends are defined via the ELEMENT TOPOLOGY data and follow on the same line after the end releases, for example:

1 1 2 3 R F F R R R K
$$\hat{k}_{12} \hat{k}_{13} [r_1 r_2 \lambda m_1 m_2]$$

or
1 1 2 3 R F F R R R N $n_{12} n_{13} [r_1 r_2 \lambda m_1 m_2]$

The character K is used to identify that the partial fixity stiffnesses $\hat{k}_{12} \hat{k}_{13}$ are being

explicitly defined, while the character N signifies that fixity factors, n_{12} n_{13} are being defined. The fixity factors are used as follows:

$$\hat{k}_{ij} = \frac{n_{ij}}{1 - n_{ij}} \, \tilde{k}_{ij}$$

The value of the factor n_{ij} ranges from zero for a pinned connection to 1.0 for a fully fixed connection.

The values r_1 and r_2 are the rigid end lengths at nodes 1 and 2 and λ is the rigidity factor (1.0 = fully rigid, the default). The factors m1 and m2 dictate how much mass to include for the rigid ends, full mass = 1.0 (default $m_1=m_2=0.0$).

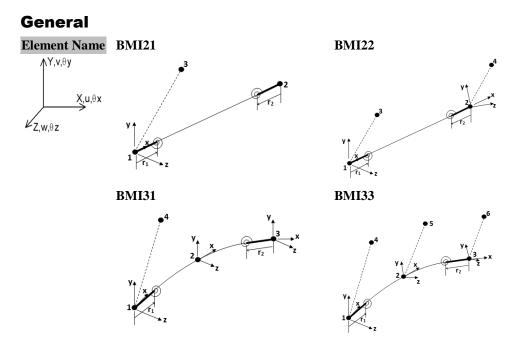
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature

Recommendations on Use

The element may be used for linear and nonlinear analysis of two dimensional beam, frame and arch structures.

3D Thick Beam Elements



Element Group	Beams
Element	Thick Beams
Subgroup	
Element	Straight and curved isoparametric degenerate thick beam elements in 3D
Description	for which shearing deformations are included. The elements can
	accommodate varying geometric properties along the length. BMI22 and
	BMI33 can consider initial twist.
Number Of	3 (BMI21), 4 (BMI22 and BMI31) and 6 (BMI33) with end release
Nodes	conditions.
	The orientation node(s) (3rd node of BMI21, 3rd and 4th nodes of
	BMI22, 4th node of BMI31, 4th, 5th and 6th nodes of BMI33) are used to define the local xy-plane.
Encodores	• 1
Freedoms	U, V, W, θx , θy , θz : at each active node.
End Releases	The element node numbers should be followed by: R restrained (default),
	F free defined in the order U, V, W, θx , θy , θz at node 1 and then U, V,
	W, θx , θy , θz at node 2 and node 3 (only for BMI31 and BMI33) related
	to local element axes (see Notes, Assumptions and Limitations).

Partial fixity	Partial fixity at each end node can be defined for all freedoms; this can take the form of a fixity reduction factor or an explicitly defined stiffness value. Partial fixities are defined with respect to the local element axes (see Notes, Assumptions and Limitations).
Rigid ends	Rigid lengths r_1 and r_2 measured from each end node can be specified for these elements. If these lengths are non zero then any end release or partial fixity is applied at the inner point defining the rigid end. A rigidity factor (1.0> λ >0.0) can be specified to make the ends semi-rigid, and options to include/exclude the masses of the rigid ends are also provided (see Notes, Assumptions and Limitations).
Node	X, Y, Z: at each node.
Coordinates	

Geometric Properties

A, Iyy, Izz, Jxx, Asz, Asy, Iyz, ez, ey SF1,SF2,SF3,SF4,SF5,SF6,SF7,SF8,SF9 MF1,MF2,MF3,MF4, MF5,MF6,MF7,MF8,MF9	
Α	Cross sectional area.
Iyy, Izz	2nd moment of area about local y, z directions (see <u>Definition</u>).
Jxx	Torsional constant.
Asz, Asy	Effective shear areas on local yz plane in local z, y directions (see <u>shear areas</u>).
Iy, Iz	1st moment of area about local y, z directions (see Definition).
Iyz	Product moment of area about local y, z axes (see Definition).
ez	Eccentricity from beam xy-plane to nodal line. (+ve in the +ve local z direction). (See Notes)
ey	Eccentricity from beam xz-plane to nodal line. (+ve in the +ve local y direction). (See Notes)

Note: For MATERIAL MODEL 29 additional geometric properties are appended to the previous 22 (BMI21 and BMI22) or 33 (BMI31 and BMI33) geometric properties (see Assumptions and Limitations).

Material Properties

Linear Isotropic: Rigidities: MATERIAL PROPERTIES (Elastic: Isotropic) RIGIDITIES 6 (Rigidities: Beam)

Matrix	Not applicable	
Joint	Not applicable	
Concrete	Not applicable	
Elasto-Plastic	Stress resultant:	MATERIAL PROPERTIES NONLINEAR 29 (Elastic: Isotropic, Plastic: Resultant) (ifcode=1 or 2, see Assumptions and Limitations)
Сгеер	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO Code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB-FIP (Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE
	IRC	(Concrete creep model to EUROCODE_2) MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC Code of Practice)
Viscoelastic	Not applicable Not applicable	
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Generic Polymer	Not applicable Not applicable Not applicable	
Loading Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, W, θx , θy , θz : at
		antine we dea

Concentrated CL Loads active nodes. Concentrated loads in global directions. Px, Py, Pz, Mx, My, Mz: at active nodes.

Element Loads	ELDS	Element loads on nodal line (load type number LTYPE *10 defines the corresponding element load type on beam axis, see Assumptions and Limitations)
		(see Assumptions and Limitations)
		LTYPE, S1, Px, Py, Pz, Mx, My, Mz
		LTYPE=11: point loads and
		moments in local directions.
		LTYPE=12: point loads and
		moments in global directions.
		LTYPE, 0, Wx, Wy, Wz, Mx, My, Mz
		LTYPE=21: uniformly distributed
		loads in local directions.
		LTYPE=22: uniformly distributed
		loads in global directions (Mx=0).
		LTYPE=23: uniformly distributed
		projected loads in global directions.
		LTYPE, S1, Wx1, Wy1, Wz1, Mx1, My1,
		Mz1, S2, Wx2, Wy2, Wz2, Mx2,
		My2, Mz2 LTYPE=31: distributed loads in
		local directions.
		LTYPE=32: distributed loads in
		global directions.
		LTYPE=33: distributed projected
		loads in global directions.
		LTYPE, S1, Wx, Wy, Wz, Mx, My, Mz
		LTYPE=41: trapezoidal loads in local directions.
		LTYPE=42: trapezoidal loads in
		global directions.
		LTYPE=43: trapezoidal projected
		loads in global directions.
Distributed Loads	UDL	Uniformly distributed loads. Wx, Wy, Wz,
		Mx, My, Mz: local forces and moments / unit length for element (see Assumptions
		and Limitations).
	FLD, FLDG	Not applicable.
Body Forces		Constant body forces for Element. Xcbf,
Douy Porces	CDI	Yebf, Zebf, Ωx , Ωy , Ωz , αx , αy , αz
	BFP, BFPE	Body force potentials at nodes/for element. ϕ_1 , ϕ_2 , ϕ_3 , 0, Xcbf, Ycbf, Zcbf
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Acceleration. Ax, Ay, Az: at nodes
	-	······································

Initial Stress/Strains	SSI, SSIE	Initial stresses/strains at nodes/for element. Fx, Fy, Fz, Mx, My, Mz: axial force, shear forces, torque and moments in local
		directions. εx , εy , εz , ψx , ψy , ψz : axial, shear and flexural strains in local directions.
	SSIG	Initial stresses/strains at Gauss points. These stresses/strains are specified in the same manner as SSI and SSIE.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. Resultants (for material model 29). Fx, Fy, Fz, Mx, My, Mz: axial force, shear forces, torque and moments in local directions.
	SSRG	Residual stresses at Gauss points. These stresses are specified in the same manner as SSR and SSRE.
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. Fx, Fy, Fz, Mx, My, Mz: axial force, shear forces, torque and moments in local directions. Ex, Ey, Ez, ψ x, ψ y, ψ z: axial,
		shear and flexural strains in local directions.
	TSSIG	Target stresses/strains at Gauss points. These stresses/strains are specified in the same manner as TSSIE and TSSIA.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, dT/dy, dT/dz, To, 0, dTo/dy, dTo/dz in local directions
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent Loads	Not applicable.	

LUSAS Output

Solver	Stress resultants (default): Fx, Fy, Fz, Mx, My, Mz: axial force, shear
	forces, torque and moments in local directions.
	Strain: εx , εy , εz , ψx , ψy , ψz : Axial, shear, torsional and flexural strains in local directions.

By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal axes.

Modeller See Results Tables (Appendix K).

Local Axes

□ Standard line element For each element/active node, the local xy-plane is defined by the local x-axis and the orientation node. The local y-axis is perpendicular to the local x-axis and positive on the side of the element where the orientation node lies. The local y and z-axes form a right-handed set with the local x-axis. See Local Element <u>Axes</u> for details

Sign Convention

□ Standard beam element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and large rotations (see Notes)
Updated	Not applicable.
Lagrangian	
Eulerian	Not applicable.
Co-rotational	For large displacements and large rotations
P-Delta	Displacements and rotations should be small (see Notes)

Integration Schemes

Stiffness	Default.	1-point (BMI21 and BMI22), 2-point (BMI31 and BMI33).
	Fine.	Same as default.
Mass	Default.	2-point (BMI21 and BMI22), 3-point (BMI31 and BMI33).
	Fine.	Same as default.

Note: A 3-point <u>Newton-Cotes integration</u> rule is also available for BMI31 and BMI33 using OPTION 134. This may be more applicable for infinitesimal strain, elasto-plastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory Manual.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- 36 Follower loads
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity (see Notes).
- **102** Switch off load correction stiffness matrix due to centripetal acceleration
- 105 Lumped mass matrix.
- **134** Gauss to <u>Newton-Cotes</u> in plane (in the local x direction) integration for elements
- 157 Material model 29 (non cross-section elements), see Notes.
- 229 Co-rotational geometric nonlinearity.
- **403** Introduce residual bending flexibility correction for 2-node thick beam BMI21, see Assumptions and Limitations (on by default).
- **404** Compute equivalent nodal loading from equilibrium considerations for 2-node thick beam BMI21, see Assumptions and Limitations.
- 405 Specify geometric properties along beam centroidal axes (on by default).
- **406** Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
- 418 Output stress resultants relative to beam centroidal axes for eccentric elements
- 421 P-Delta analysis, see Notes
- 432 Use P-Delta geometric stiffness matrix of thick beams for linear buckling analysis

Notes, Assumptions and Limitations

- 1. The element is formulated from the so-called degenerate continuum concept, i.e. enforcing directly the modified Timoshenko hypothesis for thick beams to the continuum theory. Plane cross-sections initially normal to the beam axis remain plane and undistorted (the shape of the cross-section remains unchanged) under deformation, but do not necessarily remain normal to the beam axis; the shear centre and centroid of cross-section coincide. Shearing deformations are included. The basic kinematic assumptions correspond to the Timoshenko beam theory and do not allow for warping effects in torsion. Although warping effects can be considered approximately by using real torsional constants, inaccuracies are likely to occur when eccentricity is present.
- 2. Input of geometric properties (OPTION 405) and loads (OPTION 406), and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axes. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line.

- 3. When OPTION 403 is specified to introduce residual bending flexibility correction (on by default), for BMI21 and BMI22, the axial force and torsion are constant, while shear forces and moments vary linearly along the length of the beam. For BMI31 and BMI33 the axial force, shear forces, moments and torsion all vary linearly along the length.
- 4. When BMI21 is used together with OPTION 403 to introduce residual bending flexibility correction, its stiffness matrix is enhanced to the order of a cubic. Note that if OPTION 403 is used with eccentrically stacked elements, slippage can occur.
- 5. When BMI21 is used together with OPTION 404, loading that varies along the element length is accounted for in the force diagrams (i.e. for a beam under CBF or internal element loading). A post-processing technique has been introduced to obtain accurate quadratic bending moments for BMI31. For BMI21 (with OPTION 404) and BMI31, internal forces and moments are output at intervals of 1/10th of the element length by specifying the Gauss point option from the Output button of the LUSAS Datafile dialog.
- 6. The end releases for this element allow a joint to be modelled between adjacent elements. These joints allow rotation and translation of one beam with respect to another without load transferral. The rotations and translations remain in the local directions of the beam elements and support large deformations.
- 7. For nonlinear material model 29 the following geometric properties are appended to those already specified (see Geometric Properties).
 - A^p , Zyy^p , Zzz^p , Zy^p , Zz^p , S^p at each node
 - A^p Plastic area (=elastic area)
 - Zyy^p, Zzz^p Plastic moduli for bending about y, z axes
 - Zy^p, Zz^p Plastic moduli for torsion about y, z axes.
 - S^p Plastic area for shear (S^p=0).

Where the fully plastic torsional moment = $\sigma y (Zy^p + Zz^p)$.

Note that if eccentricity has been specified the plastic properties must be defined with reference to the **nodal line** and **not** the beam axes, i.e. the eccentricity is not used to automatically modify the plastic properties, they must be defined via modified geometry.

For nonlinear material model 29 the following **ifcode** parameters are applicable: **ifcode=1** for circular hollow sections and **ifcode=2** for solid rectangular sections

- 9. Temperature dependent properties cannot be used with material model 29.
- 10. The <u>rigidity matrix</u> is evaluated explicitly from the geometric properties for both linear and nonlinear materials.

- 11. OPTION 36 is only applicable for use with element load types ELDS and UDL. Specifying this option makes these element loads follow the element geometry as the analysis progresses.
- 12. When a nonlinear material is used with this element the transverse shear stresses are excluded from the plasticity computations i.e. the transverse shear stresses are assumed to remain elastic. This means that if a nonlinear material is used in applications where transverse shear tends to dominate the stress field the equivalent von Mises and maximum principal stresses can exceed the uniaxial yield stress.
- 13. When a step by step dynamic analysis is carried out using BMI elements with distributed loading, the "free body force diagrams" pertaining to applied loading, are not superimposed on the nodal values, to do so would lead to erroneous results until a steady state is reached. It should therefore be noted that different force diagrams will be obtained for BMI elements if static and dynamic analyses are directly compared.
- 14. OPTION 87 considers large displacements and large rotations using a Total Lagrangian formulation; OPTION 229 considers large displacements and large rotations using a co-rotational formulation. In general the co-rotational formulation works better. When options 87 and 229 are true, a local Total Lagrangian formulation will be used together with a global co-rotational formulation.
- 15. OPTION 229 considers large displacements and large rotations using a co-rotational formulation. When both options 87 and 229 are true, a local Total Lagrangian formulation will be used within a global co-rotational framework. Note that OPTION 87 has no effect when specified without OPTION 229.
- 16. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command.
- 17. The P-Delta formulation is only applicable to lower order (2-noded) beams, higher order beams used in a P-Delta analysis will default to co-rotational GNL.
- 18. Partial fixities and rigid ends are defined via the ELEMENT TOPOLOGY data and follow on the same line after the end releases, for example:

1 1 2 3 R F R R F R R R R R R R R R R
$$\hat{k}_{12} \hat{k}_{15} [r_1 r_2 \lambda m_1 m_2]$$

or
1 1 2 3 R F R R F R R R R R R R R R N $n_{12} n_{15} [r_1 r_2 \lambda m_1 m_2]$

The character K is used to identify that the partial fixity stiffnesses $\hat{k}_{12} \hat{k}_{13}$ are being explicitly defined, while the character N signifies that fixity factors, $n_{12} n_{13}$ are being defined. The fixity factors are used as follows:

$$\hat{k}_{ij} = \frac{n_{ij}}{1 - n_{ij}} \tilde{k}_{ij}$$

The value of the factor n_{ij} ranges from zero for a pinned connection to 1.0 for a fully fixed connection.

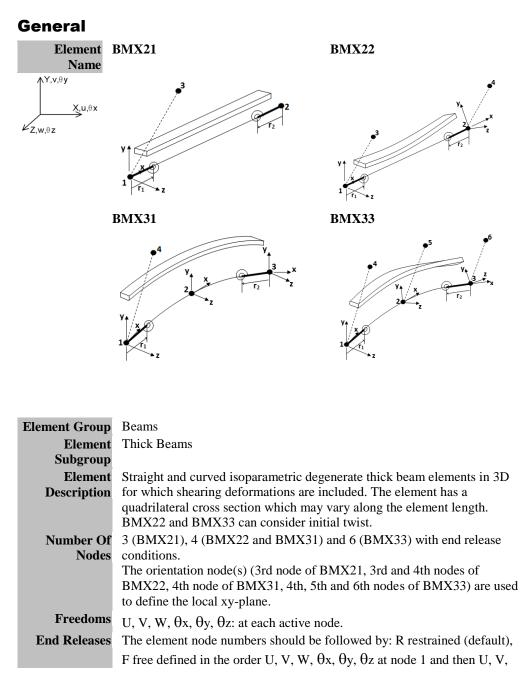
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature

Recommendations on Use

• The elements may be used for linear and material nonlinear analysis of three dimensional beam, frame and arch structures, and can also be used to model cables in cable stayed structures. BMI21 and BMI22 may also be used as a stiffener for the QTS4 shell element; while BMI31 and BMI33 may be used as a stiffener for the QTS8 shell element, e.g. space frames.

3D Thick Beam Elements with Quadrilateral Cross-Section

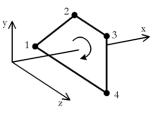


Partial fixity	W, θx , θy , θz at node 2 and node 3 (only for BMX31 and BMX33) related to local element axes (see Notes). Partial fixity at each end node can be defined for all freedoms; this can take the form of a fixity reduction factor or an explicitly defined stiffness value. Partial fixities are defined with respect to the local element axes (see Notes, Assumptions and Limitations).
Rigid ends	
Node Coordinates	X, Y, Z: at each node.

Geometric Properties

y1, z1, y2, z2, y3, z3, y4, z4: local cross section coordinate pairs at each node; followed by nt12, nt14: number of <u>Newton-Cotes</u> integration points in the direction defined by the local cross-section points 1-2 and 1-4 (zero indicates default values). Multiple quadrilateral cross-sections can be used to build up complex beam cross-sections.

Note. The corners of the quadrilateral are numbered clockwise about the local x-axis (the beam nodal line), that is, a right-hand screw rule in the direction of increasing x.



Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
Matrix	Not applicable	
Joint	Not applicable	
Concrete		MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi Crack Concrete)
Elasto-Plastic	Stress resultant: Tresca:	Not applicable. MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker-Prager:	MATERIAL PROPERTIES NONLINEAR 64

	Mohr-Coulomb:	(Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular) MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Optimised Implicit Von Mises:	MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic)
	Volumetric Crushing:	Not applicable.
G	Stress Potential	STRESS POTENTIAL VON_MISES (Isotropic: von Mises, Modified von Mises)
Creep	AASHTO	CREEP PROPERTIES (Creep) MATERIAL PROPERTIES NONLINEAR 86 AASHTO
		(Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB-FIP (Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2)
	IRC	(Concrete creep model to LOROCODE_2) MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic Shrinkage	Not applicable	SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Generic Polymer	Not applicable Not applicable Not applicable	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, W, θx , θy , θz : at active nodes.
Concentrated Loads	CL	Concentrated loads in global directions. Px, Py, Pz, Mx, My, Mz: at active nodes (global).
Element Loads	ELDS	Element loads on nodal line (load type number LTYPE *10 defines the corresponding element load type on beam axis, see Assumptions and Limitations) LTYPE, S1, Px, Py, Pz, Mx, My, Mz LTYPE=11: point loads and moments in local directions. LTYPE=12: point loads and moments in global directions.
		LTYPE, 0, Wx, Wy, Wz, Mx, My, Mz LTYPE=21: uniformly distributed loads in local directions. LTYPE=22: uniformly distributed loads in global directions (Mx=0). LTYPE=23: uniformly distributed projected loads in global directions.
		LTYPE, S1, Wx1, Wy1, Wz1, Mx1, My1, Mz1, S2, Wx2, Wy2, Wz2, Mx2, My2, Mz2 LTYPE=31: distributed loads in local directions. LTYPE=32: distributed loads in global directions. LTYPE=33: distributed projected loads in global directions.
		LTYPE, S1, Wx, Wy, Wz, Mx, My, Mz LTYPE=41: trapezoidal loads in local directions. LTYPE=42: trapezoidal loads in global directions. LTYPE=43: trapezoidal projected loads in global directions.
Distributed Loads	UDL	Uniformly distributed loads. Wx, Wy, Wz, Mx, My, Mz: local forces and moments / unit length for element in local directions. See Assumptions and Limitations.

	FLD	Not applicable.
Body Forces	CBF	Constant body forces for Element. Xcbf,
		Yebf, Zebf, Ωx , Ωy , Ωz , αx , αy , αz
	BFP, BFPE	Body force potentials at nodes/for element.
		φ1, φ2, φ3, 0, Xcbf, Ycbf, Zcbf
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Acceleration. Ax, Ay, Az: at nodes
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element.
Stress/Strains		Components: Fx, Fy, Fz, Mx, My, Mz, &x,
		εy, εz, ψx, ψy, ψz, (σx, σxy, σxz ,εx,
		Exy, Exz) Bracketed terms repeated for each fibre integration point.
	SSIG	Initial stresses/strains at Gauss points. These stresses/strains are specified in the same manner as SSI and SSIE.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. Components: 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0,
		0, (σx , σxy , σxz) Bracketed terms repeated for each fibre integration point.
	SSRG	Residual stresses at Gauss points. These stresses are specified in the same manner as SSR and SSRE.
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element.Components: Fx, Fy, Fz, Mx, My,
		Mz, εx, εy, εz, ψx, ψy, ψz, (σx, σxy,
		σ xz , ε x, ε xy, ε xz) Bracketed terms repeated for each fibre integration point.
	TSSIG	Target stresses/strains at Gauss points. These stresses/strains are specified in the same manner as TSSIE and TSSIA.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, dT/dy, dT/dz, To, 0, dTo/dy, dTo/dz in local directions
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent Loads	Not applicable.	

LUSAS Output

Solver Stress resultants (default): Fx, Fy, Fz, Mx, My, Mz: axial force, shear forces, torque and moments in local directions.
Continuum stresses (OPTION 172): σx, σxy, σxz: in local directions.
Strain: εx, εy, εz, ψx, ψy, ψz: Axial, shear, torsional and flexural strains in local directions.
Continuum strains (OPTION 172): εx, εxy, εxz: in local directions.
By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal axes.

Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

Standard line element For each element/active node, the local xy-plane is defined by the local x-axis and the orientation node. The local y-axis is perpendicular to the local x-axis and positive on the side of the element where the orientation node lies. The local y and z-axes form a right-handed set with the local x-axis. See Local Element Axes for details

Sign Convention

□ Standard beam element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and rotations (see Notes)
Updated	Not applicable.
Lagrangian	
Eulerian	Not applicable.
Corotational	For large displacements and rotations
P-Delta	Displacements and rotations should be small (see Notes)

Integration Schemes

Stiffness	Default.	1-point (BMX21 and BMX22), 2-point (BMX31 and BMX33).
	Fine.	Same as default.
Mass	Default.	2-point (BMX21 and BMX22), 3-point (BMX31 and BMX33).

Fine. Same as default.

Note: A 3-point <u>Newton-Cotes integration</u> rule is also available for BMX31 and BMX33 using OPTION 134. This may be more applicable for infinitesimal strain, elasto-plastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory Manual.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- 36 Follower loads
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity (see Notes).
- 102 Switch off load correction stiffness matrix due to centripetal acceleration
- 105 Lumped mass matrix.
- **134** Gauss to <u>Newton-Cotes</u> in plane (in the local x direction) integration for elements.
- 139 Output yielded integration points only.
- 172 Form the <u>rigidity matrix</u> by numerical cross section integration.
- **229** Co-rotational geometric nonlinearity.
- **403** Introduce residual bending flexibility correction for 2-node thick beam BMI21, see Assumptions and Limitations (on by default).
- **404** Compute equivalent nodal loading from equilibrium considerations for 2-node thick beam BMX21, see Notes (on by default).
- 406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
- 418 Output stress resultants relative to beam centroidal axes for eccentric elements
- 421 P-Delta analysis, see Notes
- 432 Use P-Delta geometric stiffness matrix of thick beams for linear buckling analysis

Notes, Assumptions and Limitations

- 1. The element is formulated from the so-called degenerate continuum concept, i.e. enforcing directly the modified Timoshenko hypothesis for thick beams to the continuum theory. Plane cross-sections initially normal to the beam axis remain plane and undistorted (the shape of the cross-section remains unchanged) under deformation, but do not necessarily remain normal to the beam axis; the shear centre and centroid of cross-section coincide. Shearing deformations are included.
- 2. Input of loads (OPTION 406) and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axis. CL is always input with respect to the nodal

line; displacements are output with respect to the nodal line. Fiber stress/strain results are output at the actual location.

- 3. When OPTION 403 is specified to introduce residual bending flexibility correction (on by default), for BMX21 and BMX22, the axial force and torsion are constant, while shear forces and moments vary linearly along the length of the beam. For BMX31 and BMX33 the axial force, shear forces, moments and torsion all vary linearly along the length.
- 4. When BMX21 is used together with OPTION 403 to introduce residual bending flexibility correction, its stiffness matrix is enhanced to the order of a cubic. Note that if OPTION 403 is used with eccentrically stacked elements, slippage can occur.
- 5. When BMX21 is used together with OPTION 404, loading that varies along the element length is accounted for in the force diagrams (i.e. for a beam under CBF or internal element loading). Internal forces and moments are output at intervals of 1/10th of the element length by specifying the Gauss point option from the Output button of the LUSAS Datafile dialog.
- 6. The end releases for this element allow a joint to be modelled between adjacent elements. These joints allow rotation and translation of one beam with respect to another without load transferral. The rotations and translations remain in the local directions of the beam elements and support large deformations.
- Computation of the <u>rigidity matrix</u> by integration through the cross-section depth of the beam is necessary for all nonlinear material models. By default OPTION 172 is invoked automatically and a 5*5 point <u>Newton-Cotes integration</u> rule is used. This allows the output of stresses at the numerical cross section integration points.
- By default, the <u>rigidity matrix</u> is evaluated explicitly for linear materials. A 3*3 point <u>Newton-Cotes integration</u> rule may be invoked using OPTION 172. Numerical cross section integration enables top, middle and bottom stress output.
- 9. OPTION 36 is only applicable for use with element load types ELDS and UDL. Specifying this option makes these element loads follow the element geometry as the analysis progresses.
- 10. For nonlinear material models, fibre integration is used across the cross-sectional area of the beam. Only axial deformation is considered in the plasticity computations, any torsional deformation is assumed to remain elastic.
- 11. OPTION 229 considers large displacements and large rotations using a co-rotational formulation. When both options 87 and 229 are true, a local Total Lagrangian formulation will be used within a global co-rotational framework. Note that OPTION 87 has no effect when specified without OPTION 229.
- 12. The P-Delta formulation is only applicable to lower order (2-noded) beams, higher order beams used in a P-Delta analysis will default to co-rotational GNL.

- 13. The Smoothed Multi Crack Concrete Model (109) can be used with this element, however, due to the "plane sections remaining plane" hypothesis, crack widths cannot be computed.
- 13. The Partial fixities and rigid ends are defined via the ELEMENT TOPOLOGY data and follow on the same line after the end releases, for example:

1 1 2 3 R F R R F R R R R R R R R R R
$$K$$
 \hat{k}_{12} \hat{k}_{15} $[r_1 r_2 \lambda m_1 m_2]$
or
1 1 2 3 R F R R F R R R R R R R R N n_{12} n_{15} $[r_1 r_2 \lambda m_1 m_2]$

The character K is used to identify that the partial fixity stiffnesses $\hat{k}_{12} \hat{k}_{15}$ are being

explicitly defined, while the character N signifies that fixity factors, n_{12} n_{15} are being defined. The fixity factors are used as follows:

$$\hat{k}_{ij} = \frac{n_{ij}}{1 - n_{ij}} \tilde{k}_{ij}$$

The value of the factor n_{ij} ranges from zero for a pinned connection to 1.0 for a fully fixed connection.

The values r_1 and r_2 are the rigid end lengths at nodes 1 and 2 and λ is the rigidity factor (1.0 = fully rigid, the default). The factors m1 and m2 dictate how much mass to include for the rigid ends, full mass = 1.0 (default $m_1=m_2=0.0$).

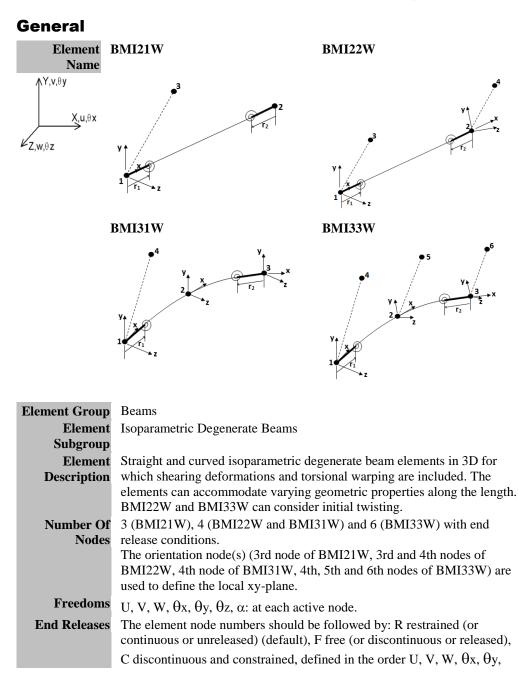
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- BMX22 and BMX33 elements are not available for selection currently within LUSAS Modeller.

Recommendations on Use

• The elements may be used for linear and nonlinear analysis of three dimensional beam, frame and arch structures. BMX21 and BMX22 may also be used as a stiffener for the QTS4 shell element; while BMX31 and BMX33 may be used as a stiffener for the QTS8 shell element.

3D Thick Beam Elements with Torsional Warping



Partial fixity	θ z at node 1 and then U, V, W, θ x, θ y, θ z at at node 2 and node 3 (only for BMI31W and BMI33W) related to local element axes (see Notes, Assumptions and Limitations).). Partial fixity at each end node can be defined for all freedoms; this can
r ar tiar fixity	take the form of a fixity reduction factor or an explicitly defined stiffness value. Partial fixities are defined with respect to the local element axes
	(see Notes, Assumptions and Limitations).
Rigid ends	Rigid lengths r_1 and r_2 measured from each end node can be specified for
	these elements. If these lengths are non zero then any end release or partial fixity is applied at the inner point defining the rigid end. A rigidity
	factor $(1.0 > \lambda > 0.0)$ can be specified to make the ends semi-rigid, and options to include/exclude the masses of the rigid ends are also provided
	(see Notes, Assumptions and Limitations).
Node	X, Y, Z: at each node.
Coordinates	

Geometric Properties

A, Iyy, Izz, Jxx, Asz, Asy, Iy, Iz, Iyz, Cw, Cwy, Cwz, Iyr, Izr, Irr, Iwr (default) or A, Iyy, Izz, Jxx,	At each node
Asz, Asy, ez, ey, Iyz, Cw, zo, yo, Iyr, Izr, Irr, Iwr (option 405)	
SF1,SF2,SF3,SF4,SF5,SF6,SF7,SF8, SF9, SF10,SF11,SF12,SF13, SF14,SF15,SF16	properties in the calculation of the stiffness and mass
MF1,MF2,MF3,MF4,MF5,MF6,MF 7,MF8, MF9,MF10,MF11,MF12,MF13,MF	
14,MF15,MF16 A	Cross sectional area.
Jxx	Torsional constant.
Asz, Asy	Effective shear areas on local yz plane in local z, y directions (see shear areas).
Iy, Iz	1st moment of area about local y, z directions (see <u>Definition</u>).
Iyz	Product moment of area about local y, z axes (see <u>Definition</u>).
Cw	Warping constant (see <u>Definition</u>).
Cwy, Cwz	1st moment of warping about local y, z directions

(see **<u>Definition</u>**).

ez	Eccentricity from beam xy-plane to nodal line. (+ve
	in the +ve local z direction). (See Notes)

- **ey** Eccentricity from beam xz-plane to nodal line. (+ve in the +ve local y direction). (See Notes)
- **Zo** z-coordinate of the shear center with respect to the centroid (+ve in +ve local z-direction)
- **Yo** y-coordinate of the shear center with respect to the centroid (+ve in +ve local y-direction)

Iyr, Izr, Irr, Iwr Wagner constants. (See Notes)

Material Properties

	Isotropic: Rigidities: Not applicable Not applicable Not applicable	MATERIAL PROPERTIES (Elastic: Isotropic) RIGIDITIES 6 (Rigidities: Beam)
Elasto-Plastic	Stress resultant:	MATERIAL PROPERTIES NONLINEAR 29
	Sitess resultant.	(Elastic: Isotropic, Plastic: Resultant) (ifcode=1 or 2, see Assumptions and Limitations)
Creep	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB-FIP (Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of

Damage	Not applicable
Viscoelastic	Not applicable
Shrinkage	

RubberNot applicableGeneric PolymerNot applicableCompositeNot applicable

Practice)

SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER

Loading

- -		
Prescribed Value	PDSP, IPDSP	Prescribed variable. U, V, W, θx , θy , θz , α : at active nodes.
Concentrated Loads	CL	Concentrated loads in global directions. Px, Py, Pz, Mx, My, Mz, Mb: at active nodes.
Element Loads	ELDS	 Element loads on nodal line (load type number LTYPE *10 defines the corresponding element load type on beam axis, see Assumptions and Limitations) (see Assumptions and Limitations) LTYPE, S1, Px, Py, Pz, Mx, My, Mz LTYPE=11: point loads and moments in local directions. LTYPE=12: point loads and moments in global directions. LTYPE, 0, Wx, Wy, Wz, Mx, My, Mz LTYPE=21: uniformly distributed loads in local directions. LTYPE=22: uniformly distributed loads in global directions (Mx=0). LTYPE=23: uniformly distributed projected loads in global directions. LTYPE, S1, Wx1, Wy1, Wz1, Mx1, My1, Mz1, S2, Wx2, Wy2, Wz2, Mx2, My2, Mz2 LTYPE=31: distributed loads in local directions. LTYPE=32: distributed loads in global directions. LTYPE=33: distributed projected loads in global directions.
		global directions. LTYPE, S1, Wx, Wy, Wz, Mx, My, Mz LTYPE=41: trapezoidal loads in local
		directions.

		LTYPE=42: trapezoidal loads in global directions.
		LTYPE=43: trapezoidal projected loads in global directions.
	DLDL, DLDG	Not applicable.
	DLEL,DLEG	Not applicable.
	PLDL, PLDG	Not applicable.
Distributed Loads	UDL	Uniformly distributed loads. Wx, Wy, Wz, Mx, My, Mz: local forces and moments / unit length for element (see Assumptions and Limitations).
	FLD, FLDG	Not applicable.
Body Forces	CBF	Constant body forces for Element. Xcbf, Ycbf, Zcbf,
		$\Omega x, \Omega y, \Omega z, \alpha x, \alpha y, \alpha z$
	BFP, BFPE	Body force potentials at nodes/for element. φ 1, φ 2,
		φ3, 0, Xcbf, Ycbf, Zcbf
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Acceleration. Ax, Ay, Az: at nodes
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element. Fx, Fy,
Stress/Strains		Fz, Mx, My, Mz, 0, 0: axial force, shear forces,
		torque and moments in local directions. Ex, Ey, Ez,
		ψx , ψy , ψz , 0, 0: axial, shear and flexural strains in local directions.
	SSIG	Initial stresses/strains at Gauss points. These stresses/strains are specified in the same manner as SSI and SSIE.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. Resultants (for material model 29). Fx, Fy, Fz, Mx, My, Mz: axial force, shear forces, torque and moments in local directions.
	SSRG	Residual stresses at Gauss points. These stresses are specified in the same manner as SSR and SSRE.
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. Fx, Fy, Fz, Mx, My, Mz, 0,0: axial force, shear forces,
		torque and moments in local directions. Ex, Ey, Ez,
		ψx , ψy , ψz , 0, 0: axial, shear and flexural strains in local directions.
	TSSIG	Target stresses/strains at Gauss points. These stresses/strains are specified in the same manner as TSSIE and TSSIA.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, dT/dy, dT/dz, To, 0, dTo/dy, dTo/dz in local directions

OverburdenNot applicable.Phreatic SurfaceNot applicable.Field LoadsNot applicable.Temp DependentNot applicable.Loads

LUSAS Output

Solver Force (default): Fx, Fy, Fz, Mx, My, Mz, Fb, Mb: axial force, shear forces, torque, moments, bishear (or warping torsion) and bimoment in local directions.
 Strain: εx, εy, εz, ψx, ψy, ψz, α, α': axial, shear, torsional, flexural strains and torsional warping strains in local directions. By default element output is with respect to the nodal line. Option 380 outputs stress/strain resultants with respect to the beam centreline.
 Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

□ Standard line element For each element/active node, the local xy-plane is defined by the local x-axis and the orientation node. The local y-axis is perpendicular to the local x-axis and positive on the side of the element where the orientation node lies. The local y and z-axes form a right-handed set with the local x-axis. See Local Element Axes for details

Sign Convention

□ Standard beam element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements, large rotations and small strains (see Notes).		
Updated	Not applicable.		
Lagrangian			
Eulerian	Not applicable.		
Co-rotational	For large displacements, large rotations and small strains.		
P-Delta	Displacements and rotations should be small (see Notes)		

Integration Schemes

Stiffness	Default.	1-point (BMI21W and BMI22W), 2-point (BMI31W and BMI33W).
	Fine.	Same as default.
Mass	Default.	2-point (BMI21W and BMI22W), 3-point (BMI31W and BMI33W).
	Fine.	Same as default.

Note: A 3-point <u>Newton-Cotes integration</u> rule is also available for BMI31W and BMI33W using option 134. This may be more applicable for infinitesimal strain, elastoplastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory Manual

Mass Modelling

- □ Consistent mass (default).
- Lumped mass.

Options

- **36** Follower loads
- **55** Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity (see Notes).
- 102 Switch off load correction stiffness matrix due to centripetal acceleration
- 105 Lumped mass matrix.
- **134** Gauss to <u>Newton-Cotes</u> in plane (in the local x direction) integration for elements
- 157 Material model 29 (non cross-section elements), see Notes.
- 229 Co-rotational geometric nonlinearity.
- 380 Output stress/strain resultants relative to beam axes for eccentric elements.
- **403** Introduce residual bending flexibility correction for 2-node thick beam BMI21, see Assumptions and Limitations.
- **404** Compute equivalent nodal loading from equilibrium considerations for 2-node thick beam BMI21, see Assumptions and Limitations.
- **405** Specify geometric properties along beam centroidal axes
- 406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
- 421 P-Delta analysis, see Notes
- 424 Include the Wagner effect in the large deformation formulation for beams
- **432** Use P-Delta geometric stiffness matrix of thick beams for linear buckling analysis

Notes, Assumptions and Limitations

- 1. The element is formulated from the so-called degenerate continuum concept, i.e. enforcing directly the modified Timoshenko hypothesis for thick beams to the continuum theory. Shearing deformations and torsional warping are included.
- 2. By default input of geometric properties and loads, and output of element stress/strain resultants are with respect to the nodal line. Option 405 inputs geometric properties, option 406 inputs loads, and option 380 outputs stress/strain resultants with respect to the beam centreline. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line.
- 3. When OPTION 403 is specified to introduce residual bending flexibility correction (on by default), for BMI21W and BMI22W, the axial force, bishear, bimoment and torsion are constant, while the other shear forces and moments vary linearly along the length of the beam. For BMI31W and BMI33W the axial force, all shear forces, all moments and torsion vary linearly along the length
- 4. When BMI21W is used together with OPTION 403 to introduce residual bending flexibility correction, its stiffness matrix is enhanced to the order of a cubic.
- 5. When BMI21W is used together with OPTION 404, loading that varies along the element length is accounted for in the force diagrams (i.e. for a beam under CBF or internal element loading). Internal forces and moments are output at intervals of 1/10th of the element length by specifying the Gauss point option from the Output button of the LUSAS Datafile dialog.
- 6. The end releases for this element allow a joint to be modelled between adjacent elements. These joints allow rotation and translation of one beam with respect to another without load transferral as well as different warping conditions in adjacent elements. The rotations and translations remain in the local directions of the beam elements and support large deformations.
- 7. The <u>rigidity matrix</u> is evaluated explicitly from the geometric properties for both linear and nonlinear materials.
- 8. Option 36 is only applicable for use with element load types ELDS and UDL. Specifying this option makes these element loads follow the element geometry as the analysis progresses.
- 9. For large deformation analyses the following geometric properties (Wagner constants) are required (see Geometric Properties) if Option 424 = T: Iyr, Igr, Irr and Iwr at each node. If these constants are set to zero, the Wagner effect will be ignored, and the results may not be correct if twist rotations are not small.
- 10. When a step by step dynamic analysis is carried out using BMI elements with distributed loading, the "free body force diagrams" pertaining to applied loading, are not superimposed on the nodal values, to do so would lead to erroneous results until a steady state is reached. It should therefore be noted that different force diagrams will be obtained for BMI elements if static and dynamic analyses are directly compared.

- 11. OPTION 229 considers large displacements and large rotations using a co-rotational formulation. When both options 87 and 229 are true, a local Total Lagrangian formulation will be used within a global co-rotational framework. Note that OPTION 87 has no effect when specified without OPTION 229.
- 12. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command.
- 13. The P-Delta formulation is only applicable to lower order (2-noded) beams, higher order beams used in a P-Delta analysis will default to co-rotational GNL.
- 14. Partial fixities and rigid ends are defined via the ELEMENT TOPOLOGY data and follow on the same line after the end releases, for example:

The character K is used to identify that the partial fixity stiffnesses $\hat{k}_{12} \hat{k}_{15}$ are being

explicitly defined, while the character N signifies that fixity factors, n_{12} n_{15} are being defined. The fixity factors are used as follows:

$$\hat{k}_{ij} = \frac{n_{ij}}{1 - n_{ij}} \tilde{k}_{ij}$$

The value of the factor n_{ij} ranges from zero for a pinned connection to 1.0 for a fully fixed connection.

The values r_1 and r_2 are the rigid end lengths at nodes 1 and 2 and λ is the rigidity factor (1.0 = fully rigid, the default). The factors m1 and m2 dictate how much mass to include for the rigid ends, full mass = 1.0 (default m₁=m₂=0.0).

Restrictions

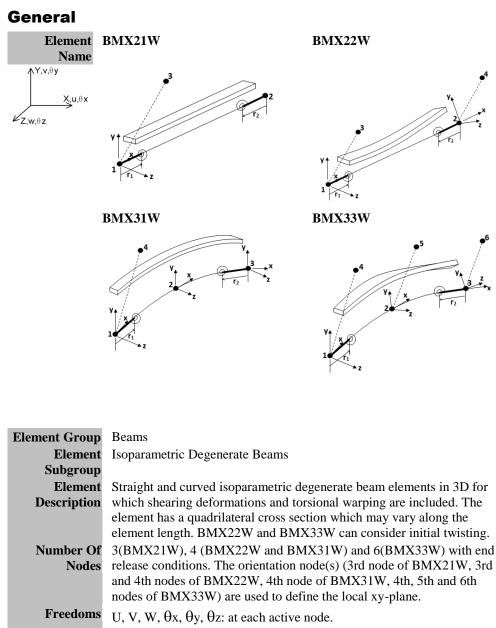
□ Ensure mid-side node centrality

- □ Avoid excessive element curvature
- □ Ensure correct warping condition at connections.

Recommendations on Use

• The elements may be used for linear and material nonlinear analysis of three dimensional beam, frame and arch structures. BMI21W and BMI22W may also be used as a stiffener for the QTS4 shell element; while BMI31W and BMI33W may be used as a stiffener for the QTS8 shell element.

3D Thick Beam Elements with Quadrilateral Cross-Section and Torsional Warping



End Releases The element node numbers should be followed by: R restrained (default),

	F free defined in the order U, V, W, θx , θy , θz at node 1 and then U, V, W, θx , θy , θz at node 2 and node 3 (only for BMX31 and BMX33) related to local element axes (see Notes).
	The element node numbers should be followed by: R restrained (or continuous or unreleased) (default), F free (or discontinuous or released),
	C discontinuous and constrained, defined in the order U, V, W, θx , θy ,
	θ_z , α and then U, V, W, θ_x , θ_y , θ_z , α at node 2 and node 3 (only for BMX31W and BMX33W) related to local element axes (see Notes).
Partial fixity	Partial fixity at each end node can be defined for all freedoms; this can take the form of a fixity reduction factor or an explicitly defined stiffness value. Partial fixities are defined with respect to the local element axes (see Notes, Assumptions and Limitations).
Rigid ends	Rigid lengths r_1 and r_2 measured from each end node can be specified for these elements. If these lengths are non zero then any end release or partial fixity is applied at the inner point defining the rigid end. A rigidity factor (1.0> λ >0.0) can be specified to make the ends semi-rigid, and options to include/exclude the masses of the rigid ends are also provided (see Notes, Assumptions and Limitations).
Node	X, Y, Z: at each node.
Coordinates	

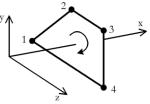
Geometric Properties

y1, z1, y2, z2, y3, z3, y4, z4: local cross section coordinate pairs for a triangle at each node; followed by nt12, nt14: specifying the number of integration points nt12* nt14 (the value nt12* nt14 determines the integration rule no matter what the values nt12 and nt14 are except when nt12* nt14 = 7, nt12 = 1 defines a cubic rule, while nt12 = 7 defines a quintic rule)

or

y1, z1, y2, z2, y3, z3, y4, z4: local cross section coordinate pairs for a quadrilateral at each node; followed by nt12, nt14: specifying the number of Newton-Cotes integration points in the direction defined by the local cross-section points 1-2 and 1-4 (zero indicates default values). Multiple quadrilateral cross-sections can be used to build up complex beam cross-sections. Number of divisions for each coarse quadrilateral (default =5) can be specified for the computation of warping of cross-section

Note. The corners of the quadrilateral are numbered clockwise about the local x-axis (the beam nodal line), that is, a right-hand screw rule in the direction of increasing x.



Material Properties

Linear Matrix Joint	Isotropic: Not applicable Not applicable	MATERIAL PROPERTIES (Elastic: Isotropic)
Concrete	11	MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi Crack Concrete)
Elasto-Plastic	Stress resultant:	Not applicable.
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker-Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr-Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Optimised Implicit Von Mises:	MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic)
	Volumetric Crushing:	Not applicable.
	Stress Potential	STRESS POTENTIAL VON_MISES (Isotropic: von Mises, Modified von Mises)
Creep		CREEP PROPERTIES (Creep)
	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO
		(Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB-FIP (Concrete creep model to CEB-FIP Model
	Chinese	Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE
		(Concrete creep model to EUROCODE_2)

IRC

Damage

Viscoelastic	Not applicable
Shrinkage	

RubberNot applicableGeneric PolymerNot applicableCompositeNot applicable

MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice) DAMAGE PROPERTIES SIMO, OLIVER (Damage)

SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, W, θx , θy , θz : at active nodes.
Concentrated Loads	CL	Concentrated loads in global directions. Px, Py, Pz, Mx, My, Mz, α: at active nodes (global).
Element Loads	ELDS	Element loads on nodal line (load type number LTYPE *10 defines the corresponding element load type on beam axis, see Assumptions and Limitations) LTYPE, S1, Px, Py, Pz, Mx, My, Mz
		LTYPE=11: point loads and moments in local directions. LTYPE=12: point loads and moments in global directions.
		LTYPE, 0, Wx, Wy, Wz, Mx, My, Mz LTYPE=21: uniformly distributed loads in local directions. LTYPE=22: uniformly distributed loads in global directions (Mx=0). LTYPE=23: uniformly distributed projected loads in global directions.
		LTYPE, S1, Wx1, Wy1, Wz1, Mx1, My1, Mz1, S2, Wx2, Wy2, Wz2, Mx2, My2, Mz2 LTYPE=31: distributed loads in local directions. LTYPE=32: distributed loads in global directions. LTYPE=33: distributed projected loads in

		global directions.
		LTYPE, S1, Wx, Wy, Wz, Mx, My, Mz
		LTYPE=41: trapezoidal loads in local
		directions.
		LTYPE=42: trapezoidal loads in global
		directions.
		LTYPE=43: trapezoidal projected loads in global directions.
	DLDL, DLDG	Not applicable.
	DLEL, DLEG	Not applicable.
	PLDL, PLDG	Not applicable.
Distributed Loads		Uniformly distributed loads. Wx, Wy, Wz, Mx, My, Mz: local forces and moments / unit length for element in local directions. See Assumptions and Limitations.
	FLD, FLDG	Not applicable.
Body Forces	CBF	Constant body forces for Element. Xcbf, Ycbf, Zcbf,
		$\Omega x, \Omega y, \Omega z, \alpha x, \alpha y, \alpha z$
	BFP, BFPE	Body force potentials at nodes/for element. φ 1, φ 2,
		φ3, 0, Xcbf, Ycbf, Zcbf
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Acceleration. Ax, Ay, Az: at nodes
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element.
Stress/Strains		Components: Fx, Fy, Fz, Mx, My, Mz, 0, 0, &x,
		ε y, ε z, ψ x, ψ y, ψ z, 0, 0, (σ x, σ xy, σ xz, ε x, ε xy,
		Exz) Bracketed terms repeated for each fibre integration point.
	SSIG	Initial stresses/strains at Gauss points. These stresses/strains are specified in the same manner as SSI and SSIE.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. Components:
		0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, $(\sigma x, 0, 0)$ Bracketed terms repeated for each fibre integration point.
	SSRG	Residual stresses at Gauss points. These stresses are specified in the same manner as SSR and SSRE.
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element.Components: Fx, Fy, Fz, Mx, My, Mz, 0, 0,
		$\epsilon_x, \epsilon_y, \epsilon_z, \psi_x, \psi_y, 0, 0, \psi_z, (\sigma_x, \sigma_{xy}, \sigma_{xz}, \epsilon_x,$
		Exy, Exz) Bracketed terms repeated for each fibre
	maara	integration point.
	TSSIG	Target stresses/strains at Gauss points. These

		stresses/strains are specified in the same manner as TSSIE and TSSIA.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, dT/dy,
		dT/dz, To, 0, dTo/dy, dTo/dz in local directions
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not applicable.	
Loads		

LUSAS Output

Solver	Force (default): Fx, Fy, Fz, Mx, My, Mz, Fb and Mb: axial force, shea forces, torque, moments, bishear and bimoments in local directions.		
	Continuum stresses (OPTION 172): σx , σxy , σxz : in local directions		
	Strain: ε_x , ε_y , ε_z , ψ_x , ψ_y , ψ_z , α , α' : axial, shear, torsional, flexural strains and torsional warping strains in local directions.		
	Continuum strains (OPTION 172): Ex, Exy, Exz: in local directions. By default element output is with respect to the nodal line. Option 380 outputs stress/strain resultants with respect to the beam centreline.		
Modeller	See Results Tables (Appendix K).		

Local Axes

Standard line element For each element/active node, the local xy-plane is defined by the local x-axis and the orientation node. The local y-axis is perpendicular to the local x-axis and positive on the side of the element where the orientation node lies. The local y and z-axes form a right-handed set with the local x-axis. See Local Element Axes for details

Sign Convention

□ Standard beam element

Formulation

Geometric Nonlinearity

Total LagrangianFor large displacements and large rotations (see Notes).UpdatedNot applicable.

Lagrangian	
Eulerian	Not applicable.
Co-rotational	For large displacements and large rotations.
P-Delta	Displacements and rotations should be small (see Notes)

Integration Schemes

Stiffness	Default.	1-point (BMX21W and BMX22W), 2-point (BMX31W and BMX33W).
	Fine.	Same as default.
Mass	Default.	2-point (BMX21W and BMX22W), 3-point (BMX31W and BMX33W).
	Fine.	Same as default.

Note: A 3-point <u>Newton-Cotes integration</u> rule is also available for BMX31W and BMX33W using option 134. This may be more applicable for infinitesimal strain, elastoplastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory manual.

Mass Modelling

- □ Consistent mass (default).
- Lumped mass.

Options

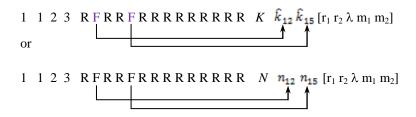
- 36 Follower loads
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity (see Notes)
- 102 Switch off load correction stiffness matrix due to centripetal acceleration
- **105** Lumped mass matrix.
- **134** Gauss to <u>Newton-Cotes</u> in plane (in the local x direction) integration for elements.
- 139 Output yielded integration points only.
- 172 Form the <u>rigidity matrix</u> by numerical cross section integration.
- 229 Co-rotational geometric nonlinearity.
- 380 Output stress/strain resultants relative to beam axes for eccentric elements
- **403** Introduce residual bending flexibility correction for 2-node thick beam BMI21, see Assumptions and Limitations (on by default).
- **404** Compute equivalent nodal loading from equilibrium considerations for 2-node thick beam BMX21, see Notes (on by default).
- 405 Specify geometric properties along beam centroidal axes.
- 406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes

- 418 Output stress resultants relative to beam centroidal axes for eccentric elements
- 421 P-Delta analysis, see Notes
- **432** Use P-Delta geometric stiffness matrix of thick beams for linear buckling analysis

Notes, Assumptions and Limitations

- 1. The element is formulated from the so-called degenerate continuum concept, i.e. enforcing directly the modified Timoshenko hypothesis for thick beams to the continuum theory. Shearing deformations and torsional warping are included.
- 2. By default input of loads and output of element stress/strain resultants are with respect to the nodal line. Option 381 inputs loads, and option 380 outputs stress/strain resultants with respect to the beam centreline. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line.
- 3. When OPTION 403 is specified to introduce residual bending flexibility correction (on by default), for BMX21W and BMX22W, the axial force, torsion, bi-shear and bimoment are constant, while the other shear forces and moments vary linearly along the length of the beam. For BMX31W and BMX33W the axial force, all shear forces, all moments and the torsion vary linearly along the length.
- 4. When BMX21W is used together with OPTION 403 to introduce residual bending flexibility correction, its stiffness matrix is enhanced to the order of a cubic. Note that if OPTION 403 is used with eccentrically stacked elements, slippage can occur.
- 5. The end releases for this element allow a joint to be modelled between adjacent elements. These joints allow rotation and translation of one beam with respect to another without load transferral as well as different warping conditions in adjacent elements. The rotations and translations remain in the local directions of the beam elements and support large deformations.
- 6. Computation of the <u>rigidity matrix</u> by integration through the cross-section depth of the beam is necessary for all linear and nonlinear material models. By default OPTION 172 is invoked automatically and a 3*3 and 5*5 point <u>Newton-Cotes</u> <u>integration</u> rule is used respectively for linear and nonlinear materials for quadrilaterals; and a 7 point cubic rule is used for both linear and nonlinear materials for triangles. This allows the output of stresses at the numerical cross section integration points.
- 7. OPTION 36 is only applicable for use with element load types ELDS and UDL. Specifying this option makes these element loads follow the element geometry as the analysis progresses.
- 8. For large deformation analyses the following geometric properties (Wagner constants) are required (see Geometric Properties) if Option 424 = T: Iyr, Igr, Irr and Iwr at each node. If these constants are set to zero, the Wagner effect will be ignored, and the results may not be correct if twist rotations are not small.

- 9. When a step by step dynamic analysis is carried out using BMI elements with distributed loading, the "free body force diagrams" pertaining to applied loading, are not superimposed on the nodal values, to do so would lead to erroneous results until a steady state is reached. It should therefore be noted that different force diagrams will be obtained for BMI elements if static and dynamic analyses are directly compared.
- 10. OPTION 229 considers large displacements and large rotations using a co-rotational formulation. When both options 87 and 229 are true, a local Total Lagrangian formulation will be used within a global co-rotational framework. Note that OPTION 87 has no effect when specified without OPTION 229.
- 11. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command.
- 12. The P-Delta formulation is only applicable to lower order (2-noded) beams, higher order beams used in a P-Delta analysis will default to co-rotational GNL.
- 13. The Smoothed Multi Crack Concrete Model (109) can be used with this element, however, due to the "plane sections remaining plane" hypothesis, crack widths cannot be computed.
- 14. Partial fixities and rigid ends are defined via the ELEMENT TOPOLOGY data and follow on the same line after the end releases, for example:



The character K is used to identify that the partial fixity stiffnesses $\hat{k}_{12} \hat{k}_{15}$ are being

explicitly defined, while the character N signifies that fixity factors, n_{12} n_{15} are being defined. The fixity factors are used as follows:

$$\hat{k}_{ij} = \frac{n_{ij}}{1 - n_{ij}} \tilde{k}_{ij}$$

The value of the factor n_{ij} ranges from zero for a pinned connection to 1.0 for a fully fixed connection.

The values r_1 and r_2 are the rigid end lengths at nodes 1 and 2 and λ is the rigidity factor (1.0 = fully rigid, the default). The factors m1 and m2 dictate how much mass to include for the rigid ends, full mass = 1.0 (default m₁=m₂=0.0).

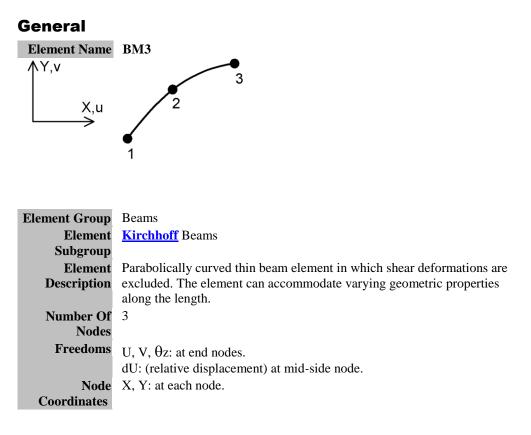
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- BMX22 and BMX33 are not available for selection currently within LUSAS Modeller.

Recommendations on Use

• The elements may be used for linear and nonlinear analysis of three dimensional beam, frame and arch structures. BMX21W and BMX22W may also be used as a stiffener for the QTS4 shell element; while BMX31W and BMX33W may be used as a stiffener for the QTS8 shell element.

2D Kirchhoff Thin Beam Elements



Geometric Properties

direction)

A, Izz, ey	At each node
SF1,SF2,SF3	Optional scale factors applied to the geometric properties in the
MF1,MF2,MF3	calculation of the stiffness and mass matrices
Α	Cross sectional area
Izz	2nd moment of area about local z-axis (see Definition).
ey	Eccentricity from beam xz-plane to nodal line (+ve in +ve local y-

For a beam with <u>eccentricity</u> e from the nodal line then $Izz=e^2A+I_{na}$ and Iz=eA ($I_{na}=I$ about centroidal axis).

For MATERIAL MODEL 29 additional geometric properties are appended to the previous 9 geometric properties; see *Notes*.

Material Properties

Matrix Joint	Isotropic: Rigidities: Not applicable Not applicable	MATERIAL PROPERTIES (Elastic: Isotropic) RIGIDITIES 3 (Rigidities:Beam)
Concrete Elasto-Plastic	Not applicable Stress resultant:	MATERIAL PROPERTIES NONLINEAR 29 (Elastic: Isotropic, Plastic: Resultant) (ifcode=1 or 2, see <i>Notes</i>)
Сгеер	AASHTO	CREEP PROPERTIES (Creep) MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP (Concrete creep model to CEB-FIP Model Code 1990)
Chinese Eurocode IRC	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
Damage Viscoelastic Shrinkage	Not applicable Not applicable	SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Rubber Generic Polymer Composite	Not applicable Not applicable Not applicable	,

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, θ z: at end nodes.	
Concentrated Loads	CL	Concentrated loads. Px, Py, Mz: at end nodes. dPx: in local x direction at mid-side node.	
Loads Element Loads	ELDS	 Element loads on nodal line (load type number LTYPE *10 defines the corresponding element load type on beam axis). LTYPE, S1, Px, Py, Mz LTYPE=11: point loads and moments in local directions. LTYPE=12: point loads and moments in global directions. LTYPE=0, Wx, Wy, Mz LTYPE=21: uniformly distributed loads in local directions. LTYPE=22: uniformly distributed loads in global directions. LTYPE=23: uniformly distributed projected loads in global directions LTYPE, S1, Wx1, Wy1, Mz1, S2, Wx2, Wy2, Mz2 LTYPE=31: distributed loads in global directions. LTYPE=33: distributed loads in global directions. LTYPE=33: distributed projected loads in global directions. 	
		LTYPE=41: trapezoidal loads in local directions. LTYPE=42: trapezoidal loads in global directions. LTYPE=43: trapezoidal projected loads in global directions	
Distributed Loads	UDL	Uniformly distributed loads. Wx, Wy: force/unit length in local directions.	
	FLD, FLDG	Not applicable.	
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Ωx , Ωy , Ωz , αz	
	BFP, BFPE	Body force potentials at nodes/for element. ϕ_1 , ϕ_2 , 0, 0, Xcbf, Ycbf	
Velocities	VELO	Velocities. Vx, Vy: at nodes.	
Accelerations	ACCE	Acceleration Ax, Ay: at nodes	
Initial Stress/Strains	SSI, SSIE	 Initial stresses/strains at nodes/for element. Fx, Mz, 0: forces, moments in local directions. εx, ψz, 0: strains in local directions. 	
	SSIG	Initial stresses/strains at Gauss points Fx, Mz, 0:	

		forces, moments in local directions. εx , ψz , 0: strains in local directions.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. Fx, Mz, 0: forces, moments in local directions.
	SSRG	Residual stresses at Gauss points Fx, Mz, 0: forces, moments in local directions.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, dT/dy, 0, To, 0, dTo/dy, 0
Target	TSSIE,	Target stresses/strains at nodes/for element. Fx, Mz,
Stress/Strains	TSSIA	0: forces, moments in local directions. Ex, ψz , 0: strains in local directions.
	TSSIG	Target stresses/strains at Gauss points Fx, Mz, 0:
		forces, moments in local directions. εx , ψz , 0: strains in local directions.
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent Loads	Not applicable.	

LUSAS Output

Solver	Force (default): Fx, Fy, Mz: forces, moments in local directions (see <i>Notes</i>).
	Strain: εx , εy , ψz : axial, flexural strains in local directions. By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal
	axis.
Iodeller	See Results Tables (Appendix K) .

Modeller See Results Tab

Local Axes

□ Standard line element

Sign Convention

□ Standard beam element

Formulation

Geometric Nonlinearity

Total Lagrangian For large displacements, small rotations and small strains.

Updated
LagrangianFor large displacements, large rotations and small strains.EulerianNot applicable.Co-rotationalNot applicable.

Integration Schemes

Stiffness	Default.	2-point.
	Fine (see Options).	3-point.
Mass	Default.	2-point.
	Fine (see Options).	3-point.

A 3-point <u>Newton-Cotes integration</u> rule is also available using option 134. This may be more applicable for infinitesimal strain, elastoplastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory manual.

Mass Modelling

- □ Consistent mass (default).
- Lumped mass.

Options

- **18** Invokes fine integration rule for element.
- 54 Updated Lagrangian geometric nonlinearity.
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity.
- 105 Lumped mass matrix
- **134** Gauss to <u>Newton-Cotes</u> in plane (in the local x direction) integration for elements.
- **157** Material model 29 (non cross-section elements), see *Notes*.
- 170 Suppress transfer of shape function arrays to disk.
- 405 Specify geometric properties along beam centroidal axes
- **406** Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes.
- 418 Output stress resultants relative to beam centroidal axes for eccentric elements

Notes on Use

- 1. The element formulation is based on the constrained super-parametric approach. The variation of axial force along the beam is linear. The variation of displacement is quadratic in the local x-direction and cubic in the local y-direction. Shear force is constant.
- 2. Input of geometric properties (OPTION 405) and loads (OPTION 406), and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axis. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line
- 3. For nonlinear material model 29 the following geometric properties are appended to those already specified (see *Geometric Properties*).
 - A^p, Zzz^p, S^p at each node (i.e. nodes 1, 2, 3)
 - A^p Plastic area (=elastic area)
 - Zzz^p Plastic modulus for bending about z axis
 - S^{p} Plastic area for shear ($S^{p}=0$)
- 4. For nonlinear material model 29 the following ifcode parameters should be
 - ifcode=1 for circular hollow sections.
 - ifcode=2 for solid rectangular sections.
- 5. Temperature dependent properties cannot be used with material model 29.
- 6. The element should not be coupled to the face of a two dimensional continuum element because of the midside node incompatibility.
- 7. The <u>rigidity matrix</u> for BM3 is evaluated explicitly from the material and geometric properties for both linear and nonlinear materials.
- 8. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command

Restrictions

□ Ensure mid-side node centrality

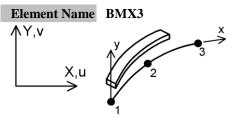
□ Avoid excessive element curvature

Recommendations on Use

The element may be used for linear and nonlinear analysis of two dimensional beam, frame and arch structures. The 2-noded straight beam (BMI2 is more effective for the linear analysis of structures containing straight members of constant cross-section, e.g. plane frames.

2D Kirchhoff Thin Beam Element with Quadrilateral Cross-Section

General

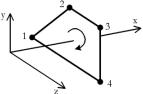


Element Group	Beams
Element	Kirchhoff Beams
Subgroup	
Element	Parabolically curved thin beam elements in which shear deformations are
Description	excluded. The quadrilateral cross-section may be eccentric and can vary
	along the element length.
Number Of	3
Nodes	
Freedoms	U, V, θ z: at end nodes.
	dU: (relative displacement) at mid-side node.
Node	X, Y: at each node.
Coordinates	

Geometric Properties

y1, z1, y2, z2, y3, z3, y4, z4: local cross section coordinate pairs at each node; followed by nt12, nt14: specifying the number of <u>Newton-Cotes integration</u> points in the direction defined by the local cross-section points 1-2 and 1-4 (zero indicates default values). See *Notes*. Multiple quadrilateral cross-sections can be used to build up complex beam cross-sections.

Note. The coordinates of the cross section are numbered clockwise about the local x-axis (the beam nodal line). That is, a right-hand screw rule in the direction of increasing x.



Material Properties

Matrix Joint	Isotropic: Not applicable Not applicable Not applicable	MATERIAL PROPERTIES (Elastic: Isotropic)
Elasto-Plastic		MATERIAL PROPERTIES NONLINEAR 29 (Elastic: Isotropic, Plastic: Resultant) (ifcode=2, see <i>Notes</i>)
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker- Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr- Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Optimised Implicit Von Mises:	MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic)
	Volumetric Crushing:	Not applicable
Сгеер	Stress Potential	STRESS POTENTIAL VON_MISES (Isotropic: von Mises, Modified von Mises) CREEP PROPERTIES (Creep)
	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO
	CEB-FIP	(Concrete creep model to AASHTO code of Practice)
		MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP (Concrete creep model to CEB-FIP Model Code
	Chinese	1990) MATERIAL PROPERTIES NONLINEAR 86 CHINESE
	Eurocode	(Chinese creep model to Chinese Code of Practice) MATERIAL PROPERTIES NONLINEAR 86
		EUROCODE (Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC

Damage		Practice) DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic	Not applicable	
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Rubber	Not applicable	
Generic Polymer	Not applicable	
Composite	Not applicable	

(Concrete creep model to Indian IRC code of

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, θz : at end nodes. dU at
		mid-side node.
Concentrated	CL	Concentrated loads. Px, Py, Mz: at end nodes
Loads		(global). dPx: at mid-side node (local).
Element Loads	LTYPE *10 defines the corresponding	Element loads on nodal line (load type number LTYPE *10 defines the corresponding element load type on beam axis).
		LTYPE, S1, Px, Py, Mz
		LTYPE=11: point loads and moments in local
		directions.
		LTYPE=12: point loads and moments in global
		directions.
		LTYPE, 0, Wx, Wy, Mz
		LTYPE=21: uniformly distributed loads in local
		directions.
		LTYPE=22: uniformly distributed loads in global
		directions.
		LTYPE=23: uniformly distributed projected loads in global directions
		LTYPE, S1, Wx1, Wy1, Mz1, S2, Wx2, Wy2, Mz2 LTYPE=31: distributed loads in local directions. LTYPE=32: distributed loads in global directions.
		LTYPE=33: distributed projected loads in global directions
		LTYPE, S1, Wx, Wy, Mz
		LTYPE=41: trapezoidal loads in local directions.
LTYPE=42: tra	LTYPE=42: trapezoidal loads in global directions.	
		LTYPE=43: trapezoidal projected loads in global
		directions

Distributed Loads	UDL	Uniformly distributed loads. Wx, Wy: force/unit length in local directions.
	FLD, FLDG	Not applicable.
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Ωx , Ωy , Ωz , αz
	BFP, BFPE	Body force potentials at nodes/for element. φ_1 , φ_2 , 0, 0, Xcbf, Ycbf
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay: at nodes
Initial Stress/Strains	SSI, SSIE	Initial stresses/strains at nodes/for element. Resultants (for linear material models without numerical cross section integration and model 29, see <i>Notes</i>): Fx, Mz, 0: forces, moments in local
		directions. εx , ψz , 0: strains in local directions.
	SSIG	 Initial stresses/strains at Gauss points. (1) Resultants (for linear material models without numerical cross section integration and model 29, see <i>Notes</i>). Fx, Mz, 0: forces, moments in local
		directions. εx , ψz , 0 strains in local directions. (2) Components (for linear material models with numerical cross section integration and all non-
		linear material models except 29): Fx, Mz, 0, Ex,
		ψz , 0, (σx , ϵx). Bracketed terms repeated at each fibre integration point.
Residual Stresses	SSR, SSRE	Not applicable.
	SSRG	 Residual stresses at Gauss points. (1) Resultants (material model 29): Fx, Mz, 0 (2) Components (all nonlinear material models except 29, also linear material models with numerical cross section integration): 0, 0, 0, 0, 0, 0, 0
		$(\sigma x, \epsilon x)$ Bracketed term repeated for each fibre integration point.
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. Resultants (for linear material models without numerical cross section integration and model 29, see <i>Notes</i>): Fx, Mz, 0: forces, moments in local
		directions. εx , ψz , 0: strains in local directions.
	TSSIG	Target stresses/strains at Gauss points. (1) Resultants (for linear material models without numerical cross section integration and model 29, see <i>Notes</i>). Fx, Mz, 0: forces, moments in local

		directions. εx , ψz , 0 strains in local directions. (2) Components (for linear material models with numerical cross section integration and all non-
		linear material models except 29): Fx, Mz, 0, &x,
		ψz , 0, (σx , ϵx). Bracketed terms repeated at each fibre integration point.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element T, 0, dT/dy, 0, To, 0, dTo/dy, 0: in local directions.
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent Loads	Not applicable.	

LUSAS Output

Solver	Force (default): Fx, Mz, Fy: forces, moment in local directions (see <i>Notes</i>)
	Continuum stresses (OPTION 172): σx : in local directions.
	Strain: εx , ψz , 0 : axial, flexural strains in local directions.
	Continuum strains (OPTION 172): Ex: in local directions. By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal axis.
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

□ Standard line element

Sign Convention

□ Standard beam element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements, small rotations and small strains.
Updated	For large displacements, large rotations and small strains.
Lagrangian	
Eulerian	Not applicable.
Co-rotational	Not applicable.

Integration Schemes

Stiffness	Default.	2-point.
	Fine (see Options).	3-point.
Mass	Default.	2-point.
	Fine (see Options).	3-point.

A 3-point <u>Newton-Cotes integration</u> rule is also available using option 134. This may be more applicable for infinitesimal strain, elastoplastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory manual.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- **18** Invokes fine integration rule for element.
- 32 Suppress stress output but not resultants
- 54 Updated Lagrangian geometric nonlinearity.
- 55 Output strains as well as stresses
- 87 Total Lagrangian geometric nonlinearity
- **105** Lumped mass matrix
- 134 Gauss to <u>Newton-Cotes</u> in plane (in the local x direction) integration for elements.
- 157 Material model 29 (non cross-section elements), see *Notes*.
- 170 Suppress transfer of shape function arrays to disk.
- 172 Formulate <u>rigidity matrix</u> by integrating across the cross-section
- 406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
- 418 Output stress resultants relative to beam centroidal axes for eccentric elements

Notes on Use

- 1. The element formulation is based on the constrained super-parametric approach. The variation of axial force along the beam is linear. The variation of displacement is quadratic in the local x-direction and cubic in the local y-direction. Shear force is constant.
- 2. Input of loads (OPTION 406), and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axis. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line. Fiber stress/strain results are output at the actual location
- 3. Initial strain resultants may be input for any material model.
- 4. The number of numerical cross-section integration points, nt12 and nt14, may be specified but for improved performance the number of integration points corresponding to the y direction can be defined correctly (the beam bends about the local z-axis) and the integration rule in the other direction may be set to 1.
- 5. For nonlinear material model 29 ifcode must be set to 2 for solid rectangular sections. Multiple quadrilateral cross-sections can be used to build up complex beam crosssections.
- 6. Temperature dependent properties cannot be used with material model 29.
- 7. The element should not be coupled to the face of a two dimensional continuum element because of the midside node incompatibility.
- 8. Computing the <u>rigidity matrix</u> by integration through the cross-section depth of the beam is necessary for all nonlinear material models (except 29). By default option 172 is invoked automatically and a 5 point <u>Newton-Cotes integration</u> rule is used.
- By default, the <u>rigidity matrix</u> is evaluated explicitly for linear materials. A 3 point <u>Newton-Cotes</u> rule may be invoked using option 172. Numerical cross section integration enables top, middle and bottom stress output.

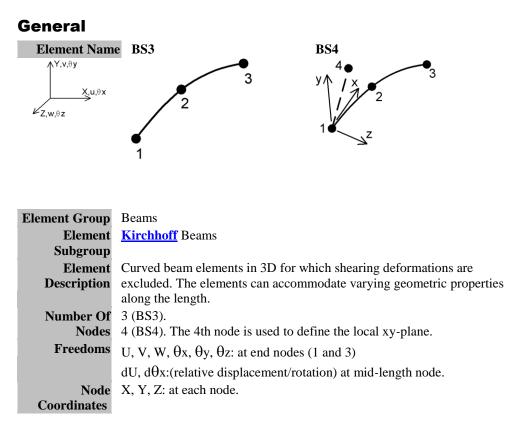
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature

Recommendations on Use

The element may be used for linear and nonlinear analysis of two dimensional beam, frame and arch structures. The 2-noded straight beam (BMI2) is more effective for linear analysis of structures containing straight members of constant cross-section, e.g. plane frames.

3D Kirchhoff Thin Beam Elements



Geometric Properties

A, Iyy, Izz, Jxx, Iy, Iz, Iyz, ez, ey	At each node
	Optional scale factors applied to the geometric
	properties in the calculation of the stiffness and mass
MF5, MF6, MF7, MF8, MF9	matrices
Α	Cross sectional area
Iyy, Izz	2nd moment of area about local y, z directions (see
	<u>Definition</u>)
Jxx	Torsional constant.
Iy, Iz	1st moment of area about local y, z directions (see
	<u>Definition</u>)
Iyz	Product moment of area (see Definition)

- ez Eccentricity from beam xy-plane to nodal line. (+ve in the +ve local z direction). (See Notes)
- **ey** Eccentricity from beam xz-plane to nodal line. (+ve in the +ve local y direction). (See Notes)

For MATERIAL MODEL 29 additional geometric properties are appended to the previous 21 geometric properties (see *Notes*).

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
Matrix Joint Concrete	Rigidities: Not applicable Not applicable Not applicable	RIGIDITIES 6 (Rigidities: Beam)
Elasto-Plastic	Stress resultant:	MATERIAL PROPERTIES NONLINEAR 29 (Elastic: Isotropic, Plastic: Resultant) (ifcode=1 or 2, see <i>Notes</i>)
Сгеер	AASHTO	CREEP PROPERTIES (Creep) MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of
	CEB-FIP	Practice) MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP (Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
Damage Viscoelastic Shrinkage	Not applicable Not applicable	SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Rubber	Not applicable	,,,

Generic Polymer	Not applicable
Composite	Not applicable

Loading

Prescribed Value	PDSP. TPDSP	Prescribed variable. U, V, W, θx , θy , θz : at end
110,011,000 (0100	,	
	CI	nodes (1 and 3). dU, d θ x: at mid-length node.
Concentrated Loads	CL	Concentrated loads. Px, Py, Pz, Mx, My, Mz: at end nodes. dPx, dMy: at mid-length node.
Element Loads	ELDS	Element loads on nodal line (load type number LTYPE *10 defines the corresponding element load type on beam axis) LTYPE, S1, Px, Py, Pz, Mx, My, Mz LTYPE=11: point loads and moments in local
		directions.
		LTYPE=12: point loads and moments in global
		directions.
		LTYPE, 0, Wx, Wy, Wz, Mx, My, Mz
		LTYPE=21: uniformly distributed loads in local
		directions.
		LTYPE=22: uniformly distributed loads in global directions.
		LTYPE=23: uniformly distributed projected loads in
		global directions.
		LTYPE, S1, Wx1, Wy1, Wz1, Mx1, My1, Mz1, S2,
		Wx2, Wy2, Wz2, Mx2, My2, Mz2
		LTYPE=31: distributed loads in local directions. LTYPE=32: distributed loads in global directions. LTYPE=33: distributed projected loads in global directions.
		LTYPE, S1, Wx, Wy, Wz, Mx, My, Mz
		LTYPE=41: trapezoidal loads in local directions.
		LTYPE=42: trapezoidal loads in global directions.
		LTYPE=43: trapezoidal projected loads in global
		directions.
Distributed Loads	UDL	Uniformly distributed loads. Wx, Wy, Wz: local forces/unit length.
	FLD, FLDG	Not applicable.
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Zcbf, Ωx , Ωy , Ωz
	BFP, BFPE	Body force potentials at nodes/for element. ϕ_1 , ϕ_2 ,

		φ3, 0, Xcbf, Ycbf, Zcbf
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay, Az: at nodes
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element. Fx, My,
Stress/Strains		Mz, Txz, Txy, 0: axial force, moments and torques
		in local directions. εx , ψy , ψz , ψxz , ψxy , 0: axial, flexural and torsional strains in local directions.
		Total torque = $Txz + Txy$, total torsional strain =
		$yxz + \psi xy.$
	SSIG	Not applicable.
Residual Stresses	SSR, SSRE	Not applicable.
	SSRG	Residual stresses at Gauss points. Resultants (for material model 29). Fx, My, Mz, Txz, Txy, 0: axial force, moments and torques in local directions.
		Total torque = $Txz + Txy$, total torsional strain =
		$yxz + \psi xy.$
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. Fx, My, Mz, Txz, Txy, 0: axial force, moments and torques
		in local directions. εx , ψy , ψz , ψxz , ψxy , 0: axial, flexural and torsional strains in local directions.
		Total torque = $Txz + Txy$, total torsional strain =
		$yxz + \psi xy.$
	TSSIG	Not applicable.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, dT/dy, dT/dz, To, 0, dTo/dy, dTo/dz
Overburden		
	applicable.	
Phreatic Surface	Not	
F !	applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not	
Loads	applicable.	

LUSAS Output

SolverForce (default): Fx, Fy, Fz, My, Mz, Txz, Txy: axial force, moments,
torques and shear forces in local directions. (Total torque = Txz+Txy).Strain: $\mathcal{E}x$, ψy , ψz , ψxz , ψxy , 0: axial, flexural and torsional strains in

local directions.

By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal axes.

Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

For BS3 the local xy-plane is defined by the 3 element nodes. The local y-axis is perpendicular to the local x-axis and positive on the convex side of the element. The local y and z-axes form a right handed set with the local x-axis.

For BS4 the local xy-plane is defined by the 2 end nodes of the beam and the 4th node. The local y-axis is perpendicular to the local x-axis and positive on the side of the element where the 4th node lies. The local y and z-axes form a right handed set with the local x-axis. See **Local Element Axes** for more details.

Sign Convention

□ Standard beam element

Formulation

Geometric Nonlinearity

Total LagrangianFor large displacements, small rotations and small strains.UpdatedFor large displacements, large rotations and small strains.LagrangianNot applicable.Co-rotationalNot applicable.

Integration Schemes

Stiffness Default.	2-point.
Fine (see	3-point.
Options).	
Mass Default.	2-point.
Fine (see	3-point.
Options).	

A 3-point <u>Newton-Cotes</u> integration rule is also available using option 134. This may be more applicable for infinitesimal strain, elastoplastic analyses of plane frames with straight

members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory manual.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- **18** Invokes fine integration rule for element.
- **54** Updated Lagrangian geometric nonlinearity.
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity.
- **102** Switch off load correction stiffness matrix due to centripetal acceleration.
- 105 Lumped mass matrix.
- **134** Gauss to <u>Newton-Cotes</u> in plane (in the local x direction) integration for elements.
- **157** Material model 29 (non cross-section elements), see *Notes*.
- 170 Suppress transfer of shape function arrays to disk.
- 405 Specify geometric properties along beam centroidal axes
- 406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
- 418 Output stress resultants relative to beam centroidal axes for eccentric elements

Notes on Use

- 1. The element formulation is based on the <u>Kirchhoff</u> hypothesis for thin beams (i.e. the exclusion of shearing deformations).
- 2. The variation of axial force, moments and torsion along the length of the beam can be regarded as linear. Shear force variations are constant.
- 3. Input of geometric properties (OPTION 405) and loads (OPTION 406), and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axes. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line.
- 4. For nonlinear material model 29 the following geometric properties are appended to those already specified (see *Geometric Properties*).
 - A^p , Zyy^p , Zzz^p , Zy^p , Zz^p , S^p at each node (i.e. nodes 1, 2, 3).
 - A^p Plastic area (=elastic area)
 - Zyy^p, Zzz^p Plastic moduli for bending about y, z axes

- Zy^p, Zz^p Plastic moduli for torsion about y, z axes.
- S^p Plastic area for shear (S^p=0).

Where the fully plastic torsional moment = $\sigma y (Zy^p + Zz^p)$.

- 5. For nonlinear material model 29 the following ifcode parameters should be used
 - ifcode=1 for circular hollow sections.
 - ifcode=2 for solid rectangular sections.
- 6. Temperature dependent properties cannot be used with material model 29.
- 7. The element should not be coupled to the edges of either continuum or shell elements because of midside node incompatibility.
- 8. The <u>rigidity matrix</u> for BS3 and BS4 is evaluated explicitly from the geometric properties for both linear and nonlinear materials.
- 9. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command.

Restrictions

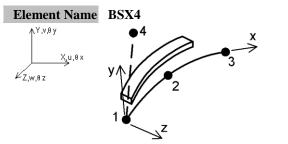
- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature

Recommendations on Use

The elements may be used for linear and nonlinear analysis of three dimensional beam, frame and arch structures. The 2-noded straight beam (BMI21) is more effective for linear analysis of structures containing straight members of constant cross-section, e.g. space frames.

3D Kirchhoff Thin Beam Element with Quadrilateral Cross-Section

General

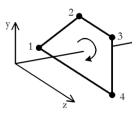


Element Group	Beams
Element	Kirchhoff Beams
Subgroup	
Element	Curved beam elements in 3D for which shearing deformations are
Description	excluded. The element has a quadrilateral cross section which may vary
	along the element length.
Number Of	4. The 4th node is used to define the local xy-plane.
Nodes	
Freedoms	U, V, W, θx , θy , θz : at the end nodes (1 and 3)
	dU, d θx : (relative displacement/rotation) at the mid-length node.
Node	X, Y, Z: at each node.
Coordinates	

Geometric Properties

y1, z1, y2, z2, y3, z3, y4, z4: local cross section coordinate pairs at each node; followed by nt12, nt14: specifying the number of <u>Newton-Cotes</u> integration points in the direction defined by the local cross-section points 1-2 and 1-4 (zero indicates default values). Multiple quadrilateral cross-sections can be used to build up complex beam cross-sections.

Note. The coordinates of the cross section are numbered clockwise about the local x-axis (the beam nodal line). That is, a right-hand screw rule in the direction of increasing x.



Material Properties

r		
	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
Matrix	Not applicable	
Joint	Not applicable	
Concrete	Not applicable	
Elasto-Plastic	Stress	Not applicable.
	resultant:	
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker-	MATERIAL PROPERTIES NONLINEAR 64
	Prager:	(Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr-	MATERIAL PROPERTIES NONLINEAR 65
	Coulomb:	(Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Optimised Implicit Von Mises:	MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic)
	Volumetric Crushing:	Not applicable
	Stress Potential	STRESS POTENTIAL VON_MISES (Isotropic: von Mises, Modified von Mises)
Creep		CREEP PROPERTIES (Creep)
	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO
	CEB-FIP	(Concrete creep model to AASHTO code of Practice)
		MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP
		(Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86

	CHINESE (Chinese creep model to Chinese Code of Practice)
Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2)
IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
	DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Not applicable	
	SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Not applicable	
	Eurocode IRC Not applicable Not applicable Not applicable Not applicable

Loading

•		
Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, W, θx , θy , θz : at the end nodes. dU, $d\theta x$: at the mid-length node.
Concentrated Loads	CL	Concentrated loads. Px, Py, Pz, Mx, My, Mz: at end nodes (global). dPx, dMx: at mid-length local node.
		Element loads on nodal line (load type number LTYPE *10 defines the corresponding element load type on beam axis)
		LTYPE, S1, Px, Py, Pz, Mx, My, Mz
		LTYPE=11: point loads and moments in local
		directions.
		LTYPE=12: point loads and moments in global directions.
		LTYPE, 0, Wx, Wy, Wz, Mx, My, Mz
		LTYPE=21: uniformly distributed loads in local
		directions.
		LTYPE=22: uniformly distributed loads in global
		directions.
		LTYPE=23: uniformly distributed projected loads in
		global directions.
		LTYPE, S1, Wx1, Wy1, Wz1, Mx1, My1, Mz1, S2,
		Wx2, Wy2, Wz2, Mx2, My2, Mz2

		LTYPE=31: distributed loads in local directions. LTYPE=32: distributed loads in global directions.
		LTYPE=33: distributed projected loads in global directions.
		LTYPE, S1, Wx, Wy, Wz, Mx, My, Mz LTYPE=41: trapezoidal loads in local directions. LTYPE=42: trapezoidal loads in global directions. LTYPE=43: trapezoidal projected loads in global
Distributed Loads	UDL	directions. Uniformly distributed loads. Wx, Wy, Wz: forces/unit length in local directions.
	FLD, FLDG	Not applicable
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Zcbf,
U		$\Omega_x, \Omega_y, \Omega_z, \alpha_x, \alpha_y, \alpha_z$
	BFP, BFPE	Body force potentials at nodes/for element. (ϕ_1, ϕ_2, ϕ_3)
		ϕ_{3} , 0, Xcbf, Ycbf, Zcbf
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay, Az: at nodes
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element.
Stress/Strains		Components: Fx, My, Mz, 0, 0, 0, 8x, \v/y, \v/z, 0,
		0, 0, (σx , σxy , σxz , σyz , εyz , εx , εxz , εyz) Bracketed terms repeated for each fibre integration point.
	SSIG	Initial stresses/strains at Gauss points. These stresses/strains are specified in the same manner as SSI and SSIE.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element.
		Components:0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0
		σ xy, σ xz, σ yz,) Bracketed terms repeated for each fibre integration point.
	SSRG	Residual stresses at Gauss points. These stresses are specified in the same manner as SSR and SSRE.
Target	TSSIE, TSSIA	Target stresses/strains at nodes/for element.
Stress/Strains		Components: Fx, My, Mz, 0, 0, 0, ε x, ψ y, ψ z, 0,
		0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0
		σ yz, ε yz, ε x, ε xz, ε yz) Bracketed terms repeated for each fibre integration point.
	TSSIG	Target stresses/strains at Gauss points. These stresses/strains are specified in the same manner as TSSIE and TSSIA.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, dT/dy,

dT/dz, To, 0, dTo/dy, dTo/dz: in local directions.

Overburden	Not
	applicable.
Phreatic Surface	Not
	applicable.
Field Loads	Not applicable
Temp Dependent	Not applicable
Loads	

LUSAS Output

Solver	Force (default): Fx, My, Mz, Txz, Txy, Fy, Fz: axial force, moments, torques and shear forces in local directions. (Total Torque = Txz + Txy).
	Continuum stresses (OPTION 172): σx , σxy , σxz , σyz : in local directions.
	Strain: εx , ψy , ψz , ψxz , ψxy : axial, flexural and torsional strains in local directions.
	Continuum strains (OPTION 172): Ex, Exy, Exz, Eyz: in local directions.
	By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal
	axes.
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

Standard line element. The local xy-plane is defined by the 2 end nodes of the beam and the 4th node. The local y-axis is perpendicular to the x-axis and positive on the side of the element where the 4th node lies.

The local y and z-axes form a right-hand set with the local x-axis.

Sign Convention

□ Standard beam element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements, small rotations and small strains.
Updated	For large displacements, large rotations and small strains.
Lagrangian	
Eulerian	Not applicable.
Co-rotational	Not applicable.

Integration Schemes

Stiffness	Default.	2-point.
	Fine (see Options).	3-point.
Mass	Default.	2-point.
	Fine (see Options).	3-point.

A 3-point <u>Newton-Cotes</u> integration rule is also available using option 134. This may be more applicable for infinitesimal strain, elastoplastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory manual.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- 18 Invokes fine integration rule for element.
- 54 Updated Lagrangian geometric nonlinearity.
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity.
- 102 Switch off load correction stiffness matrix due to centripetal acceleration.
- 105 Lumped mass matrix.
- **134** Gauss to <u>Newton-Cotes</u> in plane (in the local x direction) integration for elements.
- **139** Output yielded integration points only.
- 170 Suppress transfer of shape function arrays to disk.
- 172 Form the <u>rigidity matrix</u> by numerical cross section integration.
- 406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
- 418 Output stress resultants relative to beam centroidal axes for eccentric elements

Notes, Assumptions and Limitations

- 1. The element formulation is based on the <u>Kirchhoff</u> hypothesis for thin beams (i.e. the exclusion of shearing deformations)
- 2. The variation of axial force, moments and torsion along the length of the beam can be regarded as linear. Shear force is constant.
- 3. Input of loads (OPTION 406), and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axes. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line. Fiber stress/strain results are output at their actual location
- 4. Computation of the <u>rigidity matrix</u> by integration over the thickness is necessary for all nonlinear material models. For nonlinear models a 5x5 <u>Newton-Cotes integration</u> rule is used as default. For linear models a 3x3 rule is used as the default. This allows the output of stresses at the numerical cross section integration points.
- 5. The torsional constant is estimated from the computed values for Iyy and Izz, Jxx = Iyy + Izz.
- 6. For nonlinear material models, fibre integration is used across the cross-sectional area of the beam. Only axial deformation is considered in the plasticity computations, any torsional deformation is assumed to remain elastic.
- 7. The element should not be coupled to the face of a two dimensional continuum element because of the midside node incompatibility
- Computing the <u>rigidity matrix</u> by integration through the cross-section depth of the beam is necessary for all nonlinear material models (except 29). By default OPTION 172 is invoked automatically and a 5*5 point <u>Newton-Cotes integration</u> rule is used.
- By default, the <u>rigidity matrix</u> is evaluated explicitly for linear materials. A 3*3 point <u>Newton-Cotes integration</u> rule may be invoked using OPTION 172. Numerical cross section integration enables top, middle and bottom stress output.

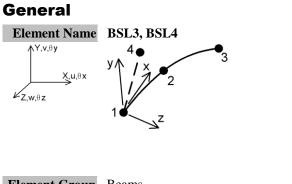
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature

Recommendations on Use

The elements may be used for linear and nonlinear analysis of three dimensional beam, frame and arch structures. The 2-noded straight beam (BMI21) is more effective for linear analysis of structures containing straight members of constant cross-section, e.g. space frames.

3D Semiloof Thin Beam Elements



Element Group	Beams
Element	Semiloof Beams
Subgroup	
Element	Curved beam elements in 3D which can be mixed with the semiloof shell
Description	elements TSL6 and QSL8. The elements can accommodate varying
	geometric properties. Shearing deformations are excluded.
Number Of	3 or 4. For BSL4 the 4th node is used to define the local xy-plane.
Nodes	
Freedoms	U, V, W, θx , θy , θz : at end nodes (1 and 3). U, V, W, θ_1 , θ_2 : at mid-side
	node (node 2) (see <i>Notes</i>).
Node	X, Y, Z: at each node.
Coordinates	

Geometric Properties

A, Iyy, Izz, Jxx, Iy, Iz, Iyz, ez, ey SF1,SF2,SF3,SF4,SF5,SF6,SF7,SF8,SF9 MF1,MF2,MF3,MF4,MF5,MF6,MF7,MF8,MF9	at nodes 1, 2 and 3 Optional scale factors applied to the geometric properties in the calculation of the stiffness and mass matrices
Α	Cross sectional area
Iyy, Izz	2nd moments of area in local y, z axes (see Definition)
Jxx	<u>Torsional constant</u> .
Iy, Iz	1st moment of area in local y, z axes (see Definition)
Iyz	Product moment of area (see Definition).
ez	Eccentricity from beam xy-plane to

nodal line (+ve in +ve local z-direction)

ey Eccentricity from beam xz-plane to nodal line (+ve in +ve local y-direction)

For MATERIAL MODEL 29 additional geometric properties are appended to the 21 properties above; see *Notes*.

Material Properties

Linear	Isotropic: Rigidities:	MATERIAL PROPERTIES (Elastic: Isotropic) RIGIDITIES Rigidities 6 (Rigidities: Beam)
	Not applicable Not applicable	
	Not applicable	
	o-Plastic Stress resultant:	MATERIAL PROPERTIES NONLINEAR 29 (Elastic: Isotropic, Plastic: Resultant) (ifcode=1 or 2, see <i>Notes</i>)
Creep		CREEP PROPERTIES (Creep)
	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO
		(Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP
		(Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinasa arean model to Chinasa Code of Bragtige)
	Eurocode	(Chinese creep model to Chinese Code of Practice)
IRC		MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
Damage Viscoelastic	Not applicable Not applicable	·····,
Shrinkage	**	SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Rubber	Not applicable	

Generic PolymerNot applicableCompositeNot applicable

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, W, θx , θy , θz : at end	
		nodes. U, V, W, θ_1 , θ_2 : at mid-side node.	
Concentrated Loads	CL	Concentrated loads. Px, Py, Pz, Mx, My, Mz: at end nodes (global). Px, Py, Pz, M1, M2: at mid-side node (M1 and M2 local).	
Element Loads	ELDS	 Element loads on nodal line (load type number LTYPE *10 defines the corresponding element load type on beam axis) LTYPE, S1, Px, Py, Pz, Mx, My, Mz LTYPE=11: point loads and moments in local directions. LTYPE=12: point loads and moments in global directions. LTYPE, 0, Wx, Wy, Wz, Mx, My, Mz LTYPE=21: uniformly distributed loads in local directions. LTYPE=22: uniformly distributed loads in global directions. LTYPE=23: uniformly distributed projected loads in global directions. LTYPE=23: uniformly distributed projected loads in global directions. 	
		LTYPE, S1, Wx1, Wy1, Wz1, Mx1, My1, Mz1, S2, Wx2, Wy2, Wz2, Mx2, My2, Mz2 LTYPE=31: distributed loads in local directions. LTYPE=32: distributed loads in global directions. LTYPE=33: distributed projected loads in global directions.	
		LTYPE, S1, Wx, Wy, Wz, Mx, My, Mz LTYPE=41: trapezoidal loads in local directions. LTYPE=42: trapezoidal loads in global directions. LTYPE=43: trapezoidal projected loads in global directions.	
Distributed Loads	UDL	Uniformly distributed loads. Wx, Wy, Wz: force/unit length in local directions for element.	
	FLD, FLDG	Not applicable.	
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Zcbf,	
		$\Omega x, \Omega y, \Omega z, \alpha x, \alpha y, \alpha z$	

	BFP, BFPE	Body force potentials at nodes/for element. φ_1 , φ_2 ,
		φ ₃ , 0, Xcbf, Ycbf, Zcbf
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Accelerations. Ax, Ay, Az: at nodes.
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element. Fx, My,
Stress/Strains		Mz, Txz, Txy, 0 in local directions. εx , ψy , ψz ,
		ψ xz, ψ xy, 0: in local directions. (see <i>Notes</i>). Total torque = Txz + Txy
	SSIG	Not applicable.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. Resultants (nonlinear model 29): Fx, My, Mz, Txz, Txy, 0: in local directions.
	SSRG	Not applicable.
Target	TSSE, TSSIA	Target stresses/strains at nodes/for element. Fx, My,
Stress/Strains		Mz, Txz, Txy, 0 in local directions. εx , ψy , ψz ,
		ψ xz, ψ xy, 0: in local directions. (see <i>Notes</i>). Total torque = Txz + Txy
	TSSIG	Not applicable.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, dT/dy, dT/dz, To, 0, dTo/dy, dTo/dz: in local directions.
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not	

LUSAS Output

Loads applicable.

Solver	Force (default): Fx, My, Mz, Txz, Txy, Fy, Fz: in local directions. (Total torque = Txz + Txy)
	Strain: εx , ψy , ψz , ψxz , ψxy : in local directions. (see <i>Notes</i>). Total
	torsional strain = $\psi xz + \psi xy$ By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal axes.
Modeller	See Results Tables (Appendix K) .

Local Axes

Standard line element. For BSL3 the local xy-plane is defined by the 3 element nodes. The local y-axis is perpendicular to the local x-axis and positive on the convex side of the element. The local y and z-axes form a right-hand set with the local x-axis.

For BSL4 the local xy-plane is defined by the 2 end nodes of the beam and the 4th node. The local y-axis is perpendicular to the x-axis and positive on the side of the element where the 4th node lies. The local y and z-axes form a right-hand set with the local x-axis.

Sign Convention

□ Standard beam element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements, small rotations and small strains.		
Updated	Not applicable.		
Lagrangian			
Eulerian	Not applicable.		
Co-rotational	Not applicable.		

Integration Schemes

Stiffness	Default.	3-point torsion, 2-point bending.
	Fine.	As default.
Mass	Default.	3-point.
	Fine.	As default.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity
- 102 Switch off load correction stiffness matrix due to centripetal acceleration.

- **105** Lumped mass matrix.
- **157** Material model 29 (non cross-section elements), see *Notes*.
- **170** Suppress transfer of shape function arrays to disk.
- **405** Specify geometric properties along beam centroidal axes
- **406** Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
- 418 Output stress resultants relative to beam centroidal axes for eccentric elements

Notes on Use

- 1. The semiloof beam element is based on a <u>Kirchhoff</u> hypothesis for thin beams (i.e. the exclusion of shearing deformations).
- 2. The variation of axial force, moments and torsion can be regarded as linear along the length of the element. Shear forces are constant along the length of the element.
- 3. The loof rotations θ_1 and θ_2 refer to rotations about the element at the loof positions. A positive loof rotation is defined by a right-hand screw rule applied to a vector running in the local x-axis direction along the element edge.
- 4. Input of geometric properties (OPTION 405) and loads (OPTION 406), and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axes. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line.
- 5. For nonlinear material model 29 the following geometric properties are appended to those already specified (see *Geometric Properties*).
 - A^p, Zyy^p, Zzz^p, Zy^p, Zz^p, S^p at each node (i.e. nodes 1, 2, 3).
 - A^p Plastic area (=elastic area)
 - Zyy^p, Zzz^p Plastic moduli for bending about y, z axes
 - Zy^p, Zz^p Plastic moduli for torsion about y, z axes.
 - S^p Plastic area for shear (S^p=0).

Where the fully plastic torsional moment = $\sigma y (Zy^p + Zz^p)$

- 6. For nonlinear material model 29 the following ifcode parameters should be
 - ifcode=1 for circular hollow sections.
 - ifcode=2 for solid rectangular sections.

- 7. Semiloof beam elements should be used with semiloof shell elements. For beam only problems, BS3/BS4 elements should be used.
- 8. Temperature dependent properties cannot be used with material model 29.
- 9. Integration of the element stiffness matrix is performed using selective integration, with a 2-point Gauss rule for the axial and flexural strain energy, and a 3-point Gauss rule for the torsional strain energy. The selective integration technique is implemented in a similar manner to the method proposed by Hughes [H4], i.e. the strain-displacement matrix for the bending and axial strains is evaluated at the reduced rule quadrature points and then extrapolated to the sampling locations of the 3-point quadrature rule. The material response is then assessed at the 3-point Gauss rule.
- 10. The <u>rigidity matrix</u> for BSL3 and BSL4 is evaluated explicitly from the geometric properties for both linear and nonlinear materials.
- 11. Stiffness and mass factors allow different geometric properties to be used in the calculation of the stiffness and mass matrices. Stiffness factors are also used in the processing of stress and strains loads whilst the mass factors are used in the processing of body forces loads. The values are input after all geometric properties and the keyword MODIFICATION_FACTORS must be added to the GEOMETRIC PROPERTIES input command

Restrictions

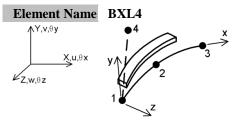
- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature

Recommendations on Use

- The primary use of this element is to provide a beam stiffener for the semiloof shell (QSL8) for analysing stiffened shell structures.
- The BS3 and BS4 elements are more effective for linear analysis of 3D frame structures with curved members and nonlinear analysis of three dimensional beam, frame and arch structures.
- The 2-noded straight beam (BMI21) is the most effective for linear analysis of structures containing straight members of constant cross-section, e.g. space frames.

3D Semiloof Thin Beam Element with Quadrilateral Cross-Section

General

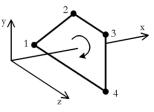


Element Group	Beams
Element	Semiloof Beams
Subgroup	
Element	A curved beam element in 3D which can be mixed with the semiloof shell
Description	element. The element has a quadrilateral cross section which may vary
	along the element. Shearing deformations are excluded.
Number Of	4. The 4th node is used to define the local xy-plane.
Nodes	
Freedoms	U, V, W, θx , θy , θz : at end nodes. U, V, W, θ_1 , θ_2 : at mid-length node.
Node	X, Y, Z: at each node.
Coordinates	

Geometric Properties

y1, z1, y2, z2, y3, z3, y4, z4: local cross section coordinate pairs at each node; followed by nt12, nt14: number of <u>Newton-Cotes</u> integration points in the direction defined by the local cross-section points 1-2 and 1-4 (zero indicates default values). Multiple quadrilateral cross-sections can be used to build up complex beam cross-sections.

Note. The corners of the quadrilateral are numbered clockwise about the local x-axis (the beam nodal line), that is, a right-hand screw rule in the direction of increasing x.



Material Properties

Matrix Joint	Isotropic: Not applicable Not applicable Not applicable	MATERIAL PROPERTIES (Elastic: Isotropic)
Elasto-Plastic	**	Not applicable.
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker- Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr- Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Optimised Implicit Von Mises:	MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic)
	Volumetric Crushing:	Not applicable
	Stress Potential	STRESS POTENTIAL VON_MISES (Isotropic: von Mises, Modified von Mises)
Creep	AASHTO	CREEP PROPERTIES (Creep)
	AASIITO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO
		(Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP
		(Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE
	IRC	(Concrete creep model to EUROCODE_2)
		MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of

Damage	Not applicable	Practice) DAMAGE PROPERTIES SIMO, OLIVER (Damage)
	Not applicable	
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Rubber	Not applicable	
Generic Polymer	Not applicable	
Composite	Not applicable	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, W, θx , θy , θz : at end
		nodes. U, V, W, θ_1 , θ_2 at mid-side node.
Concentrated Loads	CL	Concentrated loads Px, Py, Pz, Mx, My, Mz at end nodes (global). Px, Py, Pz, M1, M2: at mid-side node (M1 and M2 local).
Element Loads	ELDS	 Element loads on nodal line (load type number LTYPE *10 defines the corresponding element load type on beam axis) LTYPE, S1, Px, Py, Pz, Mx, My, Mz LTYPE=11: point loads and moments in local directions. LTYPE=12: point loads and moments in global directions. LTYPE=12: point loads and moments in global directions. LTYPE=21: uniformly distributed loads in local directions. LTYPE=22: uniformly distributed loads in global directions. LTYPE=23: uniformly distributed projected loads in global directions. LTYPE=23: uniformly distributed projected loads in global directions. LTYPE, S1, Wx1, Wy1, Wz1, Mx1, My1, Mz1, S2, Wx2, Wy2, Wz2, Mx2, My2, Mz2 LTYPE=31: distributed loads in global directions. LTYPE=32: distributed projected loads in global directions. LTYPE=31: distributed loads in global directions. LTYPE=31: distributed projected loads in global directions. LTYPE=31: distributed projected loads in global directions. LTYPE=41: trapezoidal loads in local directions. LTYPE=42: trapezoidal loads in global directions. LTYPE=43: trapezoidal projected loads in global

		directions.
Distributed Loads	UDL	Uniformly distributed loads. Wx, Wy, Wz: for element in local directions.
	FLD, FLDG	Not applicable.
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Zcbf, Ωx , Ωy , Ωz , αx , αy , αz
	BFP, BFPE	Body force potentials at nodes/for element. ϕ_1 , ϕ_2 ,
		φ3, 0, Xcbf, Ycbf, Zcbf
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Accelerations. Ax, Ay, Az: at nodes.
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element.
Stress/Strains		Components: Fx, My, Mz, 0,0, 0, &x, ψ y, ψ z, 0, 0,
		0, (σx , σxy , σxz , σyz , εx , εxy , εxz , εyz) Bracketed terms repeated for each fibre integration point.
	SSIG	Initial stresses/strains at Gauss points. These stresses/strains are specified in the same manner as SSI and SSIE
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element.
		Components: $0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0$
		σ xy, σ xz, σ yz,) Bracketed terms repeated for each fibre integration point.
	SSRG	Residual stresses at Gauss points. These stresses are specified in the same manner as SSR and SSRE.
Target	TSSIE, TSSIA	Target stresses/strains at nodes/for element.
Stress/Strains		Components: Fx, My, Mz, 0,0, 0, ε x, ψ y, ψ z, 0, 0,
		0, (σx, σxy, σxz, σyz, εx, εxy, εxz, εyz) Bracketed terms repeated for each fibre integration point.
	TSSIG	Target stresses/strains at Gauss points. These stresses/strains are specified in the same manner as TSSIE and TSSIA
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, dT/dy, dT/dz, To, 0, dTo/dy, dTo/dz
Overburden	Not applicable.	
Phreatic Surface		
	applicable.	
Field Loads	Not applicable.	

Temp Dependent Not Loads applicable.

LUSAS Output

Solver Force (default): Fx, My, Mz, Txz, Txy, Fy, Fz: in local directions. Total torque = Txz+Txy. Continuum stresses (Option 172): σx , σxy , σxz , σyz : in local directions. Strain/curvatures (default): εx , ψy , ψz , ψxz , ψxy , γyz : in local directions (see *Notes*). Total torsional strain = $\psi xy + \psi yz$. Continuum strains (Option 172): Ex, Exy, Exz, Eyz: in local directions. By default element output is with respect to the nodal line. OPTION 418 outputs stress/strain resultants with respect to the beam centroidal axes.

Modeller See Results Tables (Appendix K).

Local Axes

□ Standard line element The local xy-plane is defined by the 2 end nodes of the beam and the 4th node. The local y-axis is perpendicular to the x-axis and positive on the side of the element where the 4th node lies. The local y and z-axes form a right-hand set with the local x-axis.

Sign Convention

Standard beam element

Formulation

Geometric Nonlinearity

Total Lagrangian For large displacements, large rotations and small strains. Updated Not applicable. Lagrangian Eulerian Not applicable. **Co-rotational** Not applicable.

Integration Schemes

Default.	2-point torsion, 2-point bending.
Fine.	As default.
Default.	3-point.
Fine.	As default.
	Fine. Default.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- 32 Suppress stress output (but not stress resultant).
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity.
- **102** Disable load correction stiffness matrix due to centripetal acceleration.
- **105** Lumped mass matrix
- 139 Output inelastic Gauss points only
- 170 Suppress transfer of shape function arrays to disk
- 172 Form the **<u>rigidity matrix</u>** by numerical cross section integration.
- 406 Specify CBF, UDL, SSI, SSR and TEMP loads along beam centroidal axes
- 418 Output stress resultants relative to beam centroidal axes for eccentric elements

Notes, Assumptions and Limitations

- 1. The semiloof beam element formulation is based on a <u>Kirchhoff</u> hypothesis for thin beams (i.e. shearing deformations are excluded). The variation of axial force, bending and torsion along the length of the element may be considered as linear. Shear forces are constant.
- 2. Input of loads (OPTION 406), and output of stress/strain resultants (OPTION 418) are with respect to the beam centroidal axes. CL is always input with respect to the nodal line; displacements are output with respect to the nodal line. Fiber stress/strain results are output at their actual location.
- 3. The torsional constant is estimated from the computed values for Iyy and Izz, Jxx = Iyy + Izz.

- 4. For nonlinear material models, fibre integration is used across the cross-sectional area of the beam. Only axial deformation is considered in the plasticity computations, any torsional deformation is assumed to remain elastic.
- 5. Computing the <u>rigidity matrix</u> by integration through the cross-section depth of the beam is necessary for all nonlinear material models (except 29). By default option 172 is invoked automatically and a 5*5 point <u>Newton-Cotes integration</u> rule is used.
- 6. By default, the **rigidity matrix** is evaluated explicitly for linear materials. A 3*3 point **Newton-Cotes integration** rule may be invoked using option 172. Numerical cross section integration enables top, middle and bottom stress output.
- 7. Integration of the element stiffness matrix is performed using selective integration, with a 2-point Gauss rule for the axial and flexural strain energy, and a 3-point Gauss rule for the torsional strain energy. The selective integration technique is implemented in a similar manner to the method proposed by Hughes, i.e. the strain-displacement matrix for the bending and axial strains is evaluated at the reduced rule quadrature points and then extrapolated to the sampling locations of the 3-point quadrature rule. The material response is then assessed at the 3-point Gauss rule.

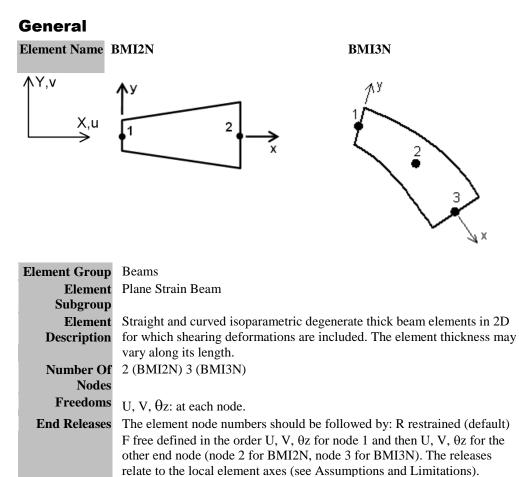
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature

Recommendations on Use

- The element's primary use is to provide a beam stiffener for the semiloof shell (QSL8) for analysing stiffened shell structures.
- The BSX4 element is more effective for linear analysis of 3D frame structures with curved members and nonlinear analysis of three dimensional beam, frame and arch structures.
- The 2-noded straight beam (BMS21) is the most effective for linear analysis of structures containing straight members of constant cross-section, e.g. space frames.

2D Plane Strain Beam Elements



Node X, Y: at each node. **Coordinates**

Geometric Properties

t1, t2, t3 Thickness at each node.

Linear Isotropic: Matrix Not applicable MATERIAL PROPERTIES (Elastic: Isotropic)

Joint	Not applicable	
Concrete	Not applicable	
Elasto-Plastic	Stress resultant	Not applicable.
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker-Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr-Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Optimised Implicit Von Mises:	MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic)
	Volumetric Crushing:	Not applicable.
	Stress Potential	STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises
Creep		Orthotropic: Hill, Hoffman) CREEP PROPERTIES (Creep)
Creep	AASHTO	MATERIAL PROPERTIES NONLINEAR 86
		AASHTO (Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB-FIP
		(Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86
		EUROCODE (Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC
		(Concrete creep model to Indian IRC code of

Damage		Practice) DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic	Not applicable	
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Rubber	Not applicable	
Generic Polymer	Not applicable	
Composite	Not applicable	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, θ z: at nodes.
Concentrated Loads	CL	Concentrated loads. Px, Py, Mz: at nodes (global).
Element Loads	ELDS	Element loads on nodal line (load type number LTYPE *10 defines the corresponding element load type on beam axis, see Notes) LTYPE, S1, Px, Py, Mz LTYPE=11: point loads and moments in local directions. LTYPE=12: point loads and moments in global directions. LTYPE, 0, Wx, Wy, 0 LTYPE=21: uniformly distributed loads in local directions. LTYPE=22: uniformly distributed loads in global directions. LTYPE=23: uniformly distributed projected loads in global directions LTYPE=31: distributed loads in local directions. LTYPE=31: distributed loads in local directions. LTYPE=32: distributed loads in global directions. LTYPE=32: distributed loads in global directions. LTYPE=33: distributed projected loads in global directions LTYPE=31: trapezoidal loads in local directions. LTYPE=41: trapezoidal loads in global directions. LTYPE=42: trapezoidal loads in global directions.

		LTYPE=43: trapezoidal projected loads in global directions
Distributed Loads	UDL	Uniformly distributed loads. Wx, Wy: forces/unit length for element in local directions.
	FLD	Not applicable.
Body Forces	CBF	Constant body forces for element.
		Xcbf, Ycbf, Ωx , Ωy , Ωz , αz
	BFP, BFPE	Body force potentials at nodes/for element. φ_1 ,
	,	ϕ_{2} , 0, 0, Xcbf, Ycbf
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations		Acceleration. Ax, Ay: at nodes.
	SSI, SSIE	Initial stresses/strains at nodes/for element.
Stress/Strains		Components: Nx, 0, Mx, 0, Sxy, ε x, 0, γ x, 0,
		ε components: Txx , 0 , Mx , 0 , Sxy , εx , 0 , $7x$, 0 , ε xy, $(\sigma x, \sigma xy, \sigma z, \varepsilon x, \varepsilon xy, \varepsilon z)$ Bracketed terms repeated for each fibre integration point.
	SSIG	Initial stresses/strains at Gauss points. These stresses/strains are specified in the same manner as SSI and SSIE.
Residual Stresses	SSR, SSRE,	Residual stresses at nodes/for element.
		Components: 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, (σ x,
		σ xy, σ z) Bracketed terms repeated for each
		fibre integration point.
	SSRG	Residual stresses at Gauss points for element
		Components: 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, (σ x,
		σ_{xy}, σ_{z}) Bracketed terms repeated for each fibre integration point.
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. Fx, Fy, Mz: axial force, shear force and moment
		in local directions. εx , εy , ψz : axial, shear and flexural strains in local directions.
	TSSIG	Target stresses/strains at Gauss points. These stresses/strains are specified in the same manner as TSSIE and TSSIA.
Temperatures	TEMP, TMPE	Temperatures at nodes/for elements. T, 0, dT/dy, 0, To, 0, dTo/dy, 0 in local directions.
Phreatic surface	Face_Pressure	The fluid pressure is applied in the –y direction of the element y axis
Field Loads	Not applicable.	

Temp Dependent Not applicable. Loads

LUSAS Output

Solver	Force. Nx, Nz, Mx, Mz, Sxy: axial and normal forces, moments/unit width in local directions, shear force. NB. The plate/shell convention is used for the moment definition.
	Strain. εx , εz , γx , γz , εxy axial, normal, flexural and shear strains.
	Continuum stresses: σx , σxy , σz in local directions.
	Strain: Ex, Exy, Ez: Axial, shear and normal strains in local directions.

Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

□ The local x-axis lies along the line of the element in the direction in which the nodes are numbered. The local y and z-axes form a right-hand set with the local x-axis such that the y-axis lies in the global XY-plane with the z-axis parallel to the global Z-axis.

Sign Convention

□ Standard shell element. Axial and circumferential moments are positive for tension on element top fibre (the top fibre lies on the positive local y side of the element).

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements, small rotations and small strains
Updated	Not applicable.
Lagrangian	
Eulerian	Not applicable.
Co-rotational	Not applicable.

Integration Schemes

Stiffness	Default.	1-point (BMI2N), 2-point (BMI3N).
	Fine.	Same as default.

MassDefault.2-point (BMI2N), 3-point (BMI3N).Fine.Same as default.

Note: A 3-point <u>Newton-Cotes integration</u> rule is also available for BMI3N using OPTION 134. This may be more applicable for infinitesimal strain, elasto-plastic analyses of plane frames with straight members since the first and third quadrature points will coincide with the frame joints. See Appendix I of the Theory Manual.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- 36 Follower loads
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity.
- 102 Switch off load correction stiffness matrix due to centripetal acceleration
- 105 Lumped mass matrix.
- 134 Gauss to <u>Newton-Cotes</u> in plane (in the local x direction) integration for elements
- 139 Output yielded integration points only.
- **403** Introduce residual bending flexibility correction for 2-node thick beam BMI21, see Assumptions and Limitations.
- **404** Compute equivalent nodal loading from equilibrium considerations for 2-node thick beam BMI21, see Assumptions and Limitations.

Notes, Assumptions and Limitations

- 1. The element is formulated from the degenerate continuum concept, i.e. enforcing directly the modified Timoshenko hypothesis for thick beams to the continuum theory. Plane cross-sections initially normal to the beam axis remain plane and undistorted (the shape of the cross-section remains unchanged) under deformation, but do not necessarily remain normal to the beam axis. Shearing deformations are included.
- 2. OPTION 36 is only applicable for use with element load types FLD, ELDS, UDL and phreatic surface pressure. Specifying this option makes these element loads follow the element geometry as the analysis progresses.
- 3. When OPTION 403 is specified to introduce residual bending flexibility correction (on by default), for BMI2N, the axial force is constant, while the shear force and moment vary linearly along the length of the beam. For BMI3N the axial force, shear force and moment all vary linearly along the length

- 4. When BMI2N is used together with OPTION 403 to introduce residual bending flexibility correction, its stiffness matrix is enhanced to the order of a cubic. As the plane strain beam can only be of rectangular cross section, a shear area based on 5/6 of the nodal thicknesses is assumed in this process.
- 5. When BMI2N is used together with OPTION 404, loading that varies along the element length is accounted for in the force diagrams (i.e. for a beam under CBF or internal element loading). A post-processing technique has been introduced to obtain accurate quadratic bending moments for BMI3N. For BMI2N (with OPTION 404) and BMI3, internal forces and moments are output at intervals of 1/10th of the element length by specifying the Gauss point option from the Output button of the LUSAS Datafile dialog.
- 6. The end releases for this element allow a joint to be modelled between adjacent elements. These joints allow rotation and translation of one beam with respect to another without load transferral. The rotations and translations remain in the local directions of the beam elements and support large deformations.
- 7. When a nonlinear material is used with this element the transverse shear stresses are excluded from the plasticity computations i.e. the transverse shear stresses are assumed to remain elastic. This means that if a nonlinear material is used in applications where transverse shear tends to dominate the stress field the equivalent von Mises and maximum principal stresses can exceed the uniaxial yield stress.
- 8. When a step by step dynamic analysis is carried out using BMI elements with distributed loading, the "free body force diagrams" pertaining to applied loading, are not superimposed on the nodal values, to do so would lead to erroneous results until a steady state is reached. It should therefore be noted that different force diagrams will be obtained for BMI elements if static and dynamic analyses are directly compared.
- 9. OPTION 87 considers large displacements and large rotations using a Total Lagrangian formulation; OPTION 229 considers large displacements and large rotations using a co-rotational formulation. In general the co-rotational formulation works better. When both options 87 and 229 are true, a local Total Lagrangian formulation will be used within a global co-rotational framework.
- 10. End releases for these elements are currently not valid for use in step-by-step dynamic analyses.

Restrictions

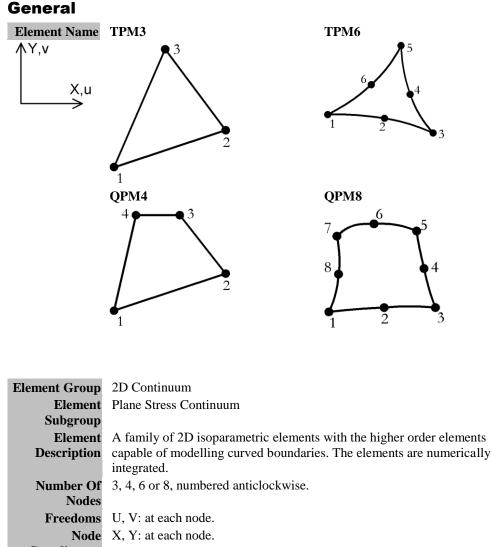
- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature

Recommendations on Use

• The element may be used for linear and nonlinear analysis of two dimensional long structures of box girder cross-sections such as tunnel linings and retaining walls for which the plane strain assumption is appropriate.

Chapter 3 : 2D Continuum Elements.

2D Plane Stress Continuum Elements



Coordinates

Geometric Properties

t1... tn Thickness at each node.

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC (Elastic: Orthotropic Plane Stress)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC 3
	Anisou opic.	(Elastic: Anisotropic Thin Plate)
	Rigidities.	RIGIDITIES 3 (Rigidities: Membrane/Thin Plate)
Matrix	Not applicable	
Joint	Not applicable	
Concrete		MATERIAL PROPERTIES NONLINEAR 105
		(Elastic: Isotropic, Plastic: Transient Smoothed Multi-Crack Concrete)
		MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi- Crack Concrete)
Elasto-Plastic	Stress resultant:	Not applicable.
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker-Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr-Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Volumetric Crushing:	Not applicable
	Interface:	MATERIAL PROPERTIES NONLINEAR 27
	Stress Potential	STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises
		Orthotropic: Hill, Hoffman)
Creep		CREEP PROPERTIES (Creep)
-	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO
		(Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86
		400

		CEB-FIP (Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE
	IRC	(Concrete creep model to EUROCODE_2) MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic	Not applicable	
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Ko Initialisation	Not applicable	
Rubber	Not applicable	
Generic Polymer	Isotropic	MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)
Composite	Not applicable	

Loading

Prescribed Value Concentrated		Prescribed variable. U, V: at nodes. Concentrated loads. Px, Py: at nodes.
Loads		
Element Loads	Not applicable.	
Distributed Loads	UDL	Not applicable.
	FLD	Face Loads. Px, Py: Local Face Axis Pressures At Nodes.
	FLDG	Global Face Loads. σx , σy , σzxy at nodes
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Ωx ,
	BFP, BFPE	$\Omega y, \Omega z, \alpha z$ Body force potentials at nodes/for element. 0, 0, 0, ϕ 4, Xcbf, Ycbf
Velocities	VELO	Velocities. Vx, Vy: at nodes.

Accelerations	ACCE	Accelerations. Ax, Ay: at nodes.
Initial Stress/Strains	SSI, SSIE	Initial stresses/strains at nodes/for element. σx , σy , σxy : global stresses. εx , εy , γxy : global strains.
	SSIG	Initial stresses/strains at Gauss points. σx , σy , σxy : global stresses. ϵx , ϵy , γxy : global strains.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. σx , σy , σxy : global stresses.
	SSRG	Residual stresses at Gauss points. σx , σy , σxy : global stresses.
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. σx , σy , σxy : global stresses. εx , εy , γxy : global strains.
	TSSIG	Target stresses/strains at Gauss points. σx , σy , σxy : global stresses. εx , εy , γxy : global strains.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0, 0
Overburden	Applicable.	
Phreatic Surface	Applicable.	
Field Loads	Not applicable.	
Temp Dependent Loads	Not applicable.	

LUSAS Output

SolverStress resultants: Nx, Ny, Nxy, Nmax, Nmin, β , Ns, NeStress (default): σx , σy , σxy , σmax , σmin , β , σs , σe (see description of principal stresses)Strain: ϵx , ϵy , γxy , ϵmax , ϵmin , β , ϵs , ϵe ModellerSee Results Tables (Appendix K).

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 2D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and large rotations.
Updated	For large displacements and large rotations.
Lagrangian	
Eulerian	For large displacement, large rotations and moderately large strains.
Co-rotational	For large displacements and large rotations.

Integration Schemes

Stiffness	Default.	1-point (TPM3), 3-point (TPM6), 2x2 (QPM4, QPM8)
	Fine (see Options).	3x3 (QPM8), 3-point (TPM3).
Mass	Default.	1-point (TPM3), 3-point (TPM6), 2x2 (QPM4, QPM8)
	Fine (see Options).	3x3 (QPM8), 3-point (TPM3).

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- **18** Invokes fine integration rule.
- **34** Output element stress resultants.
- **36** Follower loads (see Notes)
- 54 Updated Lagrangian geometric nonlinearity.
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity.
- 91 Invokes fine integration rule for mass matrix.
- 105 Lumped mass matrix.
- **123** Clockwise node numbering.
- 139 Output yielded Gauss points only
- **167** Eulerian geometric nonlinearity.
- 229 Co-rotational geometric nonlinearity

Notes on Use

- 1. The element formulations are based on the standard isoparametric approach. The variation of stresses within an element can be regarded as constant for the lower order (corner node only) elements, and linear for the higher (mid-side node) elements.
- 2. All elements pass the patch test.
- 3. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the face loading (FLD).
- 4. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it is only applicable if **every** element is numbered **clockwise**. Surface normals should be visualised and if necessary corrected in the pre-processing stage.
- 5. If applying an initial stress/strain or thermal load that varies across an element, a higher order element (6 or 8 nodes) should be used. A limitation of the standard isoparametric approach when used for lower order elements (3 or 4 nodes) is that only constant stress/strain fields can be imposed correctly.

Restrictions

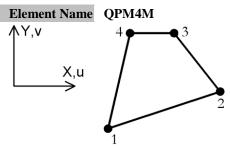
- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

Recommendations on Use

- The 8-noded element with a 2*2 Gauss rule is usually the most effective element, as the under-integration of the stiffness matrix prevents locking, which may occur either when the element is subjected to <u>parasitic shear</u>, or as the material reaches the incompressible limit (elasto-plasticity). The Gauss point stresses are also sampled at the most accurate locations for the element. However, the element does possess one spurious zero energy mode. This mode is very rarely activated in linear analysis, but it may occur in both materially and geometrically nonlinear analyses. Therefore, a careful examination of the solution should be performed, to check for spurious stress oscillations and peculiarities in the deformed configuration.
- The 8-noded element with a 3*3 Gauss rule may be used if a spurious mechanism is excited with the 2*2 Gauss rule.
- The 4-noded element should not be used for analyses where in-plane bending effects are significant as the element tends to lock in <u>parasitic shear</u> [C1], e.g. if QPM4 elements are employed to model a cantilever subject to a point load, the solution obtained will be over-stiff.

2D Plane Stress Continuum Element with Enhanced Strains

General



Element Group	2D Continuum
Element	Plane Stress Continuum
Subgroup	
Element	A 2D isoparametric element with an assumed strain field. This mixed
Description	assumed strain element demonstrates a superior performance to QPM4
	(see Notes). The elements are numerically integrated.
Number Of	4, numbered anticlockwise.
Nodes	
Freedoms	U, V: at each node.
Node	X, Y: at each node.
Coordinates	

Geometric Properties

t1... tn Thickness at each node.

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC
		(Elastic: Orthotropic Plane Stress)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC 3
		(Elastic: Anisotropic Thin Plate)

Matrix Joint	Rigidities: Not applicable Not applicable	RIGIDITIES 3 (Rigidities: Membrane/Thin Plate)
Concrete		MATERIAL PROPERTIES NONLINEAR 105 (Elastic: Isotropic, Plastic: Transient Smoothed Multi-Crack Concrete) MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Elasto-Plastic	Stress resultant:	Not applicable
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker- Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr- Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Volumetric Crushing:	Not applicable
	Stress Potential	STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
Creep	AASHTO	CREEP PROPERTIES (Creep)
	AASHIO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP (Concrete creep model to CEB-FIP Model Code
	Chinasa	1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2)

Damage	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice) DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic	Not applicable	
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Ko Initialisation	Not applicable	
Rubber	Ogden:	MATERIAL PROPERTIES RUBBER OGDEN (Rubber: Ogden) (Rubber: Ogden)
	Mooney- Rivlin:	MATERIAL PROPERTIES RUBBER MOONEY_RIVLIN (Rubber: Mooney-Rivlin)
	Neo-Hookean:	MATERIAL PROPERTIES RUBBER NEO_HOOKEAN (Rubber: Neo-Hookean)
	Hencky:	MATERIAL PROPERTIES RUBBER HENCKY (Rubber: Hencky)
Generic Polymer	Isotropic	MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)
Composite	Not applicable	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V: at nodes.
Concentrated Loads	CL	Concentrated loads. Px, Py: at nodes.
Element Loads	Not applicable.	
Distributed Loads	UDL	Not applicable.
	FLD	Face loads. Px, Py: local face axis pressures at nodes.
Body Forces	FLD	Global Face Loads. σx, σy, σxy at nodes
	CBF	Constant body forces for element. Xcbf, Ycbf, Ωx ,
	BFP, BFPE	Ω y, Ω z, α z Body force potentials at nodes/for element. 0, 0, 0, 04, Xcbf, Ycbf
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Accelerations. Ax, Ay: at nodes.
Initial Stress/Strains	SSI, SSIE	Initial stresses/strains at nodes/for element. σx , σy ,
		σ xy: global stresses. ε x, ε y, γ xy: global strains.

Residual Stresses Target Stress/Strains	SSIG	Initial stresses/strains at Gauss points. σx , σy , σxy : global stresses. ϵx , ϵy , γxy : global strains.
	SSR, SSRE	Residual stresses at nodes/for element. σx , σy , σxy : global stresses.
	SSRG	Residual stresses at Gauss points. σx , σy , σxy : global stresses.
	TSSIE, TSSIA	Target stresses/strains at nodes/for element. σx , σy , σxy : global stresses. εx , εy , γxy : global strains.
	TSSIG	Target stresses/strains at Gauss points. σx , σy , σxy : global stresses. εx , εy , γxy : global strains.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0, 0
Overburden	Applicable.	
Phreatic Surface	Applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not applicable.	
Loads		

Output

Solver	Stress resultants: Nx, Ny, Nxy, Nmax, Nmin, β , Ns, Ne		
	Stress (default): σx , σy , σxy , σmax , σmin , β , σs , σe (see <u>description</u> <u>of principal stresses</u>)		
Strain: ε_x , ε_y , γ_{xy} , ε_{max} , ε_{min} , β , ε_s , ε_e			
	Stretch (for rubber only): V11, V22, V12, λ 1, λ 2, λ 3, $\theta\lambda$, det F. Where		
	V_{ii} are components of the left stretch tensors, λ_i the principal stretches		
	$\theta\lambda$ the angle between the maximum principal stretch and the global X axis, and det F the determinant of the deformation gradient or volume ratio.		
Modeller	See <u>Results Tables (Appendix K)</u> .		

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 2D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and large rotations.
Updated Lagrangian	For large displacements and large rotations.
Eulerian Co-rotational	For large displacements, large rotations and moderately large strains. For large displacements and large rotations (large strains with rubber).

Integration Schemes

Stiffness Default.	2x2
Fine.	As default.
Mass Default.	2x2
Fine.	As default.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- **34** Output element stress resultants.
- 36 Follower loads.
- **39** Stress smoothing for rubber material models.
- 54 Updated Lagrangian geometric nonlinearity.
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity.
- 91 Invokes fine integration rule for mass matrix.
- **105** Lumped mass matrix.
- 123 Clockwise node numbering (see *Notes*).
- 139 Output yielded Gauss points only
- **167** Eulerian geometric nonlinearity.
- 225 Use alternative number of parameters for enhanced strain interpolation (see *Notes*).
- **229** Co-rotational geometric nonlinearity.

Notes on Use

- 1. The variation of stresses within an element can be regarded as linear.
- 2. The element passes the patch test and the large strain patch test for rubber.
- 3. The strain field for this element consists of two parts: the compatible strains derived from an assumed displacement field and the assumed enhanced strains (see *LUSAS Theory Manual*). The assumed enhanced strain field is defined using 5 or 4 parameters for linear and nonlinear applications respectively. Option 225 switches on the higher 5 parameter enhanced strain interpolation function for nonlinear analysis.
- 4. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility. The load does not have to be normal to the face and may also vary over the face.
- 5. To apply a non-conservative (follower) pressure load (load type FLD) with corotational geometric nonlinearity, Option 36 must be specified. Note that this load must be normal to the face and constant for all the nodes of the element face.
- 6. The converged stresses for rubber are Kirchoff stresses (see LUSAS Theory Manual).
- 7. When using the rubber material model, converged strain output is replaced by the left stretch tensor, the principal stretches and the angle defining these principal directions. The value of det $F = \lambda_1 \lambda_2$ (the Volume ratio) is only available for Gauss-point output. (Refer to the *LUSAS Theory Manual* for more details.)
- 8. For rubber, the iterative values of stress and strain are output in local co-rotated directions at the Gauss points only.
- 9. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it is only applicable if **every** element is numbered **clockwise**. Surface normals should be visualised and if necessary corrected in the pre-processing stage.
- 10. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.
- 11. Convergence difficulties can sometimes arise when using enhanced strain elements with nonlinear materials, particularly if the material is elastic perfectly plastic or if a very shallow hardening curve is defined. In such cases it is recommended that the standard element formulation is used.
- 12. In analyses where significant in-plane bending is thermally induced it is recommended that a nonlinear solution is used. If a linear solution is required, then quadratic plane strain elements QPN8 are recommended.

Restrictions

- □ Avoid excessive aspect ratio
- □ Rubber material models can only be applied in conjunction with the co-rotational formulation, Option 229.

Recommendations on Use

These elements exhibit an improved performance when compared with the parent element QPM4. The integration rules are the same as those given for QPM4, but the elements do not suffer from locking due to parasitic shear when the material approaches the incompressible limit. The elements are also free of any zero energy modes.

2D Plane Stress Continuum Crack Tip Elements

General	
Element Name	TPK6 QPK8
∧Y,v X,u	7 6 1 2 Crack specified at Node 1 7 8 1 2 Crack specified at Node 1
Element Group	
Element	Plane Stress Continuum
Subgroup	
Element Description	
Description	be located at any corner node. The mid-side nodes are moved to the quarter points to produce a singularity at the crack tip. The strains vary as the square root of 1/R, where R is the distance from the crack tip. These elements are used at the crack tip only and should be mixed with the higher order plane strain continuum elements. The elements are numerically integrated.
	6 or 8 numbered anticlockwise.
Nodes	
End Releases	
Freedoms	
Node Coordinates	X, Y: at each node.

Geometric Properties

t1... tn Thickness at each node.

Material Properties

Linear Isotropic:

MATERIAL PROPERTIES (Elastic: Isotropic)

	Orthotropic	MATERIAL PROPERTIES ORTHOTROPIC (Elastic: Orthotropic Plane Stress)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC 3 (Elastic: Anisotropic Thin Plate)
	Rigidities.	RIGIDITIES 3 (Rigidities: Membrane/Thin Plate)
Matrix	Not applicable	
Joint	Not applicable	
Concrete		MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Elasto-Plastic		Not applicable.
	resultant:	
	Interface:	MATERIAL PROPERTIES NONLINEAR 27
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker- Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr- Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Volumetric Crushing:	Not applicable.
	Stress Potential	STRESS POTENTIAL VON_MISES, HILL, HOFFMAN
Creep		(Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman) CREEP PROPERTIES (Creep)
ercep	AASHTO	MATERIAL PROPERTIES NONLINEAR 86
		AASHTO (Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP
	Chinese	(Concrete creep model to CEB-FIP Model Code 1990)
		MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86

(Concrete creep model to EUROCODE_2)

Damage	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice) DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic Shrinkage	Not applicable	SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Ko Initialisation Rubber	Not applicable Not applicable	
Generic Polymer	Isotropic	MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)
Composite	Not applicable	

EUROCODE

Loading

PDSP, TPDSP CL	Prescribed variable. U, V: at nodes. Concentrated loads. Px, Py: at nodes.
Not applicable.	
UDL	Not applicable.
FLD	Face loads. Px, Py: local face axis pressures at nodes.
FLDG	Global Face Loads. σx , σy , σxy at nodes
CBF	Constant body forces for element. Xcbf, Ycbf, Ωx ,
	Ω y, Ω z, α z
BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0, φ4, Xcbf, Ycbf
VELO	Velocities. Vx, Vy: at nodes.
ACCE	Accelerations. Ax, Ay: at nodes.
SSI, SSIE	Initial stresses/strains at nodes/for element. σx , σy ,
	σ xy: global stresses. Ex, Ey, γ xy: global strains.
SSIG	Initial stresses/strains at Gauss points. σx , σy , σxy :
	global stresses. Ex, Ey, Yxy: global strains.
SSR, SSRE	Residual stresses at nodes/for element. σx , σy , σxy : global stresses.
	CL Not applicable. UDL FLD FLDG CBF BFP, BFPE VELO ACCE SSI, SSIE SSIG

	SSRG	Residual stresses at Gauss points. σx, σy, σxy: global stresses.
Target Stress/Strains	,	Target stresses/strains at nodes/for element. σx , σy ,
		σ xy: global stresses. Ex, Ey, γ xy: global strains.
	TSSIG	Target stresses/strains at Gauss points. σx , σy , σxy :
		global stresses. εx, εy, γxy: global strains.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0, 0
Overburden	Applicable.	
Phreatic Surface	Applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not applicable.	
Loads		

LUSAS Output

Solver	Stress resultants: Nx, Ny, Nxy, Nmax, Nmin, β , Ns, Ne		
	Stress (default): σ_x , σ_y , σ_{xy} , σ_{max} , σ_{min} , β , σ_s , σ_e (see <u>description</u> <u>of principal stresses</u>)		
	Strain: ε_x , ε_y , γ_{xy} , ε_{max} , ε_{min} , β , ε_s , ε_e		
Modeller	See <u>Results Tables (Appendix K)</u> .		

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 2D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and large rotations.
Updated	For large displacements and large rotations.
Lagrangian	
Eulerian	For large displacements, large rotations and moderately large strains.

Co-rotational For large displacements and large rotations.

Integration Schemes

Stiffness	Default.	6-point (TPK6), 3x3 (QPK8)
	Fine (see Options).	12-point (TPK6).
Mass	Default.	6-point (TPK6), 3x3 (QPK8)
	Fine (see Options).	12-point (TPK6).

Mass Modelling

□ Consistent mass (default).

□ Lumped mass.

Options

- **18** Invokes finer integration rule.
- **34** Output element stress resultants.
- 54 Updated Lagrangian geometric nonlinearity.
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity.
- 91 Invokes fine integration rule for mass matrix.
- **105** Lumped mass matrix.
- **123** Clockwise node numbering.
- **139** Output yielded Gauss points only.
- 167 Eulerian geometric nonlinearity.
- 229 Co-rotational geometric nonlinearity.

Notes on Use

- 1. The element formulations are based on the standard isoparametric approach. Moving the mid-side nodes to the quarter points creates a singularity with theoretically infinite stress at the corner node.
- 2. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility.

- 3. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it is only applicable if **every** element is numbered **clockwise**. Surface normals should be visualised and if necessary corrected in the pre-processing stage.
- 4. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.

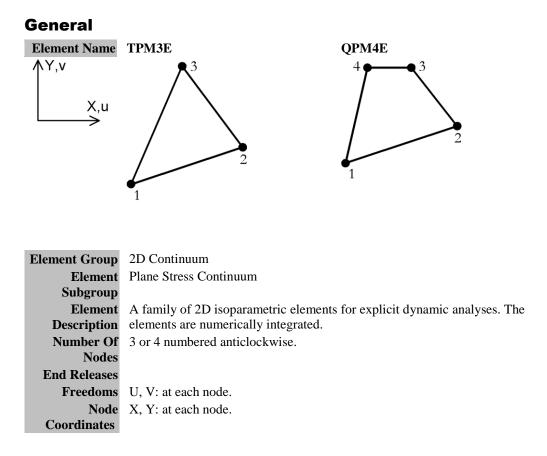
Restrictions

- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

Recommendations on Use

The QPK8 and TPK6 elements are specifically designed for application to fracture mechanics problems and may used to model the singularities that occur at the crack tip. The mid-side nodes near the crack tip are shifted to the quarter point. This ensures a singularity is present at the crack tip and that the strains vary as 1/square root of r where r is the distance from the crack tip. The triangular TPK6 element is more effective than the quadrilateral element.

2D Plane Stress Explicit Dynamics Elements



Geometric Properties

t1... tn Thickness at each node.

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC
		(Elastic: Orthotropic Plane Stress)
	Anisotropic:	Not applicable
	Rigidities.	Not applicable

Distributed Loads UDL

FLD

FLDG

Matrix	Not applicable	
Joint	Not applicable	
Concrete	Not applicable	
Elasto-Plastic	Stress resultant:	Not applicable
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker- Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr- Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Volumetric Crushing:	Not applicable
	Stress Potential	STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
Creep	Not applicable	
-	Not applicable	
U	Not applicable	
	Not applicable	
Ko Initialisation	Not applicable	
Rubber	Not applicable	
Generic Polymer	Not applicable	
Composite	Not applicable	
Loading		
Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V: at each node.
Concentrated Loads	CL	Concentrated loads. Px, Py: at each node.
Element Loads	Not applicable.	
D'.4.1		NT - (1, 1, 1,

Ie. Not applicable. <u>Face loads</u>. Px, Py: local face axis pressures at nodes. Not applicable.

Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Ωx ,
		$\Omega_{y}, \Omega_{z}, \alpha_{z}$
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0, 0, 0, 4, Xcbf, Ycbf
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Accelerations. Ax, Ay: at nodes.
Initial Stress/Strains	SSI, SSIE	Initial stresses/strains at nodes/for element. σx , σy , σxy : global stresses. εx , εy , γxy : global strains.
	SSIG	Initial stresses/strains at Gauss points σx , σy , σxy : global stresses. εx , εy , γxy : global strains.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. σx , σy , σxy : global stresses.
	SSRG	Residual stresses at Gauss points. σx , σy , σxy : global stresses.
Target		
Stress/Strains	applicable.	
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0, 0
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	
Field Loads	Not applicable.	
T T T	Not applicable.	

LUSAS Output

Solver	Stress (default): σ_x , σ_y , σ_{xy} , σ_{max} , σ_{min} , β , σ_s , σ_e (see <u>description</u>
	<u>of principal stresses</u>)
	Strain: εx , εy , γxy , εmax , εmin , β , εs , εe
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 2D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	Not applicable.
Updated	Not applicable.
Lagrangian	
Eulerian	For large displacements, large rotations and moderately large strains.
Co-rotational	For large displacements and large rotations.

Integration Schemes

Default.	1-point (see Notes).
Fine.	As default.
Default.	1-point (see Notes).
Fine.	As default.
	Fine. Default.

Mass Modelling

Lumped mass only (see Notes).

Options

- **34** Output element stress resultants.
- **55** Output strains as well as stresses.
- **105** Lumped mass matrix (see *Notes*).
- 139 Output yielded Gauss points only.

Notes on Use

1. The element formulations are based on the standard isoparametric approach. The variation of stresses within an element can be regarded as constant.

- 2. The system parameter HGVISC is used to restrict element mechanisms due to underintegration. The default value is usually sufficient.
- 3. The bulk viscosity coefficients are used to restrict numerical oscillations due to the traversal of stress waves. The default bulk viscosity coefficients (BULKLF and BULKQF) may be altered as SYSTEM parameters.
- 4. These elements **must** be used with the dynamic central difference scheme and a lumped mass matrix.
- 5. These elements are **not** applicable. for static or eigenvalue analyses.
- 6. Automatic time step calculations are implemented.
- 7. As the element geometry is always updated in an explicit dynamic analysis, a nonlinear solution is obtained. When using explicit dynamics elements nonlinear control must be specified.
- 8. If creep properties are defined, explicit time integration must be specified.
- 9. Non-conservative loading is invoked when the FLD loading facility is applied.
- 10. Rayleigh damping coefficients are not supported by these elements.
- 11. Constraint equations are not available for use with these elements.
- 12. Nodes **must** be specified in an anticlockwise order. Option 123 is **not** applicable for this element. When using Modeller ensure surface normal is in the +ve z direction.

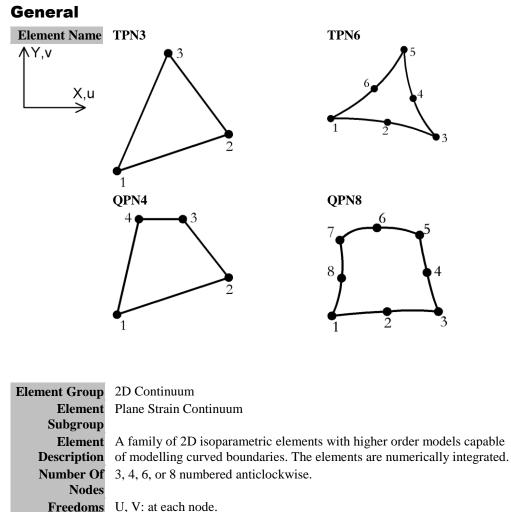
Restrictions

□ Avoid excessive aspect ratio

Recommendations on Use

Explicit dynamics elements may be used to define surface boundaries which will be active in a slideline analysis.

2D Plane Strain Continuum Elements



Node

Coordinates

X, Y: at each node.

Geometric Properties

Not applicable (a unit thickness is assumed).

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC
	-	PLANE STRAIN (Elastic: Orthotropic Plane Strain)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC 4 (Not
		supported in LUSAS Modeller)
	Rigidities.	RIGIDITIES 4 (Not supported in LUSAS Modeller)
Matrix	Not applicable	
Joint	Not applicable	
Concrete		MATERIAL PROPERTIES NONLINEAR 105
		(Elastic: Isotropic, Plastic: Transient Smoothed Multi-
		Crack Concrete)
		MATERIAL PROPERTIES NONLINEAR 109
		(Elastic: Isotropic, Plastic: Smoothed Multi-Crack
		Concrete)
Elasto-Plastic		Not applicable.
	resultant:	
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61
		(Elastic: Isotropic, Plastic: Tresca, Hardening:
		Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker-	MATERIAL PROPERTIES NONLINEAR 64
	Prager:	(Elastic: Isotropic, Plastic: Drucker-Prager,
	Taget.	Hardening: Granular)
	Mohr-	MATERIAL PROPERTIES NONLINEAR 65
	Coulomb:	(Elastic: Isotropic, Plastic: Mohr-Coulomb,
		Hardening: Granular with Dilation)
	Modified	MATERIAL PROPERTIES
	Mohr-	MODIFIED MOHR_COULOMB (Elastic:
	Coulomb:	Isotropic, Plastic: Mohr-Coulomb/Tresca, non-
		associative Hardening with tension/compression
	M. 1.C. 1	cut-off)
	Modified Cam-clay	MATERIAL PROPERTIES CAM_CLAY MODIFIED (Elastic: Isotropic, Plastic)
	Optimised	MATERIAL PROPERTIES NONLINEAR 75
	Implicit Von	(Elastic: Isotropic, Plastic: Von Mises, Hardening:
	Mises:	Isotropic & Kinematic)
	Volumetric	MATERIAL PROPERTIES NONLINEAR 81
	Crushing:	(Volumetric Crushing or Crushable Foam)
	Interface:	MATERIAL PROPERTIES NONLINEAR 27
	Stress	STRESS POTENTIAL VON_MISES, HILL,
	Potential	HOFFMAN
		(Isotropic: von Mises, Modified von Mises
		-

Creep AASI		Orthotropic: Hill, Hoffman) CREEP PROPERTIES (Creep)
	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of
	CEB-FIP	Practice) MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP (Concrete creep model to CEB-FIP Model Code
	Chinese	1990) MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2)
IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)	
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic		VISCO ELASTIC PROPERTIES
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Ko Initialisation		
Rubber Generic Polymer	Not applicable Isotropic	MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)
Composite	Not applicable	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V: at nodes.
Concentrated	CL	Concentrated loads. Px, Py: at nodes.
Loads		
Element Loads	Not applicable.	
Distributed Loads	UDL	Not applicable.
	FLD	Face Loads. Px, Py: local face axis pressures at
		nodes.
	FLDG	Global Face Loads. σ_x , σ_y , σ_{xy} at nodes

Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, 0, 0, Ωz , αz
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0, 0, 0, 0, Xcbf, Ycbf
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay: at nodes.
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element. σx , σy ,
Stress/Strains		σxy, $σz$: global stresses. $εx$, $εy$, $γxy$: global strains.
	SSIG	Initial stresses/strains at Gauss points. σx , σy , σxy ,
		σz: global stresses. εx, εy, γxy: global strains.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. σx , σy , σxy , σz : global stresses.
	SSRG	Residual stresses at Gauss points. σx , σy , σxy , σz global stresses.
Target	TSSIE, TSSIA	Target stresses/strains at nodes/for element. σx , σy ,
Stress/Strains		$σ_{xy}$, $σ_{z}$: global stresses. $ε_x$, $ε_y$, $γ_{xy}$: global strains.
	TSSIG	Target stresses/strains at Gauss points. σx , σy , σxy , σz : global stresses. εx , εy , γxy : global strains.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0
Overburden	Applicable.	
Phreatic Surface	Applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not applicable.	

Loads

LUSAS Output

Solver	Stress (default): σ_x , σ_y , σ_{xy} , σ_z , σ_{max} , σ_{min} , β , σ_s , σ_e (see description of principal stresses)
	Strain: ε_x , ε_y , γ_{xy} , $\varepsilon_z = 0$, ε_{max} , ε_{min} , β , ε_s , ε_e
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 2D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and large rotations.
Updated	For large displacements and large rotations.
Lagrangian	
Eulerian	For large displacements, large rotations and moderately large strains.
Co-rotational	For large displacements and large rotations.

Integration Schemes

V 8)
V 8)
1

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- **18** Invokes finer integration rule.
- **36** Follower loads.
- 54 Updated Lagrangian geometric nonlinearity
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity.
- 91 Invokes fine integration rule for mass matrix.
- 105 Lumped mass matrix.
- 123 Clockwise node numbering.

- 139 Output yielded Gauss points only.
- **167** Eulerian geometric nonlinearity.
- 229 Co-rotational geometric nonlinearity

Notes on Use

- 1. The element formulations are based on the standard isoparametric approach. The variation of stresses within an element can be regarded as constant for the lower order (corner node only) elements, and linear for the higher order (mid-side node) elements.
- 2. All elements pass the **<u>patch test</u>**.
- 3. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility.
- 4. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it is only applicable if **every** element is numbered **clockwise**. Surface normals should be visualised and if necessary corrected in the pre-processing stage.
- 5. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.
- 6. If applying an initial stress/strain or thermal load that varies across an element, a higher order element (6 or 8 nodes) should be used. A limitation of the standard isoparametric approach when used for lower order elements (3 or 4 nodes) is that only constant stress/strain fields can be imposed correctly.

Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

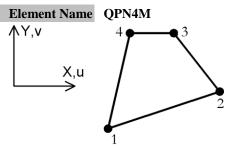
Recommendations on Use

• The 8-noded element with a 2*2 Gauss rule is usually the most effective element, as the under-integration of the stiffness matrix prevents locking, which may occur either when the element is subjected to <u>parasitic shear</u>, or as the material reaches the incompressible limit (elasto-plasticity). The Gauss point stresses are also sampled at the most accurate locations for the element. However, the element does possess one spurious zero energy mode. This mode is very rarely activated in linear analysis, but it may occur in both materially and geometrically nonlinear analyses. Therefore, a careful examination of the solution should be performed, to check for spurious stress oscillations and peculiarities in the deformed configuration.

- The 8-noded element with a 3*3 Gauss rule may be used if a spurious mechanism is excited with the 2*2 Gauss rule.
- The 4-noded element should not be used for analyses where in-plane bending effects are significant as the element tends to lock in **parasitic shear**, e.g. if QPN4 elements are employed to model a cantilever subject to a point load, the solution obtained will be over-stiff.

2D Plane Strain Continuum Element with Enhanced Strains

General



Element Group	2D Continuum
Element	Plane Strain Continuum
Subgroup	
Element	A 2D isoparametric element with an assumed strain field. This mixed
Description	assumed strain element demonstrates a superior performance to QPN4
	(see Notes). The element is numerically integrated.
Number Of	4, numbered anticlockwise.
Nodes	
Freedoms	U, V: at each node.
Node	X, Y: at each node.
Coordinates	

Geometric Properties

Not applicable (a unit thickness is assumed).

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC
		PLANE STRAIN (Elastic: Orthotropic Plane Strain)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC 4 (Not
		supported in LUSAS Modeller)
	Rigidities.	RIGIDITIES 4 (Not supported in LUSAS Modeller)
Matrix	Not applicable	

Joint	Not applicable	
Concrete		MATERIAL PROPERTIES NONLINEAR 105 (Elastic: Isotropic, Plastic: Transient Smoothed Multi- Crack Concrete)
		MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Elasto-Plastic	Stress resultant:	Not applicable.
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker- Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Modified Mohr- Coulomb:	MATERIAL PROPERTIES MODIFIED MOHR_COULOMB (Elastic: Isotropic, Plastic: Mohr-Coulomb/Tresca, non- associative Hardening with tension/compression cut-off)
	Modified Cam-clay Optimised Implicit Von Mises:	MATERIAL PROPERTIES CAM_CLAY MODIFIED (Elastic: Isotropic, Plastic) MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic)
	Volumetric Crushing: Stress Potential	MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam) STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
Сгеер	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP (Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE

		(Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic		VISCO ELASTIC PROPERTIES
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Ko Initialisation	Applicable	
Rubber	Ogden	MATERIAL PROPERTIES RUBBER OGDEN (Rubber: Ogden)
	Mooney-	MATERIAL PROPERTIES RUBBER
	Rivlin	MOONEY_RIVLIN (Rubber: Mooney-Rivlin)
	Neo-Hookean	MATERIAL PROPERTIES RUBBER NEO_HOOKEAN (Rubber: Neo-Hookean)
	Hencky	MATERIAL PROPERTIES RUBBER HENCKY (Rubber: Hencky)
Generic Polymer	Isotropic	MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)
Composite	Not applicable	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V: at nodes.
Concentrated Loads	CL	Concentrated loads. Px, Py: at nodes.
Element Loads	Not applicable.	
Distributed Loads	UDL	Not applicable.
	FLD	Face loads. Px, Py: local face axis pressures at nodes.
	FLDG	Global Face Loads. σx , σy , σxy at nodes
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, 0, 0,
		$\Omega z, \alpha z$
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0, φ4, Xcbf, Ycbf
Velocities	VELO	Velocities. Vx, Vy: at nodes.

Accelerations	ACCE	Acceleration Ax, Ay: at nodes.
Initial Stress/Strains	SSI, SSIE	Initial stresses/strains at nodes/for element. $\sigma x,\sigma y,$
Stress/Strains		σ xy, σ z: global stresses. ε x, ε y, γ xy: global strains.
	SSIG	Initial stresses/strains at Gauss points. σx , σy , σxy ,
		σ z: global stresses. Ex, Ey, γ xy: global strains.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. $\sigma x,\sigma y,\sigma xy,$
		σz: global stresses.
	SSRG	Residual stresses at Gauss points. σx, σy, σxy, σz global stresses.
Target	TSSIE TSSIA	Target stresses/strains at nodes/for element. σx , σy ,
Stress/Strains		σ xy, σ z: global stresses. ε x, ε y, γ xy: global strains.
	TSSIG	Target stresses/strains at Gauss points. σx , σy , σxy , σz : global stresses. εx , εy , γxy : global strains.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0, 0
Overburden	Applicable.	
Phreatic Surface	Applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not applicable.	
Loads		

LUSAS Output

Solver	Stress (default): σ_x , σ_y , σ_{xy} , σ_z , σ_{max} , σ_{min} , β , σ_s , σ_e (see description of principal stresses)
	Strain: ε_x , ε_y , γ_{xy} , $\varepsilon_z = 0$, ε_{max} , ε_{min} , β , ε_s , ε_e
	Stretch (for rubber only): V11, V22, V12, λ 1, λ 2, λ 3=1, $\theta\lambda$, det F. Where
	Vii are components of the left stretch tensors, λ_i the principal stretches,
	$\theta\lambda$ the angle between the maximum principal stretch and the global X axis, and det F the determinant of the deformation gradient or volume ratio.
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 2D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and large rotations.
Updated	For large displacements and large rotations.
Lagrangian	
Eulerian	For large displacements, large rotations and moderately large strains.
Co-rotational	For large displacements and large rotations (large strains with rubber).

Integration Schemes

Stiffness	Default.	2x2
	Fine.	As default.
Mass	Default.	2x2
	Fine.	As default.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Output

- **36** Follower loads.
- **39** Stress smoothing for rubber material models.
- 54 Updated Lagrangian geometric nonlinearity.
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity.
- 91 Invokes fine integration rule for mass matrix.
- 105 Lumped mass matrix.
- **123** Clockwise node numbering.

- 139 Output yielded Gauss points only
- **167** Eulerian geometric nonlinearity.
- **225** Use alternative number of parameters for enhanced strain interpolation (see *Notes*).
- 229 Co-rotational geometric nonlinearity.

Notes on Use

- 1. The variation of stresses within an element can be regarded as linear.
- 2. The element passes the patch test and the large strain patch test for rubber.
- 3. The strain field for this element consists of two parts: the compatible strains derived from an assumed displacement field and the assumed enhanced strains; see *LUSAS Theory Manual*. The assumed enhanced strain field is defined using 5 or 4 parameters for linear and nonlinear applications respectively. Option 225 switches on the higher 5 parameter enhanced strain interpolation function for nonlinear analysis.
- 4. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility. The load does not have to be normal to the face and may also vary over the face.
- 5. To apply a non-conservative (follower) pressure load (load type FLD) with corotational geometric nonlinearity, Option 36 must be specified. Note that this load should be normal to the face and constant for all the nodes of the element face.
- 6. The converged stresses for rubber are <u>Kirchhoff</u> stresses (see *LUSAS Theory Manual*).
- 7. Option 39 is used to smooth the stress output. It is particularly useful when the rubber material model is applied and the element is under very high compression where oscillatory stresses may appear (checker-board pattern).
- 8. When using the rubber material model, converged strain output is replaced by the left stretch tensor, the principal stretches and the angle defining these principal directions. The value of det $F = \lambda_1 \lambda_2$ (the Volume ratio) is only available for Gauss-point output. (Refer to the *LUSAS Theory Manual* for more details.)
- 9. For rubber, the iterative values of stress and strain are output in local co-rotated directions at the Gauss points only.
- 10. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it is only applicable if **every** element is numbered **clockwise**. Surface normals should be visualised and if necessary corrected in the pre-processing stage.
- 11. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.

- 12. Convergence difficulties can sometimes arise when using enhanced strain elements with nonlinear materials, particularly if the material is elastic-perfectly plastic or if a very shallow hardening curve is defined. In such cases it is recommended that the standard element formulation is used.
- 13. In analyses where significant in-plane bending is thermally induced it is recommended that a nonlinear solution is used. If a linear solution is required, then quadratic plane strain elements QPN8 are recommended.

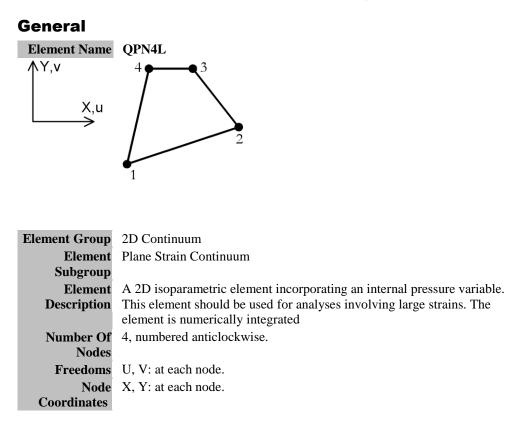
Restrictions

- Rubber material models can only be applied in conjunction with the co-rotational formulation, Option 229.
- □ Avoid excessive aspect ratio

Recommendations on Use

These elements exhibit an improved performance when compared with the parent element QPN4. The integration rules are the same as the parent element. The elements do not suffer from locking due to parasitic shear or when the material approaches the incompressible limit. The elements are also free of any zero energy modes.

2D Plane Strain Continuum Element for Large Strains



Geometric Properties

Not applicable (a unit thickness is assumed).

Material Properties

Linear	Not applicable
Matrix	Not applicable
Joint	Not applicable
Concrete	Not applicable
Elasto-Plastic	Implicit
	Optimised
	Von Mises
	Stress

MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic)

STRESS POTENTIAL VON_MISES (Isotropic: von

	Potential	Mises)
Creep	Not applicable	
Damage	Not applicable	
Viscoelastic	Not applicable	
Shrinkage	Not applicable	
Ko Initialisation	Not applicable	
Rubber	Ogden	MATERIAL PROPERTIES RUBBER OGDEN (Rubber: Ogden)
	Mooney- Rivlin	MATERIAL PROPERTIES RUBBER MOONEY_RIVLIN (Rubber: Mooney-Rivlin)
	Neo-Hookean	MATERIAL PROPERTIES RUBBER NEO_HOOKEAN (Rubber: Neo-Hookean)
	Hencky	MATERIAL PROPERTIES RUBBER HENCKY (Rubber: Hencky)
Generic Polymer	Not applicable	
Composite	Not applicable	

Loading

Prescribed Value Concentrated Loads	,	Prescribed variable. U, V: at nodes. Concentrated loads. Px, Py: at nodes.
Element Loads	**	
Distributed Loads	UDL	Not applicable.
	FLD	Face loads. Px, Py: local face axis pressures at nodes.
	FLDG	Global Face Loads. σx , σy , σxy at nodes
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, 0,0,
		$\Omega_{z, \alpha z}$
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0, φ4, Xcbf, Ycbf
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay: at nodes.
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element. σx , σy ,
Stress/Strains		σ xy, σ z: global stresses. ε x, ε y, γ xy: global strains.
	SSIG	Initial stresses/strains at Gauss points. σx , σy , σxy ,
		σ z: global stresses. Ex, Ey, γ xy: global strains.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. $\sigma x, \sigma y, \sigma xy,$

		σz: global stresses.
	SSRG	Residual stresses at Gauss points. σx , σy , σxy , σz global stresses.
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. σx , σy , σxy , σz : global stresses. εx , εy , γxy : global strains.
	TSSIG	Target stresses/strains at Gauss points. σx , σy , σxy ,
Temperatures	TEMP, TMPE	σ z: global stresses. Ex, Ey, γ xy: global strains. Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0, 0
Overburden	Applicable.	
Phreatic Surface	Applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not applicable.	
Loads		

LUSAS Output

Solver

Stress (default): σ_x , σ_y , σ_x , σ_z , σ_max , σ_min , β , σ_s , σ_e (see <u>description of</u> <u>principal stresses</u>)

Principal stretches, λ_1 , λ_2 , $\lambda_3=1$, $\theta\lambda$, det F. Where V_{ii} are components of the left stretch tensors, λ_i the principal stretches, $\theta\lambda$ the angle between the maximum principal stretch and the global X axis, and det F the determinant of the deformation gradient or volume ratio.

Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 2D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	Not applicable.
Updated	Not applicable.
Lagrangian	
Eulerian	For large displacements and large strains.
Co-rotational	For large displacements and large rotations.

Integration Schemes

Stiffness	Default.	2x2
	Fine.	As default.
Mass	Default.	2x2
	Fine.	As default.

Mass Modelling

- □ Consistent mass (default).
- Lumped mass.

Options

- 55 Output stretches as well as stresses.
- 91 Invokes fine integration rule for mass matrix.
- **105** Lumped mass matrix.
- 123 Clockwise node numbering.

Notes on Use

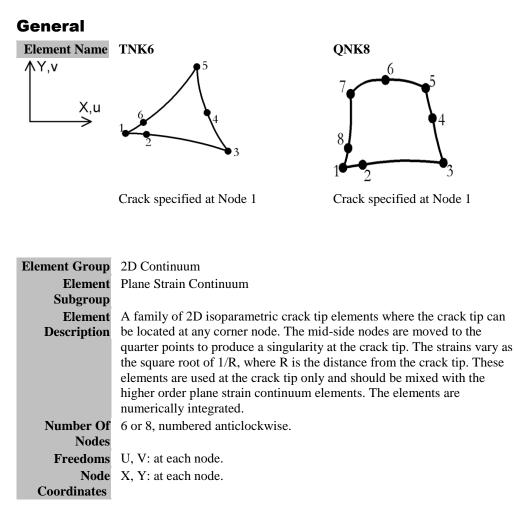
- 1. The element formulations are based on the standard **isoparametric** approach. The variation of stresses within an element can be regarded as linear.
- 2. The element passes the large strain patch test for rubber.
- 3. Non-conservative loading is available with this element when using FLD loading.
- 4. The stresses output are <u>Kirchhoff</u> stresses (see *LUSAS Theory Manual*).

- 5. Stretch output consists of the principal stretches and the angle defining the principal directions. The value of det $F = \lambda_1 \ \lambda_2$ is also output. (Refer to the *LUSAS Theory Manual*.)
- 6. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it is only applicable if **every** element is numbered **clockwise**. Surface normals should be visualised and if necessary corrected in the pre-processing stage.
- 7. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.
- 8. This element is based on a formulation that tackles the problem of volumetric locking in a different way to that used in QPN4M. It should be preferred to the QPN4M in cases where Eulerian description (with a current configuration taken as reference) is more appropriate than the co-rotational description (e.g. inflation problems).

Restrictions

- Avoid excessive aspect ratio
- $\hfill\square$ Avoid non-uniform initial and thermal strains with coarse meshes.

2D Plane Strain Continuum Crack Tip Elements



Geometric Properties

Not applicable (a unit thickness is assumed).

Material Properties

Linear Isotropic:

MATERIAL PROPERTIES (Elastic: Isotropic)

	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC PLANE STRAIN (Elastic: Orthotropic Plane
	Anisotropic:	Strain) MATERIAL PROPERTIES ANISOTROPIC 4 (Not supported in LUSAS Modeller)
	Rigidities.	RIGIDITIES 4 (Not supported in LUSAS Modeller)
Matrix	Not applicable	
Joint	Not applicable	
Concrete		MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Elasto-Plastic	Stress resultant:	Not applicable.
	Interface:	MATERIAL PROPERTIES NONLINEAR 27
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker-Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr-Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Modified Mohr- Coulomb:	MATERIAL PROPERTIES MODIFIED MOHR_COULOMB (Elastic: Isotropic, Plastic: Mohr-Coulomb/Tresca, non- associative Hardening with tension/compression cut-off)
	Modified Cam- clay	MATERIAL PROPERTIES CAM_CLAY MODIFIED (Elastic: Isotropic, Plastic)
	Optimised Implicit Von Mises: Volumetric Crushing:	MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic) MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam)

	Stress Potential	STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
Creep		CREEP PROPERTIES (Creep)
	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP (Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic		VISCO ELASTIC PROPERTIES
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Ko Initialisation	Applicable	
Rubber	Not applicable	
Generic Polymer	Isotropic	MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)
Composite	Not applicable	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V: at nodes.
Concentrated Loads	CL	Concentrated loads. Px, Py: at nodes.
Element Loads	Not applicable.	
Distributed Loads	UDL	Not applicable.
	FLD	Face loads. Px, Py: local face axis pressures at nodes.
	FLDG	Global Face Loads. σx , σy , σxy at nodes
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, 0, 0, Ωz , αz
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0, φ4, Xcbf, Ycbf
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay: at nodes.
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element. σx , σy ,
Stress/Strains		σ xy, σ z: global stresses. ε x, ε y, γ xy: global strains.
	SSIG	Initial stresses/strains at Gauss points. σx , σy , σxy ,
		σ z: global stresses. ε x, ε y, γ xy: global strains.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. σx , σy , σxy ,
		σ z: global stresses.
	SSRG	Residual stresses at Gauss points. σx , σy , σxy , σz : global stresses.
Target	TSSIE, TSSIA	Target stresses/strains at nodes/for element. σx , σy ,
Stress/Strains		σ xy, σ z: global stresses. ε x, ε y, γ xy: global strains.
	TSSIG	Target stresses/strains at Gauss points. σx , σy , σxy , σz : global stresses. εx , εy , γxy : global strains.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, $0, 0$
Overburden	Applicable.	
Phreatic Surface	Applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not applicable.	
Loads		

LUSAS Output

Solver Stress (default): σ_x , σ_y , σ_{xy} , σ_{max} , σ_{min} , β , σ_s , σ_e (see <u>description</u> of principal stresses)

Strain: ε_x , ε_y , γ_{xy} , ε_{max} , ε_{min} , β , ε_s , ε_e

Modeller See Results Tables (Appendix K).

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 2D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and large rotations.
Updated	For large displacements and large rotations.
Lagrangian	
Eulerian	For large displacements, large rotations and moderately large strains.
Co-rotational	For large displacements and large rotations.

Integration Schemes

Stiffness	Default.	
	Fine (see Options).	
Mass	Default.	
	Fine (see Options).	

6-point (TNK6), 3x3 (QNK8) 12-point (TNK6) 6-point (TNK6), 3x3 (QNK8) 12-point (TNK6)

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

18 Invokes finer integration rule.

- 54 Updated Lagrangian geometric nonlinearity.
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity.
- 91 Invokes fine integration rule for mass matrix.
- **105** Lumped mass matrix.
- 123 Clockwise node numbering.
- 139 Output yielded Gauss points only.
- 167 Eulerian geometric nonlinearity.
- 229 Co-rotational geometric nonlinearity.

Notes on Use

- 1. The element formulations are based on the standard isoparametric approach. Moving the mid-side nodes to the quarter points creates a singularity with theoretically infinite stress at the corner node.
- 2. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility.
- Option 123 will not operate on a mesh with a mixture of clockwise and anticlockwise elements, it is only applicable if every element is numbered clockwise. Surface normals should be visualised and if necessary corrected in the pre-processing stage.
- 4. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.

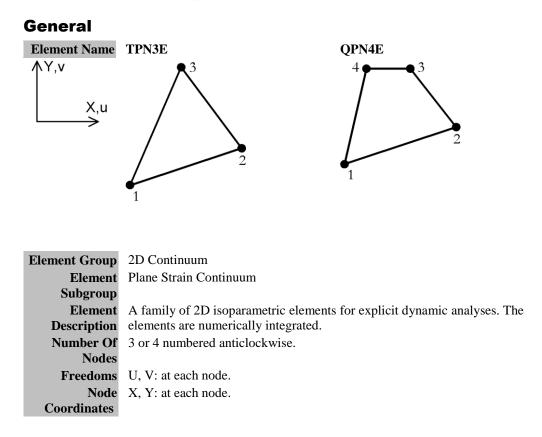
Restrictions

- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

Recommendations on Use

Elements QNK8 and TNK6 are specifically designed for application to fracture mechanics problems and may be used to model the singularities that occur at the crack tip. The mid-side nodes near the crack tip are shifted to the quarter point. This ensures a singularity is present at the crack tip and that the strains vary as 1/square root of r where r is the distance from the crack tip.The triangular TNK6 element is more effective than the quadrilateral element.

2D Plane Strain Explicit Dynamics Elements



Geometric Properties

Not applicable (a unit thickness is assumed).

Material Properties

Linear	Isotropic: Orthotropic:	MATERIAL PROPERTIES (Elastic: Isotropic) MATERIAL PROPERTIES ORTHOTROPIC PLANE STRAIN (Elastic: Orthotropic Plane Strain)
	Anisotropic:	Not applicable.
	Rigidities.	Not applicable.
Matrix	Not applicable	
Joint	Not applicable	
Concrete	Not applicable	

Elasto-Plastic	Stress	Not applicable.
	resultant:	III III
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker-	MATERIAL PROPERTIES NONLINEAR 64
	Prager:	(Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr-	MATERIAL PROPERTIES NONLINEAR 65
	Coulomb:	(Elastic: Isotropic, Plastic: Mohr-Coulomb,
		Hardening: Granular with Dilation)
	Modified	MATERIAL PROPERTIES
	Mohr-	MODIFIED MOHR_COULOMB (Elastic:
	Coulomb:	Isotropic, Plastic: Mohr-Coulomb/Tresca, non- associative Hardening with tension/compression cut-off)
	Optimised Implicit Von Mises:	MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic)
	Volumetric Crushing:	MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam)
	Stress Potential	STRESS POTENTIAL VON_MISES, HILL, HOFFMAN
		(Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
Creep		CREEP PROPERTIES (Creep) (see Notes)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic		VISCO ELASTIC PROPERTIES
Shrinkage	Not applicable	
Ko Initialisation	Not applicable	
Rubber	Not applicable	
~		

Loading

Prescribed ValuePDSP, TPDSPConcentratedCLLoadsNotElement LoadsNotapplicable.

Generic Polymer Not applicable Composite Not applicable

> Prescribed variable. U, V: at each node. Concentrated loads. Px, Py: at each node.

Distributed Loads	UDL	Not applicable.
	FLD	Face loads. Px, Py: local face axis pressures at nodes.
	FLDG	Not applicable
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, 0, 0, Ωz , αz
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0, φ4, Xcbf, Ycbf
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay: at nodes.
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element. σx , σy ,
Stress/Strains		σ_{xy} , σ_{z} : global stresses. ε_x , ε_y , γ_{xy} global strains.
	SSIG	Initial stresses/strains at Gauss points. σx , σy , σxy ,
		σ z: global stresses. Ex, Ey, γ xy: global strains.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. σx , σy , σxy ,
		σ z: global stresses.
	SSRG	Residual stresses at Gauss points. σx, σy, σxy, σz: global stresses.
Target	Not	
Stress/Strains	applicable.	
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0, 0
Overburden		
	applicable.	
Phreatic Surface	Not	
	applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not	
Loads	applicable.	
	TT	

LUSAS Output

Solver	Stress (default): σ_x , σ_y , σ_{xy} , σ_z , σ_{max} , σ_{min} , β , σ_s , σ_e (see <u>description of principal stresses</u>)
--------	--

Strain: ε_x , ε_y , γ_{xy} , ε_{max} , ε_{min} , β , ε_s , ε_e

Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 2D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	Not applicable.
Updated	Not applicable.
Lagrangian	
Eulerian	For large displacements, large rotations and moderately large strains.
Co-rotational	For large displacements and large rotations.

Integration Schemes

Stiffness	Default.	1-point (see Notes).
	Fine.	As default.
Mass	Default.	1-point (see Notes).
	Fine.	As default.

Mass Modelling

□ Lumped mass only (see *Notes*).

Options

- 55 Output strains as well as stresses.
- **105** Lumped mass matrix (see *Notes*).
- **139** Output yielded Gauss points only.

Notes on Use

- 1. The element formulations are based on the standard
- 2. The system parameter HGVISC is used to restrict element mechanisms due to underintegration. The default value is usually sufficient.
- The bulk viscosity coefficients are used to restrict numerical oscillations due to the traversal of stress waves. The default bulk viscosity coefficients (BULKLF and BULKQF) may be altered as SYSTEM parameters.
- 4. These elements must be used with a dynamic central difference scheme and a lumped mass matrix in order to obtain the maximum efficiency from the numerical algorithms.
- 5. These elements are not applicable for static or eigenvalue analyses.
- 6. Automatic time step calculations are implemented.
- 7. As the element geometry is always updated in an explicit dynamic analysis, a nonlinear solution is obtained. When using explicit dynamics elements NONLINEAR CONTROL must be specified.
- 8. If CREEP PROPERTIES are defined, explicit time integration must be specified in VISCOUS CONTROL.
- 9. Non-conservative loading is invoked when the FLD loading facility is applied.
- 10. Rayleigh damping coefficients are not supported by these elements.
- 11. Constraint equations are not available for use with these elements.
- 12. Nodes **must** be specified in an anticlockwise order. Option 123 is **not** applicable for this element. When using Modeller ensure surface normal is in the +ve z direction.

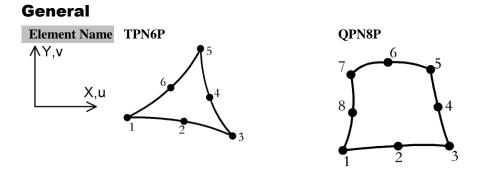
Restrictions

□ Avoid excessive aspect ratio

Recommendations on Use

Explicit dynamics elements may be used to define surface boundaries which will be active in a slideline analysis.

2D Plane Strain Two Phase Continuum Elements



Element Group	2D Continuum
Element	Plane Strain Continuum
Subgroup	
Element	A family of 2D isoparametric elements with higher order models capable
Description	of modelling curved boundaries. The elements are numerically integrated.
Number Of	6 or 8 numbered anticlockwise.
Nodes	
Freedoms	U, V, P at corner nodes. U, V at midside nodes.
Node	X, Y: at each node.
Coordinates	

Geometric Properties

Not applicable (a unit thickness is assumed).

Material Properties

Linear	Isotropic: Orthotropic:	MATERIAL PROPERTIES (Elastic: Isotropic) MATERIAL PROPERTIES ORTHOTROPIC PLANE STRAIN (Elastic: Orthotropic Plane Strain)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC 4 (Not supported in LUSAS Modeller)
	Rigidities.	RIGIDITIES 4 (Not supported in LUSAS Modeller)
Matrix	Not applicable	
Joint	Not applicable	
Concrete		MATERIAL PROPERTIES NONLINEAR 109

		(Elastic: Isotropic, Plastic: Smoothed Multi Crack Concrete)
Elasto-Plastic	Stress resultant:	Not applicable.
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker- Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr- Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Modified Mohr-	MATERIAL PROPERTIES
	Coulomb:	MODIFIED MOHR_COULOMB (Elastic: Isotropic, Plastic: Mohr-Coulomb/Tresca, non- associative Hardening with tension/compression cut-off)
	Modified	MATERIAL PROPERTIES CAM_CLAY
	Cam-clay Optimised	MODIFIED (Elastic: Isotropic, Plastic) MATERIAL PROPERTIES NONLINEAR 75
	Implicit Von Mises:	(Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic)
	Volumetric	MATERIAL PROPERTIES NONLINEAR 81
	Crushing:	(Volumetric Crushing or Crushable Foam)
	Interface	MATERIAL PROPERTIES NONLINEAR 27
	Stress Potential	STRESS POTENTIAL VON_MISES, HILL, HOFFMAN
		(Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
Creep		CREEP PROPERTIES (Creep)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic		VISCOELASTIC PROPERTIES
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER

Ko Initialisation	Not applicable
Rubber	Not applicable
Generic Polymer	

Composite Not applicable

MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, P at corner nodes. U, V at midside nodes.
Concentrated Loads	CL	Concentrated loads. Px, Py, Q at corner nodes. Px, Py at midside nodes.
Element Loads	Not applicable.	
Distributed Loads	UDL	Not applicable.
	FLD	Face Loads. Px, Py, Q: face pressures/flux per unit area at corner nodes relative to local face axes. Px, Py: face pressures at midside nodes relative to local face axes.
	FLDG	Global Face Loads. σx , σy , σxy at nodes
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, 0, 0, Ωz , αz , gx, gy (see Notes on Use)
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0, φ4, Xcbf, Ycbf, gx, gy (see Notes on Use)
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay: at nodes.
Initial Stress/Strains	SSI, SSIE	Initial stresses/strains at nodes/for element. σx , σy , σxy , σz , σp global stresses. εx , εy , γxy : global strains.
	SSIG	Initial stresses/strains at Gauss points. σx , σy , σxy , σz , σp : global stresses. εx , εy , γxy : global strains.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. σx , σy , σxy , σz , σp : global stresses.
	SSRG	Residual stresses at Gauss points. σx , σy , σxy , σz , σp global stresses.
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. σx , σy , σxy , σz , σp global stresses. εx , εy , γxy : global strains.
	TSSIG	Target stresses/strains at Gauss points. σx , σy , σxy ,
T	TEMD TMPE	$σ_z$, $σ_p$: global stresses. Ex, Ey, γxy: global strains.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0, 0
Overburden	Applicable.	

Phreatic SurfaceApplicable.Field LoadsNot applicable.Temp DependentNot applicable.Loads

LUSAS Output

Solver	Stress (default): σ_x , σ_y , σ_{xy} , σ_z , σ_p , σ_{max} , σ_{min} , β , σ_s , σ_e (see <u>description of principal stresses</u>)
	Strain: ε_x , ε_y , γ_{xy} , $\varepsilon_z = 0$, ε_v , ε_{max} , ε_{min} , β , ε_s , ε_e
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 2D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and large rotations.		
Updated	For large displacements and large rotations.		
Lagrangian			
Eulerian	For large displacements, large rotations and moderately large strains.		
Co-rotational	For large displacements and large rotations.		

Integration Schemes

Stiffness	Default.	3-point (TPN6P), 2x2 (QPN8P)
	Fine (see Options).	3x3 (QPN8P)
Mass	Default.	3-point (TPN6P), 2x2 (QPN8P)
	Fine (see Options).	3x3 (QPN8P)

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- **18** Invokes finer integration rule.
- **36** Follower loads.
- 54 Updated Lagrangian geometric nonlinearity
- 55 Output strains as well as stresses
- 87 Total Lagrangian geometric nonlinearity.
- 91 Invokes fine integration rule for mass matrix.
- **105** Lumped mass matrix.
- 123 Clockwise node numbering.
- **139** Output yielded Gauss points only.
- **167** Eulerian geometric nonlinearity.
- 229 Co-rotational geometric nonlinearity.

Notes on Use

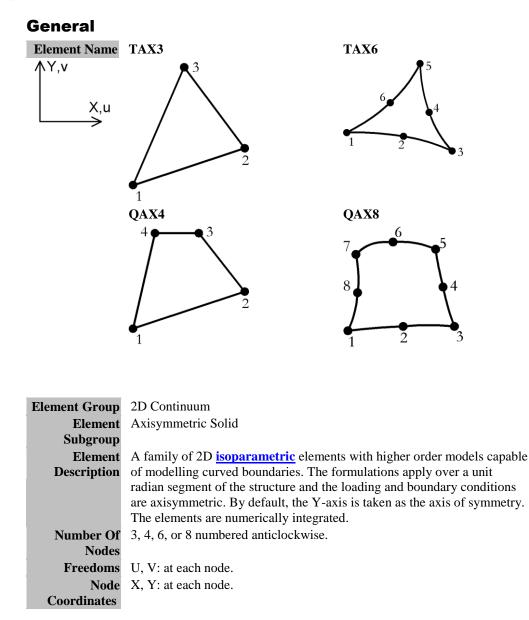
- 1. Two phase material parameters must be used with these elements for undrained and consolidation analysis.
- 2. The element formulations are based on the standard isoparametric approach. The variation of isoparametric stresses and pore pressures within an element can be considered linear.
- 3. All elements pass the **<u>patch test</u>**.
- 4. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it is only applicable if **every** element is numbered **clockwise**. Surface normals should be visualised and if necessary corrected in the pre-processing stage. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.
- 5. Non-conservative loading is available with these elements when using Updated Lagrangian, Eulerian or co-rotational (with OPTION 36) geometric nonlinear formulations together with the FLD loading facility.

6. The global components of gravity acting on the fluid phase are defined by gx and gy under CBF and BFP loading.

Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

2D Axisymmetric Solid Continuum Elements



Geometric Properties

Not applicable (a unit radian segment is assumed).

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC AXISYMMETRIC (Elastic: orthotropic Axisymmetric)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC 4 (Not supported in LUSAS Modeller)
	Rigidities.	Not applicable.
Matrix	Not applicable	
Joint	Not applicable	
Concrete		MATERIAL PROPERTIES NONLINEAR 105
		(Elastic: Isotropic, Plastic: Transient Smoothed
		Multi-Crack Concrete)
		MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Elasto-Plastic	Stress resultant:	Not applicable.
	Interface:	MATERIAL PROPERTIES NONLINEAR 27.
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker-Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr-Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Modified Mohr- Coulomb:	MATERIAL PROPERTIES MODIFIED MOHR_COULOMB (Elastic: Isotropic, Plastic: Mohr-Coulomb/Tresca, non- associative Hardening with tension/compression cut-off)
	Modified Cam- clay	MATERIAL PROPERTIES CAM_CLAY MODIFIED (Elastic: Isotropic, Plastic)
	Optimised Implicit Von	MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening:
	Mises:	Isotropic & Kinematic)
	Volumetric	MATERIAL PROPERTIES NONLINEAR 81

	Crushing: Stress Potential	(Volumetric Crushing or Crushable Foam) STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
Сгеер	CEB-FIP	CREEP PROPERTIES (Creep) MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP (Concrete creep model to CEB-FIP Model Code 1990)
	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP (Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic Shrinkage		VISCO ELASTIC PROPERTIES SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Ko Initialisation	Applicable	
Rubber	Not applicable	
Generic Polymer	Isotropic	MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)
Composite	Not applicable	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V: at nodes.
Concentrated Loads	CL	Concentrated loads. Px, Py: force per unit radian at nodes.
Element Loads		
Distributed Loads	UDL	Not available.
	FLD	<u>Face loads</u> . Px, Py: local face pressures at nodes (force per unit area).
	FLDG	Global Face Loads. σx , σy , σxy at nodes
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Ωx , Ωy (angular velocity must be applied about axis of
		symmetry), 0, 0.
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0, φ4, Xcbf, Ycbf
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay: at nodes.
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element. σx , σy ,
Stress/Strains		σ xy, σ z: global stresses. Ex, Ey, γ xy, Ez: global strains.
	SSIG	Initial stresses/strains at Gauss points. σx , σy , σxy ,
		σ z: global stresses. Ex, Ey, γ xy, Ez: global strains.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. σx , σy , σxy ,
		σz: global stresses.
	SSRG	Residual stresses at Gauss points. σx , σy , σxy , σz :
		global stresses.
•	TSSIE, TSSIA	Target stresses/strains at nodes/for element. σx , σy ,
Stress/Strains		σ_{xy}, σ_{z} : global stresses. $\varepsilon_x, \varepsilon_y, \gamma_{xy}, \varepsilon_z$: global strains.
	TSSIG	Target stresses/strains at Gauss points. σx , σy , σxy ,
		σ z: global stresses. Ex, Ey, γ xy, Ez: global strains.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0, 0
Overburden		
Phreatic Surface		
	Not applicable.	
Temp Dependent Loads	Not applicable.	

LUSAS Output

Solver	Stress (default): σ_x , σ_y , σ_{xy} , σ_z , σ_{max} , σ_{min} , β , σ_s , σ_e (see description of principal stresses)
	Strain: ε_x , ε_y , γ_{xy} , ε_z , ε_{max} , ε_{min} , β , ε_s , ε_e
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 2D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and large rotations.		
Updated	For large displacements and large rotations.		
Lagrangian			
Eulerian	For large displacements, large rotations and moderately large strains.		
Co-rotational	Not applicable.		

Integration Schemes

Stiffness	Default.	1-point (TAX3), 3-point (TAX6), 2x2 (QAX4, QAX8)
	Fine (see Options).	3x3 (QAX8), 3-point (TAX3).
Mass	Default.	1-point (TAX3), 3-point (TAX6), 2x2 (QAX4, QAX8)
	Fine (see Options).	3x3 (QAX8), 3-point (TAX3).

Mass Modelling

- □ Consistent mass (default).
- Lumped mass.

Options

- **18** Invokes finer integration rule.
- 47 X-axis taken as axis of symmetry
- 54 Updated Lagrangian geometric nonlinearity.
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity.
- 91 Invokes fine integration rule for mass matrix.
- **105** Lumped mass matrix.
- 123 Clockwise node numbering.
- **139** Output yielded Gauss points only.
- **167** Eulerian geometric nonlinearity.

Notes on Use

- 1. The element formulations are based on the standard **isoparametric** approach. The variation of stresses within an element can be regarded as constant for the lower order (corner node only) elements, and linear for the higher order (mid-side node) elements.
- 2. All elements pass the **patch test**.
- 3. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility.
- 4. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it is only applicable if **every** element is numbered **clockwise**. Surface normals should be visualised and if necessary corrected in the pre-processing stage.
- 5. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.
- 6. The maximum and minimum principal stress computations for axisymmetric elements do not include the σz term as this is implicitly a principal stress in a biaxial stress field.
- 7. An initial stress/strain or thermal load that varies across an element should not be applied to this element. A limitation of the standard isoparametric approach when used for lower order elements is that only constant stress/strain fields can be imposed correctly.

Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature

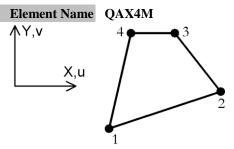
□ Avoid excessive aspect ratio

Recommendations on Use

- The 8-noded element with a 2*2 Gauss rule is usually the most effective element, as the under-integration of the stiffness matrix prevents locking, which may occur either when the element is subjected to <u>parasitic shear</u>, or as the material reaches the incompressible limit (elasto-plasticity). The Gauss point stresses are also sampled at the most accurate locations for the element. However, the element does possess one spurious zero energy mode. This mode is very rarely activated in linear analysis, but it may occur in both materially and geometrically nonlinear analyses. Therefore, a careful examination of the solution should be performed, to check for spurious stress oscillations and peculiarities in the deformed configuration.
- The 8-noded element with a 3*3 Gauss rule may be used if a spurious mechanism is excited with the 2*2 Gauss rule.
- The 4-noded element should not be used for analyses where in-plane bending effects are significant as the element tends to lock in **parasitic shear**.

2D Axisymmetric Solid Continuum Element with Enhanced Strains

General



Element Group	2D Continuum		
Element	Axisymmetric Solid		
Subgroup			
Element	A 2D isoparametric element with an assumed strain field. This mixed		
Description	assumed strain element demonstrates a superior performance to QAX4		
	(see Notes). The formulations apply over a unit radian segment of the		
	structure, and the loading and boundary conditions are axisymmetric. By		
	default, the Y-axis is taken as the axis of symmetry. The element is		
	numerically integrated.		
Number Of	4, numbered anticlockwise.		
Nodes			
Freedoms	U, V: at each node.		
Node	X, Y: at each node.		
Coordinates			

Geometric Properties

Not applicable (a unit radian segment is assumed).

Material Properties

Linear Isotropic: Orthotropic: MATERIAL PROPERTIES (Elastic: Isotropic) MATERIAL PROPERTIES ORTHOTROPIC AXISYMMETRIC (Elastic: Orthotropic Axisymmetric)

	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC 4 (Not supported in LUSAS Modeller)
Matrix Joint	Rigidities. Not applicable Not applicable	Not applicable
Concrete	i tot applicable	MATERIAL PROPERTIES NONLINEAR 105 (Elastic: Isotropic, Plastic: Transient Smoothed Multi- Crack Concrete)
		MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Elasto-Plastic	Stress resultant:	Not applicable.
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker-	MATERIAL PROPERTIES NONLINEAR 64
	Prager:	(Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr- Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Modified Mohr- Coulomb:	MATERIAL PROPERTIES MODIFIED MOHR_COULOMB (Elastic: Isotropic, Plastic: Mohr-Coulomb/Tresca, non- associative Hardening with tension/compression cut-off)
	Modified Cam-clay	MATERIAL PROPERTIES CAM_CLAY MODIFIED (Elastic: Isotropic, Plastic)
	Optimised Implicit Von Mises:	MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic)
	Volumetric Crushing:	MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam)
	Stress Potential	STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
Creep		CREEP PROPERTIES (Creep)
Ĩ	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of

		Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP
		(Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE
		(Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE
		(Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic		VISCO ELASTIC PROPERTIES
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Ko Initialisation	Applicable	
Rubber	Not applicable	
Generic Polymer	Isotropic	MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)
Composite	Not applicable	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V: at nodes.
Concentrated Loads	CL	Concentrated loads. Px, Py: force per unit radian at nodes.
Element Loads	Not applicable.	
Distributed Loads	UDL	Not available.
	FLD	Face loads. Px, Py: local face pressures at nodes (force per unit area).
	FLDG	Global Face Loads. σx , σy , σxy at nodes
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Ωx ,
		Ω y (angular velocity must be applied about axis of symmetry), 0,0.
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0, φ4, Xcbf, Ycbf

Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay: at nodes.
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element. σx , σy ,
Stress/Strains		σ xy, σ z: global stresses. Ex, Ey, γ xy, Ez: global strains.
	SSIG	Initial stresses/strains at Gauss points. σx , σy , σxy ,
		σ z: global stresses. Ex, Ey, γ xy, Ez: global strains.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. σx , σy , σxy , σz : global stresses.
	SSRG	Residual stresses at Gauss points. σx , σy , σxy , σz : global stresses.
Target	TSSIE, TSSIA	Target stresses/strains at nodes/for element. σx , σy ,
Stress/Strains		σ xy, σ z: global stresses. Ex, Ey, γ xy, Ez: global strains.
	TSSIG	Target stresses/strains at Gauss points. σx , σy , σxy ,
		σ z: global stresses. Ex, Ey, γ xy, Ez: global strains.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0, 0
Overburden	Applicable.	
Phreatic Surface	Applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not applicable.	
Loads		

LUSAS Output

Solver	Stress (default): σ_x , σ_y , σ_{xy} , σ_z , σ_{max} , σ_{min} , β , σ_s , σ_e (see description of principal stresses)
	Strain: $\mathcal{E}x$, $\mathcal{E}y$, γxy , $\mathcal{E}z$, $\mathcal{E}max$, $\mathcal{E}min$, β , $\mathcal{E}s$, $\mathcal{E}e$
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 2D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and large rotations.
Updated	For large displacements and large rotations.
Lagrangian	
Eulerian	For large displacements, large rotations and moderately large strains.
Co-rotational	Not applicable.

Integration Schemes

Stiffness Default.	2x2
Fine.	As default.
Mass Default.	2x2
Fine.	As default.

Mass Modelling

□ Consistent mass (default).

□ Lumped mass.

Options

- 47 X-axis taken as axis of symmetry
- 54 Updated Lagrangian geometric nonlinearity
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity.
- 91 Invokes fine integration rule for mass matrix.
- **105** Lumped mass matrix.
- **123** Clockwise node numbering.
- **139** Output yielded Gauss points only.
- **167** Eulerian geometric nonlinearity.

Notes on Use

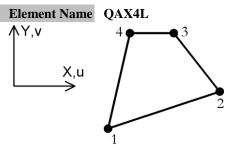
- 1. The element formulations are based on the standard **<u>isoparametric</u>** approach. The variation of stresses within an element can be regarded as linear.
- 2. All elements pass the **<u>patch test</u>**.
- 3. The strain field for this element consists of two parts: the compatible strains derived from an assumed displacement field and the assumed enhanced strains; see *LUSAS Theory Manual*. The assumed enhanced strain field is defined using 5 parameters for both linear and nonlinear applications.
- 4. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility.
- 5. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it will only work if **every** element is numbered **clockwise**. The best way to avoid a mixture is to check and appropriately reverse the surface definitions in the pre-processing stage of modelling.
- 6. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.
- 7. The maximum and minimum principal stress computations for axisymmetric elements do not include the σz term as this is implicitly a principal stress in a biaxial stress field.
- 8. Convergence difficulties can sometimes arise when using enhanced strain elements with nonlinear materials, particularly if the material is elastic-perfectly plastic or if a very shallow hardening curve is defined. In such cases it is recommended that the standard element formulation is used.
- 9. This element exhibits an improved performance when compared with its parent element QAX4. The integration rules are the same as the parent element. The elements do not suffer from locking due to <u>parasitic shear</u> or when the material approaches the incompressible limit. The elements are also free of any <u>zero energy</u> <u>modes</u>.
- 10. In analyses where significant in-plane bending is thermally induced it is recommended that a nonlinear solution is used. If a linear solution is required, then quadratic plane strain elements QPN8 are recommended.

Restrictions

□ Avoid excessive aspect ratio

2D Axisymmetric Solid Continuum Element for Large Strains

General



Element Group	2D Continuum
Element	Axisymmetric Solid
Subgroup	
Element	A 2D isoparametric element incorporating an internal pressure variable.
Description	This element should be used for analyses involving large strains. The
	formulations apply over a unit radian segment of the structure and the
	loading and boundary conditions are axisymmetric. By default, the Y-axis
	is taken as the axis of symmetry. The element is numerically integrated.
Number Of	4, numbered anticlockwise.
Nodes	
Freedoms	U, V: at each node.
Node	X, Y: at each node.
Coordinates	

Geometric Properties

Not applicable (a unit radian segment is assumed).

Material Properties

Linear	Not applicable
Matrix	Not applicable
Joint	Not applicable
Concrete	Not applicable
Elasto-Plastic	Implicit

MATERIAL PROPERTIES NONLINEAR 75

	Optimised Von Mises Stress Potential	(Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic) STRESS POTENTIAL VON_MISES (Isotropic: von Mises)
Creep	Not applicable	
Damage	Not applicable	
Viscoelastic	Not applicable	
Shrinkage	Not applicable	
Ko Initialisation	Not applicable	
Rubber	Ogden	MATERIAL PROPERTIES RUBBER OGDEN (Rubber: Ogden)
	Mooney- Rivlin	MATERIAL PROPERTIES RUBBER MOONEY_RIVLIN (Rubber: Mooney-Rivlin)
	Neo-Hookean	MATERIAL PROPERTIES RUBBER NEO_HOOKEAN (Rubber: Neo-Hookean)
	Hencky	MATERIAL PROPERTIES RUBBER HENCKY (Rubber: Hencky)
Generic Polymer	Not applicable	
Composite	Not applicable	

Loading

Prescribed Value	PDSP. TPDSP	Prescribed variable. U, V: at nodes.
Concentrated Loads		Concentrated loads. Px, Py: force per unit radian at nodes.
Element Loads	Not applicable.	
Distributed Loads	UDL	Not available.
	FLD	Face loads. Px, Py: local face pressures at nodes (force per unit area).
	FLDG	Global Face Loads. σx , σy , σxy at nodes
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Ωx ,
		Ω y, (angular velocity must be applied about axis of symmetry), 0,0.
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0, φ4, Xcbf, Ycbf
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay: at nodes.
Initial Stress/Strains	SSI, SSIE	Initial stresses/strains at nodes/for element. σx ,
Su essi su allis		σy, σxy, σz: global stresses. εx, εy, γxy, εz:

		global strains.
	SSIG	Initial stresses/strains at Gauss points. σx , σy ,
		σ xy, σ z: global stresses. ϵ x, ϵ y, γ xy, ϵ z: global strains.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. σx , σy ,
		σxy, σz: global stresses.
	SSRG	Residual stresses at Gauss points. σx , σy , σxy ,
		σz: global stresses.
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. σx ,
		σy, σxy, σz: global stresses. εx, εy, γxy, εz: global strains.
	TSSIG	Target stresses/strains at Gauss points. σx , σy ,
		σ xy, σ z: global stresses. Ex, Ey, γ xy, Ez: global strains.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0
Overburden	Applicable.	
Phreatic Surface	Applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not applicable.	
Loads		

LUSAS Output

Solver	Stress (default): σ_x , σ_y , σ_{xy} , σ_z , σ_{max} , σ_{min} , β , σ_s , σ_e (see description of principal stresses)
	Principal stretches, λ_1 , λ_2 , λ_31 , $\theta\lambda$, det F. Where λ_i are the principal stretches, $\theta\lambda$ the angle between the maximum principal stretch and the global X axis, and det F the determinant of the deformation gradient or volume ratio.
Modeller	See <u>Results Tables (Appendix K).</u>

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 2D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	Not applicable.
Updated	Not applicable.
Lagrangian	
Eulerian	For large displacements and large strains.
Co-rotational	Not applicable.

Integration Schemes

Stiffness	Default.	2x2
	Fine.	As default.
Mass	Default.	2x2
	Fine.	As default.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- 47 X-axis taken as axis of symmetry.
- 55 Output stretches as well as stresses.
- 91 Invokes fine integration rule for mass matrix.
- 105 Lumped mass matrix
- 123 Clockwise node numbering.

Notes on Use

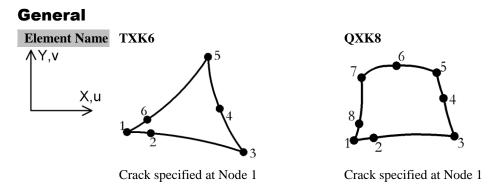
- 1. The element formulations are based on the standard **<u>isoparametric</u>** approach. The variation of stresses within an element can be regarded as linear.
- 2. The element passes the large strain patch test for rubber.

- 3. Non-conservative loading is available with this element when using FLD loading.
- 4. The stresses output are <u>Kirchhoff</u> stresses (see *LUSAS Theory Manual*).
- 5. Stretch output consists of the principal stretches and the angle defining the principal directions. The value of det $F = \lambda_1 \ \lambda_2$ is also output. (Refer to the *LUSAS Theory Manual* for more details.)
- 6. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it will only work if **every** element is numbered **clockwise**. The best way to avoid a mixture is to check and appropriately reverse the surface definitions in the pre-processing stage of modelling.
- 7. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.
- 8. The maximum and minimum principal stress computations for axisymmetric elements do not include the σz term as this is implicitly a principal stress in a biaxial stress field.

Restrictions

- □ Avoid excessive aspect ratio
- $\hfill\square$ Avoid non-uniform initial and thermal strains with coarse meshes

2D Axisymmetric Solid Continuum Crack Tip Elements



Element Group	2D Continuum
Element	Axisymmetric Solid
Subgroup	
Element	A family of 2D isoparametric crack tip elements where the crack tip can
Description	be located at any node. The mid-side nodes are moved to the quarter points to produce a singularity at the crack tip. The strains vary as the square root of 1/R, where R is the distance from the crack tip. These elements are used at the crack tip only and should be mixed with the higher order axisymmetric solid continuum elements. The formulations apply over a unit radian segment of the structure, and the loading and boundary conditions are axisymmetric. By default, the Y-axis is taken as the axis of symmetry. The elements are numerically integrated.
	6 or 8 numbered anticlockwise.
Nodes	
Freedoms	U, V: at each node.
Node	X, Y: at each node.
Coordinates	

Geometric Properties

Not applicable (a unit radian segment is assumed).

Material Properties

Linear Isotropic: Orthotropic: MATERIAL PROPERTIES (Elastic: Isotropic) MATERIAL PROPERTIES ORTHOTROPIC

		AXISYMMETRIC (Elastic: Orthotropic Axisymmetric)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC 4 (Not supported in LUSAS Modeller)
	Rigidities.	Not applicable.
Matrix	Not applicable	
Joint	Not applicable	
Concrete		MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Elasto-Plastic	Stress resultant:	Not applicable.
	Interface:	MATERIAL PROPERTIES NONLINEAR 27
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker-Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr-Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Modified Mohr- Coulomb:	MATERIAL PROPERTIES MODIFIED MOHR_COULOMB (Elastic: Isotropic, Plastic: Mohr-Coulomb/Tresca, non- associative Hardening with tension/compression cut-off)
	Modified Cam- clay	MATERIAL PROPERTIES CAM_CLAY MODIFIED (Elastic: Isotropic, Plastic)
	Optimised Implicit Von Mises:	MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic)
	Volumetric Crushing:	MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam)
	Stress Potential	STRESS POTENTIAL VON_MISES, HILL, HOFFMAN
		(Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
Creep		CREEP PROPERTIES (Creep)
	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO
		(Concrete creep model to AASHTO code of Practice)

	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP (Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic		VISCO ELASTIC PROPERTIES
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Shrinkage	Applicable	
Rubber	Not applicable	
Generic Polymer	Isotropic	MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)
Composite	Not applicable	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V: at nodes.
Concentrated Loads	CL	Concentrated loads. Px, Py: at nodes.
Element Loads	Not applicable.	
Distributed	UDL	Not applicable.
Loads		
	FLD	Face loads. Px, Py: local face axis pressures at nodes.
	FLDG	Global Face Loads. σx , σy , σxy at nodes
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Ωx , Ωy (angular velocity must be applied about axis of symmetry), 0, 0.
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0, φ_4 ,

Velocities Accelerations Initial Stress/Strains	VELO ACCE SSI, SSIE	Xcbf, Ycbf Velocities. Vx, Vy: at nodes. Acceleration Ax, Ay: at nodes. Initial stresses/strains at nodes/for element. σx, σy, σxy, σz: global stresses. εx, εy, γxy, εz: global strains.
	SSIG	Initial stresses/strains at Gauss points. σx , σy , σxy , σz :
Residual Stresses	SSR, SSRE	global stresses. ε_x , ε_y , γ_{xy} , ε_z : global strains. Residual stresses at nodes/for element. σ_x , σ_y , σ_{xy} , σ_z : global stresses.
	SSRG	Residual stresses at Gauss points. σx, σy, σxy, σz: global stresses.
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. σx , σy , σxy , σz : global stresses. εx , εy , γxy , εz : global stresses. εx , εy , γxy , εz : global stresses.
	TSSIG	Target stresses/strains at Gauss points. σx , σy , σxy , σz : global stresses. εx , εy , γxy , εz : global strains.
	TEMP, TMPE Applicable. Applicable.	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0
Surface	Not applicable.	
Temp Dependent Loads	Not applicable.	

LUSAS Output

Solver	Stress (default): σ_x , σ_y , σ_{xy} , σ_z , σ_{max} , σ_{min} , β , σ_s , σ_e (see description of principal stresses)
	Strain: ε_x , ε_y , γ_{xy} , ε_z , ε_{max} , ε_{min} , β , ε_s , ε_e
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 2D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and large rotations.		
Updated	For large displacements and large rotations.		
Lagrangian			
Eulerian	For large displacements, large rotations and moderately large strains.		
Co-rotational	Not applicable.		

Integration Schemes

Default.	6-point (TXK6), 3x3 (QXK8)
Fine (see Options).	12-point (TXK6).
Default.	6-point (TXK6), 3x3 (QXK8)
Fine (see Options).	12-point (TXK6).
	Fine (see <i>Options</i>). Default.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- **18** Invokes finer integration rule.
- 47 X-axis taken as axis of symmetry.
- 54 Updated Lagrangian geometric nonlinearity.
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity.
- 91 Invokes fine integration rule for mass matrix.
- **105** Lumped mass matrix
- **123** Clockwise node numbering.
- **139** Output yielded Gauss points only.
- **167** Eulerian geometric nonlinearity.

Notes on Use

- 1. The element formulations are based on the standard **isoparametric** approach. Moving the mid-side nodes to the quarter points creates a singularity with theoretically infinite stress at the corner node.
- 2. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility.
- 3. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it will only work if **every** element is numbered **clockwise**. The best way to avoid a mixture is to check and appropriately reverse the surface definitions in the pre-processing stage of modelling.
- 4. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.
- 5. The maximum and minimum principal stress computations for axisymmetric elements do not include the σz term as this is implicitly a principal stress in a biaxial stress field.

Restrictions

- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

Recommendations on Use

The QXK8 and TXK6 elements are specifically designed for application to fracture mechanics problems and may used to model the singularities that occur at the crack tip. The mid-side nodes near the crack tip are shifted to the quarter point. This ensures a singularity is present at the crack tip and that the strains vary as 1/square root of r where r is the distance from the crack tip. The triangular TPK6 element is more effective than the quadrilateral element.

2D Axisymmetric Solid Explicit Dynamics Elements

General Element Name	TAX3E QAX4E 4 4 1 2	
Element Group	2D Continuum	
Element	Axisymmetric Solid Continuum	
Subgroup	A family of 2D ison provide allower to family and is it demonsion and have	
Element Description	A family of 2D isoparametric elements for explicit dynamic analyses. The formulations apply over a unit radian segment of structure and	
	loading boundary conditions are axisymmetric. By default, the Y-axis is taken as the axis of symmetry. The elements are numerically integrated.	
Number Of		
Nodes		
	U, V: at each node.	
	X, Y: at each node.	
Coordinates		

Geometric Properties

Not applicable (a unit radian segment is assumed).

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC
		AXISYMMETRIC (Elastic: Orthotropic
		Axisymmetric)
	Anisotropic:	Not applicable
	Rigidities.	Not applicable
	-	

Joint	Not applicable Not applicable Not applicable	
Elasto-Plastic	Stress resultant:	Not applicable
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker- Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr- Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Modified Mohr- Coulomb:	MATERIAL PROPERTIES MODIFIED MOHR_COULOMB (Elastic: Isotropic, Plastic: Mohr-Coulomb/Tresca, non- associative Hardening with tension/compression cut-off)
	Optimised Implicit Von Mises: Volumetric Crushing: Stress Potential	MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic) MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam) STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises
Сгеер	AASHTO	Orthotropic: Hill, Hoffman) CREEP PROPERTIES (Creep) (See <i>Notes</i>) MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP (Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)

Composite Not applicable

	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic		VISCO ELASTIC PROPERTIES
Shrinkage	Not applicable	
Ko Initialisation	Applicable	
Rubber	Not applicable	
Generic Polymer	Not applicable	

Loading

Prescribed Value Concentrated	PDSP, TPDSP CL	Prescribed variable. U, V: at each node. Concentrated loads. Px, Py: at each node.
Loads Element Loads	Not applicable.	
Distributed Loads	UDL	Not applicable.
	FLD	Face loads. Px, Py: local face axis pressures at nodes.
	FLDG	Not applicable.
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Ωx ,
		Ω y (angular velocity must be applied about axis of symmetry), 0,0.
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0, ϕ_4 , Xcbf, Ycbf
Velocities	VELO	Velocities. Vx, Vy at nodes.
Accelerations	ACCE	Acceleration. Ax, Ay at nodes.
Initial SSI, SSIE Stress/Strains SSIG	SSI, SSIE	Initial stresses/strains at nodes/for element. $\sigma x, \sigma y,$
		σ_{xy}, σ_{z} : global stresses. $\varepsilon_x, \varepsilon_y, \gamma_{xy}, \varepsilon_z$: global strains.
	SSIG	Initial stress/strains at Gauss points. σx, σy, σxy,
		$\sigma_{z:}$ global stress. ϵ_x , ϵ_y , γ_{xy} , $\epsilon_{z:}$ global strains.

Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element σx , σy , σxy , σz : global stresses.
	SSRG	Residual stresses at Gauss points. σx , σy , σxy , σz : global stresses.
Target	Not	
Stress/Strains	applicable.	
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0, 0
Overburden	Not applicable	
Phreatic Surface	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not	
Loads	applicable.	

LUSAS Output

Solver	Stress (default): σ_x , σ_y , σ_{xy} , σ_z , σ_{max} , σ_{min} , β , σ_s , σ_e (see description of principal stresses)		
	Strain: ε_x , ε_y , γ_{xy} , ε_z , ε_{max} , ε_{min} , β , ε_s , ε_e		
Modeller	See <u>Results Tables (Appendix K)</u>		

Local Axes

Not applicable.

Sign Convention

□ Standard 2D continuum element

Formulation

Geometric Nonlinearity

Total LagrangianNot applicable.UpdatedNot applicable.LagrangianNot applicable.

EulerianFor large displacements, large rotations and moderately large strains.Co-rotationalNot applicable.

Integration Schemes

Default.	1-point (see Notes)
Fine.	As default.
Default.	1-point (see Notes)
Fine.	As default.
	Fine. Default.

Mass Modelling

□ Lumped mass (see *Notes*).

Options

- 47 X-axis taken as axis of symmetry
- **55** Output strains as well as stresses.
- **105** Lumped mass matrix (see *Notes*).
- **139** Output yielded Gauss points only.

Notes on Use

- 1. The element formulations are based on the standard
- 2. The system parameter HGVISC is used to restrict element mechanisms due to underintegration. The default value is usually sufficient.
- 3. The bulk viscosity coefficients are used to restrict numerical oscillations due to the traversal of stress waves. The default bulk viscosity coefficients (BULKLF and BULKQF) may be altered as a SYSTEM parameter.
- 4. These elements must be used with a dynamic central difference scheme and a lumped mass matrix.
- 5. These elements are not applicable to static or eigenvalue analyses.
- 6. Automatic time step calculations are implemented.
- 7. As the element geometry is always updated in an explicit dynamic analysis, a nonlinear solution is obtained. When using explicit dynamics elements Nonlinear Control must be specified.

- 8. If CREEP PROPERITES are defined explicit time integration must be specified in VISCOUS CONTROL.
- 9. Non-conservative loading is invoked when the face loading (FLD) is applied.
- 10. Rayleigh damping coefficients are not supported by these elements.
- 11. Constraint equations are not available for use with these elements.
- 12. Nodes **must** be specified in an anticlockwise order. Option 123 is **not** applicable for this element. When using Modeller ensure surface normal is in the +ve z direction.
- 13. The maximum and minimum principal stress computations for axisymmetric elements do not include the σz term as this is implicitly a principal stress in a biaxial stress field.

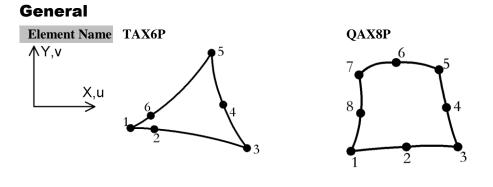
Restrictions

□ Avoid excessive aspect ratio

Recommendations on Use

Explicit dynamics elements may be used to define surface boundaries which will be active in a slideline analysis.

2D Axisymmetric Solid Two Phase Continuum Elements



Element Group	2D Continuum
Element	Axisymmetric Solid
Subgroup	
Element	A family of 2D isoparametric elements with higher order models capable
Description	of modelling curved boundaries. The formulations apply over a unit
	radian segment of the structure and the loading and boundary conditions
	are axisymmetric. By default, the Y-axis is taken as the axis of symmetry.
	The elements are numerically integrated.
Number Of	6 or 8 numbered anticlockwise.
Nodes	
Freedoms	U, V, P: at corner nodes. U, V: at midside nodes.
Node	X, Y: at each node.
Coordinates	

Geometric Properties

Not applicable (a unit radian segment is assumed).

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC
		AXISYMMETRIC (Elastic: orthotropic,
		Axisymmetric)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC 4 (Not supported in LUSAS Modeller)

Matrix Joint	Rigidities. Not applicable Not applicable	Not applicable.
Concrete		MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Elasto-Plastic	Stress resultant:	Not applicable.
	Interface:	MATERIAL PROPERTIES NONLINEAR 27.
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker-Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr-Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Modified Mohr- Coulomb:	MATERIAL PROPERTIES MODIFIED MOHR_COULOMB (Elastic: Isotropic, Plastic: Mohr-Coulomb/Tresca, non- associative Hardening with tension/compression cut-off)
	Modified Cam- clay	MATERIAL PROPERTIES CAM_CLAY MODIFIED (Elastic: Isotropic, Plastic)
	Optimised Implicit Von Mises:	MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic)
	Volumetric Crushing:	MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam)
	Stress Potential	STRESS POTENTIAL VON_MISES, HILL, HOFFMAN
		(Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
Creep		CREEP PROPERTIES (Creep)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic		VISCO ELASTIC PROPERTIES
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Ko Initialisation	Applicable	
Rubber	Not applicable	
Generic Polymer	Isotropic	MATERIAL PROPERTIES NONLINEAR 89

(Generic Polymer Model)
Composite Not applicable

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, P: at corner nodes. U, V:at midsaide nodes.
Concentrated Loads	CL	Concentrated loads. Px, Py, Q: force/flux per unit radian at corner nodes. Px,Py: force per unit radian at midside nodes.
Element Loads		
Distributed Loads		Not available.
	FLD	<u>Face loads</u> . Px, Py, Q: local face pressures/flux at corner nodes (force/flux per unit area). Px, Py: local face pressures at midside nodes.
	FLDG	Global Face Loads. σx , σy , σxy at nodes
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Ωx ,
		Ω y (angular velocity must be applied about axis of symmetry), 0, 0, gx, gy. (See Notes on Use)
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0,
		φ4, Xcbf, Ycbf, gx, gy. (See Notes on Use)
Velocities		Velocities. Vx, Vy: at nodes.
Accelerations		Acceleration Ax, Ay: at nodes.
Initial SSI, SS Stress/Strains	SSI, SSIE	Initial stresses/strains at nodes/for element. σx , σy ,
		σ xy, σ z, σ p: global stresses. ε x, ε y, γ xy, ε z: global strains.
	SSIG	Initial stresses/strains at Gauss points. σx , σy , σxy ,
		σ z, σ p: global stresses. ε x, ε y, γ xy, ε z: global strains.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. σx , σy , σxy ,
		σ z, σ p: global stresses.
	SSRG	Residual stresses at Gauss points. σx , σy , σxy , σz ,
		σp: global stresses.
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. σx , σy ,
SUESSISU'AIIIS		σ xy, σ z, σ p: global stresses. ε x, ε y, γ xy, ε z: global strains.
	TSSIG	Target stresses/strains at Gauss points. $\sigma x, \sigma y, \sigma xy,$

 σz , σp : global stresses. ϵx , ϵy , γxy , ϵz : global strains.

Temperatures TEMP, TMPE

Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0, 0

OverburdenApplicable.Phreatic SurfaceApplicable.Field LoadsNot applicable.Temp DependentNot applicable.Loads

LUSAS Output

Solver	Stress (default): σ_x , σ_y , σ_{xy} , σ_z , σ_p , σ_{max} , σ_{min} , β , σ_s , σ_e (see <u>description of principal stresses</u>)
	Strain: εx , εy , γxy , εz , εmax , εmin , β , εs , εe
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 2D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and large rotations.		
Updated	For large displacements and large rotations.		
Lagrangian			
Eulerian	For large displacements, large rotations and moderately large strains.		
Co-rotational	Not applicable.		

Integration Schemes

Stiffness	Default.	3-point (TAX6P), 2x2 (QAX8P)
	Fine (see Options).	3x3 (QAX8P)
Mass	Default.	3-point (TAX6P), 2x2 (QAX8P)
	Fine (see Options).	3x3 (QAX8P)

Mass Modelling

□ Consistent mass (default).

Lumped mass.

Options

- **18** Invokes finer integration rule.
- 47 X-axis taken as axis of symmetry
- 54 Updated Lagrangian geometric nonlinearity.
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity.
- 91 Invokes fine integration rule for mass matrix.
- **105** Lumped mass matrix.
- 123 Clockwise node numbering.
- **139** Output yielded Gauss points only.
- **167** Eulerian geometric nonlinearity.

Notes on Use

- 1. Two phase material parameters must be used with these elements for undrained and consolidation analysis.
- 2. The element formulations are based on the standard **isoparametric** approach. The variation of isoparametric stresses and pore pressures within an element can be regarded as linear.
- 3. All elements pass the **<u>patch test</u>**.
- 4. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility.
- 5. Option 123 will not operate on a mesh with a mixture of clockwise and anti-clockwise elements, it is only applicable if **every** element is numbered **clockwise**. Surface normals should be visualised and if necessary corrected in the pre-processing stage.

- 6. Using Option 123 with local loading types, such as FLD and UDL, will cause load reversal.
- 7. The global components of gravity acting on the fluid phase are defined by gx and gy under CBF and BFP loading.
- 8. The maximum and minimum principal stress computations for axisymmetric elements do not include the □z term as this is implicitly a principal stress in a biaxial stress field.

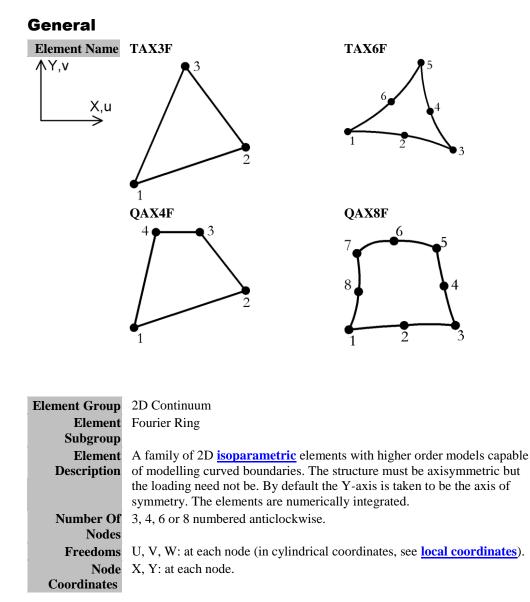
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

Recommendations on Use

- The 8-noded element with a 2*2 Gauss rule is usually the most effective element, as the under-integration of the stiffness matrix prevents locking, which may occur either when the element is subjected to <u>parasitic shear</u>, or as the material reaches the incompressible limit (elasto-plasticity). The Gauss point stresses are also sampled at the most accurate locations for the element. However, the element does possess one spurious zero energy mode. This mode is very rarely activated in linear analysis, but it may occur in both materially and geometrically nonlinear analyses. Therefore, a careful examination of the solution should be performed, to check for spurious stress oscillations and peculiarities in the deformed configuration.
- The 8-noded element with a 3*3 Gauss rule may be used if a spurious mechanism is excited with the 2*2 Gauss rule.

2D Axisymmetric Fourier Ring Elements



Geometric Properties

Not applicable.

Material Properties

Linear	Isotropic:
	Orthotropic:
	-
	Anisotropic:
	Rigidities.
Matrix	Not applicable
Joint	Not applicable
Concrete	Not applicable
Elasto-Plastic	Not applicable
Creep	Not applicable
Damage	Not applicable
Viscoelastic	Not applicable
Shrinkage	Not applicable
Ko Initialisation	Not applicable
Rubber	Not applicable
Generic Polymer	Not applicable
Composite	Not applicable

MATERIAL PROPERTIES (Elastic: Isotropic) MATERIAL PROPERTIES ORTHOTROPIC (Elastic: Orthotropic Plane Stress) MATERIAL PROPERTIES ORTHOTROPIC SOLID (Elastic: Orthotropic Solid) Not applicable Not applicable

Loading

Prescribed Value Concentrated	,	Prescribed variable. U, V, W: at each node. Concentrated loads. Px, Py, Pz: at each node (global,
Loads	N.T	may also be applied locally, see options).
Element Loads	Not applicable.	
Distributed Loads	UDL	Not applicable.
	FLD	Face loads. Px, Py, Pz: local face axis pressures at
		nodes Pz in the direction of increasing θ .
	FLDG	Not applicable.
Body Forces	CBF	Constant body forces for element (see Notes). Xcbf,
		Yebf, Zebf, Ωx , $\Omega y \Omega z$, αx , αy , αz , Xo, Yo, Zo, $d\theta/dt$
	BFP, BFPE	Body force potentials at nodes/for element. Xcbf,

		Ycbf, Zcbf
Velocities	VELO	Velocities. Vx, Vy, Vz at nodes.
Accelerations	ACCE	Acceleration. Ax, Ay, Az at nodes.
	SSI, SSIE	Initial stresses/strains at nodes/for element. σx , σy ,
Stress/Strains		σz, $σxy$, $σyz$, $σxz$: local stresses. $εx$, $εy$, $εz$, $γxy$,
		γyz, γxz: local strains.
	SSIG	Initial stresses/strains at Gauss points. σx , σy , σz ,
		σxy, σyz, σxz: local stresses. $εx$, $εy$, $εz$, $γxy$, $γyz$,
		γxz: local strains.
Residual Stresses	Not	
	applicable.	
Target		
Stress/Strains		
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0, 0
Overburden		
	applicable.	
Phreatic Surface	Not applicable.	
Field Loads		
Field Loads	applicable.	
Temp Dependent		
	applicable.	

LUSAS Output

Solver	Stress (default): σ_x , σ_y , σ_z , σ_{xy} , σ_{yz} , σ_{xz} , σ_{max} , σ_{min} , β , σ_s , σ_e (see description of principal stresses)
	Strain: ε_x , ε_y , ε_z , γ_{xy} , γ_{yz} , γ_{xz} , ε_{max} , ε_{min} , β , ε_s , ε_e
	Use LUSAS Modeller to access results at various angles around the structure. See Local and Global Results in the Modeller User Manual
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

 \Box Cylindrical coordinates (see *Appendix F*).

The element axes are defined in the cylindrical coordinate system x,y,z, with associated displacements u,v,w. The tangential displacement w is positive in the direction of increasing θ, where θ is the positive rotation defined by the right-hand coordinate system about the axis of symmetry. u and v are positive in the direction of increasing x and y respectively and may be either axial or radial displacements depending on the definition of the axis of symmetry.

Sign Convention

□ Standard 3D continuum element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Stiffness	Default.	1-point (TAX3F), 3-point (TAX6F), 2x2 (QAX4F, QAX8F)
Mass	Fine (see <i>Options</i>). Default.	3x3 (QAX8F), 3-point (TAX3F) 1-point (TAX3F), 3-point (TAX6F), 2x2 (QAX4F, QAX8F)
	Fine (see Options).	3x3 (QAX8F), 3-point (TAX3F)

Mass Modelling

□ Consistent mass (default).

□ Lumped mass.

Options

- **18** Invokes fine integration rule.
- 47 X-axis taken as axis of symmetry.
- 55 Output strains as well as stresses.
- **102** Switch off load correction stiffness matrix due to centripetal acceleration.
- 105 Lumped mass matrix.
- **202** Apply concentrated loads in cylindrical coordinates.

Notes on Use

- 1. CBF loads are always applied as acceleration loading. Xo, Yo, Zo, permit a shift in the original point of the global coordinate system (about which the rotations are applied). $d\theta/dt$ is the local angular velocity about the finite element coordinate system.
- 2. The application of the CBF loading depends on the particular element material model selected. See the description of Fourier analysis in *Chapter 2* of the *LUSAS User Guide*.
- 3. If CBF loads are used the structure must be axisymmetric about the X-axis (option 47).
- 4. Fourier elements cannot be mixed with other element types.
- 5. Temperature fields cannot be used in dynamic or harmonic response analyses.
- 6. Centripetal load stiffening has been applied to the n=0 term, but there is no nonlinear stress stiffening contribution. The centripetal load stiffening matrix, contrary, to its name, actually decreases the stiffness of the structure. Centripetal forces are proportional to the angular rotation squared and the lever arm of the mass from the centre of rotation. As the body spins, the lever arm is lengthened by positive displacements, which increases the applied load. This may, conversely, be thought of as reducing the stiffness. The centripetal load stiffness is applied by default, but is may be omitted by setting option 102.
- 7. The maximum and minimum principal stress computations for axisymmetric elements do not include the σz term as this is implicitly a principal stress in a biaxial stress field.

Restrictions

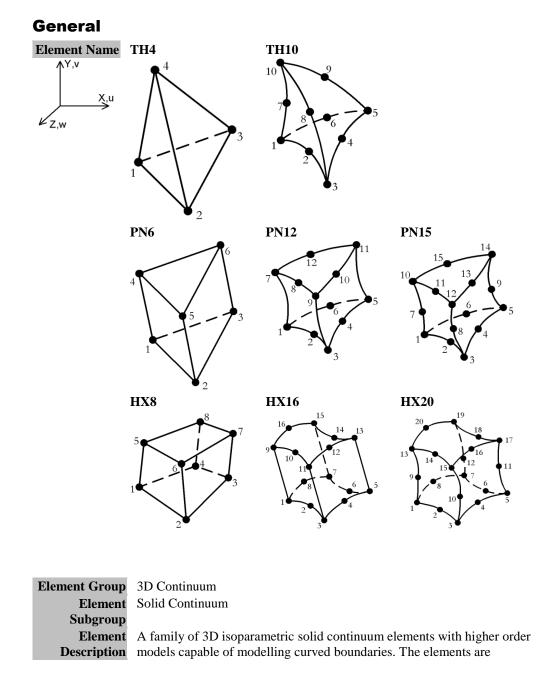
- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

Recommendations on Use

- The element is designed to model fairly solid structures, but it also performs well in comparison to standard shell analyses and may be an effective alternative for axisymmetric problems. The QAX8F is the most effective element of the family.
- If eigenvalues are required from a thin shelled structure such as a cylinder, the Fourier elements provide an efficient means of checking a range of circumferential harmonics and will indicate the permissible coarseness of a finite element mesh which will adequately represent the 3D variation.

Chapter 4 : 3D Continuum Elements.

3D Solid Continuum Elements



	numerically integrated.
Number Of	4 or 10 (tetrahedra). 6, 12 or 15 (pentahedra). 8, 16 or 20 (hexahedra).
Nodes	The elements are numbered according to a right-hand screw rule in the
	local z-direction.
Freedoms	U, V, W: at each node.
Node	X, Y, Z: at each node.
Coordinates	

Geometric Properties

Not applicable.

Material Properties

Linear	Isotropic: Orthotropic:	MATERIAL PROPERTIES (Elastic: Isotropic) MATERIAL PROPERTIES ORTHOTROPIC SOLID (Elastic: Orthotropic Solid)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC SOLID (Elastic: Anisotropic Solid)
	Rigidities.	Not applicable.
Matrix	Not applicable.	
Joint	Not applicable.	
Concrete		MATERIAL PROPERTIES NONLINEAR 105 (Elastic: Isotropic, Plastic: Transient Smoothed Multi- Crack Concrete) MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Elasto-Plastic	Stress resultant:	Not applicable.
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker- Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr- Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)

	Modified Mohr- Coulomb:	MATERIAL PROPERTIES MODIFIED MOHR_COULOMB (Elastic: Isotropic, Plastic: Mohr-Coulomb/Tresca, non- associative Hardening with tension/compression
	Modified Cam-clay Optimised Implicit Von Mises: Volumetric Crushing: Stress Potential:	cut-off) MATERIAL PROPERTIES CAM_CLAY MODIFIED (Elastic: Isotropic, Plastic) MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic) MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam) STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
Creep	AASHTO	CREEP PROPERTIES (Creep)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of Practice) MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP
	Chinese	(Concrete creep model to CEB-FIP Model Code 1990) MATERIAL PROPERTIES NONLINEAR 86 CHINESE
	Eurocode	(Chinese creep model to Chinese Code of Practice) MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
Damage Viscoelastic		DAMAGE PROPERTIES SIMO, OLIVER (Damage) VISCO ELASTIC PROPERTIES
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Ko Initialisation	Applicable	

Elasto- Plastic Interface		MATERIAL PROPERTIES NONLINEAR 26
Rubber	Not applicable.	
Generic Polymer	Isotropic	MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)
Composite	Not applicable	

Loading

Prescribed Value Concentrated Loads		Prescribed variable. U, V, W: at each node. Concentrated loads. Px, Py, Pz: at each node.
Element Loads	Not applicable.	
Distributed Loads	UDL	Not applicable.
	FLD	Face Loads. Px, Py, Pz: local face pressures at nodes.
	FLDG	Global Face Loads. σx , σy , σz , σxy , σyz , σxz at nodes
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Zcbf, Ωx , Ωy , Ωz , αx , αy , αz
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0, φ ₄ , Xcbf, Ycbf, Zcbf
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay, Az: at nodes.
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element. σx , σy ,
Stress/Strains		σz, σxy, σyz, σxz: global stresses. εx, εy, εz,
		γxy, γyz, γxz: global strains.
	SSIG	Initial stresses/strains at Gauss points σx , σy , σz , σxy , σyz , σxz : global stresses. εx , εy , εz , γxy ,
		γ yz, γ xz: global strains.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. σx , σy , σz ,
	SSDC	σ xy, σ yz, σ xz: global stresses.
	SSRG	Residual stresses at Gauss points. σx , σy , σz , σxy ,
_		σ yz, σ xz global stresses.
Target	TSSIE, TSSIA	Target stresses/strains at nodes/for element. σx , σy ,

Stress/Strains	TSSIG	 σz, σxy, σyz, σxz: global stresses. εx, εy, εz, γxy, γyz, γxz: global strains. Target stresses/strains at Gauss points σx, σy, σz, σxy, σyz, σxz: global stresses. εx, εy, εz, γxy, γyz, γxz: global strains.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0, 0
Overburden	Applicable.	
Phreatic Surface	Applicable.	
Field Loads	Not applicable.	
Temp Dependent Loads	Not applicable.	

LUSAS Output

Solver	Stress (default): σx , σy , σz , σxy , σyz , σxz , σe : global stresses.
	Strain: Ex, Ey, Ez, Yxy, Yyz, Yxz, Ee: global strains.
	For optional principal stress/strain output, together with the corresponding direction cosines, use Option 77.
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 3D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and large rotations.
Updated	For large displacements and large rotations.
Lagrangian	
Eulerian	For large displacements, large rotations and moderately large strains.

Co-rotational For large displacements and large rotations.

Integration Schemes

Stiffness	Default.	1-point (TH4), 4-point (TH10), 3x2 (PN6, PN12, PN15), 2x2x2 (HX8, HX16, HX20)
	Fine (see <i>Options</i>).	5-point (TH10), 3x3x2 (HX16), 3x3x3 (HX20)
	Coarse (see <i>Options</i>)	13-point (HX20), 14-point (HX20)
Mass	Default.	1-point (TH4), 4-point (TH10), 3x2 (PN6, PN12, PN15), 2x2x2 (HX8, HX16, HX20)
	Fine (see	4-point (TH4) 11-point (TH10), 14-point (TH10)
	Options).	3x3x2 (HX16), 3x3x3 (HX20)
	Coarse (see <i>Options</i>)	13-point (HX20), 14-point (HX20)

Mass Modelling

- □ Consistent mass (default).
- Lumped mass.

Options

- **18** Invokes fine integration rule.
- **36** Follower loads
- 54 Updated Lagrangian geometric nonlinearity
- 55 Output strains as well as stresses.
- 77 Output principal stresses and direction cosines.
- 87 Total Lagrangian geometric nonlinearity.
- 91 Invoke finer integration of the mass matrix.
- 102 Switch off load correction stiffness due to centripetal acceleration.
- **105** Lumped mass matrix.
- 139 Output yielded Gauss points only.
- **155** Use 14-point integration rule for HX20.
- **156** Use 13-point integration rule for HX20.
- 167 Eulerian geometric nonlinearity.
- 229 Co-rotational geometric nonlinearity.
- **395** Use 14-point integration rule for mass matrix of TH10 (used together with Option 91).

398 For HX20 and HX16 with fine integration use all integration points for stress extrapolation.

Notes on Use

- 1. The elements are based on the standard isoparametric approach. The variation of stresses within an element may be regarded as constant for the lower order elements (corner nodes only), and linear for the higher order elements (with mid-side nodes).
- 2. All elements pass the **<u>patch test</u>**.
- 3. When using table input format for temperature dependent ORTHOTROPIC SOLID or ANISOTROPIC SOLID material properties, the value of nset used is that defined in the first line of the property table.
- 4. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility.

Restrictions

- Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

Recommendations on Use

- The 3D solid elements should be used if the stress field is fully 3D, i.e. it cannot be approximated with any of the 2D elements, e.g. as for a non-axisymmetric pressure vessel.
- For linear materials, the 20-noded element with a 2*2*2 Gauss rule is usually the most effective element, as this under-integration of the stiffness matrix prevents locking, i.e. over-stiff solutions will occur if the elements are used with a 3*3*3 Gauss integration rule to model structures subjected to bending. However, the element possesses six <u>zero energy modes</u>. Therefore, a careful examination of the solution should be performed to check for spurious stress oscillations and peculiarities in the deformed configuration. Either the 14-point or 3*3*3 Gauss rules should be used for materially nonlinear problems or materially linear problems that exhibit spurious deformations.
- The 8-noded element should not be used for analyses where bending effects are significant as the element tends to lock in **parasitic shear** [C1]. The 8-noded element will perform poorly if it is highly distorted. The 4-noded tetrahedron TH4 element is generally not effective and should only be used if the geometry requires elements of this shape.

3D Solid Continuum Element with Enhanced Strains

General	
Element Name	HX8M
X,u Z,w	
Element Group	3D Continuum
Element	Solid Continuum
Subgroup	
Element	A 3D isoparametric solid element with an incompatible strain field. This
Description	mixed assumed strain element demonstrates a much superior performance to that of the HX8 element.
Number Of	8. The element is numbered according to a right-hand screw rule in the
Nodes	local z-direction.
Freedoms	U, V, W: at each node.
Node	X, Y, Z: at each node.
Coordinates	

Geometric Properties

Not applicable.

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC SOLID (Elastic: Orthotropic Solid)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC SOLID (Elastic: Anisotropic Solid)
Matrix	Rigidities. Not applicable.	Not applicable.

Joint	Not applicable.	
Concrete	аррисаоне.	MATERIAL PROPERTIES NONLINEAR 105 (Elastic: Isotropic, Plastic: Transient Smoothed Multi- Crack Concrete)
		MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Elasto-Plastic	Stress resultant:	Not applicable.
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker- Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr- Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Modified Mohr- Coulomb:	MATERIAL PROPERTIES MODIFIED MOHR_COULOMB (Elastic: Isotropic, Plastic: Mohr-Coulomb/Tresca, non- associative Hardening with tension/compression cut-off)
	Modified Cam-clay Optimised Implicit Von Mises: Volumetric Crushing: Stress Potential	MATERIAL PROPERTIES CAM_CLAY MODIFIED (Elastic: Isotropic, Plastic) MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic) MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam) STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises
Сгеер	AASHTO CEB-FIP	Orthotropic: Hill, Hoffman) MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of Practice)
	CED-FIF	MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP (Concrete creep model to CEB-FIP Model Code

	Chinese	1990) MATERIAL PROPERTIES NONLINEAR 86 CHINESE
	Eurocode	(Chinese creep model to Chinese Code of Practice) MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic		VISCO ELASTIC PROPERTIES
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Ko Initialisation	Applicable	
Rubber	Ogden:	MATERIAL PROPERTIES RUBBER OGDEN (Rubber: Ogden)
	Mooney- Rivlin:	MATERIAL PROPERTIES RUBBER MOONEY_RIVLIN (Rubber: Mooney-Rivlin)
	Neo-Hookean:	MATERIAL PROPERTIES RUBBER NEO_HOOKEAN (Rubber: Neo-Hookean)
	Hencky:	MATERIAL PROPERTIES RUBBER HENCKY (Rubber: Hencky)
Generic Polymer	Isotropic	MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)
Composite	Not applicable.	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, W: at each node.
Concentrated	CL	Concentrated loads. Px, Py, Pz: at each node.
Loads		
Element Loads	Not applicable.	
Distributed Loads	UDL	Not applicable.
	FLD	Face Loads. Px, Py, Pz: local face pressures at nodes.
	FLDG	Global Face Loads. σx , σy , σz , σxy , σyz , σxz at nodes
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Zcbf,

		$\Omega x, \Omega y, \Omega z, \alpha x, \alpha y, \alpha z$
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0,
		φ ₄ , Xcbf, Ycbf, Zcbf
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay, Az: at nodes.
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element. σx , σy ,
Stress/Strains		σz, σxy, σyz, σxz: global stresses. εx, εy, εz,
		γxy, γyz, γxz: global strains.
	SSIG	Initial stresses/strains at Gauss points σx , σy , σz ,
		σxy, σyz, σxz: global stresses. εx, εy, εz, γxy,
		γyz, γxz: global strains.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. σx , σy , σz ,
		σ xy, σ yz, σ xz: global stresses.
	SSRG	Residual stresses at Gauss points. σx , σy , σz , σxy ,
		σyz, σxz global stresses.
Target	TSSIE, TSSIA	Target stresses/strains at nodes/for element. σx , σy ,
Stress/Strains		σz, σxy, σyz, σxz: global stresses. εx, εy, εz,
		γxy, γyz, γxz: global strains.
	TSSIG	Target stresses/strains at Gauss points σx , σy , σz ,
		$\sigma_{xy}, \sigma_{yz}, \sigma_{xz}$: global stresses. $\varepsilon_x, \varepsilon_y, \varepsilon_z, \gamma_{xy}, \varepsilon_z$
		γ yz, γ xz: global strains.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0,
_		0, 0
Overburden		
Phreatic Surface	Applicable.	
	Not applicable.	
Temp Dependent Loads	not applicable.	

LUSAS Output

Solver	Stress (default): σx , σy , σz , σxy , σyz , σxz , σe : global stresses.
	Strain: Ex, Ey, Ez, Yxy, Yyz, Yxz, Ee: global strains.
	Stretch (for rubber only): V11, V22, V33, V12, V23, V13, $\lambda 1, \lambda 2, \lambda 3,$ det F.

Where V_{ii} are components of the left stretch tensors, λ_i the principal

stretches, $\theta\lambda$ the angle between the maximum principal stretch and the global X axis, and det F the determinant of the deformation gradient or volume ratio.

For optional principal stress/strain output, together with the corresponding direction cosines, use Option 77.

Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 3D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and large rotations.		
Updated	For large displacements and large rotations.		
Lagrangian			
Eulerian	For large displacements, large rotations and moderately large strains.		
Co-rotational	For large displacements and large rotations (large strains with the rubber material model).		

Integration Schemes

Stiffness	Default.	2x2x2
	Fine.	As default.
Mass	Default.	2x2x2
	Fine.	As default.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- **39** Stress smoothing for rubber material models.
- 54 Updated Lagrangian geometric nonlinearity.
- **55** Output strains as well as stresses.
- 77 Output principal stresses and direction cosines.
- 87 Total Lagrangian geometric nonlinearity.
- **102** Switch off load correction stiffness due to centripetal acceleration.
- 105 Lumped mass matrix.
- 139 Output yielded Gauss points only.
- 167 Eulerian geometric nonlinearity.
- 225 Use alternative number of parameters for enhanced strain interpolation (see *Notes*).
- 229 Co-rotational geometric nonlinearity.

Notes on Use

- 1. The element is based on the standard isoparametric approach. The variation of stresses within an element may be regarded as linear.
- 2. The strain field for this element consists of two parts: the compatible strains derived from the assumed displacement field and the assumed enhanced strains; see *LUSAS Theory Manual*. By default, 18 parameters are used to define the assumed enhanced strain. In general, the default number of parameters should be used. However, 9 parameters may be specified using Option 225. In most cases the use of 9 or 18 parameters will give an equivalent solution. However, in some instances a better response may be obtained using more parameters at the expense of increased computation time.
- 3. The element passes the <u>patch test</u> and the large strain patch test for rubber.
- 4. When using table input format for temperature dependent ORTHOTROPIC SOLID or ANISOTROPIC SOLID material properties, the value of nset used is that defined in the first line of the property table.
- 5. Non-conservative (follower) loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility. The load does not have to be normal to the face and may also vary over the face.
- 6. To apply a non-conservative (follower) pressure load (load type FLD) with corotational geometric nonlinearity, Option 36 must be specified. Note that this load must be normal to the face and constant for all the nodes of the element face.
- 7. The converged stresses for the rubber material model are <u>Kirchhoff</u> stresses (see *LUSAS Theory Manual*).

- 8. Option 39 is used to smooth the stress output. It is particularly useful when the rubber material model is applied and the element is under very high compression where oscillatory stresses may appear (checker-board pattern).
- 9. For the rubber material model, converged values for strain output are replaced by the left stretch tensor V, the principal stretches of the vectors defining these principal directions. The principal stretches and directions can be obtained using Option 77. The value of det $F = \lambda_1 \lambda_2 \lambda_3$ (the volume ratio) is only available for Gauss point output.
- 10. For the rubber material model, the iterative values of stress and strain are output in local co-rotated directions at the Gauss points only.
- 11. Convergence difficulties can sometimes arise when using enhanced strain elements with nonlinear materials, particularly if the material is elastic-perfectly plastic or if a very shallow hardening curve is defined. In such cases it is recommended that the standard element formulation is used.

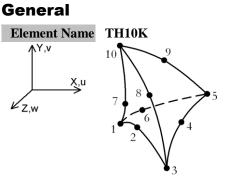
Restrictions

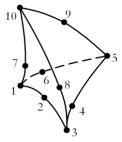
- □ Avoid excessive aspect ratio
- □ Rubber material models can only be applied in conjunction with the co-rotational formulation, Option 229.

Recommendations on Use

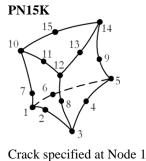
This element exhibits an improved performance when compared with the parent element HX8. The integration rules are the same as the parent element. The HX8M element does not suffer from locking due to **parasitic shear** or when the material approaches the incompressible limit. No zero energy modes exist for this element.

3D Solid Continuum Crack Tip Elements

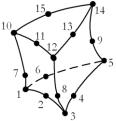




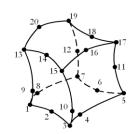
Crack specified at Node 1



Crack specified along edge 1-2-3



Crack specified along edge 1-2-3



Crack specified along edge 1-2-3

Element Group Solid Continuum Element Subgroup Element Description

A family of 3D isoparametric crack tip elements where the crack tip can be located at any corner node or along any edge of an element. The mid-

3D Continuum

Crack specified at Node 1

HX20K

13



	side nodes are moved to the quarter points to produce a singularity at the crack tip. The strains vary as the square root of 1/R, where R is the distance from the crack tip. These elements are used at the crack tip only. The elements are numerically integrated.
Number Of	
Nodes	numbered according to a right-hand screw rule in the local z-direction.
Freedoms	U, V, W: at each node.
Node	X, Y, Z: at each node.
Coordinates	

Geometric Properties

Not applicable.

Material Properties

-	pic)
Orthotropic: MATERIAL PROPERTIES ORTHOTROP (Elastic: Orthotropic Solid)	IC SOLID
Anisotropic: MATERIAL PROPERTIES ANISOTROPIC (Elastic: Anisotropic Solid)	C SOLID
Rigidities. Not applicable.	
Matrix Not applicable.	
Joint Not applicable.	
Concrete MATERIAL PROPERTIES NONLINEAR (Elastic: Isotropic, Plastic: Smoothed Multi- Concrete)	10)
Elasto-Plastic Stress Not applicable. resultant:	
Tresca: MATERIAL PROPERTIES NONLINEAR (Elastic: Isotropic, Plastic: Tresca, Harden Isotropic Hardening Gradient, Isotropic Pla Strain or Isotropic Total Strain)	ing:
Drucker- Prager: MATERIAL PROPERTIES NONLINEAR (Elastic: Isotropic, Plastic: Drucker-Prager Hardening: Granular)	
Mohr-MATERIAL PROPERTIES NONLINEARCoulomb:(Elastic: Isotropic, Plastic: Mohr-Coulomb Hardening: Granular with Dilation)	
Modified MATERIAL PROPERTIES	

	Mohr- Coulomb:	MODIFIED MOHR_COULOMB (Elastic: Isotropic, Plastic: Mohr-Coulomb/Tresca, non- associative Hardening with tension/compression cut-off)
Сгеер	Modified Cam-clay Optimised Implicit Von Mises: Volumetric Crushing: Stress Potential:	MATERIAL PROPERTIES CAM_CLAY MODIFIED (Elastic: Isotropic, Plastic) MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic) MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam) STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
	AASHTO	CREEP PROPERTIES (Creep) MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP (Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE
	IRC	(Concrete creep model to EUROCODE_2) MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
Damage Viscoelastic		DAMAGE PROPERTIES SIMO, OLIVER (Damage) VISCO ELASTIC PROPERTIES
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Ko Initialisation Elasto- Plastic Interface	Applicable	MATERIAL PROPERTIES NONLINEAR 26

Rubber	Not applicable.	
Generic Polymer	Isotropic	MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)
Composite	Not applicable	

Loading

Prescribed Value Concentrated Loads		Prescribed variable. U, V, W: at each node. Concentrated loads. Px, Py, Pz: at each node.
Element Loads Distributed Loads	Not applicable. UDL FLD	Not applicable. Face Loads. Px, Py, Pz: local face pressures at nodes.
	FLDG	Global Face Loads. σx , σy , σz , σxy , σyz , σxz at nodes
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Zcbf, Ωx , Ωy , Ωz , αx , αy , αz
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0, ϕ_4 , Xcbf, Ycbf, Zcbf
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay, Az: at nodes.
Initial Stress/Strains	SSI, SSIE	Initial stresses/strains at nodes/for element. σx , σy , σz , σxy , σyz , σxz : global stresses. ϵx , ϵy , ϵz ,
	SSIG	 γxy, γyz, γxz: global strains. Initial stresses/strains at Gauss points σx, σy, σz, σxy, σyz, σxz: global stresses. εx, εy, εz, γxy,
Residual Stresses	SSR, SSRE	 γyz, γxz: global strains. Residual stresses at nodes/for element. σx, σy, σz, σxy, σyz, σxz: global stresses.
	SSRG	Residual stresses at Gauss points. σx , σy , σz , σxy , σyz , σxz global stresses.
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. σx , σy , σz , σxy , σyz , σxz : global stresses. εx , εy , εz ,

	TSSIG	 γxy, γyz, γxz: global strains. Target stresses/strains at Gauss points σx, σy, σz, σxy, σyz, σxz: global stresses. εx, εy, εz, γxy,
Temperatures	TEMP, TMPE	γyz, γxz: global strains.Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0
Overburden	Applicable.	
Phreatic Surface	Applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not applicable.	
Loads		

LUSAS Output

Solver	Stress (default): σx , σy , σz , σxy , σyz , σxz , σe : global stresses.
	Strain: Ex, Ey, Ez, Yxy, Yyz, Yxz, Ee: global strains.
	For optional principal stress/strain output, together with the corresponding direction cosines, use Option 77.
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 3D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and large rotations.	
Updated	For large displacements and large rotations.	
Lagrangian		
Eulerian	For large displacements, large rotations and moderately large strains.	
Co-rotational	For large displacements and large rotations.	

Integration Schemes

Stiffness	Default.	4-point (TH10K), 6x3 (PN15K), 3x3x3 (HX20K)
	Fine (see Options).	11-point (TH10K), 12x4 (HX15K)
Mass	Default.	4-point (TH10K), 6x3 (PN15K), 3x3x3 (HX20K)
	Fine (see Options).	11-point (TH10K), 14-point (TH10K), 12x4 (HX15K)

Mass Modelling

- □ Consistent mass (default).
- Lumped mass.

Options

- **18** Invokes fine integration rule.
- 36 Follower loads
- 54 Updated Lagrangian geometric nonlinearity
- 55 Output strains as well as stresses.
- 77 Output principal stresses and direction cosines.
- 87 Total Lagrangian geometric nonlinearity.
- 91 Invoke finer integration of the mass matrix.
- 102 Switch off load correction stiffness due to centripetal acceleration.
- **105** Lumped mass matrix.
- 139 Output yielded Gauss points only.
- 167 Eulerian geometric nonlinearity.
- 229 Co-rotational geometric nonlinearity.
- **395** Use 14-point integration rule for mass matrix of TH10 (used together with Option 91).
- **398** For HX20 and HX16 with fine integration use all integration points for stress extrapolation.

Notes on Use

- 1. The elements are based on the standard isoparametric approach. Moving the mid-side nodes to the quarter points creates a singularity with theoretically infinite stress at the crack tip.
- 2. When using table input format for temperature dependent ORTHOTROPIC SOLID or ANISOTROPIC SOLID material properties, the value of nset used is that defined in the first line of the property table.
- 3. Non-conservative loading is available with these elements when using either Updated Lagrangian or Eulerian geometric nonlinear formulations together with the FLD loading facility.

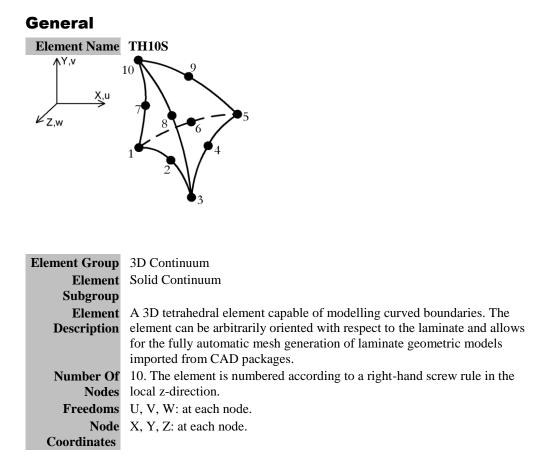
Restrictions

- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

Recommendations on Use

- The 3D solid crack tip elements should be used if the stress field is fully 3D, i.e. it cannot be approximated with any of the 2D crack tip elements.
- Elements TH10K, PN15K and HX20K are specifically designed for application to fracture mechanics problems and may be used to model the singularities that occur at the crack tip. The mid-side nodes near the crack tip are shifted to the quarter point. This ensures a singularity is present at the crack tip and that strains vary as 1 over the square root of r where r is the distance from the crack tip.

3D Solid Continuum Composite Elements (Tetrahedral)



Geometric Properties

See **<u>Composites</u>** in the Modeller Reference Manual

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC SOLID
		(Elastic: Orthotropic Solid)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC SOLID
		(Elastic: Anisotropic Solid)
	Rigidities.	Not applicable.

Matrix		
Joint	applicable. Not	
	applicable.	
Concrete		MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Elasto-Plastic	Stress resultant:	Not applicable.
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker- Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr- Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Modified Mohr- Coulomb:	MATERIAL PROPERTIES MODIFIED MOHR_COULOMB (Elastic: Isotropic, Plastic: Mohr-Coulomb/Tresca, non- associative Hardening with tension/compression cut-off)
	Volumetric Crushing:	Not applicable.
	Stress Potential	STRESS POTENTIAL VON_MISES, HILL, HOFFMAN
Сгеер		(Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
	AASHIO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP (Concrete creep model to CEB-FIP Model Code
	Chinese	1990) MATERIAL PROPERTIES NONLINEAR 86 CHINESE
	Eurocode	CHINESE (Chinese creep model to Chinese Code of Practice) MATERIAL PROPERTIES NONLINEAR 86

		EUROCODE (Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic		VISCO ELASTIC PROPERTIES
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Ko Initialisation	Not applicable	
Rubber	Not applicable.	
Generic Polymer		MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)
Resin Cure Model		MATERIAL PROPERTIES NONLINEAR CURE LAYER, FIBRE_RESIN
Composite	Composite solid:	COMPOSITE PROPERTIES (Elastic: Orthotropic Solid)

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, W: at each node.
Concentrated Loads	CL	Concentrated loads. Px, Py, Pz: at each node.
Element Loads	Not applicable.	
Distributed Loads	UDL	Not applicable.
	FLD	Face Loads . Px, Py, Pz: local face pressures at nodes.
	FLDG	Global Face Loads. σx , σy , σz , σxy , σyz , σxz at nodes
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Zcbf,
	BFP, BFPE	$\Omega x, \Omega y, \Omega z, \alpha x, \alpha y, \alpha z$ Body force potentials at nodes/for element. 0, 0, 0, ϕ_4 , Xcbf, Ycbf, Zcbf
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay, Az: at nodes.
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element.
Stress/Strains		σx , σy , σz , σxy , σyz , σxz : global stresses.
		εx, εy, εz, γxy, γyz, γxz: global strains.

Residual Stresses	SSIG SSR, SSRE	 Initial stresses/strains at Gauss points (see <i>Notes</i>). σx, σy, σz, σxy, σyz, σxz: global stresses. ɛx, ɛy, ɛz, γxy, γyz, γxz: global strains. Residual stresses at nodes/for element. σx, σy, σz, σxy, σyz, σxz: global stresses.
	SSRG	Residual stresses at Gauss points (see Notes).
Target Stress/Strains	TSSIE, TSSIA	 σx, σy, σz, σxy, σyz, σxz global stresses. Target stresses/strains at nodes/for element. σx, σy, σz, σxy, σyz, σxz: global stresses. ɛx, ɛy, ɛz, γxy, γyz, γxz: global strains.
	TSSIG	Target stresses/strains at Gauss points (see <i>Notes</i>).
		$\sigma_x, \sigma_y, \sigma_z, \sigma_{xy}, \sigma_{yz}, \sigma_{xz}$: global stresses.
Temperatures	TEMP, TMPE	 εx, εy, εz, γxy, γyz, γxz: global strains. Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0
Overburden	Applicable.	
Phreatic Surface	Applicable.	
Field Loads	Not applicable.	
Temp Dependent Loads	Not applicable.	

LUSAS Output

Solver	Stress (default): σx , σy , σz , σxy , σyz , σxz : local stresses.
	Strain: Ex, Ey, Ez, Yxy, Yyz, Yxz: local strains.
	Stresses and strains are output at the Gauss and corner points of the subdivision(s) of each layer. For optional principal stress/strain output, together with the corresponding direction cosines, use Option 77.
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

The local axes for each layer are defined by the LAMINAR DIRECTIONS specified for its bottom surface. The three node set in LAMINAR DIRECTIONS define the local Cartesian set origin, the x-axis and the positive quadrant of the xy-plane respectively. The local z-axis forms an orthonormal coordinate system with x and y.

Sign Convention

□ Standard 3D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	Not applicable.
Updated	Not applicable.
Lagrangian	
Eulerian	Not applicable.
Co-rotational	For large displacements and large rotations.

Integration Schemes

Stiffness	Default.	1-point for a tetrahedral subdivision (see Notes), 3-point for a pentahedral/pyramid subdivision, 2x2 for a hexahedral/wrick subdivision
	Fine (see <i>Options</i>).	1-point for a tetrahedral subdivision (see Notes), 3x2 for a pentahedral/pyramid subdivision, 2x2 x2 for a hexahedral/wrick subdivision
Mass	Default	5-point for the whole element or (see Options) 1-point for a tetrahedral subdivision, 3x2 for a pentahedral/pyramid subdivision, 2x2 x2 for a hexahedral/wrick subdivision
	Fine (see <i>Options</i>).	11-point or (see Options) 14 -point for the whole element

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- **18** Invokes fine integration rule.
- 36 Follower loads.
- **55** Output strains as well as stresses.
- 77 Output principal stresses and direction cosines.
- 91 Formulate element mass with fine integration.
- 105 Lumped mass matrix.
- **139** Output yielded Gauss points only.

- 229 Co-rotational geometric nonlinearity.
- 266 Layer by layer computation of mass matrix.
- **394** Lamina directions supported.
- **395** Use 14-point fine integration rule for mass matrix of TH10 family (used together with 91).

Notes on Use

- 1. The element is based on the standard isoparametric approach. The variation of strains within an element may be regarded as linear.
- 2. All elements pass the **patch test**.
- 3. The LAMINAR DIRECTIONS and COMPOSITE PROPERTIES data chapters must be used with this element in conjunction with the COMPOSITE ASSIGNMENTS data chapter.
- 4. The stresses obtained from a geometric nonlinear analysis are <u>Kirchhoff</u> stresses.
- 5. If the whole tetrahedral element is embedded in a single lamina, a 4-point integration rule will be used for this tetrahedral subdivision; otherwise a 1-point rule will be used.
- 6. The mass matrix can be computed using a layer by layer integration (OPTION 266), however this should only be used when the densities of the layers vary considerably because the computation time can be greatly increased when this OPTION is specified.
- 7. Numerical integration through the thickness is performed. The integration points are located in the subdivisions of each layer. Each subdivision forms the shape of a regular 3D solid continuum element and the integration points are located accordingly within the subdivision as described above.
- 8. SSIG and SSRG loads have to be applied at the Gauss point positions for the subdivision(s) of each layer.
- 9. Layer 1 is always the bottom layer.

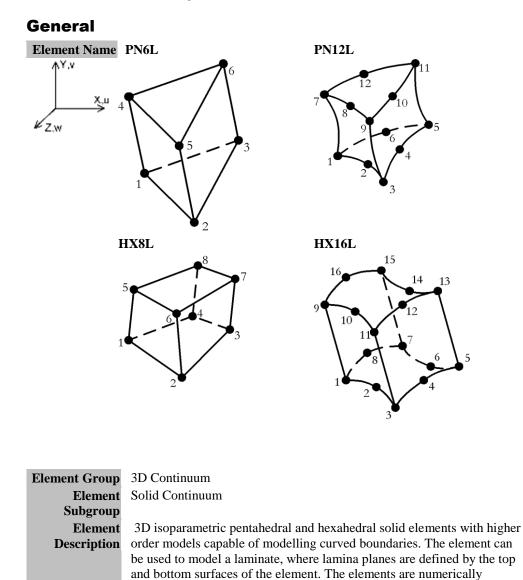
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

Recommendations on Use

- 3D solid composite elements should be used for modelling thick composite structures comprising laminae of differing material properties where the computational cost of modelling each lamina with an individual solid element would be prohibitive.
- As these elements can be arbitrarily oriented with respect to the laminate, they are particularly aimed at the use of fully automatic mesh generation of laminate geometric models imported from CAD packages.

3D Solid Continuum Composite Elements (Pentahedral and Hexahedral)



 integrated.
 Number Of Nodes
 Freedoms
 integrated.
 6 or 12 (pentahedra), 8 or 16 (hexahedra). The elements are numbered according to a right-hand screw rule in the local z-direction.
 U, V, W: at each node. **Node** X, Y, Z: at each node. **Coordinates**

Geometric Properties

See <u>Composites</u> in the Modeller Reference Manual

Material Properties

Linear	Isotropic: Orthotropic: Anisotropic: Rigidities.	MATERIAL PROPERTIES (Elastic: Isotropic) MATERIAL PROPERTIES ORTHOTROPIC SOLID (Elastic: Orthotropic Solid) MATERIAL PROPERTIES ANISOTROPIC SOLID (Elastic: Anisotropic Solid) Not applicable.
Matrix	Not applicable.	
Joint	Not applicable.	
Concrete		MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Elasto-Plastic	Stress resultant:	Not applicable.
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker- Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr- Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Modified Mohr- Coulomb:	MATERIAL PROPERTIES MODIFIED MOHR_COULOMB (Elastic: Isotropic, Plastic: Mohr-Coulomb/Tresca, non- associative Hardening with tension/compression cut-off)
	Volumetric Crushing:	Not applicable.
	Stress Potential	STRESS POTENTIAL VON_MISES, HILL, HOFFMAN

-		(Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
Creep	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO
		(Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP
	~ .	(Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE
	Eurocode	(Chinese creep model to Chinese Code of Practice)
		MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2)
	IRC	
		MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic		VISCO ELASTIC PROPERTIES
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Ko Initialisation	Not applicable	
Rubber	Not	
a . b l	applicable.	
Generic Polymer		MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)
Resin Cure Model		MATERIAL PROPERTIES NONLINEAR CURE LAYER, FIBRE_RESIN
Composite	Composite solid:	COMPOSITE PROPERTIES (Elastic: Orthotropic Solid)

Loading

Prescribed Value PDSP, TPDSP Prescribed variable. U, V, W: at each node. Concentrated loads. Px, Py, Pz: at each node. Concentrated CL Loads Element Loads Not applicable.

Distributed Loads	UDL	Not applicable.
	FLD	Face Loads. Px, Py, Pz: local face pressures at nodes.
	FLDG	Global Face Loads. σx , σy , σz , σxy , σyz , σxz at nodes
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Zcbf,
		$\Omega_{x}, \Omega_{y}, \Omega_{z}, \alpha_{x}, \alpha_{y}, \alpha_{z}$
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0,
		φ ₄ , Xcbf, Ycbf, Zcbf
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay, Az: at nodes.
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element.
Stress/Strains		σx , σy , σz , σxy , σyz , σxz : global stresses.
		εx, εy, εz, γxy, γyz, γxz: global strains.
	SSIG	Initial stresses/strains at Gauss points (see Notes).
		σx , σy , σz , σxy , σyz , σxz : global stresses.
		εx, εy, εz, γxy, γyz, γxz: global strains.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element.
		σx , σy , σz , σxy , σyz , σxz : global stresses.
	SSRG	Residual stresses at Gauss points (see Notes).
		σx , σy , σz , σxy , σyz , σxz global stresses.
Target	TSSIE, TSSIA	Target stresses/strains at nodes/for element.
Stress/Strains		σx , σy , σz , σxy , σyz , σxz : global stresses.
		εx, εy, εz, γxy, γyz, γxz: global strains.
	TSSIG	Target stresses/strains at Gauss points (see Notes).
		σx , σy , σz , σxy , σyz , σxz : global stresses.
		εx, εy, εz, γxy, γyz, γxz: global strains.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0
Overburden	Applicable.	
Phreatic Surface	11	
	Not applicable.	
Temp Dependent Loads	Not applicable.	

LUSAS Output

Solver Stress (default): σx , σy , σz , σxy , σyz , σxz : local stresses.

Strain: Ex, Ey, Ez, Yxy, Yyz, Yxz: local strains.

Stresses and strains are output at the top and bottom of each layer. For optional principal stress/strain output, together with the corresponding direction cosines, use Option 77.

Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

The local axes for each layer are defined using the convention for <u>standard area elements</u>. Local axes are computed at the top and bottom surfaces (at the Gauss points) and average values are interpolated for the mid-surface. The top and bottom faces of the element are as shown, e.g. nodes 1, 2, 3, 4 define the bottom face of HX8L. Every layer uses the same averaged values.

Sign Convention

□ Standard 3D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	Not applicable.
Updated	Not applicable.
Lagrangian	
Eulerian	Not applicable.
Co-rotational	For large displacements and large rotations.

Integration Schemes

Stiffness	Default.	1-point for each layer (PN6L), 3-point for each layer (PN12L), 2x2 for each layer (HX8L,HX16L)
	Fine (see <i>Options</i>).	3-point for each layer (PN6L), 3x3 for each layer (HX16L)
Mass	Default	3x2 for the whole element (PN6L,PN12L) or (see Options) 1-point for each layer (PN6L), 3-point for each layer (PN12L),2x2x2 for the

whole element or 2x2 for each layer (HX8L,HX16L)

Fine (see 3x2 for the whole element or 3-point for each layer (PN6L),3x3x2 for *Options*). the whole element or 3x3 for each layer (HX16L)

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- **18** Invokes fine integration rule.
- **36** Follower loads.
- 55 Output strains as well as stresses.
- 77 Output principal stresses and direction cosines.
- **105** Lumped mass matrix.
- 139 Output yielded Gauss points only.
- 229 Co-rotational geometric nonlinearity.
- **266** Layer by layer computation of mass matrix.
- **303** Exclude incompatible modes for solid composite elements.

Notes on Use

- 1. The elements are based on the standard isoparametric approach. The variation of stresses within an element may be regarded as constant for the lower order elements (corner nodes only), and linear in the plane of the quadratic element faces for the higher order elements.
- 2. All elements pass the **<u>patch test</u>**.
- The COMPOSITE GEOMETRY and COMPOSITE PROPERTIES data chapters must be used with this element in conjunction with the COMPOSITE ASSIGNMENTS data chapter.
- 4. The stresses obtained from a geometric nonlinear analysis are <u>Kirchhoff</u> stresses.
- 5. The mass matrix can be computed using a layer by layer integration (Option 266), however this should only be used when the densities of the layers vary considerably because the computation time can be greatly increased applying this option.
- 6. Numerical integration through the thickness is performed. The integration points are located at the top and bottom surface of each layer.
- 7. SSIG and SSRG loads have to be applied at the Gauss point positions for the top and bottom surfaces of each layer.

8. Layer 1 is always the bottom layer.

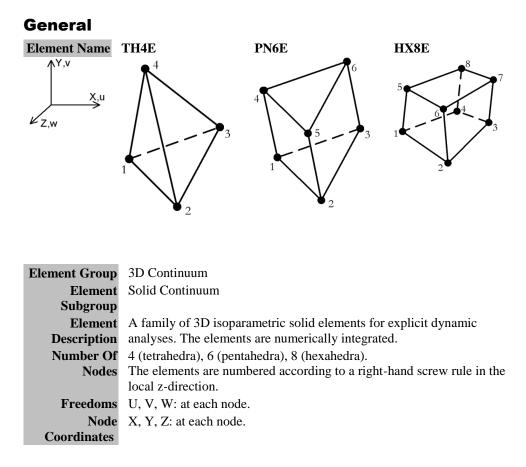
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

Recommendations on Use

- The 3D solid composite elements should be used for modelling thick composite structures comprising laminae of differing material properties where the computational cost of modelling each lamina with an individual solid element would be prohibitive.
- Because of the numerical integration through the thickness, by increasing the number of layers the accuracy of solution will increase. This can be achieved by dividing each single layer into two or three identical layers.

3D Solid Continuum Explicit Dynamics Elements



Geometric Properties

Not applicable.

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC
		SOLID (Elastic: Orthotropic Solid)
	Anisotropic:	Not applicable.
	Rigidities.	Not applicable.
Matrix	Not applicable	

Generic PolymerNot applicableCompositeNot applicable

Joint	Not applicable	
Concrete	Not applicable	
Elasto-Plastic	Stress resultant:	Not applicable.
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker- Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr- Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Modified Mohr-	MATERIAL PROPERTIES MODIFIED MOHR_COULOMB (Elastic:
	Coulomb:	Isotropic, Plastic: Mohr-Coulomb/Tresca, non- associative Hardening with tension/compression cut-off)
	Modified	MATERIAL PROPERTIES CAM_CLAY
	Cam-clay Optimised	MODIFIED (Elastic: Isotropic, Plastic) MATERIAL PROPERTIES NONLINEAR 75
	Implicit Von Mises:	(Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic)
	Volumetric Crushing:	MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam)
	Stress Potential	STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises
		Orthotropic: Hill, Hoffman)
Creep		CREEP PROPERTIES (Creep) (see <i>Notes</i>)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic		VISCO ELASTIC PROPERTIES
Shrinkage	Not applicable	
Ko Initialisation	Not applicable	
Rubber	Not applicable	
a b b	NT . 11 1.1	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, W: at each node.
Concentrated	CL	Concentrated loads. Px, Py, Pz: at each node.
Loads		
Element Loads	Not	
	applicable.	
Distributed Loads	UDL	Not applicable.
	FLD	Face Loads. Px, Py, Pz: local face pressures at nodes.
	FLDG	Not applicable
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Zcbf,
		$\Omega x, \Omega y, \Omega z, \alpha x, \alpha y, \alpha z$
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0,
		φ ₄ , Xcbf, Ycbf, Zcbf
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay, Az: at nodes.
	SSI, SSIE	Initial stresses/strains at nodes/for element. σx , σy ,
Stress/Strains		$\sigma_z, \sigma_{xy}, \sigma_{yz}, \sigma_{xz}$: global stresses. Ex, Ey, Ez,
		γ xy, γ yz, γ xz: global strains.
	SSIG	Not applicable.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. σx , σy , σz ,
		σxy, σyz, σxz: global stresses.
	SSRG	
	5510	Residual stresses at Gauss points. σx , σy , σz , σxy ,
		σ yz, σ xz: global stresses.
Target		
Stress/Strains	applicable.	
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0, 0
Overburden	Not	
	applicable.	
Phreatic Surface	Not	
Field Loads	applicable. Not	
r ieiu Loaus	applicable.	
Temp Dependent	Not	
Loads	applicable.	

LUSAS Output

 Solver Stress(default): σx, σy, σz, σxy, σyz, σxz, σe: global stresses. Strain: not available (see *Notes*). For optional principal stress output, together with the corresponding direction cosines, use Option 77.
 Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 3D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	Not applicable.
Updated	Not applicable.
Lagrangian	
Eulerian	For large displacements, large rotations and moderately large strains.
Co-rotational	For large displacements and large rotations.

Integration Schemes

Stiffness	Default.	1-point (see Notes).
	Fine.	As default.
Mass	Default.	1-point (see Notes).
	Fine.	As default.

Mass Modelling

□ Lumped mass only (see *Notes*).

Options

77 Output principal stresses and direction cosines.

- 105 Lumped mass matrix.
- **139** Output yielded Gauss points only.

Notes on Use

- 1. The elements are based on the standard isoparametric approach. Stresses within an element may be regarded as constant.
- 2. When using tabular input for ORTHOTROPIC SOLID the value of nset used is that defined in the first line of the property table.
- 3. The system parameter HGVISC is used to restrict element mechanisms due to underintegration. The default value is usually sufficient.
- 4. The bulk viscosity coefficients are used to restrict numerical oscillations due to the traversal of stress waves. The default bulk viscosity coefficients (BULKLF and BULKQF) may be altered as SYSTEM parameters.
- 5. These elements must be used with a dynamic central difference scheme and a lumped mass matrix.
- 6. These element are Not applicable. for static or eigenvalue analyses.
- 7. Automatic time step length calculations are implemented.
- 8. As element geometry is always updated in an explicit dynamic analysis, the solution is nonlinear. When using explicit dynamic elements NONLINEAR CONTROL must be specified.
- 9. If CREEP PROPERTIES are defined, explicit time integration must be specified in VISCOUS CONTROL.
- 10. Strains are computed incrementally and therefore total strains are not available for output.
- 11. Non-conservative loading is invoked when the FLD loading facility is applied.
- 12. Rayleigh damping coefficients are not supported by these elements.
- 13. Constraint equations are not available for use with these elements.

Restrictions

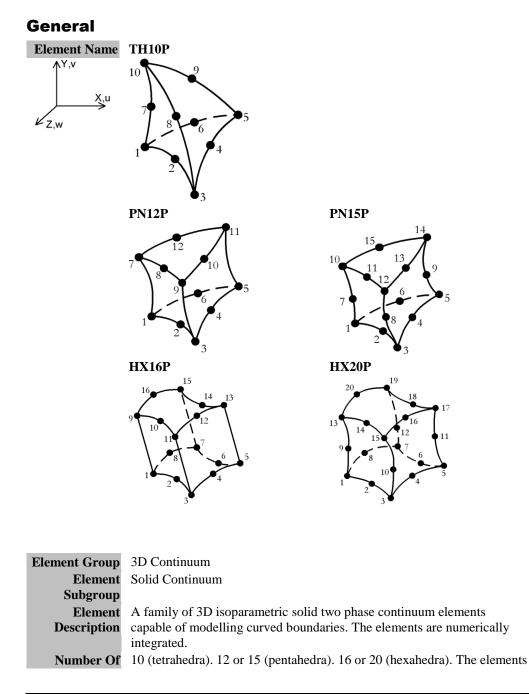
□ Avoid excessive aspect ratio

Recommendations on Use

• Explicit dynamics elements may be used to define surface boundaries which will be active in a slideline analysis.

• The 3D explicit dynamics elements should be used if the stress field is fully 3D, i.e. it cannot be approximated with any of the 2D elements, e.g. a non-axisymmetric pressure vessel.

3D Solid Two Phase Continuum Elements



Nodesare numbered according to a right-hand screw rule in the local z-direction.FreedomsU, V, W, P: at corner nodes, U, V, W at mid-side nodes.NodeX, Y, Z: at each node.CoordinatesImage: Coordinates of the local destruction of the local des

Geometric Properties

Not applicable.

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC SOLID (Elastic: Orthotropic Solid)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC SOLID (Elastic: Anisotropic Solid)
	Rigidities.	Not applicable.
Matrix	Not	
	applicable.	
Joint		
	applicable.	
Concrete		MATERIAL PROPERTIES NONLINEAR 109
		(Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Elasto-Plastic	Stress	Not applicable.
	resultant:	
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61
		(Elastic: Isotropic, Plastic: Tresca, Hardening:
		Isotropic Hardening Gradient, Isotropic Plastic
	Drucker-	Strain or Isotropic Total Strain) MATERIAL PROPERTIES NONLINEAR 64
	Prager:	(Elastic: Isotropic, Plastic: Drucker-Prager,
	Tidget.	Hardening: Granular)
	Mohr-	MATERIAL PROPERTIES NONLINEAR 65
	Coulomb:	(Elastic: Isotropic, Plastic: Mohr-Coulomb,
		Hardening: Granular with Dilation)
	Modified	MATERIAL PROPERTIES
	Mohr-	MODIFIED MOHR_COULOMB (Elastic:
	Coulomb:	Isotropic, Plastic: Mohr-Coulomb/Tresca, non- associative Hardening with tension/compression cut-off)
	Modified	MATERIAL PROPERTIES CAM_CLAY

	Cam-clay	MODIFIED (Elastic: Isotropic, Plastic)
	Optimised Implicit Von Mises:	MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic)
	Volumetric Crushing: Stress Potential:	MATERIAL PROPERTIES NONLINEAR 81 (Volumetric Crushing or Crushable Foam) STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises
		Orthotropic: Hill, Hoffman)
Creep		CREEP PROPERTIES (Creep)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic		VISCO ELASTIC PROPERTIES
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Ko Initialisation Elasto- Plastic Interface	Applicable	MATERIAL PROPERTIES NONLINEAR 26
Rubber	Not applicable.	
Generic Polymer	Isotropic	MATERIAL PROPERTIES NONLINEAR 89 (Generic Polymer Model)
Composite	Not applicable	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, W, P: at corner nodes, U, V, W at mid-side nodes.	
Concentrated	CL	Concentrated loads. Px, Py, Pz, Q: at corner nodes,	
Loads		.Px, Py, Pz at mid-side nodes.	
Element Loads	Not applicable.		
Distributed Loads	UDL	Not applicable.	
	FLD	Face Loads . Px, Py, Pz, Q: face pressures/flux per unit area at corner nodes relative to local face axes. Px, Py, Pz: face pressures at midside nodes relative to local face axes.	
	FLDG	Global Face Loads. σx, σy, σz, σxy, σyz, σxz at nodes	

Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Zcbf, Ωx , Ωy , Ωz , αx , αy , αz , $g x$, $g y$, $g z$. (See notes on use)
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0, φ4, Xcbf, Ycbf, Zcbf, gx, gy, gz. (See notes on use)
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay, Az: at nodes.
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element. σx , σy ,
Stress/Strains		σz, $σxy$, $σyz$, $σxz$, $σp$ global stresses. $εx$, $εy$, $εz$, γxy, $γyz$, $γxz$: global strains.
	SSIG	Initial stresses/strains at Gauss points σx , σy , σz ,
		σ xy, σ yz, σ xz, σ p: global stresses. Ex, Ey, Ez,
		γxy, γyz, γxz: global strains.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. σx , σy , σz , σxy , σyz , σxz , σp : global stresses.
	SSRG	Residual stresses at Gauss points. σx , σy , σz , σxy ,
Target Stress/Strains	TSSIE, TSSIA	 σyz, σxz, σp global stresses. Target stresses/strains at nodes/for element. σx, σy, σz, σxy, σyz, σxz, σp global stresses. εx, εy, εz, γxy, γyz, γxz: global strains.
	TSSIG	Target stresses/strains at Gauss points σx , σy , σz , σxy , σyz , σxz , σp : global stresses. εx , εy , εz , γxy , γyz , γxz : global strains.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0, 0
Overburden	Applicable.	
Phreatic Surface	Applicable.	
Field Loads	Not applicable.	
Temp Dependent Loads	Not applicable.	

LUSAS Output

Solver Stress (default): σ_x , σ_y , σ_z , σ_{xy} , σ_{yz} , σ_{xz} , σ_p , σ_e : global stresses.

Strain: εx , εy , εz , γxy , γyz , γxz , εv , εe : global strains. For optional principal stress/strain output, together with the corresponding direction cosines, use Option 77.

Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard 3D continuum element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and large rotations.		
Updated	For large displacements and large rotations.		
Lagrangian			
Eulerian	For large displacements, large rotations and moderately large strains.		
Co-rotational	For large displacements and large rotations.		

Integration Schemes

Stiffness	Default.	4-point (TH10P), 3x2 (PN12P, PN15P), 2x2x2 (HX16P, HX20P)
	Fine (see <i>Options</i>).	5-point (TH10P), 3x3x2 (HX16P), 3x3x3 (HX20P)
	Coarse (see <i>Options</i>)	13-point (HX20P), 14-point (HX20P)
Mass	Default.	4-point (TH10P), 3x2 (PN12P, PN15P), 2x2x2 (HX16P, HX20P)
	Fine (see <i>Options</i>).	11-point (TH10P),14-point (TH10P), 3x3x2 (HX16P), 3x3x3 (HX20P)
	Coarse (see <i>Options</i>)	13-point (HX20P), 14-point (HX20P)

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- **18** Invokes fine integration rule.
- **36** Follower loads
- 54 Updated Lagrangian geometric nonlinearity
- 55 Output strains as well as stresses.
- 77 Output principal stresses and direction cosines.
- 87 Total Lagrangian geometric nonlinearity.
- **91** Invoke finer integration of the mass matrix.
- **102** Switch off load correction stiffness due to centripetal acceleration.
- 105 Lumped mass matrix.
- **139** Output yielded Gauss points only.
- **155** Use 14-point integration rule for HX20P.
- **156** Use 13-point integration rule for HX20P.
- 167 Eulerian geometric nonlinearity.
- 229 Co-rotational geometric nonlinearity.
- **398** For HX20P and HX16P with fine integration use all integration points for stress extrapolation.

Notes on Use

- 1. Two phase material parameters must be used with these elements for undrained and consolidation analysis.
- 2. The elements are based on the standard isoparametric approach. The variation of stresses and pore pressures within an element may be regarded linear, except for elements PN12P and HX16P where the stress is constant in the z direction.
- 3. All elements pass the **<u>patch test</u>**.
- 4. When using table input format for temperature dependent ORTHOTROPIC SOLID or ANISOTROPIC SOLID material properties, the value of nset used is that defined in the first line of the property table.
- 5. Non-conservative loading is available with these elements when using Updated Lagrangian, Eulerian or co-rotational (with OPTION 36) geometric nonlinear formulations together with the FLD loading facility.
- 6. The global components of gravity acting on the fluid phase are defined by gx and gy under CBF and BF loading.

Restrictions

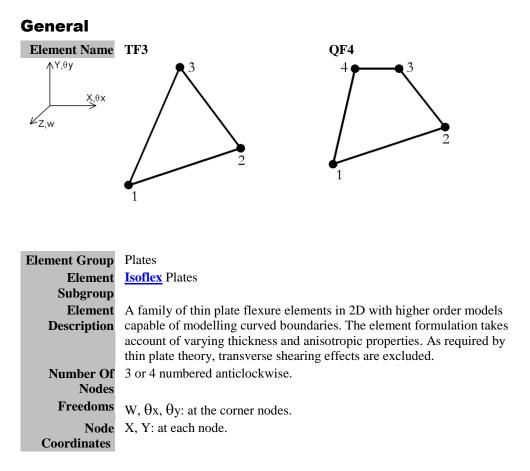
- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

Recommendations on Use

- The 3D solid two phase elements should be used if the stress field is fully 3D, i.e. it cannot be approximated with any of the 2D elements, e.g. a non-axisymmetric pressure vessel.
- For linear materials, the 20-noded element with a 2*2*2 Gauss rule is usually the most effective element, as this under-integration of the stiffness matrix prevents locking, i.e. over-stiff solutions will occur if the elements are used with a 3*3*3 Gauss integration rule to model structures subjected to bending. However, the element possesses six zero energy modes. Therefore, a careful examination of the solution should be performed to check for spurious stress oscillations and peculiarities in the deformed configuration. Either the 14-point or 3*3*3 Gauss rules should be used for materially nonlinear problems or materially linear problems that exhibit spurious deformations.
- In general, PN15P and HX20P give the best performance; TH10P is less accurate and needs to be used with a finer mesh. HX16P and PN12P should only be used to overcome connectivity problems when meshing.

Chapter 5: Plate Elements.

2D Isoflex Thin Plate Flexure Elements



Geometric Properties

t1 ... tn Thickness at each node.

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC
		(Elastic: Orthotropic Plane Stress)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC 3
	-	(Elastic: Anisotropic Thin Plate)

Rigidities.	RIGII
Not applicable	
	Not applicable Not applicable Not applicable Not applicable Not applicable Not applicable Not applicable Not applicable Not applicable Not applicable

RIGIDITIES 3 (Rigidities: Membrane/Thin Plate)

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. W, θx , θy : at the corner nodes.
Concentrated Loads	CL	Concentrated loads. Pz, Mx, My: at corner nodes.
Element Loads	Not applicable.	
Distributed Loads	UDL	Uniformly distributed loads. Wz: normal pressure for element (global).
	FLD, FLDG	Not applicable.
Body Forces	CBF	Constant body forces for element. Zcbf
	BFP, BFPE	Body force potentials at nodes/for element. $\phi \imath, Zcbf$
Velocities	VELO	Velocities. Vz: at nodes.
Accelerations	ACCE	Accelerations. Az: at nodes.
Initial Stress/Strains	SSI, SSIE	Initial stresses/strains at nodes/for element. Mx, My, Mxy: moments/unit width (global).
		ψx, ψy, ψxy: flexural strains (global).
	SSIG	Not applicable.
Residual Stresses	Not applicable.	
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. Mx, My, Mxy: moments/unit width (global).
		ψx, ψy, ψxy: flexural strains (global).
	TSSIG	Not applicable.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. 0, 0, 0, dT/dz, 0, 0, 0, dTo/dz

Not
applicable.
Not
applicable.
Not
applicable.
Not
applicable.

LUSAS Output

Solver	Stress resultant: Mx, My, Mxy: moments/unit width (global).
	Strain: ψx, ψy, ψxy: flexural strains (global).
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard plate element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Stiffness	Default. Fine.	3-point (TF3), 2x2 (QF4). As default.
Mass	Default. Fine.	3-point (TF3), 2x2 (QF4). As default.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- **18** Invokes fine integration rule for element.
- 55 Output strains as well as stresses.
- 143 Output shear forces for low order thin plate bending elements.
- 170 Suppress transfer of shape function arrays to disk.

Notes on Use

- 1. The element formulations are based on an Kirchhoff hypothesis for thin plates.
- 2. The variation of moments within the elements can be regarded as linear.
- 3. The elements pass the <u>patch test</u> for convergence for mixed triangular and quadrilateral element geometry.
- 4. The averaged nodal values produced with ELEMENT OUTPUT do not include the thin *isoflex* plate shear stresses if Option 143 is invoked.
- 5. When Option 143 is invoked shear stresses are only computed for the low order isoflex elements (QF4,TF3).

Restrictions

□ Avoid excessive aspect ratio

Recommendations on Use

- This element may be used to analyse any 2D plate type structures where transverse shear effects do not influence the solution, e.g. thin cantilever plates.
- The thick plate elements QTF8 and TTF6 are recommended for thick plates where transverse shear strains are no longer negligible.

The following element combinations should be used for ribbed plates;

Ribs with small or no eccentricity

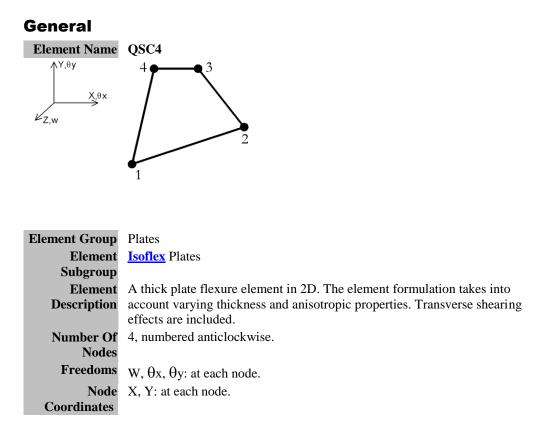
- □ QSI4/TS3 elements with BMI21 elements,
- □ QTS4/TTS3 elements with BMI21 elements.

Ribs with large eccentricity

- □ QSL8/TSL6 elements with BSL3/BSL4/BXL4 elements.
- □ QTS4/TTS3 elements with BMI21 elements.

The through thickness integration is performed explicitly.

2D Isoflex Thick Plate Flexure Element



Geometric Properties

t1... tn At each node.

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC THICK (Elastic: Orthotropic Thick)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC 5
		(Elastic: Anisotropic Thick Plate)
	Rigidities:	RIGIDITIES 5 (Rigidities: Thick Plate)
Matrix	Not applicabl	
Joint	Not applicable	

Concrete	Not applicable
Elasto-Plastic	Not applicable
Creep	Not applicable.
Damage	Not applicable
Viscoelastic	Not applicable
Shrinkage	Not applicable
Rubber	Not applicable
Generic Polymer	Not applicable
Composite	Not applicable

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. W, θx , θy : at nodes.
Concentrated Loads	CL	Concentrated loads. Pz, Mx, My: at nodes.
Element Loads	Not applicable.	
Distributed Loads	UDL	Uniformly distributed loads. Wz: normal pressure for element (global).
	FLD, FLDG	Not applicable.
Body Forces	CBF	Constant body forces for element. Zcbf
	BFP, BFPE	Body force potentials at nodes/for element. ϕ_1 , Zcbf
Velocities	VELO	Velocities. Vz: at nodes.
Accelerations	ACCE	Accelerations. Az: at nodes.
Initial Stress/Strains	SSI, SSIE	Initial stresses/strains at nodes/for element. Mx, My, Mxy: moments/unit width (global).
		ψx, ψy, ψxy: flexural strains (global).
	SSIG	Not applicable.
Residual Stresses	Not applicable.	
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. Mx, My, Mxy: moments/unit width (global).
		ψx, ψy, ψxy: flexural strains (global).
	TSSIG	Not applicable.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. 0, 0, 0, dT/dz, 0, 0, 0, dTo/dz
Overburden	Not applicable.	
Phreatic Surface	Not	

applicable. Field Loads Not applicable. Temp Dependent Not Loads applicable.

LUSAS Output

Solver Stress resultant: Mx, My, Mxy, Sx, Sy: moments, shear forces/unit width (global)
 Strain: ψx, ψy, ψxy, γxz, γyz: flexural, shear strains (global).
 Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard plate element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Stiffness	Default.	2x2
	Fine.	As default.
Mass	Default.	2x2
	Fine.	As default.

Mass Modelling

□ Consistent mass (default).

□ Lumped mass.

Options

- 55 Output strains as well as stresses.
- 105 Lumped mass matrix.
- 170 Suppress transfer of shape function arrays to disk.

Notes on Use

- 1. The element formulation involves imposing an assumed bi-linear shear strain field on the isoflex thin plate element QF4.
- 2. Though this element cannot model nonlinear behaviour, it can be mixed with other elements in a nonlinear analysis.
- 3. The element passes the <u>patch test</u> for convergence with rectangular and parallelogram element geometry.
- 4. The QF4,QF8,TF3,TF8 elements are usually more effective elements for thin plate analyses.
- 5. The QTF8 and TTF6 elements are usually more effective for thick plate analyses, and in such cases should be preferred to QSC4.
- 6. 3D solid elements should be used if the normal stress in the transverse direction is not insignificant in comparison with the in-plane stresses.
- 7. The following element combinations should be used for ribbed plates

Ribs with small or no eccentricity

- QSI4/TS3 elements with BMI21 elements,
- QTS4/TTS3 elements with BMI21 elements.

Ribs with large eccentricity

- QSL8/TSL6 elements with BSL3/BSL4/BXL4 elements,
- QTS4/TTS3 elements with BMI21 elements.
- 8. The through-thickness integration is performed explicitly.

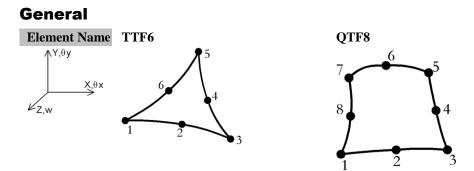
Restrictions

□ Avoid excessive aspect ratio

Recommendations on Use

This element may be used to analyse any 2D plate type structures where transverse shear effects influence the solution, e.g. perforated thick plates.

2D Mindlin Thick Plate Flexure Element



Element Group	Plates
Element	Mindlin Plates
Subgroup	
Element	A family of thick plate flexure elements based on a Mindlin plate
Description	formulation. The elements can accommodate curved boundaries and varying thicknesses. Transverse shear deformations are included.
Number Of	6 or 8, numbered anticlockwise.
Nodes	
Freedoms	W, θx , θy : at each node.
Node	X, Y: at each node.
Coordinates	

Geometric Properties

t1... tn Thickness at each node.

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC
		THICK (Elastic: Orthotropic Thick)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC 5
		(Elastic: Anisotropic Thick Plate)
	Rigidities.	RIGIDITIES 5 (Rigidities: Thick Plate)
Matrix	Not applicable	
Joint	Not applicable	

Concrete	Not applicable
Elasto-Plastic	Not applicable
Creep	Not applicable
Damage	Not applicable
Viscoelastic	Not applicable
Shrinkage	Not applicable
Rubber	Not applicable
Generic Polymer	Not applicable
Composite	Not applicable

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. W, θx , θy : at nodes.
Concentrated Loads	CL	Concentrated loads. Pz, Mx, My: at nodes.
Element Loads	Not applicable.	
Distributed Loads	UDL	Uniformly distributed loads. Wz: normal pressure for element (global).
	FLD, FLDG	Not applicable.
Body Forces	CBF	Constant body forces for element. Zcbf
	BFP, BFPE	Body force potentials at nodes/for element. ϕ_1 , Zcbf
Velocities	VELO	Velocities. Vz: at nodes.
Accelerations	ACCE	Accelerations. Az: at nodes.
	SSI, SSIE	Initial stresses/strains at nodes/for element.
Stress/Strains		Mx, My, Mxy, Sx, Sy: moments, shear forces/unit width (global).
		Ψx, Ψy, Ψxy, γxz, γyz: flexural, shear strains /unit width (global).
	SSIG	Not applicable.
Residual Stresses	Not applicable.	
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. Mx, My, Mxy, Sx, Sy: moments, shear forces/unit width (global).
		Ψx, Ψy, Ψxy, γxz, γyz: flexural, shear strains /unit width (global).
	TSSIG	Not applicable.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. 0, 0, 0, dT/dz, 0, 0, 0, dTo/dz

Overburden	Not
	applicable.
Phreatic Surface	Not
	applicable.
Field Loads	Not
	applicable.
Temp Dependent	Not
Loads	applicable.

Output

Solver	Stress resultant: Mx, My, Mxy, Sx, Sy: moments, shear forces/unit width (global).
	Strain: ψx , ψy , ψxy , γxz , γyz : flexural, shear strains /unit width (global).
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard plate element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Stiffness	Default.	3-point (TTF6), 2x2 (QTF8)
	Fine (see Options).	3x3 (QTF8).
Mass	Default.	3-point (TTF6), 2x2 (QTF8)
	Fine (see Options).	3x3 (QTF8).

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- **18** Invokes fine integration rule for element.
- 55 Output strains as well as stresses.
- 105 Lumped mass matrix.
- **170** Suppress transfer of shape function arrays to disk.

Notes on Use

- 1. The element formulations are based on an isoparametric approach. The variation of moments and shears within the element may be regarded as linear.
- 2. Though this element cannot model nonlinear behaviour, it can be mixed with other elements in a nonlinear analysis.
- 3. The elements pass the <u>patch test</u> for convergence with triangular and parallelogram element geometry.
- 4. These elements are usually more effective than the QSC4 thick shell element (section 7.6.2).
- 5. The elements tend to lock as the plate thickness approaches the thin plate limit since shear strain energy dominates the element stiffness. Therefore, a thin plate or shell element should be used when the depth/span ratio exceeds 1/50.
- 6. 3D solid elements should be used if the normal stress in the transverse direction is not insignificant in comparison with the in-plane stresses.
- 7. The following element combinations should be used for ribbed plates

Ribs with small or no eccentricity

- QSI4/TS3 elements with BMI21 elements,
- QTS4/TTS3 elements with BMI21 elements.

Ribs with large eccentricity

- QSL8/TSL6 elements with BSL3/BSL4/BXL4 elements,
- QTS4/TTS3 elements with BMI21 elements.

- 8. The QTF8 element with 2*2 Gauss quadrature is generally more effective than the 3*3 rule. The 2*2 rule does, however, exhibit one zero energy mode which can be eliminated using option 18.
- 9. The through-thickness integration is performed explicitly.

Restrictions

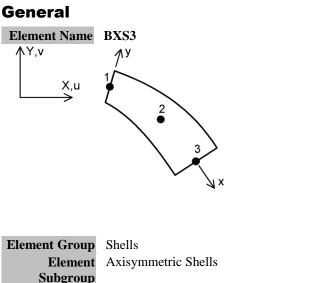
- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

Recommendations on Use

These elements may be used to analyse any 2D plate type structures where transverse shear effects influence the solution, e.g. perforated thick plates.

Chapter 6 : Shell Elements.

2D Axisymmetric Thin Shell Element



r	
Element	Axisymmetric Shells
Subgroup	
Element	A parabolically curved axisymmetric thin shell element in 2D in which
Description	shear deformations are excluded. The geometric properties may vary
	along the length of the element.
Number Of	3.
Nodes	
End Releases	
Freedoms	U, V, θ z: at end nodes.
	dU: (relative local in-plane displacement) at the mid-length node.
Node	X, Y: at each node.
Coordinates	

Geometric Properties

t1, t2, t3 Thickness at each node.

Material Properties

Linear Isotropic: Orthotropic: MATERIAL PROPERTIES (Elastic: Isotropic) MATERIAL PROPERTIES ORTHOTROPIC (Elastic: Orthotropic Plane Stress) MATERIAL PROPERTIES ORTHOTROPIC SOLID (Elastic: Orthotropic Thick)

	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC 2 (Not supported in LUSAS Modeller)
Joint	Rigidities: Not applicable. Not applicable. Not applicable.	Not applicable.
Elasto-Plastic	Stress resultant:	MATERIAL PROPERTIES NONLINEAR 29 (Elastic: Isotropic, Plastic: Resultant) (ifcode not required)
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker- Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr- Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Optimised Implicit Von Mises:	MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic)
	Volumetric Crushing:	Not applicable.
	Stress Potential	STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
Creep		CREEP PROPERTIES (Creep)
	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO Code of
	CEB-FIP	Practice)
	CED-FIF	MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP (Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE

		(Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC Code of Practice)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic	Not applicable.	
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Rubber	Not applicable.	
Generic Polymer	Not applicable	
Composite	Not applicable.	

Loading

•		
Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, θ z: at end nodes. dU: at the mid-length node.
Concentrated Loads	CL	Concentrated loads. Px, Py, Mx: point loads, moments/unit length/radian at end nodes (global). DPx: point load/unit length/radian at mid-length node (local).
Element Loads	ELDS	Element loads LTYPE, S1, Px, Py, Mx LTYPE=11: point loads and moments in local directions. LTYPE=12: point loads and moments in global directions. LTYPE, 0, Wx, Wy, Mx LTYPE=21: uniformly distributed loads in local directions. LTYPE=22: uniformly distributed loads in global directions. LTYPE=23: uniformly distributed projected loads in global directions LTYPE=31: distributed loads in local directions. LTYPE=31: distributed loads in local directions. LTYPE=33: distributed loads in global directions. LTYPE=33: distributed projected loads in global directions LTYPE=34: trapezoidal loads in local directions. LTYPE=41: trapezoidal loads in global directions. LTYPE=42: trapezoidal loads in global directions.

		LTYPE=43: trapezoidal projected loads in global directions
Distributed Loads	UDL	Uniformly distributed loads. Wx, Wy: forces/unit length/radian in local x, y directions for element.
	FLD FLDG	Face Loads . Px, Py: local face pressures at nodes. Not applicable.
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Ωx , Ωy , Ωz , αz
	BFP, BFPE	Body force potentials at nodes/for element. φ1, φ2, 0, 0, Xcbf, Ycbf
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Accelerations. Ax, Ay: at nodes.
Initial Stress/Strains	SSI, SSIE	Initial stresses/strains at nodes/for element. Resultants (for linear material models without cross section integration and material model 29). Nx, Nθ, Mx, Mθ, O: axial and circumferential
		forces, moments/unit width. Ex, E θ , ψ x, $\psi = \theta$, 0, axial and circumferential strains (all models).
	SSIG	 Initial stresses/strains at Gauss points. (1) Resultants (for linear material models without cross section integration and material model 29). Nx, Nθ, Mx, Mθ,O : axial and circumferential
		forces, moments/unit width. εx , $\varepsilon \theta$, ψx , $\psi \theta$, 0: axial and circumferential strains (all models). (2) Components (for linear material models with cross section integration and all nonlinear material
		models except 29). 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, (σ x,
		σ_{θ} , ϵ_x , ϵ_{θ}) Bracketed terms repeated for each fibre integration point.
Residual Stresses	SSR, SSRE	Not applicable.
	SSRG	 Residual stresses at Gauss points. (1) Resultants (model 29). Nx, Nθ, Mx, Mθ, 0 (2) Components (all models except 29) 0, 0, 0, 0,
		$0, 0, 0, 0, 0, 0, (\sigma x, \sigma \theta)$ Bracketed terms repeated for each fibre integration point.
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. Resultants (for linear material models without cross section integration and material model 29). Nx, Nθ, Mx, Mθ, O: axial and circumferential
		forces, moments/unit width. Ex, ε_{θ} , ψx , ψ_{θ} , 0, axial and circumferential strains (all models).

	TSSIG	Target stresses/strains at Gauss points. (1) Resultants (for linear material models without cross section integration and material model 29). Nx, Nθ, Mx, Mθ,0 : axial and circumferential
		 forces, moments/unit width. εx, εθ, ψx, ψθ, 0: axial and circumferential strains (all models). (2) Components (for linear material models with cross section integration and all nonlinear material
		models except 29). 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, (σ x,
		σ_{θ} , ϵ_{x} , ϵ_{θ}) Bracketed terms repeated for each fibre integration point.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, dT/dy, 0, To, 0, dTo/dy, 0: in local directions.
Overburden	Not applicable.	
Phreatic Surface	Applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not applicable.	
Loads		

LUSAS Output

Solver	Force. Nx, N $_{\theta}$, Mx, M $_{\theta}$: axial and circumferential forces, moments/unit width in local directions.
	Strain. $\mathcal{E}x$, \mathcal{E}_{θ} , γx , γ_{θ} : axial and circumferential strains.
	Layer stress and strain output is also available when using the nonlinear continuum material models.
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

The local x-axis lies along the line of the element in the direction in which the nodes are numbered. The local y and z-axes form a right-hand set with the local x-axis such that the y-axis lies in the global XY-plane with the z-axis parallel to the global Z-axis.

Sign Convention

□ Standard shell element. Axial and circumferential moments are positive for tension on element top fibre (the top fibre lies on the positive local y side of the element).

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements, rotations up to 1 radian, and small strains.
Updated	For large displacements, rotation increments up to 1 radian and small
Lagrangian	strains.
Eulerian	Not applicable.
Co-rotational	Not applicable.

Integration Schemes

Stiffness	Default.	2-point.
	Fine (see Options).	3-point.
Mass	Default.	2-point.
	Fine (see Options).	3-point.

Mass Modelling

□ Consistent mass (default).

Lumped mass.

Options

- **18** Invokes fine integration rule for element
- 47 X-axis taken as axis of symmetry
- 54 Updated Lagrangian geometric nonlinearity.
- 55 Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity
- 105 Lumped mass matrix.
- 157 Material model 29 (non cross-section elements), see *Notes*.
- 170 Suppress transfer of shape function arrays to disk.

Notes on Use

- 1. The element formulation is based on a constrained super-parametric approach.
- 2. The variation of axial force and moment along the length of the element is linear. The variation of displacements is cubic in the local y-direction, and quadratic in the local x direction.
- 3. Temperature dependent properties cannot be used with material model 29.

4. The through-thickness integration is performed explicitly for linear and stress resultant plasticity models and with a 5-point <u>Newton-Cotes</u> rule for all other material models.

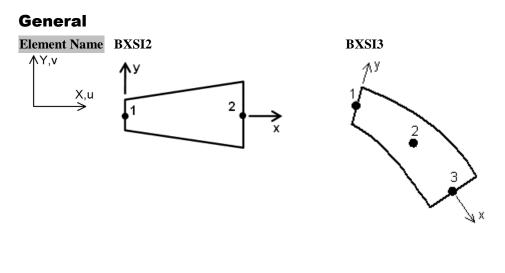
Restrictions

- Ensure mid-side node centrality
- □ Avoid excessive element curvature

Recommendations on Use

The element can be used for analysing shell structures which are axisymmetric, e.g. pressure vessels or pipes.

2D Axisymmetric Thick Shell Elements



Element Group	Shells
Element	Axisymmetric Shells
Subgroup	
Element	Straight and curved isoparametric degenerate thick axisymmetric shell
Description	elements in 2D for which shearing deformations are included. The
	element thickness may vary along the length.
Number Of	2 (BXSI2), 3 (BXSI3)
Nodes	
End Releases	
Freedoms	U, V, θz : at end nodes.
Node	X, Y: at each node.
Coordinates	

Geometric Properties

t1, t2, t3 Thickness at each node.

Material Properties

Linear Isotropic: Orthotropic: MATERIAL PROPERTIES (Elastic: Isotropic) MATERIAL PROPERTIES ORTHOTROPIC (Elastic: Orthotropic Plane Stress) MATERIAL PROPERTIES ORTHOTROPIC

Joint	Anisotropic: Rigidities: Not applicable. Not applicable. Not applicable.	SOLID (Elastic: Orthotropic Thick) MATERIAL PROPERTIES ANISOTROPIC 2 (Not supported in LUSAS Modeller) Not applicable.
Elasto-Plastic	Stress	Not applicable.
	resultant: Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker- Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr- Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Optimised Implicit Von Mises: Volumetric	MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic) Not applicable.
	Crushing: Stress Potential	STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman) CREEP PROPERTIES (Creep)
Сгеер	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP (Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE

		(Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of Practice)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic	Not applicable.	
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Rubber	Not applicable.	
Generic Polymer	Not applicable	

Loading

Composite Not applicable.

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, θ z: at end nodes.
Concentrated Loads	CL	Concentrated loads. Px, Py, Mx at nodes.
Element Loads	ELDS	Element loads on nodal line LTYPE, S1, Px, Py, Mz LTYPE=11: point loads and moments in local directions. LTYPE=12: point loads and moments in global directions. LTYPE, 0, Wx, Wy, Mz LTYPE=21: uniformly distributed loads in local directions. LTYPE=22: uniformly distributed loads in global directions. LTYPE=23: uniformly distributed projected loads in global directions LTYPE, S1, Wx1, Wy1, Mz1, S2, Wx2, Wy2, Mz2 LTYPE=31: distributed loads in global directions. LTYPE=32: distributed loads in global directions. LTYPE=33: distributed loads in global directions. LTYPE=31: distributed loads in global directions. LTYPE=31: distributed loads in global directions. LTYPE=31: distributed projected loads in global directions LTYPE=41: trapezoidal loads in local directions. LTYPE=42: trapezoidal loads in global directions. LTYPE=43: trapezoidal projected loads in global directions

Distributed Loads	UDL	Uniformly distributed loads. Wx, Wy: forces/unit length/radian in local x, y directions for element.
	FLD	Face Loads. Px, Py: local face pressures at nodes.
	FLDG	Not applicable.
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Ωx ,
		$\Omega_y, \Omega_z, \alpha_z$
	BFP, BFPE	Body force potentials at nodes/for element. φ1, φ2, 0, 0, Xcbf, Ycbf
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Accelerations. Ax, Ay: at nodes.
	SSI, SSIE	Initial stresses/strains at nodes/for element.
Stress/Strains		Components: 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, (σ x, σ xy,
		σ_z , ϵ_x , ϵ_{xy} , ϵ_z) Bracketed terms repeated for each fibre integration point
	SSIG	Initial stresses/strains at Gauss points. These stresses/strains are specified in the same manner as SSI and SSIE.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element. Components:
		$0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, (\sigma x, \sigma xy, \sigma z)$ Bracketed terms repeated for each fibre integration point.
	SSRG	Residual stresses at Gauss points for element.
		Components: $0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, (\sigma x, \sigma xy, $
		σ z) Bracketed terms repeated for each fibre integration point.
Target	TSSIE, TSSIA	Target stresses/strains at nodes/for element.
Stress/Strains		Components: $0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, (\sigma x, \sigma xy, $
		σ z) Bracketed terms repeated for each fibre integration point.
	TSSIG	Target stresses/strains at Gauss points. These stresses/strains are specified in the same manner as TSSIE and TSSIA.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, dT/dy, 0, To, 0, dTo/dy, 0: in local directions.
Overburden	Not applicable.	
Phreatic Surface		The fluid pressure is applied in the –y direction of the element y axis.
Field Loads	Not	-
	applicable.	
Temp Dependent	Not	

Loads applicable.

LUSAS Output

Solver	Force. Nx, Ne, Mx, Me, Sxy: axial and hoop forces, moments/uniwidth in local directions, shear force		
	Strain. Ex, \mathcal{E}_{\Box} , γx , $\Box \theta$, $\mathcal{E}xy$ axial, hoop, flexural and shear strains.		
	Continuum stresses: σx , σxy , $\sigma \theta$ in local directions.		
	Strain: ε_x , ε_x , ε_{\Box} : Axial, shear and hoop strains in local directions.		
Modeller	See <u>Results Tables (Appendix K)</u> .		

Local Axes

The local x-axis lies along the line of the element in the direction in which the nodes are numbered. The local y and z-axes form a right-hand set with the local x-axis such that the y-axis lies in the global XY-plane with the z-axis parallel to the global Z-axis.

Sign Convention

□ Standard shell element. Axial and circumferential moments are positive for tension on element top fibre (the top fibre lies on the positive local y side of the element).

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements, rotations up to 1 radian, and small strains.
Updated	Not applicable.
Lagrangian	
Eulerian	Not applicable.
Co-rotational	Not applicable.

Integration Schemes

Stiffness	Default.	1-point (BXSI2), 2-point (BXSI3).
	Fine (see Options).	Same as default.
Mass	Default.	2-point (BXSI2), 3-point (BXSI3).

Fine (see *Options*). Same as default.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- 18 Invokes fine integration rule for element
- **55** Output strains as well as stresses.
- 87 Total Lagrangian geometric nonlinearity
- 102 Switch off load correction stiffness matrix due to centripetal acceleration
- 105 Lumped mass matrix.
- 134 Gauss to Newton-Cotes in plane (in the local x direction) integration for elements.
- 139 Output yielded integration points only.

Notes on Use

- 1. The element is formulated from the degenerate continuum concept, i.e. enforcing directly the modified Timoshenko hypothesis for thick beams to the continuum theory. Plane cross-sections initially normal to the x axis remain plane and undistorted (the shape of the cross-section remains unchanged) under deformation, but do not necessarily remain normal to the x axis. Shearing deformations are included.
- 2. The axial force, hoop force, shear force and moments are constant in BXSI2 and vary linearly along the length of the beam in BXSI3.
- 3. OPTION 36 is only applicable for use with element load types FLD, ELDS, UDL and phreatic surface pressure. Specifying this option makes these element loads follow the element geometry as the analysis progresses.

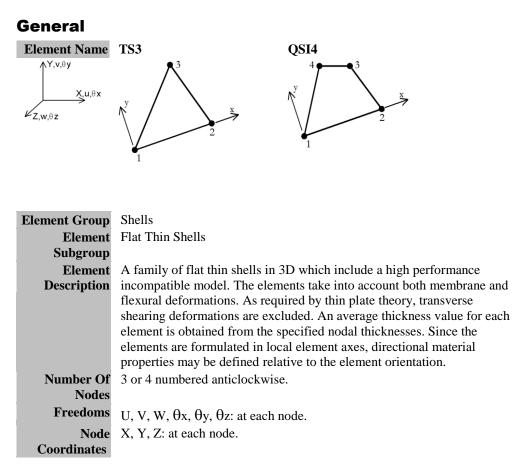
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature

Recommendations on Use

The element can be used for analysing linear and nonlinear shell structures which are axisymmetric, e.g. pressure vessels or pipes.

3D Flat Thin Shell Elements



Geometric Properties

Ez, t1... tn Eccentricity and thickness at each node.

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC
		(Elastic: Orthotropic Plane Stress)
		MATERIAL PROPERTIES ORTHOTROPIC
		SOLID (Elastic: Orthotropic Thick)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC 3

		(Elastic: Anisotropic Thin Plate)
	Rigidities.	RIGIDITIES 6 (Rigidities: Shell) (D7, D8, D9,
		D11, D12, D13, D16, D17, D18=0)
Matrix	Not applicable	
Joint	Not applicable	
Concrete	Not applicable	
Elasto-Plastic	Not applicable	
Creep	Not applicable	
Damage	Not applicable	
Viscoelastic	Not applicable	
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Rubber	Not applicable	
Generic Polymer	Not applicable	
Composite	Not applicable	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, W, θx , θy , θz : at nodes.
Concentrated Loads	CL	Concentrated loads. Px, Py, Pz, Mx, My, Mz: at nodes.
Element Loads	Not applicable.	
Distributed Loads	UDL	Uniformly distributed loads. Wx, Wy, Wz: local surface pressures for element (see Notes).
	FLD, FLDG	Not applicable.
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Zcbf (see Notes).
	BFP, BFPE	Body force potentials at nodes/for element. ϕ_1 , ϕ_2 ,
		φ ₃ (see Notes).
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Accelerations. Ax, Ay, Az: at nodes.
Initial Stress/Strains	SSI, SSIE	Initial stresses/strains at nodes/for element. Resultants. Nx, Ny, Nxy, Mx, My, Mxy: forces,
		moments/unit width in local directions. Ex, Ey,
		γ xy, ψ x, ψ y, ψ xy: membrane, flexural strains in local directions (see Notes).
	SSIG	Not applicable.

Residual Stresses	Not applicable.	
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. Resultants. Nx, Ny, Nxy, Mx, My, Mxy: forces,
		moments/unit width in local directions. Ex, Ey, γ xy, ψ x, ψ y, ψ xy: membrane, flexural strains in local directions (see Notes).
	TSSIG	Not applicable.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, dT/dz, To, 0, 0, dTo/dz: in local directions. (see Notes)
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	
Field Loads	Not applicable.	
	Not applicable.	

LUSAS Output

Solver	Stress resultant: Nx, Ny, Nxy, Mx, My, Mxy: forces, moments/unit width in local directions.
	Stress (default): σ_x , σ_y , σ_{xy} , σ_{max} , σ_{min} , β , σ_e : in local directions (see <i>Notes</i>).
	Strain: εx , εy , γxy , ψx , ψy , ψxy : membrane, flexural strains in local directions.
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

□ Standard area element

Sign Convention

□ Thin shell element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Stiffness	Default.	 1-point for the in-plane incompatible modes, (QSI4), 2x2 for the in-plane compatible modes, (QSI4), 2x2 for bending (QSI4). 1-point for in-plane (TS3), 3-point for bending (TS3).
	Fine.	As default.
Mass	Default.	 1-point for the in-plane incompatible modes, (QSI4), 2x2 for the in-plane compatible modes, (QSI4), 2x2 for bending (QSI4). 1-point for in-plane (TS3), 3-point for bending (TS3).
	Fine.	As default.

Mass Modelling

Lumped mass only.

Options

- **32** Suppress stress output but not stress resultants.
- **34** Outputs stress resultants.
- 55 Outputs strains as well as stresses.
- **59** Outputs local direction cosines for elements.
- **170** Suppresses transfer of shape function arrays to disk.

Notes on Use

- 1. The element formulations are based on the standard **isoflex** approach for the flexural matrices.
- 2. The variation of membrane stresses within the element can be regarded as constant for TS3 and linear for QSI4. The higher order membrane performance of QSI4 is due to

the addition of four incompatible in-plane displacement modes. The variation of flexural stresses can be regarded as linear for all elements.

- 3. The stress results are most easily interpreted if the local element axes are all parallel.
- 4. The elements pass the **patch test** for mixed triangular and quadrilateral geometry.
- 5. Stress output to the LUSAS output file is on 4 lines:
 - Stresses due to membrane action.
 - Top surface stresses due to bending action.
 - Top surface stresses due to membrane and bending action.
 - Bottom surface stresses due to membrane and bending action.

Gauss point output is not available.

- 6. All distributed loading will be lumped at the nodes.
- 7. For effective analysis of curved shell structures, a flat shell element should not extend over more than 15 degrees of arc.
- 8. Though this element cannot model nonlinear behaviour, it can be mixed with other elements in a nonlinear analysis.
- 9. A system variable is used to alter the artificial stiffness for in-plane rotations.
- 10. A fine discretisation will be required to reproduce the correct behavioural response for curved structures. Therefore, the Semiloof shell elements (QSL8,TSL6) or the thick shell elements (QTS8, TTS6) may be more appropriate.
- 11. The ORTHOTROIC SOLID material model may be used with either composite or non-composite thin shell elements. Using a Solid rather than a Thick orthotropic material means that a local coordinate may be used to orientate the material.
- 12. Element loading on elements with eccentricity is applied as follows:
 - SSI, SSIE, TSSIE, TSSIA, TEMP, TMPE at the mid-plane of the element.
 - UDL, CBF, BFP, BFPE at the nodal plane.

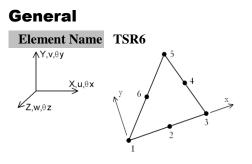
Restrictions

- □ Avoid excessive aspect ratio.
- □ Avoid excessive warping.

Recommendations on Use

- The flat thin shell elements are suitable for modelling both flat and curved thin shell structures which exhibit negligible transverse shear deformations.
- A fine discretisation will be required to reproduce the correct behavioural response for curved structures. Therefore, the Semiloof shell elements (QSL8,TSL6) or the thick shell elements (QTS8, TTS6) may be more appropriate.
- The Semiloof shell elements (QSL8,TSL6) or the thick shell elements (QTS8, TTS6) are more effective for structures containing multiple shell intersections.
- The Semiloof shell elements (QSL8,TSL6) or the thick shell elements (QTS4, QTS8, TTS3, TTS6) may be more effective for eigen-analyses since a consistent mass matrix is available.
- The Semiloof shell elements (QSL8,TSL6) should be utilised for nonlinear analyses.
- The elements can be combined with BMI21 beam elements for analysing ribbed shells with small or no eccentricity. However, the Semiloof shell (QSL8,TSL6) and beam (BSL3,BSL4,BXL4) are more effective for thin ribbed shells with larger eccentricity. For thick ribbed shells with larger eccentricity the thick shell (QTS4, QTS8, TTS3, TTS6) and co-rotational beam (BMI21) are recommended.

3D Flat Thin Nonlinear Shell Element



Element Group	Shells
Element	Flat Thin Shells
Subgroup	
Element	A triangular shell element for the analysis of faceted shell geometries,
Description	including multiple branched junctions. The elements can accommodate varying thickness and anisotropic material properties. The element is based on the "Morley shell" formulation and assumes constant membrane and bending strains across the element. As required by thin shell theory, transverse shearing deformations are excluded.
Number Of Nodes	6 numbered anticlockwise.
Freedoms	U, V, W: at corner nodes. θ_1 : (loof rotation) at mid-side nodes (see <i>Notes</i>).
Node	X, Y, Z: at each node.
Coordinates	

Geometric Properties

Orthotropic:

t1... tn Thickness at each node.

Material Properties

Linear Isotropic: MATERIAL PROPERTIES (Elastic: Isotropic)

MATERIAL PROPERTIES ORTHOTROPIC (Elastic: Orthotropic Plane Stress) MATERIAL PROPERTIES ORTHOTROPIC SOLID (Elastic: Orthotropic Thick)

	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC 3 (Elastic: Anisotropic Thin Plate)
	Rigidities.	RIGIDITIES 6 (Rigidities: Shell)
Matrix	Not applicable	
Joint	Not applicable	
Concrete		MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Elasto-Plastic	Stress resultant:	MATERIAL PROPERTIES NONLINEAR 29 (Elastic: Isotropic, Plastic: Resultant) (ifcode not required)
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker- Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr- Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Volumetric Crushing:	Not applicable.
	Stress Potential	STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman)
Creep		CREEP PROPERTIES (Creep)
	AASHTO	Not applicable

	CEB-FIP	Not applicable
	Chinese	Not applicable
	Eurocode	Not applicable
	IRC	Not applicable
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic	Not applicable	
Shrinkage		GENERAL, USER
Rubber	Not applicable.	
Generic Polymer	Not applicable	
Composite	Not applicable	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, W: at corner nodes. θ_1 : at mid-side nodes.
Concentrated Loads	CL	Concentrated loads. Px, Py, Pz: at corner nodes. M1: at mid-side nodes.
Element Loads	Not applicable.	
Distributed Loads	UDL	Uniformly distributed loads. Wx, Wy, Wz: mid- surface local pressures for element.
Body Forces	FLD, FLDG CBF	Not applicable. Constant body forces for element. Xcbf, Ycbf, Zcbf,

		$\Omega x, \Omega y, \Omega z, \alpha x, \alpha y, \alpha z$
	BFP, BFPE	Body force potentials at nodes/for element. ϕ_1 , ϕ_2 ,
		φ_3 , 0, Xcbf, Ycbf, Zcbf, where φ_1 , φ_2 , φ_3 are the
Velocities	VELO	face loads in the local coordinate system. Velocities. Vx, Vy, Vz: at corner nodes.
Accelerations	ACCE	Accelerations. Ax, Ay, Az: at corner nodes.
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element.
Stress/Strains		
	SSIG	Initial stresses/strains at Gauss points. (1) Resultants (for model 29 and RIGIDITIES) Nx,
		Ny, Nxy, Mx, My, Mxy, εx , εy , γxy , ψx , ψy ,
		 Wxy: forces, moments/unit width and membrane/flexural strains in local directions. (2) Components (in all other cases except for nonlinear model 29 and RIGIDITIES), 0, 0, 0, 0, 0,
		0, 0, 0, 0, 0, 0, 0, (σx, σy, σxy, εx, εy, γxy). Bracketed terms repeat for each layer.
Residual Stresses	SSR, SSRE	Residual stresses at nodes/for element
	SSRG	 Residual stresses at Gauss points. (1) Resultants (for model 29) Nx, Ny, Nxy, Mx, My, Mxy: forces, moments/unit width in local directions. (2) Components (for all nonlinear material models except model 29): 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0
		(σx , σy , σxy). Bracketed terms repeat for each layer.
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element.
	TSSIG	Target stresses/strains at Gauss points. (1) Resultants (for model 29 and RIGIDITIES) Nx,
		Νy, Νxy, Μx, Μy, Μxy, εx, εy, γxy, ψx, ψy,
		 ψxy: forces, moments/unit width and membrane/flexural strains in local directions. (2) Components (in all other cases except for nonlinear model 29 and RIGIDITIES), 0, 0, 0, 0, 0,
		0, 0, 0, 0, 0, 0, 0, (σx, σy, σxy, εx, εy, γxy). Bracketed terms repeat for each layer.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, dT/dz, To, 0, 0, dTo/dz
Overburden	Not applicable.	

Phreatic SurfaceNot
applicable.Field LoadsNot
applicable.Temp DependentNot
LoadsLoadsapplicable.

LUSAS Output

Solver Stress resultant: Nx, Ny, Nxy, Mx, My, Mxy: forces, moments/unit width in local directions.

Stress (default): σx , σy , σxy , σmax , σmin , β , σe : in local directions (see *Notes*).

Strain: εx , εy , γxy , ψx , ψy , ψxy : membrane, flexural strains in local directions.

Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

<u>Standard area element</u>

Sign Convention

□ Thin shell element

Formulation

Geometric Nonlinearity

Total LagrangianNot applicable.UpdatedNot applicable.LagrangianNot applicable.EulerianNot applicable.Co-rotationalFor large displacements and rotations

Integration Schemes

Stiffness Default.	1-point
Fine.	1-point
Coarse.	1-point
Mass Default.	1-point
Fine.	1-point

Mass Modelling

□ Consistent mass.

Options

- **32** Suppresses stress output but not resultants.
- **34** Outputs element stress resultants.
- **55** Outputs strains as well as stresses.
- **59** Outputs local direction cosines at nodes and Gauss points.
- 77 Output principal stresses and directions.
- **139** Output yielded Gauss points only.

Notes on Use

- 1. The element formulations are based on a <u>Kirchhoff</u> hypothesis for thin shells.
- 2. The stresses are constant within the elements.
- 3. The loof rotations refer to rotations about the element edge at the mid-side nodes. The positive direction of a loof rotation is defined by a right-hand screw rule applied to a vector running in the direction of the lower to higher numbered corner nodes. It should be noted that this direction is enforced on a global level which means that the loof rotations along the adjoining edge of several elements will be consistent in terms of direction and ordering.
- 4. The element edges must remain straight even though the elements have mid-side nodes.
- 5. The elements pass the <u>patch test</u> for convergence.
- 6. Stresse will not be output when using RIGIDITIES or material model 29.
- The through-thickness integration is performed explicitly for linear analyses and a 5point <u>Newton-Cotes</u> rule is utilised for materially nonlinear analyses with continuum material models. The through-thickness integration rules are as follows:

- Linear models: 3-layers.
- Nonlinear models: 5-layers.

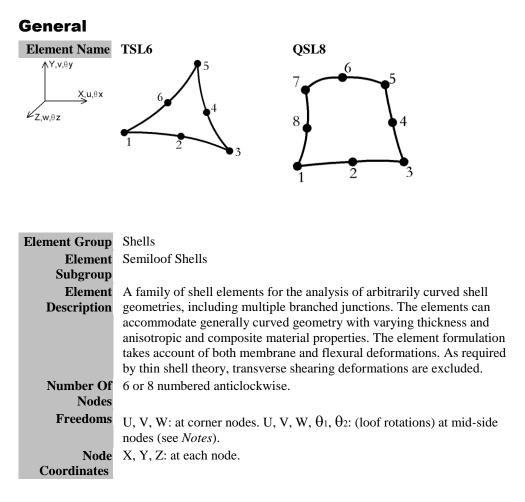
Restrictions

- Ensure mid-side node centrality and straight element edges
- □ Avoid excessive aspect ratio

Recommendations on Use

- These elements may be utilised for analysing flat and faceted 3D shell structures where the transverse shear effects do not influence the solution. The configuration of the nodal freedoms provides an element suitable for modelling intersecting shells.
- The elements are recommended for geometrically nonlinear problems where large displacements and rotations occur. The single Gauss point integration scheme gives rise to a computationally efficient solution, however, the mesh may need to be refined if there is an unacceptable differentiation in stresses between adjacent elements..

Semiloof Curved Thin Shell Elements



Geometric Properties

t1... tn Thickness at each node. Also see Composite Geometry data chapter.

Material Properties

Linear Isotropic:

MATERIAL PROPERTIES (Elastic: Isotropic)

	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC (Elastic: Orthotropic Plane Stress) MATERIAL PROPERTIES ORTHOTROPIC SOLID (Elastic: Orthotropic Solid)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC 3 (Elastic: Anisotropic Thin Plate)
	Rigidities.	RIGIDITIES 6 (Rigidities: Shell)
Matrix	Not applicable	
Joint	Not applicable	
Concrete		MATERIAL PROPERTIES NONLINEAR 109 (Elastic: Isotropic, Plastic: Smoothed Multi-Crack Concrete)
Elasto-Plastic	Stress resultant:	MATERIAL PROPERTIES NONLINEAR 29 (Elastic: Isotropic, Plastic: Resultant) (ifcode not required)
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61 (Elastic: Isotropic, Plastic: Tresca, Hardening: Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker- Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr- Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Volumetric Crushing:	Not applicable.
	Stress Potential	STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises
Creep		Orthotropic: Hill, Hoffman) CREEP PROPERTIES (Creep)

	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB FIP (Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE
	IRC	(Concrete creep model to EUROCODE_2) MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC code of
Damage		Practice) DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic	Not applicable	
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Rubber	Not applicable.	
Generic Polymer	Not applicable	
Composite	Composite shell:	COMPOSITE PROPERTIES

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, W: at corner nodes. U, V,
		W, θ_1 , θ_2 : at mid-side nodes.
Concentrated	CL	Concentrated loads. Px, Py, Pz: at corner nodes. Px,

Loads Element Loads	Not	Py, Pz, M1, M2: at mid-side nodes.
Liement Lieuus	applicable.	
Distributed Loads	UDL	Uniformly distributed loads. Wx, Wy, Wz: mid- surface local pressures for element.
	FLD, FLDG	Not applicable.
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Zcbf,
		$\Omega x, \Omega y, \Omega z, \alpha x, \alpha y, \alpha z$
	BFP, BFPE	Body force potentials at nodes/for element. φ_1 , φ_2 ,
		φ_3 , 0, Xcbf, Ycbf, Zcbf, where φ_1 , φ_2 , φ_3 are the face loads in the local coordinate system.
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Accelerations. Ax, Ay, Az: at nodes.
Initial	SSI, SSIE	Not applicable.
Stress/Strains	SSIG	Initial strasses/strains at Cause points
	2210	Initial stresses/strains at Gauss points. (1) Resultants (for linear analysis and model 29)
		Nx, Ny, Nxy, Mx, My, Mxy, $\mathcal{E}x$, $\mathcal{E}y$, γxy , Ψx , Ψy ,
		ψxy: forces, moments/unit width and membrane/flexural strains in local directions.
		(2) Components (for all other nonlinear material
		models) are: 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, $(\sigma x, \sigma x)$
		σ y, σ xy, ε x, ε y, γ xy) - with the bracketed terms repeated for each of the five layers. (See note 7 in the Notes of Use) section.
Residual Stresses	SSR, SSRE	Not applicable.
	SSRG	 Residual stresses at Gauss points. (1) Resultants (for model 29) Nx, Ny, Nxy, Mx, My, Mxy: forces, moments/unit width in local directions. (2) Components (for all other nonlinear material models) are:0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, (σx, σy, σy)
		σ_{xy} - with the bracketed terms repeated for each of the five layers. (See note 7 in the Notes of Use) section.
Target	TSSIE, TSSIA	Not applicable.
Stress/Strains		
	TSSIG	 Target stresses/strains at Gauss points. (1) Resultants (for linear analysis and model 29) Nx, Ny, Nxy, Mx, My, Mxy, εx, εy, γxy, ψx, ψy, ψxy: forces, moments/unit width and

		membrane/flexural strains in local directions. (2) Components (for all other nonlinear material
		models) are: 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0,
		σ_y , σ_{xy} , ε_x , ε_y , γ_{xy}) - with the bracketed terms repeated for each of the five layers. (See note 7 in the Notes of Use) section.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, dT/dz, To, 0, 0, dTo/dz
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent Loads	Not applicable.	

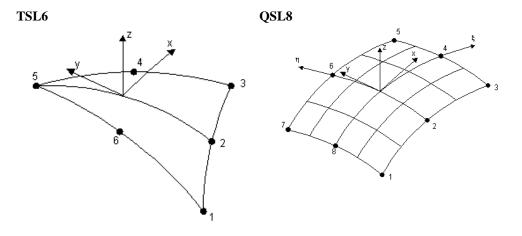
LUSAS Output

Solver	Stress resultant: Nx, Ny, Nxy, Mx, My, Mxy: forces, moments/unit width in local directions.
	Stress (default): σx , σy , σxy , σmax , σmin , β , σe : in local directions (see <i>Notes</i>).
	Strain: εx , εy , γxy , ψx , ψy , ψxy : membrane, flexural strains in local directions.
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

- Local y axis The local element y-axis at a point coincides with a curvilinear line ξ = constant in the natural coordinate system which lies in the shell mid-surface.
- Local x axis The local x-axis at a point is perpendicular to the local y-axis in the positive η direction and is tangential to the shell mid-surface.

• Local z axis The local z-axis forms a right-hand set with the x and y axes and the direction is given by the ordering of the element nodes according to a right-hand screw rule. The local z-axis +ve direction defines the element top surface.



Sign Convention

□ Thin shell element (see*Notes*).

Formulation

Geometric Nonlinearity

Total LagrangianFor large displacements, rotations up to 1 radian and small strains.UpdatedFor large displacements, rotation increments up to 1 radian and smallLagrangianstrains.EulerianNot applicable.Co-rotationalNot applicable.

Integration Schemes

Stiffness Default.	3-point (TSL6), 5-point (QSL8).
Fine (see	3x3 (QSL8)
Options).	
Coarse (see	2x2 (QSL8)
Options).	
Mass Default.	3-point (TSL6), 5-point (QSL8).

Fine (see3x3 (QSL8)Options).

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- **18** Invokes fine integration rule.
- **19** Invokes coarse integration rule.
- 32 Suppresses stress output but not resultants.
- 34 Outputs element stress resultants.
- 54 Updated Lagrangian geometric nonlinearity.
- 55 Outputs strains as well as stresses
- **59** Outputs local direction cosines at nodes and Gauss points.
- 87 Total Lagrangian geometric nonlinearity.
- **102** Switch off load correction stiffness due to centripetal acceleration.
- 105 Lumped mass matrix.
- **138** Output yield flags only.
- 139 Output yielded Gauss points only.
- **169** Suppress extrapolation of stresses to nodes.
- 170 Suppress transfer of shape function arrays to disk.

Notes on Use

- 1. The element formulations are based on a <u>Kirchhoff</u> hypothesis for thin shells.
- 2. The variation of stresses within the elements may be regarded as linear.
- 3. The loof rotations refer to rotations about the element edge at the loof points. The positive direction of a loof rotation is defined by a right-hand screw rule applied to a vector running in the direction of the lower to higher numbered corner nodes. It should be noted that this direction is enforced on a global level which means that the loof rotations along the adjoining edge of several elements will be consistent in terms of direction and ordering. The ordering is such that loof point 1 is located between the lower numbered node and the appropriate mid-side node. Similarly loof point 2 lies between the mid-side node and the higher numbered node along an element edge. The loof rotations are actually specified at the element mid-side nodes.
- 4. The elements pass the <u>patch test</u> for convergence for mixed triangular and quadrilateral element geometry.

- 5. Stress output to the LUSAS output file is on 4 lines:
 - Stresses due to membrane action.
 - Top surface stresses due to bending action.
 - Top surface stresses due to membrane and bending action.
 - Bottom surface stresses due to membrane and bending action.
- 6. Stresses will not be output when using RIGIDITIES or material model 29. Averaged stresses will not be processed when using RIGIDITIES.
- 7. The through-thickness integration is performed explicitly for linear analyses and a 5-point <u>Newton-Cotes</u> rule is utilised for materially nonlinear analyses with continuum material models. The through-thickness integration rules are as follows:
 - Linear models: 3-layers.
 - Nonlinear models: 5-layers.
 - Composite model: Variable.
- 8. The quadrature points of the 3-point rule are non-standard.
- 9. The coarse 2*2 quadrature rule provides the most effective element if the mesh is highly constrained. However, the element possesses two mechanisms, the usual inplane hourglass mechanism encountered when reduced integration is utilised with 8-noded elements and an out of plane mechanism. The in-plane mechanism is rarely activated but the out-of-plane mechanism may be more troublesome, particularly where elements are regular and have one zero principal curvature, e.g. a cylinder subject to internal pressure. Provided the mechanisms are not activated the element with 2*2 provides the best results.
- 10. The 5-point quadrature rule provides an element with a performance below that of the element with 2*2 quadrature, but considerably better than the element with 3*3 quadrature. However, the element possesses a 'near' mechanism which may be activated for lightly constrained meshes, particularly if out of plane loads are present.
- 11. The middle integration point of the 5 point rule is only implemented as a method of reducing the excitation of spurious modes (or mechanisms) which are present with the 2*2 integration rule. The 5th integration point is actually weighted with an arbitrarily small value which has the effect of stabilising the results. For these reasons, values from the middle integration point are not taken into account for the nodal extrapolation.
- 12. The 3*3 quadrature rule provides an element that has no mechanisms but tends to provide over-stiff solutions. Therefore, a finer discretisation is required than if the 5-point quadrature rule is used.

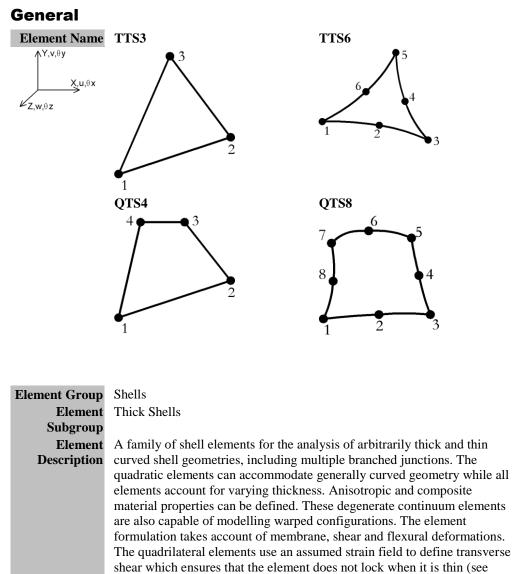
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

Recommendations on Use

- These elements may be utilised for analysing flat and curved 3D shell structures where the transverse shear effects do not influence the solution. The configuration of the nodal freedoms provides an element suitable for modelling intersecting shells, e.g. tubular joints and also for use with solid elements (HX20).
- The elements may be combined with the Semiloof beam (BSL3,BSL4,BXL4) for analysing ribbed plates and shells.

3D Thick Shell Elements



	Notes).
Number Of	3, 4, 6 or 8 numbered anticlockwise.
Nodes	
Freedoms	Default: 5 degrees of freedom are associated with each node U, V, W,
	$\theta \alpha$, $\theta \beta$. To avoid singularities, the rotations $\theta \alpha$ and $\theta \beta$ relate to axes

	defined by the orientation of the normal at a node, see <u>Thick Shell Nodal</u> <u>Rotation</u> . These rotations may be transformed to relate to the global axes in some instances (see <i>Notes</i>). Degrees of freedom relating to global axes:
	U, V, W, θx , θy , θz may be enforced using the Nodal Freedom data input, or for all shell nodes by using option 278 (see <i>Notes</i>).
Node	X, Y, Z: at each node.
Coordinates	
Nodal	5 or 6.
Freedoms	

Geometric Properties

ez, t1... tn Eccentricity and thickness at each node.

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC
		THICK (Elastic: Orthotropic Thick)
		MATERIAL PROPERTIES ORTHOTROPIC
		SOLID (Elastic: Orthotropic Thick)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC 5
		(Elastic: Anisotropic Thick Plate)
	Rigidities.	Not applicable.
Matrix	Not applicable	
Joint	Not applicable	
Concrete		MATERIAL PROPERTIES NONLINEAR 109
		(Elastic: Isotropic, Plastic: Smoothed Multi-Crack
		Concrete)
Elasto-Plastic	Stress	Not applicable.
	resultant:	
	Tresca:	MATERIAL PROPERTIES NONLINEAR 61
		(Elastic: Isotropic, Plastic: Tresca, Hardening:
		Isotropic Hardening Gradient, Isotropic Plastic
		Strain or Isotropic Total Strain)
	Drucker-	MATERIAL PROPERTIES NONLINEAR 64
	Prager:	(Elastic: Isotropic, Plastic: Drucker-Prager,
		Hardening: Granular)
	Mohr-	MATERIAL PROPERTIES NONLINEAR 65
	Coulomb:	(Elastic: Isotropic, Plastic: Mohr-Coulomb,
		Hardening: Granular with Dilation)
	Volumetric	Not applicable.

Сгеер	Crushing: Stress Potential	STRESS POTENTIAL VON_MISES, HILL, HOFFMAN (Isotropic: von Mises, Modified von Mises Orthotropic: Hill, Hoffman) CREEP PROPERTIES (Creep)
	AASHTO	MATERIAL PROPERTIES NONLINEAR 86 AASHTO (Concrete creep model to AASHTO Code of Practice)
	CEB-FIP	MATERIAL PROPERTIES NONLINEAR 86 CEB- FIP (Concrete creep model to CEB-FIP Model Code 1990)
	Chinese	MATERIAL PROPERTIES NONLINEAR 86 CHINESE (Chinese creep model to Chinese Code of Practice)
	Eurocode	MATERIAL PROPERTIES NONLINEAR 86 EUROCODE (Concrete creep model to EUROCODE_2)
	IRC	MATERIAL PROPERTIES NONLINEAR 86 IRC (Concrete creep model to Indian IRC Code of Practice)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic	Not applicable	
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Rubber	Not applicable	
Generic Polymer		
Composite	Composite shell:	COMPOSITE PROPERTIES
Loading		

Prescribed Value	PDSP, TPDSP	Prescribed variable. 5 degrees of freedom: U, V, W, $\theta \alpha$, $\theta \beta$ or 6 degrees of freedom: U, V, W, θx , θy ,
		θz
Concentrated	CL	Concentrated loads. 5 degrees of freedom: Px, Py,

Loads		Pz, M α , M β , where M α and M β relate to axes defined by $\theta\alpha$ and $\theta\beta$ respectively. 6 degrees of freedom: Px, Py, Pz, Mx, My, Mz.
Element Loads Distributed Loads	Not applicable. UDL FLD, FLDG	Uniformly distributed loads. Wx, Wy, Wz: mid- surface local pressures for element (see Notes). Not applicable.
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Zcbf, Ωx , Ωy , Ωz , αx , αy , αz (see Notes).
	BFP, BFPE	Body force potentials at nodes/for element. φ_1 , φ_2 , φ_3 , 0, Xcbf, Ycbf, Zcbf, where φ_1 , φ_2 , φ_3 are the face loads in the local coordinate system (see Notes).
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Accelerations. Ax, Ay, Az: at nodes.
Initial Stress/Strains	SSI, SSIE	Initial stresses/strains at nodes/for element (see Notes).
	SSIG	 Initial stresses/strains at Gauss points. Stress/strain components relating to local axes at Gauss points: σx, σy, σxy, σyz, σxz, εx, εy, γxy, γyz, γxz. All of these 10 terms are repeated for each fibre integration point through the thickness (see <i>Notes</i>).
Residual Stresses	SSR, SSRE	Not applicable.
	SSRG	Residual stresses at Gauss points. Stress components
		 relating to local axes at Gauss points: σx, σy, σxy, σyz, σxz all of these 5 terms are repeated for each fibre integration point through the thickness
		(see Notes).
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element (see Notes).
	TSSIG	Target stresses/strains at Gauss points. Stress/strain components relating to local axes at Gauss points:
		σ_x , σ_y , σ_{xy} , σ_{yz} , σ_{xz} , ε_x , ε_y , γ_{xy} , γ_{yz} , γ_{xz} . All of these 10 terms are repeated for each fibre integration point through the thickness (see <i>Notes</i>).
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, dT/dz, To, 0, 0, dTo/dz (see Notes).
Overburden	Applicable.	
Phreatic Surface	Applicable.	
Field Loads	Not applicable.	

Temp Dependent Not applicable. Loads

LUSAS Output

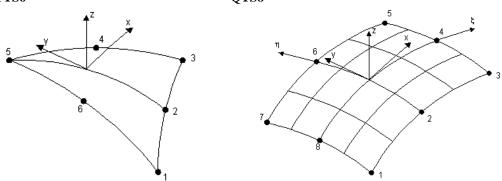
Solver Stress resultant: Nx, Ny, Nxy, Mx, My, Mxy, Sx, Sy: forces, moments/unit width in local directions.
 Stress (default): σx, σy, σxy, σyz σxz, σe: in local directions (see *Notes*).
 Strain: εx, εy, γxy, γyz, γxz, εe: in local directions (see *Notes*).
 Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

The local element x-axis at a point coincides with a curvilinear line η = constant in the natural coordinate system which lies in the shell mid-surface. The local z-axis at a point is obtained from the cross product of a curvilinear line ξ = constant in the natural coordinate system and the local x-axis. The local y-axis forms a right-hand set with the x and z axes and the direction is given by the ordering of the element nodes according to a right-hand screw rule. The local z-axis +ve direction defines the element top surface.

TTSTTS6





Sign Convention

□ Thick shell element (see*Notes*).

Formulation

Geometric Nonlinearity

Total LagrangianFor large displacements, large rotations and small strains.UpdatedNot applicable.LagrangianNot applicable.Co-rotationalNot applicable.

Integration Schemes

Default.	1-point (TTS3), 3-point (TTS6), 2x2 (QTS4, QTS8).
Fine (see Options).	3-point (TTS3), 5-point (QTS8)
Default.	1-point (TTS3), 3-point (TTS6), 2x2 (QTS4, QTS8).
Fine (see Options).	3-point (TTS3), 5 point (QTS8)
	Default.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- **18** Invokes fine integration rule.
- 32 Suppresses stress output but not resultants.
- **34** Outputs element stress resultants.
- 55 Outputs strains as well as stresses.
- 59 Outputs local direction cosines at nodes and Gauss points.
- 77 Outputs principal stresses.
- 87 Total Lagrangian geometric nonlinearity.
- 102 Switch off load correction stiffness due to centripetal acceleration.
- 105 Lumped mass matrix.
- 110 Use assumed shear strain field for TTS6 and QTS8 thick shell elements.
- **139** Output yielded Gauss points only.
- **169** Suppress extrapolation of stresses to nodes.
- 171 Switch off assumed strain field for QTS4 elements.
- 278 Six degrees of freedom.
- **396** Invokes the improved transverse shear calculation ('on' by default for models created by version 14.4 and above, and 'off' for models created by previous

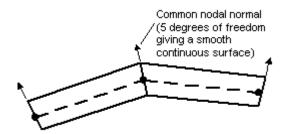
versions).

- 417 Introduce residual bending flexibility correction for 3-node thick shell TTS3.
- **422** Use assumed transverse shear strain field for TTS3 thick shell element.

Notes on Use

- 1. For TTS3 elements all moments and shears are constant for the element. For QTS4 the variations of moments, out of plane shears and in-plane loads is near-constant and the variation of in-plane shear is near-linear. For TTS6 and QTS8 elements the variation of moments and in-plane shear is near-linear while the variation of out of plane shears is near-constant.
- 2. Shear locking is much more of an issue for lower order elements, and hence an assumed shear strain field is always switched on for TTS3/QTS4 elements; if it were switched off, these elements would always lock and perform very badly. Higher order elements are less prone to shear locking, and the situation is not quite so clear cut. It has been found that using an assumed shear strain field with QTS8 elements when transverse shear strain dominates can lead to poor results. The view has therefore been taken that the assumed shear strain field should be switched off by default for the higher order TTS6/QTS8 elements.
- 3. The QTS8 element fails the shear <u>patch test</u> when the assumed strain field is utilised with 2*2 or 5 point integration rule. When carrying out analyses involving these elements that are dominated by transverse shear effects, e.g. a shear wall, it is recommended, as discussed above, that the assumed strain field is disabled. This is the default setting for QTS8 elements. Option 110 may be used to invoke the assumed strain interpolation but this is not recommended for general use.
- 4. The assumed strain field is invoked automatically for QTS4 elements. The assumed strain field may be revoked for QTS4 by specifying Option 171.
- 5. The introduction of assumed transverse shear strains (Option 422) significantly improves the performance of the TTS3 element. The RBF correction (Option 417) further improves the TTS3 element, especially for very thin shells. For elasto-plastic materials, the correction matrix is computed using the linear material properties
- 6. Continuum stresses (and strains using Option 55) at each fibre integration point are output by default. For linear materials these stresses relate to the top, middle and bottom surfaces of the element. If a nonlinear material is specified then stresses are output at 5 points through the thickness after material yield.
- 7. Option 55 must be specified if nonlinear state variables are to be written to the LUSAS output file.
- 8. The through-thickness integration rules are as follows:
 - Linear material models: 3-layers.

- Nonlinear material models: 5-layers.
- Composite model: variable.
- 7. Initial stresses/strains must be specified at 3 layers for a linear material or 5 layers for a nonlinear material. Residual stresses must be specified for 5 layers. In all instances the stresses/strains are specified sequentially from the bottom surface to the top.
- 8. There are usually 2 rotational degrees of freedom and a common nodal normal associated with each node giving a smooth surface to the shell assembly:



The direction of the axes defining the rotations depends upon the orientation of the normal at a node (see <u>Thick Shell Nodal Rotation</u>). In certain circumstances 3 rotational degrees of freedom relating to global axes will be assigned to a node. This is done automatically:

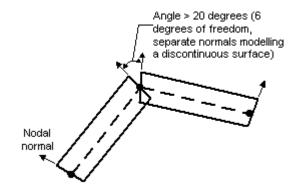
- When connecting with beam elements, joint elements or other types of shells, eg.QSI4.
- When a Concentrated Load is applied in LUSAS Modeller.
- When a Support is applied in LUSAS Modeller.
- When the angle between adjacent shell normals exceeds the SYSTEM parameter SHLANG (see below).
- When option 278 is specified.

If Option 278 is specified then all nodes for these shell element types will be assigned six global degrees of freedom. To overcome the problems associated with in-plane drilling rotations an artificial stiffness is automatically included for the rotation about the shell normal. The use of Option 278 is not recommended for analyses that involve large displacements or rotations. LUSAS Modeller will automatically specify Option 278 but it can be switched off in Modeller via File > Model Properties > Solution > Element options.

Option 278 should be switched **off** if QTS4 elements are to be used to model thick curved shells in which membrane action leads to a significant difference between the in-plane strains in the top and bottom surface of the shell. If Option 278 is not disabled under these circumstances the moments associated with this in-plane strain

differential are not accurately accounted for. An alternative approach would be to switch to QTS8 elements as these elements produce more accurate moments under these conditions.

When the maximum angle between adjacent normals at a node is greater than 20 degrees, e.g., branched shell structures. (20 degrees is a default value which may be changed using the SYSTEM parameter SHLANG); if the nodal freedom command has **not** been specified for that node.



- 9. A system variable (STFINP) is used to alter the artificial stiffness for in-plane rotations. This system parameter can only be used in conjunction with Option 278.
- 10. The desired number of rotational degrees of freedom for a node may be enforced through the NODAL FREEDOMS data input. Care must be taken if 6 degrees of freedom are specified in this manner as a singularity may occur if appropriate in-plane rotations are not restrained. This facility is provided together with the TRANSFORMED FREEDOMS data chapter to allow more flexibility in the specification of boundary conditions. In these circumstances, the in-plane rotation about the normal of the shell must usually be restrained to avoid singularities. In general, wherever possible, 5 degrees of freedom should be used when the shell surface is smooth.
- 11. The TTS3 and QTS8 elements possess one out of plane mechanism when using the default integration rules. The 3 noded element is most effective using the one point rule.
- 12. The through-thickness integration is performed by utilising a 3 point <u>Newton-Cotes</u> rule for linear materials and a 5 point rule for nonlinear materials and creep. In an analysis involving material nonlinearity, a 3 point rule is used until the material yields and then a 5 point rule is invoked.
- 13. The thick shell formulation assumes constant transverse shear deformation. In the post-processing stage, after the application of the constitutive relationship, this results in a constant transverse shear stress. This result can be improved by taking into

account the true parabolic shear stress distribution while preserving the same shear resultant. Thus, when Option 396 is used, the transverse shear stresses for a non-layered shell are set to zero at the top and bottom and to 1.5 times the constant value at the middle. For a layered shell, the distribution of the transverse shear depends on the in-plane stiffness of the layers. The output results are for the middle of the layer, thus the top and bottom layers will not have zero transverse shear.

- 14. The ORTHOTROPIC SOLID material model may be used with either composite or non-composite thick shell elements. Using a Solid rather than a Thick orthotropic material means that a local coordinate may be used to orientate the material.
- 15. If applying an initial stress/strain or thermal load that varies across an element, a higher order element (6 or 8 nodes) should be used. A limitation of the standard isoparametric approach when used for lower order elements (3 or 4 nodes) is that only constant stress/strain fields can be imposed correctly.
- 16. For an element with eccentricity the following load types are applied at the mid-plane of the element (not the nodal plane): UDL, CBF, BFP, BFPE, SSI, SSIE, SSIG, SSRG, TSSIE, TSSIA, TSSIG, TEMP, TMPE.
- 17. The Smoothed Multi Crack Concrete Model (109) can be used with this element, however, due to the "plane sections remaining plane" hypothesis, crack widths cannot be computed.

Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

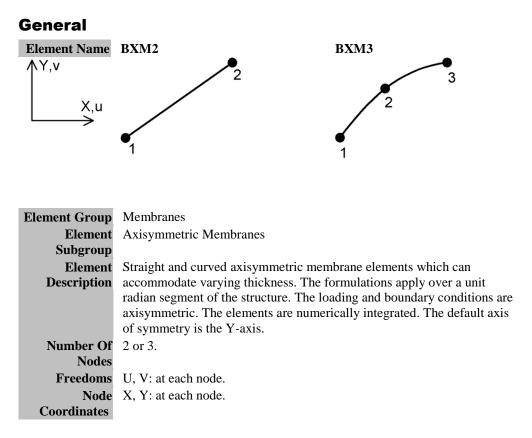
Recommendations on Use

- These elements may be utilised for analysing flat and curved 3D shell structures where it is necessary to account for transverse shear. This typically involves thick shell structures where transverse shear deformation can have a considerable influence on the response. The degenerate continuum formulation also allows the low order quadrilateral element (QTS4) to successfully model warped shell configurations.
- The elements may be used for modelling intersecting shells or branched shell junctions. In this instance the nodal rotation freedoms are transformed to relate to the global axes. For modelling stiffened shell structures, the shells may be connected to beam elements BMI21.
- This family of thick shell elements offers a consistent formulation of the tangent stiffness which makes them particularly effective in geometrically nonlinear applications.
- Be aware that when the shell is defined with eccentricity to a reference surface and this reference surface does not pass through the centroid of the cross section,

membrane forces or displacements prescribed/calculated at the nodes will cause bending.

Chapter 7 : Membrane Elements.

2D Axisymmetric Membrane Elements



Geometric Properties

t1... tn Thickness at each node.

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
Matrix	Not applicable	
	Not applicable	
Concrete	Not applicable	
Elasto-Plastic	Tresca:	MATERIAL PROPERTIES NONLINEAR 61
		(Elastic: Isotropic, Plastic: Tresca, Hardening:

		Isotropic Hardening Gradient, Isotropic Plastic Strain or Isotropic Total Strain)
	Drucker-Prager:	MATERIAL PROPERTIES NONLINEAR 64 (Elastic: Isotropic, Plastic: Drucker-Prager, Hardening: Granular)
	Mohr-Coulomb:	MATERIAL PROPERTIES NONLINEAR 65 (Elastic: Isotropic, Plastic: Mohr-Coulomb, Hardening: Granular with Dilation)
	Optimised Implicit Von Mises:	MATERIAL PROPERTIES NONLINEAR 75 (Elastic: Isotropic, Plastic: Von Mises, Hardening: Isotropic & Kinematic)
	Volumetric Crushing:	Not applicable.
	Stress Potential	STRESS POTENTIAL VON_MISES (Isotropic: von Mises, Modified von Mises)
Creep		CREEP PROPERTIES (Creep)
Damage		DAMAGE PROPERTIES SIMO, OLIVER (Damage)
Viscoelastic	Not applicable	
Shrinkage		SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER
Rubber	Ogden:	MATERIAL PROPERTIES RUBBER OGDEN (Rubber: Ogden) (See Restrictions)
	Mooney-Rivlin:	MATERIAL PROPERTIES RUBBER MOONEY_RIVLIN (Rubber: Mooney-Rivlin) (See Restrictions)
	Neo-Hookean:	MATERIAL PROPERTIES RUBBER NEO_HOOKEAN (Rubber: Neo-Hookean) (See Restrictions)
	Hencky:	Not applicable.
Generic Polymer	Not applicable	
Composite	Not applicable	
Field	Not applicable	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V: at nodes.
Concentrated Loads	CL	Concentrated loads. Px, Py: at nodes.
Element Loads	Not applicable.	

Distributed Loads	UDL	Not applicable.
	FLD	Face Loads. Px, Py: local face pressure at nodes.
	FLDG	Not applicable
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Ωx , Ωy , Ωz , αz
	BFP, BFPE	Body force potentials at nodes/for element. 0, 0, 0, 0, Xcbf, Ycbf
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Accelerations. Ax, Ay: at nodes.
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element.
Stress/Strains		σx , $\sigma \theta$: axial, circumferential stress.
		Ex, εθ: axial, circumferential strain.
	SSIG	Initial stresses/strains at Gauss points.
		σx , σ_{θ} : axial, circumferential stress.
		εx, εθ: axial, circumferential strain.
Residual Stresses	SSR, SSRE	Not applicable.
	SSRG	Residual stresses at Gauss points. σx , $\sigma \theta$: axial, circumferential stress.
Target	TSSIE, TSSIA	Target stresses/strains at nodes/for element.
Stress/Strains		σx , $\sigma \theta$: axial, circumferential stress.
		Ex, E0: axial, circumferential strain.
	TSSIG	Target stresses/strains at Gauss points.
		σx , $\sigma \theta$: axial, circumferential stress.
		εx, εθ: axial, circumferential strain.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent Loads	Not applicable.	

LUSAS Output

Solver	Stress (default): σx , σ_{θ} : axial, circumferential stress.
	Strain: Ex, E0: axial, circumferential strain.

Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

□ Standard line element

Sign Convention

□ Standard membrane element

Formulation

Geometric Nonlinearity

Total Lagrangian	For large displacements and small strains.
Updated	Not applicable.
Lagrangian	
Eulerian	Not applicable.
Co-rotational	Not applicable.

Integration Schemes

Stiffness Default. Fine (see *Options*). Mass Default. Fine (see *Options*). 1-point (BXM2), 2-point (BXM3). 2-point (BXM2).

1-point (BXM2), 2-point (BXM3). 2-point (BXM2).

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- **18** Invokes fine integration rule.
- **36** Follower loads (see *Notes*).
- 47 Use the X-axis as the axis of symmetry.
- 55 Output strains as well as stresses.

- 87 Total Lagrangian geometric nonlinearity.
- 105 Lumped mass matrix.
- 170 Suppress transfer of shape function arrays to disk

Notes on Use

- 1. The element formulation is based on the standard isoparametric approach.
- 2. The variation of stress along the element is constant for BXM2 and linear for BXM3.
- 3. To apply a non-conservative (follower) pressure load (load type FLD), Option 36 must be specified. Note that this load should be normal to the face and constant for all the nodes of the element. Follower load can only be used with BXM2 elements.
- 4. The elements should not be used as 'stand-alone' elements if any bending effects are present. The thin axisymmetric shell element BXS3 should be used for this case.
- 5. The BXM3 element has a zero energy mode which may be excited if the midside node is free and not connected to any other element.
- 6. When BXM2 elements are used with either variable nodal thicknesses, temperature dependent material properties or utilised in materially nonlinear analyses the 2-point Gauss rule is most effective.

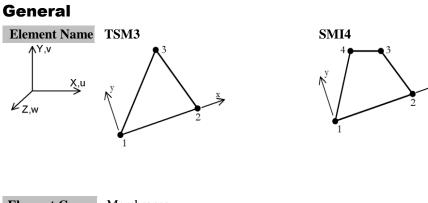
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Rubber material models can only be used with element BXM2 and must be used with Total Lagrangian geometric nonlinearity (Option 87).

Recommendations on Use

The elements may be used alone to model circular plates or pipes, or coupled with axisymmetric solid elements to provide stiffeners, e.g. radial reinforcement.

3D Space Membrane Elements



Element Group	Membranes
Element	Space Membranes
Subgroup	
Element	A family of space membrane elements in 3D which include a high
Description	performance incompatible model (SMI4 only). The elements are intended
	for 3D membrane structures (they possess no bending stiffness). The
	elements are formulated in the local element axes which allows
	directional material properties to be defined relative to the element
	orientation. The elements can accommodate varying thickness.
Number Of	3 or 4 numbered anticlockwise.
Nodes	
Freedoms	U, V, W: at each node.
Node	X, Y, Z: at each node.
Coordinates	

Geometric Properties

t1... tn Thickness at each node.

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES ORTHOTROPIC
		(Elastic: Orthotropic Plane Stress)
	Anisotropic:	MATERIAL PROPERTIES ANISOTROPIC 3
		(Elastic: Anisotropic Thin Plate)
	Rigidities:	RIGIDITIES 3 (Rigidities: Membrane/Thin
		Plate)

Matrix	Not applicable
Joint	Not applicable
Concrete	Not applicable
Elasto-Plastic	Not applicable
Creep	Not applicable
Damage	Not applicable
Viscoelastic	Not applicable
Shrinkage	

RubberNot applicableGeneric PolymerNot applicableCompositeNot applicable

SHRINKAGE CEB_FIP_90, EUROCODE_2, GENERAL, USER

Loading

Prescribed Value Concentrated Loads	,	Prescribed variable. U, V, W: at nodes. Concentrated loads. Px, Py, Pz: at nodes.
Element Loads	Not applicable.	
Distributed Loads	UDL	Uniformly distributed loads. Wx, Wy, Wz: local surface pressures for element.
	FLD, FLDG	Not applicable.
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Zcbf,
		$\Omega x, \Omega y, \Omega z, \alpha x, \alpha y, \alpha z$
	BFP, BFPE	Body force potentials at nodes/for element. φ_1 , φ_2 ,
X 7 - 1 * 4 *	VELO	φ ₃
Velocities		Velocities. Vx, Vy, Vz: at nodes.
Accelerations		Accelerations. Ax, Ay, Az: at nodes.
	SSI, SSIE	Initial stresses/strains at nodes/for element. Nx, Ny,
Stress/Strains		Nxy: forces in local directions. ε_x , ε_y , γ_{xy} : membrane strains in local directions.
	SSIG	Initial stresses/strains at Gauss points. Nx, Ny, Nxy:
		forces in local directions. ε_X , ε_y , γ_{XY} : membrane strains in local directions.
Residual Stresses	Not applicable.	
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. Nx, Ny, Nxy: forces in local directions. εx , εy , γxy :

	TSSIG	Target stresses/strains at Gauss points. Nx, Ny, Nxy:
		forces in local directions. ε_x , ε_y , γ_{xy} : membrane strains in local directions.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0, 0
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not	
Loads	applicable.	

Output

Solver Stress resultant: Nx, Ny, Nxy, Nmax, Nmin, β : forces/unit length in local directions. Stress (default): σx , σy , σxy , σmax , σmin , β : membrane stresses in local

Strain: ε_{x} , ε_{y} , γ_{xy} , ε_{max} , ε_{min} , β : membrane strains in local directions.

Modeller See Results Tables (Appendix K).

Local Axes

□ Standard area element

directions.

Sign Convention

□ Standard membrane element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Stiffness	Default.	1-point (TSM3), 2x2 (SMI4).
	Fine.	As default.
Mass	Default.	1-point (TSM3), 2x2 (SMI4).
	Fine.	As default.

Mass Modelling

Lumped mass only.

Options

- **32** Suppress stress output but not stress resultants.
- **34** Output stress resultants.
- 55 Output strains as well as stresses.
- **59** Output local direction cosines for elements.
- 77 Output averaged global stresses.

Notes on Use

- 1. The element formulations are based on the standard
- 2. The variation of stresses within an element may be regarded as constant for TSM3 and linear for SMI4.
- 3. The higher performance of SMI4 is due to the addition of 4 incompatible displacement modes.
- 4. The elements pass the <u>patch test</u> for mixed triangular and quadrilateral geometry.
- 5. Distributed loads are lumped at the nodes.
- 6. The element is formulated so that the material response is evaluated in the local Cartesian system.
- 7. The SMI4 element is generally the most effective element due to its quadratic displacement accuracy. However, its behaviour tends to deteriorate as the element become distorted.
- 8. The element matrices are formed using 1-point Gauss quadrature for TSM3. Selective integration is utilised for the evaluation of the element matrices for SMI4. The method used is similar to that proposed by Hughes, with the contribution of the incompatible modes to the strain-displacement matrix being evaluated at the 1-point Gauss rule sampling location and then extrapolated to the 2*2 Gauss rule sampling locations. The element matrices are then formed using the 2*2 Gauss rule.

Restrictions

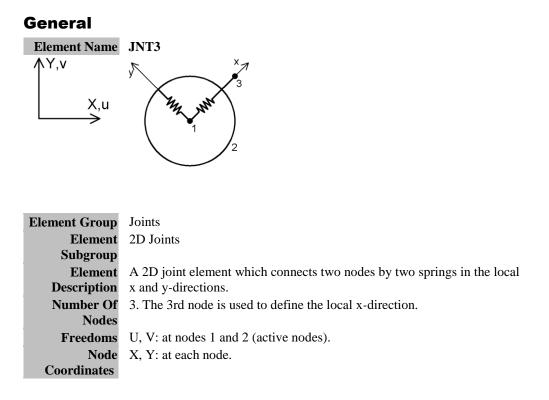
- □ Avoid excessive aspect ratio.
- □ Avoid excessive warping.

Recommendations on Use

- The space membrane elements have limited 'stand-alone' use because of their inability to support any loading except membrane loading. However, they can be utilised with the flat shell elements (QSI4, TS3) to model very thin membranes in structural components.
- If a structure is composed of exactly co-planar flat space membrane elements that are not stiffened by plate or shell elements, singularities may arise since there is no out-of-plane stiffness.
- If there is a possibility of bending behaviour then a thin shell should be utilised for the analysis.

Chapter 8 : Joint Elements.

2D Joint Element for Bars, Plane Stress and Plane Strain



Geometric Properties

Not applicable.

Material Properties

Linear	Not applicable	
Matrix	Stiffness:	MATRIX PROPERTIES STIFFNESS 4 K1,,
		K10 element stiffness matrix (Not supported in
		LUSAS Modeller)
	Mass:	MATRIX PROPERTIES MASS 4 M1,, M10
		element mass matrix (Not supported in
		LUSAS Modeller)
	Damping:	MATRIX PROPERTIES DAMPING 4 C1,,
		C10 element damping matrix (Not supported
		in LUSAS Modeller)

Joint	Standard:	JOINT PROPERTIES 2 (Joint: 2/Spring Stiffness Only)
	Dynamic general:	JOINT PROPERTIES GENERAL 2 (Joint: 2/General Properties)
	Elasto-plastic:	JOINT PROPERTIES NONLINEAR 31 2 (Joint: 2/Elasto-Plastic (Tension and Compression Equal))
	Elasto-plastic:	JOINT PROPERTIES NONLINEAR 32 2 (Joint: 2/Tension and Compression Unequal)
	Nonlinear contact:	JOINT PROPERTIES NONLINEAR 33 2 (Joint: 2/Smooth Contact)
	Nonlinear friction:	JOINT PROPERTIES NONLINEAR 44 2 (Joint: 2/Frictional Contact)
	Viscous damping:	JOINT PROPERTIES NONLINEAR 35 2 (Joint: 2/Viscous Damper)
	Lead-rubber:	JOINT PROPERTIES NONLINEAR 36 2 (Joint: 2/Lead Rubber Bearing)
	Friction pendulum:	JOINT PROPERTIES NONLINEAR 37 2 (Joint: 2/Frictional Pendulum System)
	Multi-linear elastic	JOINT PROPERTIES NONLINEAR 40 2 (Joint: 2/Multi-Linear Elastic)
	Multi-linear	JOINT PROPERTIES NONLINEAR 41 2
	hysteresis	(Joint: 2/Multi-Linear Hysteresis)
	Multi-linear	JOINT PROPERTIES NONLINEAR 42 2
	compound hysteresis	(Joint: 2/Multi-Linear Compound Hysteresis)
	Axial force	JOINT PROPERTIES NONLINEAR 43 2
	dependent multi- linear elastic	(Joint: 2/Axial Force Dependent Multi-Linear Elastic)
Concrete	Not applicable	
Elasto-Plastic	Not applicable	
Creep	Not applicable	
Damage	Not applicable	
Viscoelastic	Not applicable	
Shrinkage	Not applicable	
Rubber	Not applicable	
Generic Polymer	Not applicable	
Composite	Not applicable	

Loading

Prescribed Value PDSP, TPDSP Prescribed var

Prescribed variable. U, V: at active nodes.

Concentrated Loads	CL	Concentrated loads. Px, Py: at active nodes.
Element Loads	Not applicable.	
Distributed Loads	Not	
Body Forces	applicable. CBF	Constant body forces for element. Xcbf, Ycbf, Ωx , Ωy , Ωz , αz
	BFP, BFPE	Not applicable.
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Accelerations. Ax, Ay: at nodes.
Initial Stress/Strains	SSI, SSIE	Initial stresses/strains at nodes/for element. Fx, Fy: at active nodes. Ex, Ey: at active nodes.
	SSIG	Not applicable.
Residual Stresses	Not applicable.	
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. Fx, Fy: at active nodes. Ex, Ey: at active nodes.
	TSSIG	Not applicable.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T1, T2, T10, T20: actual and initial spring temperatures.
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent Loads		

LUSAS Output

Solver	Force: Fx, Fy: spring forces in local directions.
	Strain: Ex, Ey: spring strains in local directions.
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

□ Standard joint element

Sign Convention

Standard joint element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Stiffness	Default.	1-point.
	Fine.	As default.
Mass	Default.	1-point.
	Fine.	As default.

Mass Modelling

Lumped mass only. The position of the mass relative to the two active joint nodes is defined in the joint material data. Point mass elements should be used to model lumped masses when no stiffness modelling is required.

Options

- 55 Output strains as well as stresses.
- **119** Invokes temperature input for joints.

Notes on Use

See Joint Element Compatibility and Notes (Appendix L).

Restrictions

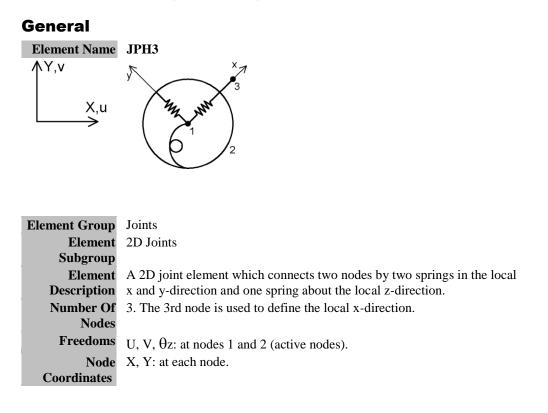
Not applicable.

Recommendations on Use

• The joint elements may be used to release degrees of freedom between elements, e.g. a hinged shell, or to provide nonlinear support conditions, e.g. friction-gap condition. Also, point masses may be represented by including a joint at an element node.

• See Joint Element Compatibility (Appendix L)

2D Joint Element for Engineering and Kirchhoff Beams



Geometric Properties

ey Eccentricity measured from the joint x axis to the nodal line (i.e. parallel to the joint y axis).

dy Parametric distance factor (between 0.0 and 1.0), which defines the position of the shear spring for the local y direction between nodes 1 and 2. It is measured from node 1 (dy=0) along the local x direction

Material Properties

Linear	Not applicable	
Matrix	Stiffness:	MATRIX PROPERTIES STIFFNESS 6 K1,, K21
		element stiffness matrix (Not supported in LUSAS
		Modeller)
	Mass:	MATRIX PROPERTIES MASS 6 M1,, M21
		element mass matrix (Not supported in LUSAS

		Modeller)
	Damping:	MATRIX PROPERTIES DAMPING 6 C1,, C21 element damping matrix (Not supported in LUSAS Modeller)
Joint	Standard:	JOINT PROPERTIES 3 (Joint: 3/Spring Stiffness Only)
	Dynamic general:	JOINT PROPERTIES GENERAL 3 (Joint: 3/General Properties)
	Elasto-plastic:	JOINT PROPERTIES NONLINEAR 31 3 (Joint: 3/Elasto-Plastic (Tension and Compression Equal))
	Elasto-plastic:	JOINT PROPERTIES NONLINEAR 32 3 (Joint: 3/Tension and Compression Unequal)
	Nonlinear contact:	JOINT PROPERTIES NONLINEAR 33 3 (Joint: 3/Smooth Contact)
	Nonlinear friction:	JOINT PROPERTIES NONLINEAR 44 3 (Joint: 3/Frictional Contact)
	Viscous damping:	JOINT PROPERTIES NONLINEAR 35 3 (Joint: 3/Viscous Damper)
	Lead-rubber:	JOINT PROPERTIES NONLINEAR 36 3 (Joint: 3/Lead Rubber Bearing)
	Friction pendulum:	JOINT PROPERTIES NONLINEAR 37 3 (Joint: 3/Frictional Pendulum System)
	Multi-linear elastic	JOINT PROPERTIES NONLINEAR 40 3 (Joint: 3/Multi-Linear Elastic)
	Multi-linear hysteresis	JOINT PROPERTIES NONLINEAR 41 3 (Joint: 3/Multi-Linear Hysteresis)
	Multi-linear compound	JOINT PROPERTIES NONLINEAR 42 3 (Joint: 3/Multi-Linear Compound Hysteresis)
	hysteresis Axial force	JOINT PROPERTIES NONLINEAR 43 3 (Joint:
	dependent multi-linear	3/Axial Force Dependent Multi-Linear Elastic)
Joint	elastic Standard:	JOINT PROPERTIES 3 (Joint: 3/Spring Stiffness Only)
	Dynamic general:	JOINT PROPERTIES GENERAL 3 (Joint: 3/General Properties)
Concrete	Not applicable	5, Conorar Proportios)
Elasto-Plastic	Not applicable	
Creep	Not applicable	
Damage	Not applicable	
Viscoelastic	Not applicable	
Shrinkage	Not applicable	

RubberNot applicableGeneric PolymerNot applicableCompositeNot applicable

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, θ z: at active nodes.
Concentrated Loads	CL	Concentrated loads. Px, Py, Mz: at active nodes.
Element Loads	Not applicable	
Distributed Loads		
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Ωx ,
		$\Omega_y, \Omega_z, \alpha_z$
	BFP, BFPE	Not applicable.
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Accelerations. Ax, Ay: at nodes.
	SSI, SSIE	Initial stresses/strains at nodes/for element.
Stress/Strains		Resultants. Fx, Fy, Mz: spring forces and moment
		in local directions. Ex, Ey, ψz : strains at nodes.
	SSIG	Not applicable.
Residual Stresses		
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. Resultants. Fx, Fy, Mz: spring forces and moment
		in local directions. Ex, Ey, ψz : strains at nodes.
	TSSIG	Not applicable.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T1, T2, T3, T10, T20, T30: actual and initial spring temperatures.
Overburden		
	applicable.	
Phreatic Surface	Not	
E , 111 1	applicable.	
Field Loads	Not applicable	
Temp Dependent Loads	Not applicable	

LUSAS Output

SolverForce: Fx, Fy, Mz: spring forces and moment in local directions.Strain: εx, εy, ψz: spring strains in local directions.ModellerSee Results Tables (Appendix K).

Local Axes

□ Standard joint element

Sign Convention

□ Standard joint element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Stiffness	Default.	1-point.
	Fine.	As default.
Mass	Default.	1-point.
	Fine.	As default.

Mass Modelling

Lumped mass only. The position of the mass relative to the two active joint nodes is defined in the joint material data. Point mass elements should be used to model lumped masses when no stiffness modelling is required.

Options

- 55 Output strains as well as stresses.
- **119** Invokes temperature input for joints.

Notes on Use

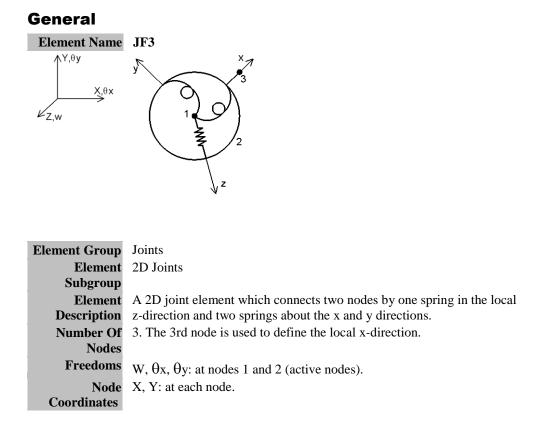
See Joint Element Compatibility and Notes (Appendix L).

Restrictions

Not applicable.

- The joint elements may be used to release degrees of freedom between elements, e.g. a hinged shell, or to provide nonlinear support conditions, e.g. friction-gap condition. Also, point masses may be represented by including a joint at an element node.
- See <u>Joint Element Compatibility (Appendix L)</u>

2D Joint Element for Grillage Beams and Plates



Geometric Properties

dz Parametric distance factor (between 0.0 and 1.0), which defines the position of the shear spring for the local z direction between nodes 1 and 2. It is measured from node 1 (dz=0) along the local x direction.

Linear	Not applicable	
Matrix	Stiffness:	MATRIX PROPERTIES STIFFNESS 6 K1,,
		K21 element stiffness matrix (Not supported
		in LUSAS Modeller)
	Mass:	MATRIX PROPERTIES MASS 6 M1,, M21
		element mass matrix (Not supported in

		LUSAS Modeller)
	Damping:	MATRIX PROPERTIES DAMPING 6 C1,,
		C21 element damping matrix (Not supported
		in LUSAS Modeller)
Joint	Standard:	JOINT PROPERTIES 3 (Joint: 3/Spring
		Stiffness Only)
	Dynamic general:	JOINT PROPERTIES GENERAL 3 (Joint:
	Electo plastic	3/General Properties) JOINT PROPERTIES NONLINEAR 31 3
	Elasto-plastic:	(Joint: 3/Elasto-Plastic (Tension and
		Compression Equal))
	Elasto-plastic:	JOINT PROPERTIES NONLINEAR 32 3
	I	(Joint: 3/Tension and Compression Unequal)
	Nonlinear contact:	JOINT PROPERTIES NONLINEAR 33 3
		(Joint: 3/Smooth Contact)
	Nonlinear friction:	Not applicable
	Viscous damping:	JOINT PROPERTIES NONLINEAR 35 3
		(Joint: 3/Viscous Damper)
	Lead-rubber:	Not applicable
	Friction pendulum:	Not applicable
	Multi-linear elastic	JOINT PROPERTIES NONLINEAR 40 3
	Multi-linear	(Joint: 3/Multi-Linear Elastic) JOINT PROPERTIES NONLINEAR 41 3
	hysteresis	(Joint: 3/Multi-Linear Hysteresis)
	Multi-linear	JOINT PROPERTIES NONLINEAR 42 3
	compound	(Joint: 3/Multi-Linear Compound Hysteresis)
	hysteresis	
	Axial force	JOINT PROPERTIES NONLINEAR 43 3
	dependent multi-	(Joint: 3/Axial Force Dependent Multi-Linear
~	linear elastic	Elastic)
Concrete	Not applicable	
Elasto-Plastic	Not applicable	
Creep	Not applicable	
Damage	Not applicable	
Viscoelastic	Not applicable.	
Shrinkage	Not applicable	
Rubber	Not applicable	
Generic Polymer	Not applicable	
Composite	Not applicable	

Loading

Prescribed Value	PDSP. TPDSP	Prescribed variable. ω , θx , θy : at active nodes.
Concentrated	,	Concentrated loads. Pz, Mx, My: at active
Loads	CL	nodes.
Element Loads	Not applicable	
Distributed Loads		
Body Forces		Constant body forces for element. Zcbf
2009 201005	BFP, BFPE	Not applicable.
Velocities		Velocities. Vz: at nodes.
Accelerations	ACCE	Accelerations. Az: at nodes.
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element. Fz,
Stress/Strains	,	Mx, My: at active nodes. εz , ψx , ψy : at active nodes.
	SSIG	Not applicable.
Residual Stresses	Not applicable	
Target	TSSIE, TSSIA	Target stresses/strains at nodes/for element. Fz,
Stress/Strains		Mx, My: at active nodes. εz , ψx , ψy : at active nodes.
	TSSIG	Not applicable.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T1, T2, T3, T10, T20, T30: actual and initial spring temperatures.
Overburden	Not applicable.	I manual second
Phreatic Surface		
	Not applicable	
Temp Dependent	Not applicable	

Loads

LUSAS Output

Solver	Force: Pz, Mx, My: spring forces in local directions.
	Strain: εz , ψx , ψy : spring strains in local directions.
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

□ Standard joint element

Sign Convention

□ Standard joint element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Stiffness	Default.	1-point.
	Fine.	As default.
Mass	Default.	1-point.
	Fine.	As default.

Mass Modelling

Lumped mass only. The position of the mass relative to the two active joint nodes is defined in the joint material data. Point mass elements should be used to model lumped masses when no stiffness modelling is required.

Options

- **55** Output strains as well as stresses.
- **119** Invokes temperature input for joints.

Notes on Use

See Joint Element Compatibility and Notes (Appendix L).

Restrictions

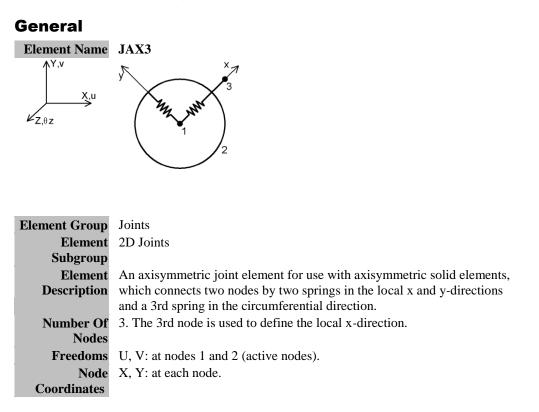
Not applicable.

Recommendations on Use

• The joint elements may be used to release degrees of freedom between elements, e.g. a hinged shell, or to provide nonlinear support conditions, e.g. friction-gap condition. Also, point masses may be represented by including a joint at an element node.

• See Joint Element Compatibility (Appendix L)

2D Joint Element for Axisymmetric Solids



Geometric Properties

Not applicable.

Linear	Not applicable	
Matrix	Stiffness:	MATRIX PROPERTIES STIFFNESS 6 K1,, K10 element stiffness matrix (Not supported in LUSAS Modeller)
	Mass:	MATRIX PROPERTIES MASS 6 M1,, M10 element mass matrix (Not supported in LUSAS Modeller)
	Damping:	MATRIX PROPERTIES DAMPING 6 C1,, C10 element damping matrix (Not supported in LUSAS Modeller)

Joint	Standard:	JOINT PROPERTIES 2 (Joint: 2/Spring
	Dynamic general:	Stiffness Only) (See notes on use) JOINT PROPERTIES GENERAL 2 (Joint:
	Dynamie general.	2/General Properties) (See notes on use)
	Elasto-plastic:	JOINT PROPERTIES NONLINEAR 31 2
	1	(Joint: 2/Elasto-Plastic (Tension and
		Compression Equal)) (See notes on use)
	Elasto-plastic:	JOINT PROPERTIES NONLINEAR 32 2
		(Joint: 2/Tension and Compression Unequal) (See notes on use)
	Nonlinear contact:	JOINT PROPERTIES NONLINEAR 33 2
		(Joint: 2/Smooth Contact) (See notes on use)
	Nonlinear friction:	JOINT PROPERTIES NONLINEAR 44 2
		(Joint: 2/Frictional Contact) (See notes on use)
	Viscous damping:	JOINT PROPERTIES NONLINEAR 35 2
	Lead-rubber:	(Joint: 2/Viscous Damper) (See notes on use) JOINT PROPERTIES NONLINEAR 36 2
	Lead-rubber:	(Joint: 2/Lead Rubber Bearing) (See notes on
		use)
	Friction pendulum:	JOINT PROPERTIES NONLINEAR 37 2
		(Joint: 2/Frictional Pendulum System) (See
	Multi-linear elastic	notes on use) JOINT PROPERTIES NONLINEAR 40 2
	Multi-Intear elastic	(Joint: 2/Multi-Linear Elastic)
	Multi-linear	JOINT PROPERTIES NONLINEAR 41 2
	hysteresis	(Joint: 2/Multi-Linear Hysteresis)
	Multi-linear	JOINT PROPERTIES NONLINEAR 42 2
	compound	(Joint: 2/Multi-Linear Compound Hysteresis)
	hysteresis	
	Axial force dependent multi-	JOINT PROPERTIES NONLINEAR 43 2 (Joint: 2/Axial Force Dependent Multi-Linear
	linear elastic	Elastic)
Concrete	Not applicable	Liuste)
Elasto-Plastic	Not applicable	
Creep	Not applicable	
Damage	Not applicable	
Viscoelastic	Not applicable	
Shrinkage	Not applicable	
Rubber	Not applicable	
Generic Polymer	Not applicable	
Composite	Not applicable	

Loading

LoadsNot applicable.Distributed LoadsNot applicable.Distributed LoadsNot applicable.Body ForcesCBFConstant body forces for element. Xcbf, Ycbf, Ωx, Ωy, Ωz, αzBody ForcesBFP, BFPENot applicable.VelocitiesSERVelocities. Vx, Vy: at nodes.AccelerationsACCEAccelerations. Ax, Ay: at nodes.Stress/StrainsSISIEInitial stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions. Ex, £y: spring strains in local directions.Residual StressesNot applicable.Stress/StrainsSISIGNot applicable.Stress/StrainsTSSIE, TSSIATarget stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions. Ex, £y: spring strains in local directions.Stress/StrainsNot applicable.TargetTSSIG, Not applicable.TemperaturesTSSIGNot applicable.TemperaturesTSSIGNot applicable.TemperaturesTSSIGNot applicable.TemperaturesTot applicable.TemperaturesNot applicable.Fleid LoadsNot applicable.Field LoadsNot applicable.	Prescribed Value Concentrated		Prescribed variable. U, V: at active nodes. Concentrated loads. Px, Py: at active nodes.
pistributed Loadsapplicable.Not applicable.CBFConstant body forces for element. Xcbf, Ycbf, Ωx, Ωy, Ωz, αzBG0y ForceCBFNot applicable.VelocitiesNot applicable.VelocitiesVELOVelocities. Vx, Vy: at nodes.AccelerationsACCEAccelerations. Ax, Ay: at nodes.Stress/StrainsSSI, SSIEInitial stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions. £x, £y: spring strains in local directions.Residual StressesNot applicable.TargetTSSIE, TSSIATarget stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions.Stress/StrainsTSSIE, TSSIATarget stresses/strains at nodes/for element. Fx, Fy: 			Concontinued Touris, TA, TY, at active nodes.
Distributed LoadsNot applicable.Body ForcesCBFConstant body forces for element. Xcbf, Ycbf, Ωx, Ωy, Ωz, αzBFP, BFPENot applicable.VelocitiesBFP, BFPENot applicable.VelocitiesXX, Vy: at nodes.AccelerationsACCEAccelerations. Ax, Ay: at nodes.Initial Stress/StrainsSSI SSIEInitial stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions. £x, £y: spring strains in local directions.Residual StressesSSIGNot applicable.Target Stress/StrainsTSSIE, TSSIATarget stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions.TemperaturesTSSIGNot applicable.TemperaturesNot applicable.Not applicable.Phreatic SurfaceNot applicable.Temperatures at nodes/for element. T1, T2, T10, T20: actual and initial spring temperatures.Phreatic SurfaceNot applicable.Not applicable.Field LoadsNot applicable.Not applicable.	Element Loads		
$\begin{array}{c} \textbf{Locy Forest} & \textbf{Locy Forest} & Constant body forces for element. Active predictions of element. Fx, Fy: spring forces in local directions. State predictions of element. Fx, Fy: spring forces in local directions. Ex, Ey: spring strains in local directions. Ex, Ey: spring strains in local directions. Ex, Ey: spring strains in local directions. TSSIG Not applicable. Temperatures at nodes/for element. T1, T2, T10, T20: actual and initial spring temperatures. Overburden Not applicable. Field Loads Not applicable. Field Loads Not applicable.$	Distributed Loads	Not	
Ωy, Ωz, αzBFP, BFPENot applicable.VelocitiesVELOVELOVelocities. Vx, Vy: at nodes.AccelerationsACCEAccelerationsACCEStress/StrainsSSI, SSIEInitialSSI, SSIEStress/StrainsInitial stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions. Ex, Ey: spring strains in local directions.Residual StressesNot applicable.TargetTSSIE, TSSIATargetTarget stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions. Ex, Ey: spring strains in local directions.Stress/StrainsTarget stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions.TargetTSSIE, TSSIATarget stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions.TemperaturesTEMP, TMPETemperaturesTemperatures at nodes/for element. T1, T2, T10, T20: actual and initial spring temperatures.OverburdenNot applicable.Phreatic SurfaceNot applicable.Field LoadsNot applicable.	Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Ωx ,
VelocitiesBFP, BFPENot applicable.VelocitiesVELOVelocities. Vx, Vy: at nodes.AccelerationsACCEAccelerations. Ax, Ay: at nodes.InitialSSI, SSIEInitial stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions. £x, £y: spring strains in local directions.Stress/StrainsSSIGNot applicable.Residual StressesNot applicable.Target stress/StrainsTargetTSSIE, TSSIATarget stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions. £x, £y: spring strains in local directions.Stress/StrainsTSSIE, TSSIATarget stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions. £x, £y: spring strains in local directions.TemperaturesTSSIGNot applicable.TemperaturesTEMP, TMPETemperatures at nodes/for element. T1, T2, T10, T20: actual and initial spring temperatures.OverburdenNot applicable.Temperatures at nodes/for element. T1, T2, T10, T20: actual and initial spring temperatures.Phreatic SurfaceNot applicable.Image: Lamping temperatures.Field LoadsNot applicable.Image: Lamping temperatures			-
VelocitiesVELOVelocities. Vx, Vy: at nodes.AccelerationsACCEAccelerations. Ax, Ay: at nodesInitialSSI, SSIEInitial stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions. Ex, Ey: spring strains in local directions.Stress/StrainsSSIGNot applicable.TargetTSSIE, TSSIATarget stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions. Ex, Ey: spring strains in local directions.Stress/StrainsTSSIE, TSSIATarget stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions.TemperaturesTSSIGNot applicable.TemperaturesTEMP, TMPETemperatures at nodes/for element. T1, T2, T10, T20: actual and initial spring temperatures.OverburdenNot applicable.Temperatures.Phreatic SurfaceNot applicable.Not applicable.Field LoadsNot applicable.Not applicable.		BFP, BFPE	
AccelerationsACCEAccelerations. Ax, Ay: at nodesInitial Stress/StrainsSSI, SSIEInitial stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions. Ex, Ey: spring strains in local directions.Residual StressesSSIGNot applicable.Target Stress/StrainsTSSIE, TSSIATarget stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions. Ex, Ey: spring strains in local directions.Target Stress/StrainsTSSIE, TSSIATarget stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions.TemperaturesTSSIGNot applicable.TemperaturesTEMP, TMPETemperatures at nodes/for element. T1, T2, T10, T20: actual and initial spring temperatures.Overburden applicable.Not applicable.Not applicable.Phreatic Surface Field LoadsNot applicable.Imitial spring temperaturesNot applicable.Not applicable.Imitial spring temperatures	Velocities	VELO	
Stress/Strainsspring forces in local directions. Ex, Ey: spring strains in local directions.Residual StressesSSIGNot applicable.TargetNot applicable.Target stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions. Ex, Ey: spring strains in local directions.Stress/StrainsTSSIGNot applicable.TemperaturesTSSIGNot applicable.OverburdenNot applicable.Temperatures at nodes/for element. T1, T2, T10, T20: actual and initial spring temperatures.OverburdenNot applicable.Temperatures at nodes/for element. T1, T2, T10, T20: actual and initial spring temperatures.Phreatic SurfaceNot applicable.Hot applicable.Field LoadsNot applicable.Not applicable.	Accelerations	ACCE	
Solution of the second secon	Initial	SSI, SSIE	Initial stresses/strains at nodes/for element. Fx, Fy:
Residual StressesNot applicable.Target Stress/StrainsNot TSSIE, TSSIATarget stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions. Ex, Ey: spring strains in local directions.Stress/StrainsTSSIGNot applicable.TemperaturesTEMP, TMPETemperatures at nodes/for element. T1, T2, T10, T20: actual and initial spring temperatures.OverburdenNot applicable.Phreatic SurfaceNot applicable.Field LoadsNot applicable.	Stress/Strains		
Target Stress/Strainsapplicable. TSSIE, TSSIATarget stresses/strains at nodes/for element. Fx, Fy: spring forces in local directions. Ex, Ey: spring strains in local directions.Stress/StrainsTSSIGNot applicable.TemperaturesTEMP, TMPETemperatures at nodes/for element. T1, T2, T10, T20: actual and initial spring temperatures.OverburdenNot applicable.Not applicable.Field LoadsNot applicable.Not applicable.		SSIG	Not applicable.
Stress/Strainsspring forces in local directions. Ex, Ey: spring strains in local directions.TemperaturesTSSIGNot applicable.TemperaturesTEMP, TMPETemperatures at nodes/for element. T1, T2, T10, T20: actual and initial spring temperatures.OverburdenNot applicable.Phreatic SurfaceNot applicable.Field LoadsNot applicable.	Residual Stresses		
Temperatures TSSIG Not applicable. Temperatures TEMP, TMPE Temperatures at nodes/for element. T1, T2, T10, T20: actual and initial spring temperatures. Overburden Not applicable. Phreatic Surface Not applicable. Field Loads Not applicable.		TSSIE, TSSIA	Target stresses/strains at nodes/for element. Fx, Fy:
Temperatures TEMP, TMPE Temperatures at nodes/for element. T1, T2, T10, T20: actual and initial spring temperatures. Overburden Not applicable. Phreatic Surface Not applicable. Field Loads Not applicable.	Stress/Strains		
actual and initial spring temperatures. Overburden Not applicable. Phreatic Surface Not applicable. Field Loads Not applicable.		TSSIG	Not applicable.
applicable. Phreatic Surface Not applicable. Field Loads Not applicable.	Temperatures	TEMP, TMPE	•
Phreatic Surface Not applicable. Field Loads Not applicable.	Overburden		
applicable. Field Loads Not applicable.			
applicable.	Phreatic Surface		
Temp Dependent Not	Field Loads		
Loads applicable.	1 1	Not applicable.	

LUSAS Output

Solver	Force: Fx, Fy, Fz: spring forces in local directions.
	Strain: Ex, Ey, Ez: spring strains in local directions.

Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

□ Standard joint element

Sign Convention

□ Standard joint element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Stiffness	Default.	1-point.
	Fine.	As default.
Mass	Default.	1-point.
	Fine.	As default.

Mass Modelling

Lumped mass only. The position of the mass relative to the two active joint nodes is defined in the joint material data. Point mass elements should be used to model lumped masses when no stiffness modelling is required.

Options

- 47 X-axis taken as axis of symmetry.
- **55** Output strains as well as stresses.
- **119** Invokes temperature input for joints.

Notes on Use

- This joint has only two degrees of freedom but requires 3 inputs. The 3rd input required is the circumferential stiffness.
- For problems where the circumferential forces are to be transmitted by adjacent elements the circumferential stiffness should be input as zero.

• This element cannot be used with axisymmetric Fourier elements.

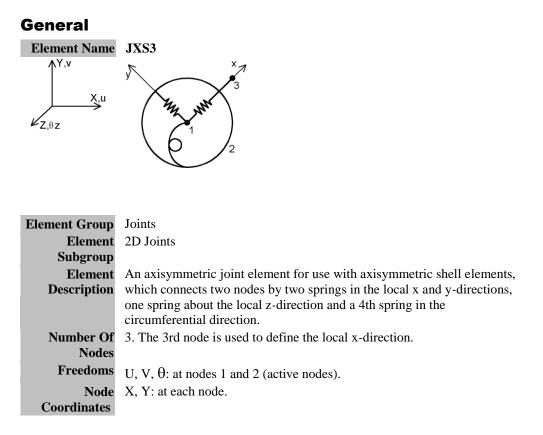
See Joint Element Compatibility and Notes (Appendix L).

Restrictions

Not applicable.

- The joint elements may be used to release degrees of freedom between elements, e.g. a hinged shell, or to provide nonlinear support conditions, e.g. friction-gap condition. Also, point masses may be represented by including a joint at an element node.
- See Joint Element Compatibility (Appendix L)

2D Joint Element for Axisymmetric Shells



Geometric Properties

dy Parametric distance factor (between 0.0 and 1.0), which defines the position of the shear spring for the local y direction between nodes 1 and 2. It is measured from node 1 (dy=0) along the local x direction.

Linear	Not applicable	
Matrix	Stiffness:	MATRIX PROPERTIES STIFFNESS 8 K1,, K21 element stiffness matrix (Not supported in LUSAS Modeller)
	Mass:	MATRIX PROPERTIES MASS 8 M1,, M21

		element mass matrix (Not supported in LUSAS Modeller)
	Damping:	MATRIX PROPERTIES DAMPING 8 C1,, C21 element damping matrix (Not supported in LUSAS Modeller)
Joint	Standard:	JOINT PROPERTIES 3 (Joint: 3/Spring Stiffness Only) (See notes on use)
	Dynamic general:	JOINT PROPERTIES GENERAL 3 (Joint: 3/General Properties) (See notes on use)
	Elasto-plastic:	JOINT PROPERTIES NONLINEAR 31 3 (Joint: 3/Elasto-Plastic (Tension and Compression Equal)) (See notes on use)
	Elasto-plastic:	JOINT PROPERTIES NONLINEAR 32 3 (Joint: 3/Tension and Compression Unequal) (See notes on use)
	Nonlinear contact:	JOINT PROPERTIES NONLINEAR 33 3 (Joint: 3/Smooth Contact) (See notes on use)
	Nonlinear friction:	JOINT PROPERTIES NONLINEAR 44 3 (Joint: 3/Frictional Contact) (See notes on use)
	Viscous damping:	JOINT PROPERTIES NONLINEAR 35 3 (Joint: 3/Viscous Damper) (See notes on use)
	Lead-rubber:	JOINT PROPERTIES NONLINEAR 36 3 (Joint:3/Lead Rubber Bearing) (See notes on use)
	Friction pendulum:	JOINT PROPERTIES NONLINEAR 37 3 (Joint: 3/Frictional Pendulum System) (See notes on use)
	Multi-linear elastic	JOINT PROPERTIES NONLINEAR 40 3 (Joint: 3/Multi-Linear Elastic)
	Multi-linear	JOINT PROPERTIES NONLINEAR 41 3 (Joint:
	hysteresis	3/Multi-Linear Hysteresis)
	Multi-linear compound	JOINT PROPERTIES NONLINEAR 42 3 (Joint: 3/Multi-Linear Compound Hysteresis)
	hysteresis	
	Axial force	JOINT PROPERTIES NONLINEAR 43 3 (Joint:
	dependent multi- linear elastic	3/Axial Force Dependent Multi-Linear Elastic)
Concrete	Not applicable	
	Not applicable	
Creep	Not applicable	
-	Not applicable	
Viscoelastic	Not applicable	
-	Not applicable	
Rubber	Not applicable	

Generic PolymerNot applicableCompositeNot applicable

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, θ : at active nodes.
Concentrated	CL	Concentrated loads. Px, Py, M: at active nodes.
Loads		
Element Loads		
	applicable.	
Distributed Loads	Not	
D 1 D	applicable.	
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Ωx ,
		Ω y, Ω z, α z
	BFP, BFPE	Not applicable.
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Accelerations. Ax, Ay: at nodes.
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element. Fx, Fy:
Stress/Strains		spring forces in local directions. Ex, Ey: spring
		strains in local directions.
	SSIG	Not applicable.
Residual Stresses	Not	
	applicable.	
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. Fx, Fy:
Stress/Strains		spring forces in local directions. Ex, Ey: spring strains in local directions.
	TSSIG	Not applicable.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T1, T2, T3, T10,
		T20, T30: actual and initial spring temperatures.
Overburden		
	applicable.	
Phreatic Surface	Not	
	applicable.	
Field Loads	Not	
	applicable.	
Temp Dependent Loads		

LUSAS Output

SolverForce: Fx, Fy, Fz,M: spring forces in local directions.Strain: εx , εy , εz , ψz : spring strains in local directions.ModellerSee Results Tables (Appendix K).

Local Axes

□ Standard joint element

Sign Convention

□ Standard joint element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Stiffness	Default.	1-point.
	Fine.	As default.
Mass	Default.	1-point.
	Fine.	As default.

Mass Modelling

Lumped mass only. The position of the mass relative to the two active joint nodes is defined in the joint material data. Point mass elements should be used to model lumped masses when no stiffness modelling is required.

Options

- 47 X-axis taken as axis of symmetry.
- 55 Output strains as well as stresses.
- **119** Invokes temperature input for joints.

Notes on Use

This joint has only three degrees of freedom but requires 4 inputs. The 4th input required is the circumferential stiffness.

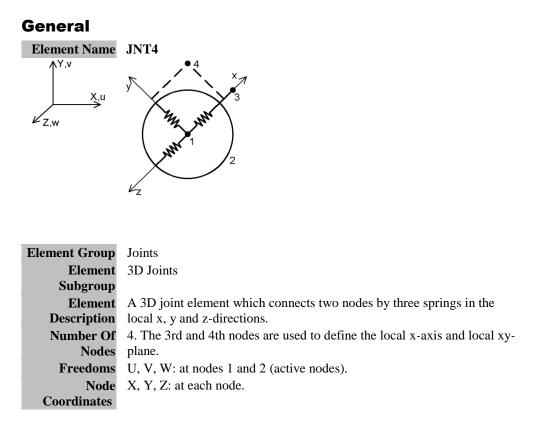
See Joint Element Compatibility and Notes (Appendix L).

Restrictions

Not applicable.

- The joint elements may be used to release degrees of freedom between elements, e.g. a hinged shell, or to provide nonlinear support conditions, e.g. friction-gap condition. Also, point masses may be represented by including a joint at an element node.
- See Joint Element Compatibility (Appendix L)

3D Joints for Bars, Solids and Space Membranes



Geometric Properties

Not applicable.

Linear	Not applicable	
Matrix	Stiffness:	MATRIX PROPERTIES STIFFNESS 6 K1,, K21 element stiffness matrix (Not supported in LUSAS Modeller)
	Mass:	MATRIX PROPERTIES MASS 6 M1,, M21 element mass matrix (Not supported in LUSAS Modeller)
	Damping:	MATRIX PROPERTIES DAMPING 6 C1,, C21 element damping matrix (Not supported

		in LUSAS Modeller)
Joint	Standard:	JOINT PROPERTIES 3 (Joint: 3/Spring Stiffness Only)
	Dynamic general:	JOINT PROPERTIES GENERAL 3 (Joint:
		3/General Properties)
	Elasto-plastic:	JOINT PROPERTIES NONLINEAR 31 3 (Joint: 3/Elasto-Plastic (Tension and Compression Equal))
	Elasto-plastic:	JOINT PROPERTIES NONLINEAR 32 3 (Joint: 3/Tension and Compression Unequal)
	Nonlinear contact:	JOINT PROPERTIES NONLINEAR 33 3 (Joint: 3/Smooth Contact)
	Nonlinear friction:	JOINT PROPERTIES NONLINEAR 44 3 (Joint: 3/Frictional Contact)
	Viscous damping:	JOINT PROPERTIES NONLINEAR 35 3 (Joint: 3/Viscous Damper)
	Lead-rubber:	JOINT PROPERTIES NONLINEAR 36 3 (Joint: 3/Lead Rubber Bearing)
	Friction pendulum:	JOINT PROPERTIES NONLINEAR 37 3 (Joint: 3/Frictional Pendulum System)
	Multi-linear elastic	JOINT PROPERTIES NONLINEAR 40 3 (Joint: 3/Multi-Linear Elastic)
	Multi-linear	JOINT PROPERTIES NONLINEAR 41 3
	hysteresis	(Joint: 3/Multi-Linear Hysteresis)
	Multi-linear	JOINT PROPERTIES NONLINEAR 42 3
	compound hysteresis	(Joint: 3/Multi-Linear Compound Hysteresis)
	Axial force	JOINT PROPERTIES NONLINEAR 43 3
	dependent multi-	(Joint: 3/Axial Force Dependent Multi-Linear
	linear elastic	Elastic)
Concrete	Not applicable	
Elasto-Plastic	Not applicable	
Creep	Not applicable	
Damage	Not applicable	
Viscoelastic	Not applicable	
Shrinkage	Not applicable	
Rubber	Not applicable	
Generic Polymer	Not applicable	
Composite	Not applicable	

Loading

Prescribed Value		Prescribed variable. U, V, W: at active nodes.
Concentrated Loads	CL	Concentrated loads. Px, Py, Pz: at active nodes.
	N-4	
Element Loads		
	applicable.	
Distributed Loads	Not	
D - J E	applicable.	Constant hade former for element Vehf Vehf Zehf
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Zcbf,
		$\Omega_{x}, \Omega_{y}, \Omega_{z}, \alpha_{x}, \alpha_{y}, \alpha_{z}$
	BFP, BFPE	Not applicable.
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Accelerations. Ax, Ay, Az: at nodes.
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element. Fx, Fy,
Stress/Strains		Fz: spring forces in local directions. ε_x , ε_y , ψ_z :
		spring strains in local directions.
	SSIG	Not applicable.
Residual Stresses	Not	
	applicable.	
Target	TSSIE, TSSIA	Target initial stresses/strains at nodes/for element.
Stress/Strains		Fx, Fy, Fz: spring forces in local directions. Ex,
		$\varepsilon_{y}, \forall z$: spring strains in local directions.
	TSSIG	Not applicable.
T oma on 4		* *
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T1, T2, T3, T10, T20, T30: actual and initial spring temperatures.
Overburden	Not	120, 130. actual and initial spring temperatures.
Overburuen	applicable.	
Phreatic Surface	Not	
Phreatic Surface	applicable.	
Field Loads		
rielu Loaus	applicable.	
Tomn Donondont		
Temp Dependent	applicable.	
Loaus	applicable.	

LUSAS Output

SolverForce: Fx, Fy, Fz: spring forces in local directions.Strain: εx, εy, εz: spring strains in local directions.

Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

□ Standard joint element

Sign Convention

□ Standard joint element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Stiffness Default.	1-point.
Fine.	As default.
Mass Default.	1-point.
Fine	As default.

Mass Modelling

Lumped mass only. The position of the mass relative to the two active joint nodes is defined in the joint material data. Point mass elements should be used to model lumped masses when no stiffness modelling is required.

Options

- 55 Output strains as well as stresses.
- **119** Invokes temperature input for joints.

Notes on Use

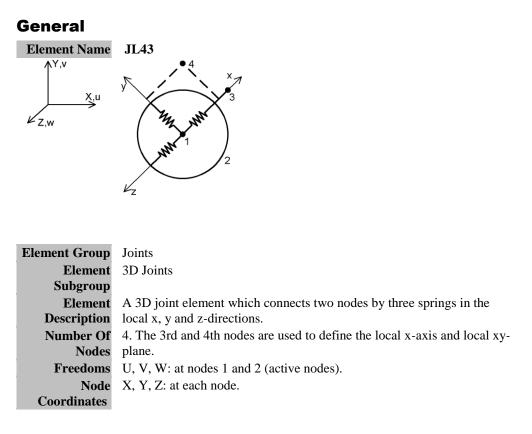
See Joint Element Compatibility and Notes (Appendix L).

Restrictions

Not applicable.

- The joint elements may be used to release degrees of freedom between elements, e.g. a hinged shell, or to provide nonlinear support conditions, e.g. friction-gap condition. Also, point masses may be represented by including a joint at an element node.
- See <u>Joint Element Compatibility (Appendix L)</u>

3D Joints for Semiloof Shells



Geometric Properties

Not applicable.

Linear	Not applicable	
Matrix	Stiffness:	MATRIX PROPERTIES STIFFNESS 6 K1,, K21 element stiffness matrix (Not supported in LUSAS Modeller)
	Mass:	MATRIX PROPERTIES MASS 6 M1,, M21 element mass matrix (Not supported in LUSAS Modeller)
	Damping:	MATRIX PROPERTIES DAMPING 6 C1,, C21 element damping matrix (Not supported

		in LUSAS Modeller)
Joint	Standard:	JOINT PROPERTIES 3 (Joint: 3/Spring
	Dynamic general:	Stiffness Only) JOINT PROPERTIES GENERAL 3 (Joint:
	Dynamic general.	3/General Properties)
	Elasto-plastic:	JOINT PROPERTIES NONLINEAR 31 3 (Joint: 3/Elasto-Plastic (Tension and Compression Equal))
	Elasto-plastic:	JOINT PROPERTIES NONLINEAR 32 3 (Joint: 3/Tension and Compression Unequal)
	Nonlinear contact:	JOINT PROPERTIES NONLINEAR 33 3 (Joint: 3/Smooth Contact)
	Nonlinear friction:	JOINT PROPERTIES NONLINEAR 44 3 (Joint: 3/Frictional Contact)
	Viscous damping:	JOINT PROPERTIES NONLINEAR 35 3 (Joint: 3/Viscous Damper)
	Lead-rubber:	JOINT PROPERTIES NONLINEAR 36 3 (Joint: 3/Lead Rubber Bearing)
	Friction pendulum:	JOINT PROPERTIES NONLINEAR 37 3 (Joint: 3/Frictional Pendulum System)
	Multi-linear elastic	JOINT PROPERTIES NONLINEAR 40 3 (Joint: 3/Multi-Linear Elastic)
	Multi-linear	JOINT PROPERTIES NONLINEAR 41 3
	hysteresis	(Joint: 3/Multi-Linear Hysteresis)
	Multi-linear	JOINT PROPERTIES NONLINEAR 42 3
	compound hysteresis	(Joint: 3/Multi-Linear Compound Hysteresis)
	Axial force	JOINT PROPERTIES NONLINEAR 43 3
	dependent multi-	(Joint: 3/Axial Force Dependent Multi-Linear
	linear elastic	Elastic)
Concrete	Not applicable	
Elasto-Plastic	Not applicable	
Creep	Not applicable	
Damage	Not applicable	
Viscoelastic	Not applicable	
Shrinkage	Not applicable	
Rubber	Not applicable	
Generic Polymer	Not applicable	
Composite	Not applicable	

Loading

•		
Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, W: at active nodes.
Concentrated	CL	Concentrated loads. Px, Py, Pz: at active nodes.
Loads		
Element Loads	Not	
	applicable.	
Distributed Loads	Not	
	applicable.	
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf, Zcbf,
		$\Omega_x, \Omega_y, \Omega_z, \alpha_x, \alpha_y, \alpha_z$
	DED DEDE	
T T T 1 /4	BFP, BFPE	Not applicable.
Velocities		Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Accelerations. Ax, Ay, Az: at nodes.
Initial	SSI, SSIE	Initial stresses/strains at nodes/for element. Fx, Fy,
Stress/Strains		Fz: spring forces in local directions. Ex, Ey, ψ z:
		spring strains in local directions.
	SSIG	Not applicable.
Residual Stresses	Not	
Residual Stresses	applicable.	
Target	TSSIE, TSSIA	Target stresses/strains at nodes/for element. Fx, Fy,
Stress/Strains	1551L, 1551A	-
Stress/Strams		Fz: spring forces in local directions. εx , εy , ψz :
		spring strains in local directions.
	TSSIG	Not applicable.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T1, T2, T3, T10,
		T20, T30: actual and initial spring temperatures.
Overburden	Not	
	applicable.	
Phreatic Surface	Not	
	applicable.	
Field Loads	Not	
	applicable.	
Temp Dependent		
Loads		
 00000	TT.	

LUSAS Output

SolverForce: Fx, Fy, Fz: spring forces in local directions.Strain: Ex, Ey, Ez: spring strains in local directions.

Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

Standard joint element

Sign Convention

□ Standard joint element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Stiffness	Default.	1-point.
	Fine.	As default.
Mass	Default.	1-point.
	Fine.	As default.

Mass Modelling

Lumped mass only. The position of the mass relative to the two active joint nodes is defined in the joint material data. Point mass elements should be used to model lumped masses when no stiffness modelling is required.

Options

- 55 Output strains as well as stresses.
- **119** Invokes temperature input for joints.

Notes on Use

• When using Modeller to assign this semiloof joint element to interface lines a JL43 joint element will be created at the semiloof shell corner nodes and a JSL4 joint element will be created at the semiloof shell mid-side nodes.

See Joint Element Compatibility and Notes (Appendix L).

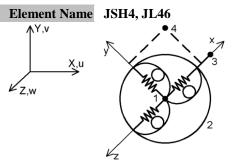
Restrictions

Not applicable.

- The joint elements may be used to release degrees of freedom between elements, e.g. a hinged shell, or to provide nonlinear support conditions, e.g. friction-gap condition. Also, point masses may be represented by including a joint at an element node.
- See <u>Joint Element Compatibility (Appendix L)</u>

3D Joint Elements for Engineering, Kirchhoff and Semiloof Beams

General



Element Group	Joints
Element	3D Joints
Subgroup	
Element	3D joint elements which connects two nodes by six springs in the local x,
Description	y and z-directions. Use JL46 for semiloof beam end nodes.
Number Of	4. The 3rd and 4th nodes are used to define the local x-axis and local xy-
Nodes	plane respectively.
Freedoms	U, V, W, θx , θy , θz : at nodes 1 and 2 (active nodes).
Node	X, Y, Z: at each node.
Coordinates	

Geometric Properties

- ez Eccentricity measured from the joint xy-plane to the nodal line.
- **dy** Parametric distance factor (between 0.0 and 1.0), which defines the position of the shear spring for the local y direction between nodes 1 and 2. It is measured from node 1 (dy=0) along the local x direction.
- **dz** Parametric distance factor (between 0.0 and 1.0), which defines the position of the shear spring for the local z direction between nodes 1 and 2. It is measured from node 1 (dz=0) along the local x direction

Linear	Not applicable	
Matrix	Stiffness:	MATRIX PROPERTIES STIFFNESS 12 K1,, K78 element stiffness matrix (Not supported in LUSAS Modeller)
	Mass:	MATRIX PROPERTIES MASS 12 M1,, M78 element mass matrix (Not supported in LUSAS Modeller)
	Damping:	MATRIX PROPERTIES DAMPING 12 C1,, C78 element damping matrix (Not supported in LUSAS Modeller)
Joint	Standard:	JOINT PROPERTIES 6 (Joint: 6/Spring Stiffness Only)
	Dynamic general:	JOINT PROPERTIES GENERAL 6 (Joint: 6/General Properties)
	Elasto-plastic:	JOINT PROPERTIES NONLINEAR 31 6 (Joint: 6/Elasto-Plastic (Tension and Compression Equal))
	Elasto-plastic:	JOINT PROPERTIES NONLINEAR 32 6 (Joint: 6/Tension and Compression Unequal)
	Nonlinear contact:	JOINT PROPERTIES NONLINEAR 33 6 (Joint: 6/Smooth Contact)
	Nonlinear friction:	JOINT PROPERTIES NONLINEAR 44 6 (Joint: 6/Frictional Contact)
	Viscous damping:	JOINT PROPERTIES NONLINEAR 35 6 (Joint: 6/Viscous Damper)
	Lead-rubber:	JOINT PROPERTIES NONLINEAR 36 6 (Joint: 6/Lead Rubber Bearing)
	Friction pendulum:	JOINT PROPERTIES NONLINEAR 37 6 (Joint: 6/Frictional Pendulum System)
	Multi-linear elastic	JOINT PROPERTIES NONLINEAR 40 6 (Joint: 6/Multi-Linear Elastic)
	Multi-linear	JOINT PROPERTIES NONLINEAR 41 6
	hysteresis	(Joint: 6/Multi-Linear Hysteresis)
	Multi-linear	JOINT PROPERTIES NONLINEAR 42 6
	compound hysteresis	(Joint: 6/Multi-Linear Compound Hysteresis)
	Axial force dependent multi-	JOINT PROPERTIES NONLINEAR 43 6 (Joint: 6/Axial Force Dependent Multi-Linear
a i	linear elastic	Elastic)
Concrete	Not applicable	
Elasto-Plastic	Not applicable	
Creep	Not applicable	

Damage	Not applicable
Viscoelastic	Not applicable
Shrinkage	Not applicable
Rubber	Not applicable
Generic Polymer	Not applicable
Composite	Not applicable

Field LoadsNot applicable.Temp DependentNot applicable.Loads

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, W, θx , θy , θz : at active nodes.
Concentrated Loads	CL	Concentrated loads. Px, Py, Pz, Mx, My, Mz: at active nodes.
Element Loads	Not applicable.	
Distributed Loads	Not applicable.	
Body Forces	CBF	Constant body forces for element. Xcbf, Ycbf,
		Zcbf, Ωx , Ωy , Ωz , αx , αy , αz
	BFP, BFPE	Not applicable.
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Accelerations. Ax, Ay, Az: at nodes.
Initial Stress/Strains	SSI, SSIE	Initial stresses/strains at nodes/for element. Fx, Fy, Fz, Mx, My, Mz: spring forces in local
		directions. εx , εy , εz , ψx , $y y$, $y z$: spring strains in local directions.
	SSIG	Not applicable.
Residual Stresses	Not applicable.	
Target Stress/Strains	TSSIE, TSSIA	Target stresses/strains at nodes/for element. Fx, Fy, Fz, Mx, My, Mz: spring forces in local
		directions. εx , εy , εz , ψx , yy , yz : spring strains in local directions.
	TSSIG	Not applicable.
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T1, T2, T3, T4, T5, T6, T10, T20, T30, T40, T50, T60: actual and initial spring temperatures.
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	

LUSAS Output

Solver Force: Fx, Fy, Fz, Mx, My, Mz spring forces in local directions.
 Strain: εx, εy, εz, ψx, ψy, ψz: spring strains in local directions.
 Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

□ Standard joint element

Sign Convention

Standard joint element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Stiffness Default.	1-point.
Fine.	As default.
Mass Default.	1-point.
Fine	As default.

Mass Modelling

Lumped mass only. The position of the mass relative to the two active joint nodes is defined in the joint material data. Point mass elements should be used to model lumped masses when no stiffness modelling is required.

Options

- 55 Output strains as well as stresses.
- **119** Invokes temperature input for joints

Notes on Use

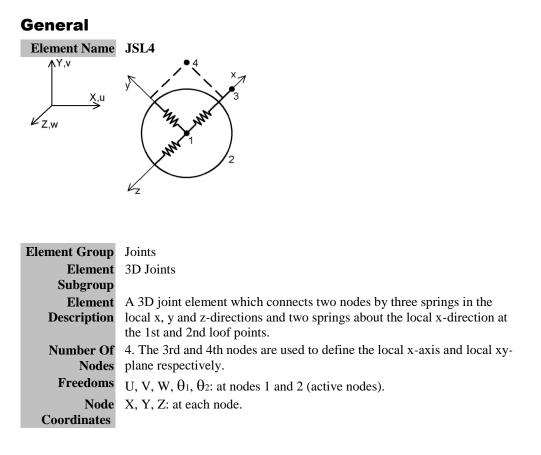
See Joint Element Compatibility and Notes.

Restrictions

Not applicable.

- The joint elements may be used to release degrees of freedom between elements, e.g. a hinged shell, or to provide nonlinear support conditions, e.g. friction-gap condition. Also, point masses may be represented by including a joint at an element node.
- See <u>Joint Element Compatibility (Appendix L)</u>

3D Joint Element for Semiloof Beams



Geometric Properties

Not applicable.

Material Properties

Linear	Not applicable	
Matrix	Stiffness:	MATRIX PROPERTIES STIFFNESS 10 K1,,
		K55 element stiffness matrix (Not supported in
		LUSAS Modeller)
	Mass:	MATRIX PROPERTIES MASS 10 M1,, M55
		element mass matrix (Not supported in

LUSAS Modeller)

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	Damping:	MATRIX PROPERTIES DAMPING 10 C1,, C55 element damping matrix (Not supported
Joint	Standard:	in LUSAS Modeller) JOINT PROPERTIES 5 (Joint: 5/Spring Stiffness Only)
	Dynamic general:	JOINT PROPERTIES GENERAL 5 (Joint: 5/General Properties)
	Elasto-plastic:	JOINT PROPERTIES NONLINEAR 31 5 (Joint: 5/Elasto-Plastic (Tension and Compression Equal))
	Elasto-plastic:	JOINT PROPERTIES NONLINEAR 32 5 (Joint:5/Tension and Compression Unequal)
	Nonlinear contact:	JOINT PROPERTIES NONLINEAR 33 5 (Joint: 5/Smooth Contact)
	Nonlinear friction:	JOINT PROPERTIES NONLINEAR 44 5 (Joint: 5/Frictional Contact)
	Viscous damping:	JOINT PROPERTIES NONLINEAR 35 5 (Joint: 5/Viscous Damper)
	Lead-rubber:	JOINT PROPERTIES NONLINEAR 36 5 (Joint: 5/Lead Rubber Bearing)
	Friction pendulum:	JOINT PROPERTIES NONLINEAR 37 5 (Joint: 5/Frictional Pendulum System)
	Multi-linear elastic	JOINT PROPERTIES NONLINEAR 40 5 (Joint: 5/Multi-Linear Elastic)
	Multi-linear hysteresis	JOINT PROPERTIES NONLINEAR 41 5 (Joint: 5/Multi-Linear Hysteresis)
	Multi-linear	JOINT PROPERTIES NONLINEAR 42 5
	compound hysteresis	(Joint: 5/Multi-Linear Compound Hysteresis)
	Axial force	JOINT PROPERTIES NONLINEAR 43 5
	dependent multi-	(Joint: 5/Axial Force Dependent Multi-Linear
Concrete	linear elastic Not applicable	Elastic)
Elasto-Plastic	Not applicable	
Creep	Not applicable	
Damage	Not applicable	
Viscoelastic	Not applicable	
Shrinkage	Not applicable	
Rubber	Not applicable	
Generic Polymer	Not applicable	
Composite	Not applicable	

Loading

Prescribed Value	PDSP, TPDSP

Concentrated CL Loads Element Loads Not applicable. Distributed Loads Not applicable. Body Forces CBF

	BFP, BFPE
Velocities	VELO
Accelerations	ACCE
Initial	SSI, SSIE
Stress/Strains	

SSIG Residual Stresses Not applicable. Target TSSIE, TSSIA Stress/Strains

TSSIG Temperatures TEMP, TMPE

OverburdenNot applicable.Phreatic SurfaceNot applicable.Field LoadsNot applicable.Temp DependentNot applicable.Loads

Prescribed variable. U, V, W, θ₁, θ₂: at active nodes.Concentrated loads. Px, Py, Pz, M₁, M₂: at active nodes.

Constant body forces for element. Xcbf, Ycbf, Zcbf, Ωx, Ωy, Ωz, αx, αy, αz Not applicable. Velocities. Vx, Vy, Vz: at nodes. Accelerations. Ax, Ay, Az: at nodes. Initial stresses/strains at nodes/for element. Fx, Fy, Fz, Mx, My, Mz: spring forces in local directions. εx, εy, εz, ψx, ψy, ψz: spring strains in local directions. Not applicable.

Target stresses/strains at nodes/for element. Fx, Fy, Fz, Mx, My, Mz: spring forces in local directions. εx, εy, εz, ψx, ψy, ψz: spring strains in local directions.
Not applicable.
Temperatures at nodes/for element. T1, T2, T3, T4, T5, T10, T20, T30, T40, T50: actual and

initial spring temperatures.

LUSAS Output

Solver	Force: Fx, Fy, Fz, M1, M2: spring forces in local directions.
	Strain: εx , εy , εz , ψ_1 , ψ_2 : spring strains in local directions.
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

□ Standard joint element

Sign Convention

□ Standard joint element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Stiffness	Default.	1-point.
	Fine.	As default.
Mass	Default.	1-point.
	Fine.	As default.

Mass Modelling

Lumped mass only. The position of the mass relative to the two active joint nodes is defined in the joint material data. Point mass elements should be used to model lumped masses when no stiffness modelling is required.

Options

- 55 Output strains as well as stresses.
- **119** Invokes temperature input for joints.

Notes on Use

See Joint Element Compatibility and Notes.

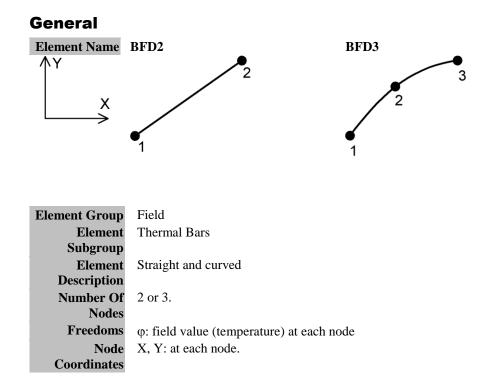
Restrictions

Not applicable.

- The joint elements may be used to release degrees of freedom between elements, e.g. a hinged shell, or to provide nonlinear support conditions, e.g. friction-gap condition. Also, point masses may be represented by including a joint at an element node.
- See Joint Element Compatibility (Appendix L)

Chapter 9 : Thermal / Field Elements.

2D Bar Field Elements



Geometric Properties

A1 ... An Cross-sectional area at each node.

Material Properties

Matrix	Not applicable
Joint	Not applicable
Composite	Not applicable
Field	Isotropic

Orthotropic:

convection/radiation:

Linear

MATERIAL PROPERTIES FIELD ISOTROPIC (Field: Isotropic) MATERIAL PROPERTIES FIELD ISOTROPIC CONCRETE(Field: Isotropic) Not applicable Not applicable Arbitrary N convection/radiation:

Not applicable

Loading

Prescribed Value	PDSP, TPDSP	φ : field variable (temperature) at nodes.
Rate of Heat Inflow at a Point	RGN	Q: field loading at nodes.
Element Loads	Not applicable.	
Distributed Loads	UDL	Not applicable.
	FFL	 qa: (Q/unit area) at nodes (positive defines heat input) (see <u>FLD Face loading applied to</u> <u>thermal bars</u>).
Rate of Heat Inflow/Unit Volume	RBC	qv: (Q/unit volume) for element.
	RBV, RBVE	qv: (Q/unit volume) at nodes/ for element.
	Not applicable.	
Accelerations	Not applicable.	
	Not applicable.	
Stress/Strains	XX	
Residual Stresses	Not applicable.	
Target Stress/Strains	Not applicable.	
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, 0,
Temperatures		0, 0, 0 (See <i>Notes</i> .)
Field Loads	ENVT	Environmental boundary conditions . φe, hc, hr: external environmental temperature, convective and radiative heat transfer coefficients. (See <i>Notes</i>)
Temp Dependent Loads	TDET	Temperature dependent environmental boundary conditions. Φe, hc, hr, T: external environmental temperature, convective and radiative heat transfer coefficients and temperature for element. (See <i>Notes</i>)
	RIHG	Internal heat generation rate. Q, T: coefficient/unit volume and temperature. (See <i>Notes</i>)

LUSAS Output

Solver Field variable (temperature). gx, qx: gradient and flow in local axes.

Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

□ Standard line element

Sign Convention

□ Standard field element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Conductivity	Default.	1-point (BFD2), 2-point (BFD3).
	Fine (see Options).	2-point (BFD2), 3-point (BFD3).
Specific Heat	Default.	1-point (BFD2), 2-point (BFD3).
	Fine (see Options).	2-point (BFD2), 3-point (BFD3).

Specific Heat Modelling

- □ Consistent specific heat (default).
- □ Lumped specific heat.

Options

- **18** Invokes fine integration rule.
- 105 Lumped specific heat.

Notes on Use

1. TEMP/TMPE loading can be used to initialise the temperature field on the first step of a nonlinear field analysis. The temperature will be applied on the first pass of iteration 0 only and the load must be specified as a manual increment.

- 2. For linear field problems only one load case is allowed if an ENVT load is to be applied.
- 3. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear solution progresses.
- 4. Automatic load incrementation under the NONLINEAR CONTROL data chapter cannot be used with TDET or RIHG loading.
- 5. When using load curves with TDET loading, the environmental temperatures will be factored but the heat coefficients will remain constant. If ENVT loading is used with load curves, any component can be controlled via a load curve.
- 6. If radiation is to be considered the problem becomes nonlinear and NONLINEAR CONTROL must be specified.

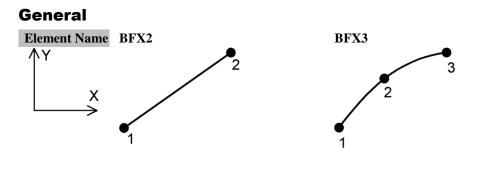
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature

Recommendations on Use

These elements may be used to analyse heat conduction along bars either individually or in conjunction with continuum field elements, e.g. supporting struts.

2D Axisymmetric Membrane Field Elements



Element Group	Field
Element	Thermal Bars
Subgroup	
Element	Straight and curved isoparametric axisymmetric thermal bar elements in
Description	2D which can accommodate varying cross sectional area.
Number Of	2 or 3.
Nodes	
Freedoms	j: field variable (temperature) at each node.
Node	X, Y: at each node.
Coordinates	

Geometric Properties

t1... tn Thickness at each node.

Material Properties

Matrix	Not applicable.	
Composite	Not applicable.	
Field	Isotropic	MATERIAL PROPERTIES FIELD ISOTROPIC (Field: Isotropic)
		MATERIAL PROPERTIES FIELD ISOTROPIC CONCRETE (Field: Isotropic)
	Orthotropic:	Not applicable
	Linear convection/radiation:	Not applicable
	Arbitrary	Not applicable

convection/radiation:

Loading

Prescribed Value	PDSP, TPDSP	ϕ : field variable (temperature) at nodes.
Rate of Heat Inflow at a Point	RGN	Q: field loading at nodes.
Element Loads	Not applicable.	
Distributed		Not applicable.
Loads		
	FFL	 qa: (Q/unit area) at nodes (positive defines heat input) (see <u>FLD Face loading applied to</u> <u>thermal bars</u>).
Rate of Heat	RBC	qv: (Q/unit volume) for element.
Inflow/Unit		
Volume		
	RBV, RBVE	qv: (Q/unit volume) at nodes/ for element.
Velocities	Not applicable.	
Accelerations	Not applicable.	
Initial	Not applicable.	
Stress/Strains		
Residual Stresses	Not applicable.	
	Not applicable.	
Stress/Strains		
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, 0, 0, 0, 0, 0, 0 (See <i>Notes</i> .)
Field Loads	ENVT	Environmental boundary conditions . φe, hc, hr: external environmental temperature, convective and radiative heat transfer coefficients. (See <i>Notes.</i>)
Тетр	TDET	Temperature dependent environmental
Dependent Loads		boundary conditions. φe, hc, hr, T: external environmental temperature, convective and radiative heat transfer coefficients and temperature. (See <i>Notes</i> .)
	RIHG	Internal heat generation rate. Q, T: coefficient/unit volume and temperature for element. (See <i>Notes</i> .)

LUSAS Output

Solver Field variable (temperature). gx, qx: gradient and flow in local axes.

Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

□ Standard line element

Sign Convention

Standard field element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Conductivity	Default.	1-point (BFX2), 2-point (BFX3).
	Fine (see Options).	2-point (BFX2), 3-point (BFX3).
Specific Heat	Default.	1-point (BFX2), 2-point (BFX3).
	Fine (see Options).	2-point (BFX2), 3-point(BFX3).

Specific Heat Modelling

- □ Consistent specific heat (default).
- □ Lumped specific heat.

Options

- **18** Invokes fine integration rule.
- 47 X-axis taken as axis of symmetry.
- **105** Lumped specific heat.

Notes on Use

- 1. TEMP/TMPE loading can be used to initialise the temperature field on the first step of a nonlinear field analysis. The temperature will be applied on the first pass of iteration 0 only and the load must be specified as a manual increment.
- 2. For linear field problems only one load case is allowed if an ENVT load is to be applied.
- 3. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear solution progresses.
- 4. Automatic load incrementation under the NONLINEAR CONTROL data chapter cannot be used with TDET or RIHG loading.
- 5. When using load curves with TDET loading, the environmental temperatures will be factored but the heat coefficients will remain constant. If ENVT loading is used with load curves, any component can be controlled via a load curve.
- 6. If radiation is to be considered the problem becomes nonlinear and NONLINEAR CONTROL must be specified.

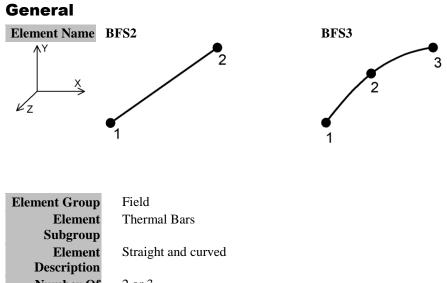
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature

Recommendations on Use

One example of the usage of these elements is the analysis of in-plane temperature flow in a thin circular plate.

3D Bar Field Elements



r	
Element	Thermal Bars
Subgroup	
Element	Straight and curved
Description	
Number Of	2 or 3.
Nodes	
Freedoms	φ : field value (temperature) at each node
Node	X, Y, Z: at each node.
Coordinates	

Geometric Properties

A1 ... An Cross sectional area at each node.

Material Properties

Linear	Not applicable
Matrix	Not applicable
Joint	Not applicable
Concrete	Not applicable
Elasto-Plastic	Not applicable
Creep	Not applicable
Damage	Not applicable
Viscoelastic	Not applicable

ShrinkageNot applicableRubberNot applicable.Generic PolymerNot applicableCompositeNot applicableFieldIsotropic

Orthotropic: Linear convection/radiation: Arbitrary convection/radiation: MATERIAL PROPERTIES FIELD ISOTROPIC (Field: Isotropic) MATERIAL PROPERTIES FIELD ISOTROPIC CONCRETE (Field: Isotropic) Not applicable. Not applicable.

Not applicable.

Loading

0		
Prescribed Value	PDSP, TPDSP	φ: field variable (temperature) at nodes.
Rate of Heat Inflow at a Point	RGN	Q: field loading at nodes.
Element Loads	Not applicable.	
Distributed Loads	UDL	Not applicable.
	FFL	 qa: (Q/unit area) at nodes (positive defines heat input) (see <u>FLD Face loading applied to</u> thermal bars).
Rate of Heat Inflow/Unit Volume	RBC	qv: (Q/unit volume) for element.
	RBV, RBVE	qv: (Q/unit volume) at nodes/ for element.
Velocities	Not applicable.	
Accelerations	Not applicable.	
Initial Stress/Strains	Not applicable.	
Residual Stresses	Not applicable.	
Target Stress/Strains	Not applicable.	
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, 0, 0, 0, 0, 0 (See <i>Notes</i> .)
Field Loads	ENVT	Environmental boundary conditions . φe, hc, hr: external environmental temperature, convective and radiative heat transfer

Temp Dependent	TDET	coefficients. (See <i>Notes</i> .) Temperature dependent environmental	
Loads		boundary conditions . φe, hc, hr, T: external environmental temperature, convective and radiative heat transfer coefficients and temperature. (See <i>Notes</i> .)	
	RIHG	Internal heat generation rate. Q, T: coefficient/unit volume, and temperature for element. (See <i>Notes</i> .)	

LUSAS Output

Solver Field variable (temperature). gx, qx: gradient and flow in local axes.Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

□ Standard line element

Sign Convention

□ Standard field element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Conductivity	Default.	1-point (BFS2), 2-point (BFS3).
	Fine (see Options).	2-point (BFS2), 3-point (BFS3).
Specific Heat	Default.	1-point (BFS2), 2-point (BFS3).
	Fine (see Options).	2-point (BFS2), 3-point (BFS3).

Specific Heat Modelling

□ Consistent specific heat (default).

□ Lumped specific heat.

Options

- **18** Invokes fine integration rule.
- **105** Lumped specific heat.

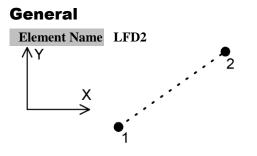
Notes on Use

- 1. TEMP/TMPE loading can be used to initialise the temperature field on the first step of a nonlinear field analysis. The temperature will be applied on the first pass of iteration 0 only and the load must be specified as a manual increment.
- 2. For linear field problems only one load case is allowed if an ENVT load is to be applied.
- 3. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear solution progresses.
- 4. Automatic load incrementation under the NONLINEAR CONTROL data chapter cannot be used with TDET or RIHG loading.
- 5. When using load curves with TDET loading, the environmental temperatures will be factored but the heat coefficients will remain constant. If ENVT loading is used with load curves, any component can be controlled via a load curve.
- 6. If radiation is to be considered the problem becomes nonlinear and NONLINEAR CONTROL must be specified.

Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature

2D Link Field Element



Element Group	Field
Element	Thermal Links
Subgroup	
Element	Straight conductive, convective or radiative thermal link element for 2D
Description	field analysis.
Number Of	2.
Nodes	
Freedoms	φ: field value (temperature) at each node.
Node	X, Y at each node.
Coordinates	

Geometric Properties

A1 ... An Cross sectional area at each node.

Material Properties

Linear	Not applicable
Matrix	Not applicable
Joint	Not applicable
Concrete	Not applicable
Elasto-Plastic	Not applicable
Creep	Not applicable
Damage	Not applicable
Viscoelastic	Not applicable
Shrinkage	Not applicable
Rubber	Not applicable

Generic Polymer	Not applicable	
Composite	Not applicable	
Field	Isotropic:	Not applicable.
	Orthotropic:	Not applicable.
	Linear	MATERIAL PROPERTIES FIELD LINK 18
	convection/radiation:	(Field: Linear Link)
	Arbitrary	MATERIAL PROPERTIES FIELD LINK 19
	convection/radiation:	(Field: Nonlinear Link)

Loading

Prescribed Value	PDSP, TPDSP	φ: field variable (temperature) at nodes.
Concentrated	Not applicable.	
Loads		
Element Loads	Not applicable.	
Distributed Loads	Not applicable.	
Body Forces	Not applicable.	
Velocities	Not applicable.	
Accelerations	Not applicable.	
Initial	Not applicable.	
Stress/Strains		
Residual Stresses	Not applicable.	
Target	Not applicable.	
Stress/Strains		
Temperatures	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not applicable.	
Loads		

LUSAS Output

Solver	Field variable (temperature). qx: flow at nodes in local directions.
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

□ Standard line element

Sign Convention

□ Standard field element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Conduction,	Default.	1-point (at element centroid).
Convection,		
Radiation		
	Fine.	As default.
Specific Heat	Default.	Not applicable.
	Fine.	Not applicable.

Specific Heat Modelling

Not applicable.

Options

Not applicable.

Notes on Use

No notes at present.

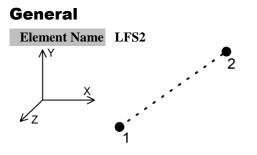
Restrictions

Not applicable.

Recommendations on Use

An example of the usage of these elements is the analysis of heat conduction at contacting interfaces.

3D Link Field Element



Element Group	Field
Element	Thermal Links
Subgroup	
Element	Straight conductive, convective or radiative thermal link element for 3D
Description	field analysis.
Number Of	2.
Nodes	
End Releases	
Freedoms	φ: field value (temperature) at each node.
Node Coordinates	X, Y, Z at each node.

Geometric Properties

A1 ... An Cross sectional area at each node.

Material Properties

Linear	Not applicable.
Matrix	Not applicable.
Joint	Not applicable.
Concrete	Not applicable.
Elasto-Plastic	Not applicable.
Rubber	Not applicable.
Generic Polymer	Not applicable
Composite	Not applicable.
Field	Isotropic:

Not applicable.

	Orthotropic:	Not applicable.
	Linear	MATERIAL PROPERTIES FIELD LINK 18
	convection/radiation:	(Field: Linear Link)
	Arbitrary	MATERIAL PROPERTIES FIELD LINK 19
	convection/radiation:	(Field: Nonlinear Link)
Stress Potential	Not applicable.	
Creep	Not applicable.	
Damage	Not applicable.	
Viscoelastic	Not applicable.	
Shrinkage	Not applicable	

Loading

PDSP, TPDSP	φ: field variable (temperature) at nodes.
Not applicable.	
Not applicable.	
Not applicable.	
Not applicable.	
Not applicable.	
Not applicable.	
Not applicable.	
	Not applicable. Not applicable. Not applicable. Not applicable. Not applicable. Not applicable. Not applicable. Not applicable. Not applicable. Not applicable.

LUSAS Output

Solver	Field variable (temperature). qx: flow at nodes in local directions.
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

□ Standard line element

Sign Convention

□ Standard field element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Conduction,
Convection,
RadiationDefault.1- point (at element centroid).Fine.Fine.As default.Specific HeatDefault.Not applicable.Fine.Not applicable.

Specific Heat Modelling

Not applicable.

Options

Not applicable.

Notes on Use

No notes at present.

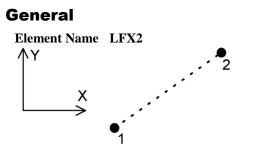
Restrictions

Not applicable.

Recommendations on Use

An example of the usage of these elements is the analysis of heat conduction at contacting interfaces.

2D Axisymmetric Link Field Element



Element Group	Field
Element	Thermal Links
Subgroup	
Element	Straight conductive, convective or radiative thermal link element for 2D
Description	axisymmetric field analysis.
Number Of	2.
Nodes	
End Releases	
Freedoms	φ: field value (temperature) at each node.
Node	X, Y at each node.
Coordinates	

Geometric Properties

t1... tn Thickness at each node.

Material Properties

Linear	Not applicable.
Matrix	Not applicable.
Joint	Not applicable.
Concrete	Not applicable.
Elasto-Plastic	Not applicable.
Rubber	Not applicable.
Generic Polymer	Not applicable
Composite	Not applicable.
Field	Isotropic:

Not applicable.

Orthotropic:	Not applicable.
Linear	MATERIAL PROPERTIES FIELD LINK 18
convection/radiation:	(Field: Linear Link)
Arbitrary	MATERIAL PROPERTIES FIELD LINK 19
convection/radiation:	(Field: Nonlinear Link)

Loading

Prescribed Value	PDSP, TPDSP	φ: field variable (temperature) at nodes.
Concentrated Loads	Not applicable.	
Element Loads	Not applicable.	
Distributed Loads	Not applicable.	
Body Forces	Not applicable.	
Velocities	Not applicable.	
Accelerations	Not applicable.	
Initial	Not applicable.	
Stress/Strains		
Residual Stresses	Not applicable.	
Target	Not applicable.	
Stress/Strains		
Temperatures	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not applicable.	
Loads		

LUSAS Output

Solver	Field variable (temperature). qx: flow at nodes in local directions.
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

□ Standard line element

Sign Convention

Standard field element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Conduction,	Default.	1- point (at element centroid).
Convection,		
Radiation		
	Fine.	As default.
Specific Heat	Default.	Not applicable.
	Fine.	Not applicable.

Specific Heat Modelling

Not applicable.

Options

47 X-axis taken as axis of symmetry.

Notes on Use

No notes at present.

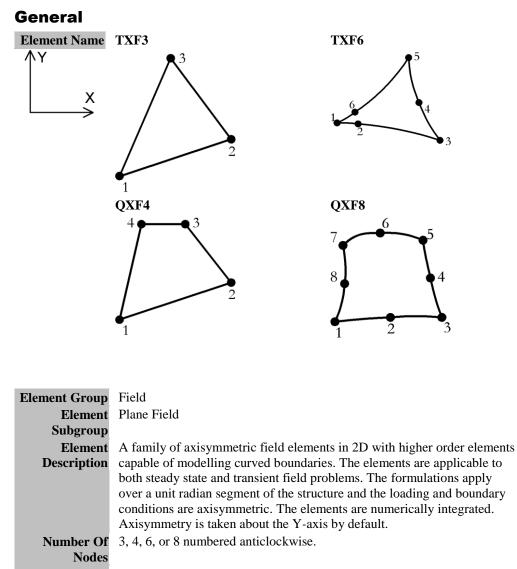
Restrictions

Not applicable.

Recommendations on Use

An example of the usage of these elements is the analysis of heat conduction at contacting interfaces.

2D Axisymmetric Field Elements



Freedoms ϕ : field variable at each node.

Node X, Y: at each node

Coordinates

Geometric Properties

Not applicable (a unit radian segment is assumed).

Material Properties

Linear	Not applicable.	
Matrix	Not applicable.	
Joint	Not applicable.	
Concrete	Not applicable.	
Elasto-Plastic	Not applicable.	
Rubber	Not applicable.	
Generic Polymer	Not applicable	
Composite	Not applicable.	
Field	Isotropic:	MATERIAL PROPERTIES FIELD ISOTROPIC (Field: Isotropic) MATERIAL PROPERTIES FIELD
		ISOTROPIC CONCRETE (Field: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES FIELD ORTHOTROPIC (Field: Orthotropic)
		MATERIAL PROPERTIES FIELD ORTHOTROPIC CONCRETE (Field: Orthotropic)
	Linear	Not applicable.

convection/radiation:	
Arbitrary	Not applicable.
convection/radiation:	

Loading

Prescribed Value	PDSP, TPDSP	φ: field variable (temperature) at nodes.
Rate of Heat Inflow at a Point	RGN	Q: field loading at nodes.
Element Loads	Not applicable.	
Distributed Loads	UDL	Not applicable.
	FFL	qa: (Q/unit area) at nodes (see FLD Face loading applied to thermal bars).
Rate of Heat Inflow/Unit Volume	RBC	qv: (Q/unit volume) for element.
	RBV, RBVE	qv: (Q/unit volume) at nodes/ for element.
Velocities	Not applicable.	

Initial Velocities Initial Stress/Strains	Not applicable.	
Residual Stresses		
Target Stress/Strains	Not applicable.	
Temperatures	Not applicable.	
Field Loads	ENVT	Environmental boundary conditions. φe, hc, hr: external environmental temperature, convective and radiative heat transfer coefficients. (See <i>Notes</i> .)
Temp Dependent Loads	TDET	Temperature dependent environmental boundary conditions. φe, hc, hr, T: external environmental temperature, convective and radiative heat transfer coefficients and temperature. (See <i>Notes</i> .)
	RIHG	Internal heat generation rate. Q, T: coefficient/unit volume and temperature for element. (See <i>Notes</i> .)

LUSAS Output

Solver Field variable (temperature). gx, gy, gz, qx, qy, qz: gradients and flows in global directions.
 Madeller See Regults Tables (Appendix K)

Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

Not applicable.

Sign Convention

□ Standard field element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Conductivity	Default.	1-point (TXF3), 3-point (TXF6), 2x2 (QXF4, QXF8)
	Fine (see <i>Options</i>).	3x3 (QXF8)
Specific Heat	Default.	1-point (TXF3), 3-point (TXF6), 2x2 (QXF4, QXF8)
	Fine.	As default.

Specific Heat Modelling

- □ Consistent specific heat (default)
- □ Lumped specific heat.

Options

- **18** Invokes fine integration rule for elements.
- 47 X-axis taken as axis of symmetry.
- 105 Lumped specific heat.

Notes on Use

- 1. The element formulations are based on the standard **isoparametric** approach. The variation of field variable (temperature) within an element is linear low order (corner node only) elements and quadratic high order (mid-side node) elements.
- 2. All elements pass the **patch test** for convergence.
- 3. For linear field problems only one load case is allowed if an ENVT load is to be applied.
- 4. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear solution progresses.
- 5. Automatic load incrementation under the NONLINEAR CONTROL data chapter cannot be used with TDET or RIHG loading.

- 6. When using load curves with TDET loading, the environmental temperatures will be factored but the heat coefficients will remain constant. If ENVT loading is used with load curves, any component can be controlled via a load curve.
- 7. If radiation is to be considered the problem becomes nonlinear and NONLINEAR CONTROL must be specified.

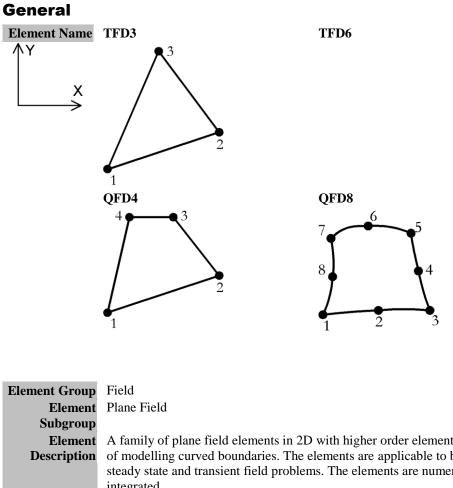
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

Recommendations on Use

The axisymmetric field elements are suitable for analysing solid field problems which exhibit geometric and loading symmetry about a given axis, e.g. temperature distribution in a pipe or radial groundwater flow into a well.

2D Plane Field Elements



-	
Element	Plane Field
Subgroup	
Element	A family of plane field elements in 2D with higher order elements capable
Description	of modelling curved boundaries. The elements are applicable to both steady state and transient field problems. The elements are numerically integrated.
Number Of	3, 4, 6 or 8 numbered anticlockwise.
Nodes	
Freedoms	φ : field value (temperature) at each node.
Node	X, Y: at each node.
Coordinates	

Geometric Properties

t1... tn Thickness at each node.

Material Properties

Linear	Not applicable
Matrix	Not applicable
Joint	Not applicable
Concrete	Not applicable
Elasto-Plastic	Not applicable
Creep	Not applicable
Damage	Not applicable
Viscoelastic	Not applicable
Shrinkage	Not applicable
Rubber	Not applicable.
Generic Polymer	Not applicable
Composite	Not applicable.
Field	Isotropic:

Orthotropic:

Linear convection/radiation: Arbitrary convection/radiation: MATERIAL PROPERTIES FIELD ISOTROPIC CONCRETE (Field: Isotropic) MATERIAL PROPERTIES FIELD ISOTROPIC (Field: Isotropic) MATERIAL PROPERTIES FIELD ORTHOTROPIC (Field: Orthotropic) MATERIAL PROPERTIES FIELD ORTHOTROPIC CONCRETE (Field: Orthotropic) Not applicable.

Not applicable.

Loading

Prescribed Value	PDSP, TPDSP	φ: field variable (temperature) at nodes
Rate of Heat	RGN	Q: field loading at nodes.
Inflow at a Point		
Element Loads	Not applicable.	
Distributed Loads	UDL	Not applicable.
	FFL	qa: (Q/unit area) at nodes (see FLD Face
		loading applied to thermal bars).

Rate of Heat Inflow/Unit Volume	RBC	qv: (Q/unit volume) for element.
	RBV, RBVE	qv: (Q/unit volume) at nodes/ for element.
Velocities	Not applicable.	
Accelerations	Not applicable.	
Initial Stress/Strains	Not applicable.	
Residual Stresses	Not applicable.	
Target Stress/Strains	Not applicable.	
Temperatures	Not applicable.	
Field Loads	ENVT	Environmental boundary conditions . φe, hc, hr: external environmental temperature, convective and radiative heat transfer coefficients. (See <i>Notes</i> .)
Temp Dependent Loads	TDET	Temperature dependent environmental boundary conditions. φe, hc, hr, T: external environmental temperature, convective and radiative heat transfer coefficients and temperature. (See <i>Notes.</i>)
	RIHG	Internal heat generation rate. Q, T: coefficient/unit volume and temperature for element. (See <i>Notes</i> .)

LUSAS Output

Solver	Field variable (temperature). gx, gy, qx, qy: gradients and flows in
	global directions.
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

□ Standard surface element

Sign Convention

□ Standard field element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Conductivity	Default.	1-point (TFD3), 3-point (TFD6), 2x2 (QFD4, QFD8).
	Fine.	As default.
Specific Heat	Default.	1-point (TFD3), 3-point (TFD6), 2x2 (QFD4, QFD8).
	Fine.	Not applicable.

Specific Heat Modelling

- □ Consistent specific heat (default).
- □ Lumped specific heat.

Options

- **18** Invokes fine integration rule for elements.
- 105 Lumped specific heat.

Notes on Use

- 1. The element formulations are based on the standard **isoparametric** approach. The variation of field variable (temperature) within an element is linear for low order (corner node only) elements and quadratic for high order (mid-side node) elements.
- 2. All elements pass the **patch test** for convergence.
- 3. For linear field problems only one load case is allowed if an ENVT load is to be applied.
- 4. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear solution progresses.
- 5. Automatic load incrementation under the NONLINEAR CONTROL data chapter cannot be used with TDET or RIHG loading.
- 6. When using load curves with TDET loading, the environmental temperatures will be factored but the heat coefficients will remain constant. If ENVT loading is used with load curves, any component can be controlled via a load curve.

7. If radiation is to be considered the problem becomes nonlinear and NONLINEAR CONTROL must be specified.

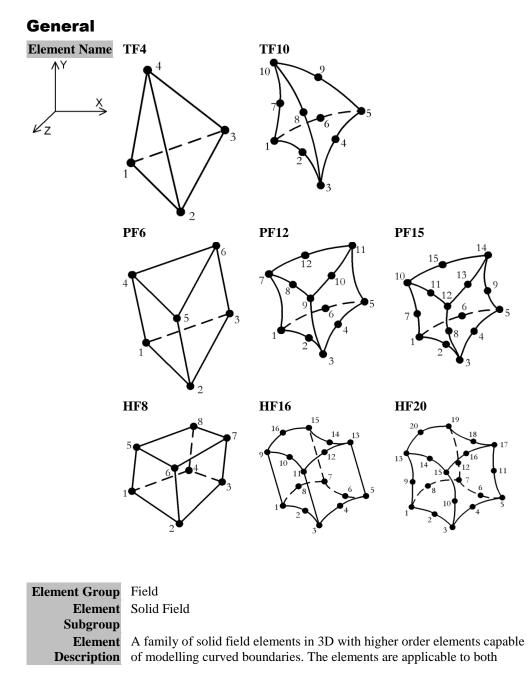
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

Recommendations on Use

The plane field elements may be utilised for analysing continuum field problems whose behaviour is essentially two dimensional, e.g. thermal analysis of a long tunnel . The elements are formulated using the 2D quasi-harmonic equation. See Theory Manuals for details.

3D Solid Field Elements



	steady state and transient field problems. The elements are numerically integrated.
Number Of	4 and 10 (tetrahedra). 6, 12 and 15 (pentahedra). 8, 16 and 20
Nodes	(hexahedra). The elements are numbered according to a right-hand screw
	rule in the local z-direction.
Freedoms	φ: field variable at each node.
Node	X, Y, Z: at each node.
Coordinates	

Geometric Properties

Not applicable.

Material Properties

Linear	Not applicable	
	Not applicable	
Joint	Not applicable	
	Not applicable	
Elasto-Plastic	Not applicable	
Creep	Not applicable	
—	Not applicable	
Viscoelastic	Not applicable	
Shrinkage	Not applicable	
Rubber	Not applicable	
Generic Polymer	Not applicable	
Composite	Not applicable	
Field	Isotropic:	MATERIAL PROPERTIES FIELD ISOTROPIC CONCRETE (Field: Isotropic) MATERIAL PROPERTIES FIELD ISOTROPIC (Field: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES FIELD ORTHOTROPIC SOLID (Field: Orthotropic Solid) MATERIAL PROPERTIES FIELD ORTHOTROPIC SOLID CONCRETE (Field: Orthotropic Solid)
	Linear convection/radiation: Arbitrary	Not applicable.
	convection/radiation:	Tot appreable.

Loading

Prescribed Value	PDSP, TPDSP	φ : field variable (temperature) at nodes.
Rate of Heat	RGN	Q: field loading at nodes.
Inflow at a Point	N 1 1. 1.	
Element Loads		NT / 11 11
Distributed Loads	UDL	Not applicable.
	FFL	qa: (Q/unit area) at nodes (see <u>FLD Face</u> <u>loading applied to thermal bars</u>).
Rate of Heat Inflow/Unit	RBC	qv: (Q/unit volume) for element.
Volume		
	RBV, RBVE	qv: (Q/unit volume) at nodes/ for element.
Velocities	Not applicable.	
Accelerations	Not applicable.	
Initial	Not applicable.	
Stress/Strains		
Residual Stresses	Not applicable.	
	Not applicable.	
Stress/Strains		
-	Not applicable.	
Field Loads	ENVT	Environmental boundary conditions. (pe, hc,
		hr: external environmental temperature, convective and radiative heat transfer coefficients. (See <i>Notes</i> .)
Temp Dependent	TDET	Temperature dependent environmental
Loads		boundary conditions. Φe, hc, hr, T: external environmental temperature, convective and radiative heat transfer coefficients and temperature. (See <i>Notes</i> .)
	RIHG	Internal heat generation rate. Q, T: coefficient/unit volume and temperature for element. (See <i>Notes</i> .)

LUSAS Output

Solver Field variable (temperature). gx, gy, gz, qx, qy, qz: gradients and flows in global directions.

Modeller See <u>Results Tables (Appendix K)</u>.

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard field element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Conductivity	Default. Fine (see <i>Options</i>).	1-point (TF4), 4-point (TF10), 3x2 (PF6, PF12, PF15), 2x2x2 (HF8, HF16, HF20) 5-point (TF10) 3x3x2 (HF16), 3x3x3 (HF20)
	Coarse (see <i>Options</i>).	1-point (HF20), 14-point (HF20)
Specific Heat	Default.	1-point (TF4), 4-point (TF10), 3x2 (PF6, PF12, PF15), 2x2x2 (HF8, HF16, HF20)
	Fine (see Options).	5-point (TF10) 3x3x2 (HF16), 3x3x3 (HF20)
	Coarse (see <i>Options</i>).	13-point (HF20), 14-point (HF20)

Specific Heat Modelling

- □ Consistent specific heat (default).
- □ Lumped specific heat.

Options

- **18** Invokes fine integration rule for elements.
- **105** Lumped specific heat.
- **155** Use 14-point integration rule for HF20.

- **156** Use 13-point integration rule for HF20.
- **398** For HF20 and HF16 with fine integration use all integration points for stress extrapolation.

Notes on Use

- 1. The element formulations are based on the standard isoparametric approach. The variation of potential within an element may be regarded as constant for low order (corner node only) elements and linear for high order (mid-side node) elements.
- 2. For linear field problems only one load case is allowed if an ENVT load is to be applied.
- 3. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear solution progresses.
- 4. Automatic load incrementation under the NONLINEAR CONTROL data chapter cannot be used with TDET or RIHG loading.
- 5. When using load curves with TDET loading, the environmental temperatures will be factored but the heat coefficients will remain constant. If ENVT loading is used with load curves, any component can be controlled via a load curve.
- 6. If radiation is to be considered the problem becomes nonlinear and NONLINEAR CONTROL must be specified.

Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

Recommendations on Use

The solid field elements may be used to analyse continuum field problems where the response is fully 3D (i.e. it cannot be approximated using the plane or axisymmetric elements), e.g. temperature distribution in a pipe intersection.

3D Solid Composite Field Element (Tetrahedral)

General	
Element Name	TF10S
X Z	
Element Group	Field
Element	Solid Field
Subgroup	
Element	3D solid field element capable of modelling curved boundaries. The
Description	element is applicable to both steady state and transient field problems. The element is numerically integrated, can be arbitrarily oriented with respect to the laminate, and allows for the fully automatic mesh generation of laminate geometric models imported from CAD packages.
	10. The element is numbered according to a right-hand screw rule in the
	local z-direction.
Freedoms	φ: field variable at each node.
Node	X, Y, Z: at each node.
Coordinates	

Geometric Properties

See <u>Composites</u> in the *Modeller Reference Manual*

Material Properties

Linear	Not applicable
Matrix	Not applicable
Joint	Not applicable
Concrete	Not applicable

Creep Damage Viscoelastic Shrinkage	Not applicable Not applicable Not applicable Not applicable Not applicable Not applicable Not applicable	
Composite	Isotropic: Orthotropic:	COMPOSITE MATERIAL MATERIAL PROPERTIES FIELD ISOTROPIC (Field: Isotropic) MATERIAL PROPERTIES FIELD ISOTROPIC CONCRETE (Field: Isotropic) MATERIAL PROPERTIES FIELD
	Linear	ORTHOTROPIC SOLID (Field: Orthotropic Solid) MATERIAL PROPERTIES FIELD ORTHOTROPIC SOLID CONCRETE (Field: Orthotropic Solid) Not applicable
	convection/radiation: Arbitrary convection/radiation:	Not applicable

Loading

Prescribed Value	PDSP, TPDSP φ: field variable (temperature) at nodes.	
Rate of Heat	RGN	Q: field loading at nodes.
Inflow at a Point		
Element Loads	Not applicable.	
Distributed Loads	UDL	Not applicable.
	FFL	qa: (Q/unit area) at nodes
Rate of Heat	RBC	qv: (Q/unit volume) for element.
Inflow/Unit		
Volume		
	RBV, RBVE	qv: (Q/unit volume) at nodes/ for element.
Velocities	Not applicable.	
Accelerations	Not applicable.	
Initial	Not applicable.	
Stress/Strains		
Residual Stresses	Not applicable.	

Target Stress/Strains	Not applicable.	
Temperatures	Not applicable.	
Field Loads	ENVT	Environmental boundary conditions φe, hc, hr: external environmental temperature, convective and radiative heat transfer coefficients. (See <i>Notes</i> .)
Temp Dependent Loads	TDET	Temperature dependent boundary conditions. φe, hc, hr, T: external environmental temperature, convective and radiative heat transfer coefficients and temperature. (See <i>Notes</i> .)
	RIHG	Internal heat generation rate. Q, T: coefficient/unit volume and temperature for element. (See <i>Notes</i> .)

LUSAS Output

Solver Field variable (temperature). gx, gy, gz, qx, qy, qz: gradients and flows. Gauss point values are in local directions. Nodal values are in global directions.

Modeller See <u>Results tables (Appendix K)</u>

Local Axes

The local axes for each layer are defined by the LAMINAR DIRECTIONS specified for its bottom surface. The three node set in LAMINAR DIRECTIONS define the local Cartesian set origin, the x-axis and the positive quadrant of the xy-plane respectively. The local z-axis forms an orthonormal coordinate system with x and y.

Sign Convention

□ Standard field elements

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Conductivity	Default.	1-point for a tetrahedral subdivision (see Notes),3-point for a pentahedral/pyramid subdivision, 2x2for a hexahedral/wrick subdivision
	Fine (see <i>Options</i>)	1-point for a tetrahedral subdivision (see Notes), 3x2 for a pentahedral/pyramid subdivision, 2x2 x2 for a hexahedral/wrick subdivision
Specific Heat	Default.	5-point for the whole element or (see Options) 1- point for a tetrahedral subdivision, 3x2 for a pentahedral/pyramid subdivision, 2x2 x2 for a hexahedral/wrick subdivision
	Fine (see <i>Options</i>)	11-point or (see Options) 14 -point for the whole element

Specific Heat Modelling

- Consistent specific heat (default).
- Lumped specific heat.

Options

- **18** Invokes fine integration rule for elements.
- 91 Formulate element specific heat with fine integration
- **105** Lumped specific heat.
- 266 Layer by layer computation of specific heat matrix.
- 394 Lamina directions supported
- **395** Use 14-point fine integration rule for specific heat matrix of TH10 family (used together with 91)

Notes on Use

- 1. The element formulations are based on the standard isoparametric approach. The variation of field gradients within an element may be regarded as linear.
- The LAMINAR DIRECTIONS and COMPOSITE MATERIAL data chapters must be used with this element in conjunction with the COMPOSITE ASSIGNMENTS data chapter.
- 3. If the whole tetrahedral element is embedded in a single lamina, a 4-point integration rule will be used for this tetrahedral subdivision; otherwise a 1-point rule will be used.

- 4. The specific heat matrix can be computed using a layer by layer integration (OPTION 266), however this should only be used when the thermal properties of the layers vary considerably because the computation time can be greatly increased when this OPTION is specified.
- 5. Numerical integration through the thickness is performed. The integration points are located in the subdivisions of each layer. Each subdivision forms the shape of a regular 3D solid field element and the integration points are located accordingly within the subdivision as described above.
- 6. For linear field problems only one load case is allowed if an ENVT load is to be applied.
- 7. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear solution progresses.
- 8. Automatic load incrementation under the NONLINEAR CONTROL data chapter cannot be used with TDET or RIHG loading.
- 9. When using load curves with TDET loading, the environmental temperatures will be factored but the heat coefficients will remain constant. If ENVT loading is used with load curves, any component can be controlled via a load curve.
- 10. If radiation is to be considered the problem becomes nonlinear and NONLINEAR CONTROL must be specified.
- 11. Layer 1 is always the bottom layer.

Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

Recommendations on Use

- 3D solid composite field elements should be used for modelling thick composite structures comprising laminae of differing material properties where the computational cost of modelling each lamina with an individual solid element would be prohibitive. This field element can be used to analyse continuum field problems where the response is fully 3D.
- As these elements can be arbitrarily oriented with respect to the laminate, they are particularly aimed at the use of fully automatic mesh generation of laminate geometric models imported from CAD packages.

3D Solid Composite Field Elements (Pentahedral and Hexahedral)

General Element Name PF6C PF12C X HF8C HF16C 15 14 13 5 Field **Element Group** Solid Field Element Subgroup Element 3D solid field elements capable of modelling curved boundaries. The Description elements are applicable to both steady state and transient field problems. The elements are numerically integrated. The composite layers are parallel to the top and bottom faces and the bottom surface of the first layer coincides with the bottom surface of the element. The top and bottom faces of the element are as shown, e.g. nodes 1, 2, 3, 4 define the bottom face of HF8C Number Of 6 or 12 (pentahedra), 8 or 16 (hexahedra). The elements are numbered Nodes according to a right-hand screw rule in the local z-direction. Freedoms φ : field variable at each node. Node X, Y, Z: at each node. **Coordinates**

Geometric Properties

See <u>Composites</u> in the Modeller Reference Manual

Material Properties

	Not applicable Not applicable	
	Not applicable	
	Not applicable	
Elasto-Plastic	Not applicable	
Creep	Not applicable	
Damage	Not applicable	
Viscoelastic	Not applicable	
Shrinkage	Not applicable	
Rubber	Not applicable	
Generic Polymer	Not applicable	
Composite		COMPOSITE MATERIAL
Field	Isotropic:	MATERIAL PROPERTIES FIELD
		ISOTROPIC (Field: Isotropic)
		MATERIAL PROPERTIES FIELD
		ISOTROPIC CONCRETE (Field: Isotropic)
	Orthotropic:	MATERIAL PROPERTIES FIELD ORTHOTROPIC SOLID (Field: Orthotropic
		Solid)
		MATERIAL PROPERTIES FIELD
		ORTHOTROPIC SOLID CONCRETE (Field:
		Orthotropic Solid)
	Linear	Not applicable
	convection/radiation:	
	Arbitrary convection/radiation:	Not applicable
	convection/radiation:	

Loading

Prescribed Value	PDSP, TPDSP φ: field variable (temperature) at r		
Rate of Heat	RGN	Q: field loading at nodes.	
Inflow at a Point			
Element Loads	Not applicable.		
Distributed Loads	UDL Not applicable.		
	FFL	qa: (Q/unit area) at nodes	
Rate of Heat	RBC	qv: (Q/unit volume) for element.	

Inflow/Unit Volume		
	RBV, RBVE	qv: (Q/unit volume) at nodes/ for element.
Velocities	Not applicable.	
Accelerations	Not applicable.	
Initial	Not applicable.	
Stress/Strains		
Residual Stresses	Not applicable.	
Target	Not applicable.	
Stress/Strains		
Temperatures	Not applicable.	
Field Loads	ENVT	Environmental boundary conditions φe, hc, hr: external environmental temperature, convective and radiative heat transfer coefficients. (See <i>Notes</i> .)
Temp Dependent	TDET	Temperature dependent boundary
Loads	RIHG	<u>conditions</u> . φe, hc, hr, T: external environmental temperature, convective and radiative heat transfer coefficients and temperature. (See <i>Notes</i> .) Internal heat generation rate. Q, T: coefficient/unit volume and temperature for element. (See <i>Notes</i> .)

LUSAS Output

- **Solver** Field variable (temperature). gx, gy, gz, qx, qy, qz: gradients and flows. Gauss point values are in local directions. Nodal values are in global directions.
- Modeller See <u>Results tables (Appendix K)</u>

Local Axes

The local axes for each layer are defined using the convention for <u>standard area elements</u>. Local axes are computed at the top and bottom quadratic surfaces (at the Gauss points) and average values are interpolated for the mid-surface. Every layer uses the same averaged values.

Sign Convention

□ Standard field elements

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Conductivity		1-point for each layer (PF6C), 3-point for each layer (PF12C), 2x2 for each layer (HF8C, HF16C) 3-point for each layer (PF6C), 3x3 for each layer (HF16C)
Specific Heat	Default. Fine (see <i>Options</i>)	3x2 for the whole element (PF6C, PF12C) or (see Options) 1-point for each layer (PF6C), 3-point for each layer (PF12C), 2x2x2 for the whole element or 2x2 for each layer (HF8C, HF16C) 3x2 for the whole element or 3-point for each layer (PF6C), 3x3x2 for the whole element or 3x3 for each layer (HF16C)

Specific Heat Modelling

- Consistent specific heat (default).
- Lumped specific heat.

Options

- **18** Invokes fine integration rule for elements.
- 105 Lumped specific heat.
- 266 Layer by layer computation of specific heat matrix.

Notes on Use

- 1. The element formulations are based on the standard isoparametric approach.
- 2. For linear field problems only one load case is allowed if an ENVT load is to be applied.
- 3. The COMPOSITE GEOMETRY and COMPOSITE MATERIAL data chapters must be used with this element in conjunction with the COMPOSITE ASSIGNMENTS data chapter.
- 4. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear solution progresses.

- 5. Automatic load incrementation under the NONLINEAR CONTROL data chapter cannot be used with TDET or RIHG loading.
- 6. When using load curves with TDET loading, the environmental temperatures will be factored but the heat coefficients will remain constant. If ENVT loading is used with load curves, any component can be controlled via a load curve.
- 7. If radiation is to be considered the problem becomes nonlinear and NONLINEAR CONTROL must be specified.
- 8. The through thickness integration is performed assuming a linear variation of the field gradient-variable matrix for each layer.
- 9. Layer 1 is always the bottom layer.
- 10. The simplifying assumptions which allow the uncoupling of in-plane and through thickness co-ordinates leads to the restriction that any individual layer should be of a constant thickness. This restriction should be considered when the finite element mesh is created and adhered to as closely as possible. In addition, out of plane lamina curvatures should also be minimised although in-plane curvature (in the x-y plane) is not restricted.

Restrictions

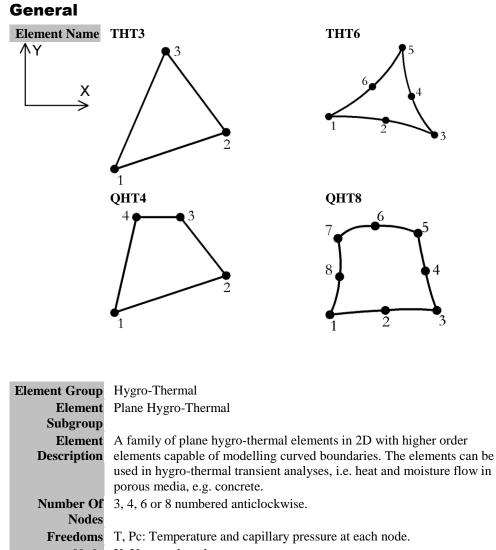
- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio
- □ Constant layer thickness for each individual layer

Recommendations on Use

The 3D solid composite field elements should be used for modelling thick composite structures comprising laminae of differing material properties where the computational cost of modelling each lamina with an individual solid element would be prohibitive. These field elements can be used to analyse continuum field problems where the response is fully 3D.

Chapter 10 : Hygro-Thermal Elements.

2D Plane Hygro-Thermal Elements



Node X, Y: at each node. **Coordinates**

Geometric Properties

t1... tn Thickness at each node.

Material Properties

Hygro-Thermal	Linear Isotropic	MATERIAL PROPERTIES HYGRO- THERMAL LINEAR
	Nonlinear Isotropic	MATERIAL PROPERTIES HYGRO- THERMAL CONCRETE

Loading

•		
Initial Conditions	TMPE	Initial temperature (T_0) and concrete relative humidity (RH) per element.
	TMP	Initial temperature (T_0) and concrete relative humidity (RH) per global nodes.
Prescribed Values	TDSP	Temperature (T) and concrete relative humidity (RH) at nodes.
	RGN	Rates of heat (QT) and/or water inflow (QW) concentrated at nodes.
	RBVE	Rates of heat and/or water inflow per unit volume, per element, can vary across the element.
	RBV	Rates of heat and/or water inflow per unit volume, per global nodes.
	RIHG	Rates of heat and/or water inflow per unit volume, per element at a specific reference nodal temperature (See Notes.)
Boundary Conditions	FFL	Rates of heat and/or water inflow per unit area (flux).
	ENVT	Environmental boundary conditions. Tenv, hc, hr, RH, hw: external environmental temperature, convective and radiative heat transfer coefficients, environmental relative humidity, water mass transfer coefficient. (See Notes.)
	TDET	Temperature dependent environmental boundary conditions. Tenv, hc, hr, RH, hw, T: external environmental temperature, convective and radiative heat transfer coefficients, environmental relative humidity, water mass transfer coefficient and reference nodal temperature. (See Notes.)

LUSAS Output

Solver Temperature gradients	G _T X, G _T Y, (in global directions)
Water saturation gradients	G _w X, G _w Y, (in global directions)
Temperature fluxes	qX, qY (in global directions)
Water fluxes	J_wX , J_wY , (in global directions)
Vapour fluxes	$J_v X$, $J_v Y$, (in global directions)
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

□ Standard surface element

Sign Convention

□ Standard field element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

1-point (THT3), 3-point (THT6), 2x2 (QHT4), 3x3 (QHT8).

Options

55 Output all element Gauss point derivatives and state variables

Notes on Use

1. The element formulations are based on the standard isoparametric approach. The variation of temperature and capillary pressure within an element is linear for the low order triangle and bi-linear for the low order quadrilateral; similarly it is quadratic for the higher order triangle and bi-quadratic for the higher order quadrilateral.

- 2. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear transient solution progresses.
- 3. Decreasing permeability and increasing water vapour convection coefficient in ENVT may result in divergence and an unstable solution. A rough estimate for the latter may be obtained by dividing the heat convection coefficient by a factor of 104 (obtained by the Chilton-Colburn analogy and scaled by an average porosity).
- 4. Variable thickness results in a heat and moisture transfer that is not in the plane of the element, this effect is neglected. The variable thickness influences only the amount of heat and moisture stored in the element's volume.
- 5. Heat of hydration loading is defined via the hygro-thermal concrete material properties.
- 6. Concrete relative humidity RH in TMPE, TMP and TPDSP is internally converted to capillary pressure (Pc).
- 7. ENVT load over the area of the element cannot be modelled.

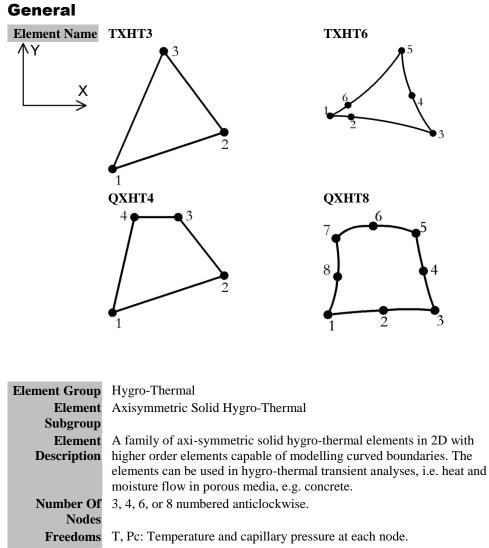
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio
- □ Certain combinations of permeability and convection boundary water vapour transfer coefficient may result in problems that do not converge.

Recommendations on Use

The plane hygro-thermal elements may be utilised for analysing continuum problems involving the heat of hydration of concrete, when behaviour is essentially two dimensional. These elements are normally used in a hygro-thermal-structural coupled analysis. They can be coupled with plane strain structural elements (since the heat/moisture exchange over the area of the element would have effect only near both ends of the 'infinite' thickness), or with thin, plane stress elements, when they are ideally isolated on both sides of their area.

2D Axisymmetric Solid Hygro-Thermal Elements



Node X, Y: at each node **Coordinates**

Geometric Properties

Not applicable (a unit radian segment is assumed).

Material Properties

Hygro-Thermal	Linear Isotropic	MATERIAL PROPERTIES HYGRO- THERMAL LINEAR
	Nonlinear Isotropic	MATERIAL PROPERTIES HYGRO- THERMAL CONCRETE

Loading

Initial Conditions	TMPE	Initial temperature (T_0) and concrete relative humidity (RH) per element.
	TMP	Initial temperature (T_0) and concrete relative humidity (RH) per global nodes.
Prescribed Values	TDSP	Temperature (T) and concrete relative humidity (RH) at nodes.
	RGN	Rates of heat (QT) and/or water inflow (QW) concentrated at nodes.
	RBVE	Rates of heat and/or water inflow per unit volume, per element, can vary across the element.
	RBV	Rates of heat and/or water inflow per unit volume, per global nodes.
	RIHG	Rates of heat and/or water inflow per unit volume, per element at a specific reference nodal temperature (See Notes.)
Boundary Conditions	FFL	Rates of heat and/or water inflow per unit area (flux).
	ENVT	Environmental boundary conditions. Tenv, hc, hr, RH, hw: external environmental temperature, convective and radiative heat transfer coefficients, environmental relative humidity, water mass transfer coefficient. (See Notes.)
	TDET	Temperature dependent environmental boundary conditions. Tenv, hc, hr, RH, hw, T: external environmental temperature, convective and radiative heat transfer coefficients, environmental relative humidity, water mass transfer coefficient and reference nodal temperature. (See Notes.)

LUSAS Output

Solver Temperature gradients	G _T X, G _T Y, (in global directions)
Water saturation gradients Temperature fluxes	G _w X, G _w Y, (in global directions) qX, qY (in global directions)
Water fluxes	J _w X, J _w Y, (in global directions)
Vapour fluxes	$J_v X$, $J_v Y$, (in global directions)
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes

□ Standard surface element

Sign Convention

□ Standard field element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

1-point (TXHT3), 3-point (TXHT6), 2x2 (QXHT4), 3x3 (QXHT8).

Options

- 47 Axisymmetry about the global X-axis
- 55 Output all element Gauss point derivatives and state variables

Notes on Use

1. The element formulations are based on the standard isoparametric approach. The variation of temperature and capillary pressure within an element is linear for the low order triangle and bi-linear for the low order quadrilateral; similarly it is quadratic for the higher order triangle and bi-quadratic for the higher order quadrilateral.

- 2. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear transient solution progresses.
- 3. Decreasing permeability and increasing water vapour convection coefficient in ENVT may result in divergence and an unstable solution. A rough estimate for the latter may be obtained by dividing the heat convection coefficient by a factor of 104 (obtained by the Chilton-Colburn analogy and scaled by an average porosity).
- 4. Variable thickness results in a heat and moisture transfer that is not in the plane of the element, this effect is neglected. The variable thickness influences only the amount of heat and moisture stored in the element's volume.
- 5. Heat of hydration loading is defined via the hygro-thermal concrete material properties.
- 6. Concrete relative humidity RH in TMPE, TMP and TPDSP is internally converted to capillary pressure (Pc).

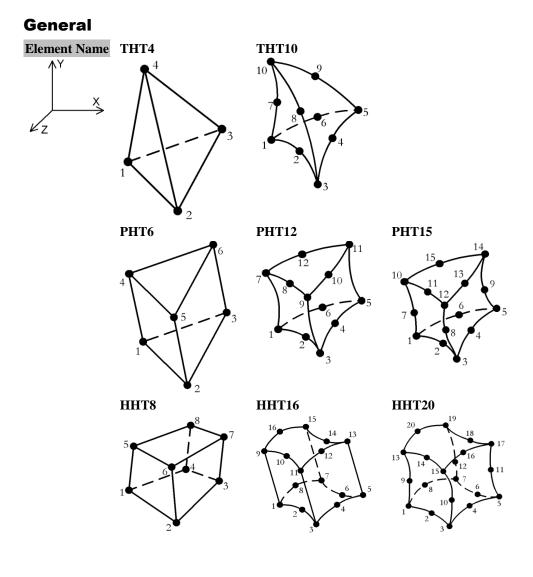
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio
- □ Certain combinations of permeability and convection boundary water vapour transfer coefficient may result in problems that do not converge.

Recommendations on Use

The axi-symmetric solid hygro-thermal elements may be utilised for analysing continuum problems involving the heat of hydration of concrete, which exhibit geometric and loading symmetry about a given axis. These elements are normally used in a hygro-thermal-structural coupled analysis.

3D Solid Hygro-Thermal Elements



Element GroupHygro-ThermalElementSolid Hygro-ThermalSubgroupA family of solid hygrElementA family of solid hygrDescriptionelements capable of m

A family of solid hygro-thermal elements in 3D with higher order elements capable of modelling curved boundaries. The elements can be

Number Of	used in hygro-thermal transient analyses, i.e. heat and moisture flow in porous media, e.g. concrete 4 and 10 (tetrahedra). 6, 12 and 15 (pentahedra). 8, 16 and 20
Nodes	(hexahedra). The elements are numbered according to a right-hand screw rule in the local z-direction.
Freedoms	T, Pc: Temperature and capillary pressure at each node.
Node	X, Y, Z: at each node.
Coordinates	

Geometric Properties

Not applicable.

Material Properties

Hygro-Thermal	Linear Isotropic	MATERIAL PROPERTIES HYGRO- THERMAL LINEAR
	Nonlinear Isotropic	MATERIAL PROPERTIES HYGRO- THERMAL CONCRETE

Loading

Initial Conditions	TMPE	Initial temperature (T_0) and concrete relative humidity (RH) per element.
	TMP	Initial temperature (T_0) and concrete relative humidity (RH) per global nodes.
Prescribed Values	TDSP	Temperature (T) and concrete relative humidity (RH) at nodes.
	RGN	Rates of heat (QT) and/or water inflow (QW) concentrated at nodes.
	RBVE	Rates of heat and/or water inflow per unit volume, per element, can vary across the element.
	RBV	Rates of heat and/or water inflow per unit volume, per global nodes.
	RIHG	Rates of heat and/or water inflow per unit volume, per element at a specific reference nodal temperature (See Notes.)
Boundary Conditions	FFL	Rates of heat and/or water inflow per unit area (flux).
	ENVT	Environmental boundary conditions . Tenv, hc, hr, RH, hw: external environmental temperature,

convective and radiative heat transfer
coefficients, environmental relative humidity,
water mass transfer coefficient. (See Notes.)TDETTemperature dependent environmental
boundary conditions. Tenv, hc, hr, RH, hw, T:
external environmental temperature, convective
and radiative heat transfer coefficients,
environmental relative humidity, water mass
transfer coefficient and reference nodal
temperature. (See Notes.)

LUSAS Output

Solver	Temperature gradients	$G_T X, G_T Y, G_T Z$ (in global directions)
	Water saturation gradients	G_WX, G_WY, G_WZ (in global directions)
	Temperature fluxes	qX, qY, qZ (in global directions)
	Water fluxes	J_wX , J_wY , J_wZ (in global directions)
	Vapour fluxes	$J_v X$, $J_v Y$, $J_w Z$ (in global directions)
Modeller	•	See <u>Results Tables (Appendix K)</u> .

Local Axes

Not applicable (global axes are the reference).

Sign Convention

□ Standard field element

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

1-point (THT4), 5-point (THT10), 3x2 (PHT6, PHT12, PHT15), 2x2x2 (HHT8), 3x3x2 (HHT16), 3x3x3 (HHT20)

Options

55 Output all element Gauss point derivatives and state variables

Notes on Use

- 1. The element formulations are based on the standard isoparametric approach. The distribution of temperature and capillary pressure within an element may be regarded as linear or bilinear for low order elements and quadratic or bi-qudratic for higher order elements.
- 2. Load curves can be used to maintain or increment ENVT, TDET or RIHG loading as a nonlinear solution progresses.
- 3. Decreasing permeability and increasing water vapour convection coefficient in ENVT may result in divergence and an unstable solution. A rough estimate for the latter may be obtained by dividing the heat convection coefficient by a factor of 104 (obtained by the Chilton-Colburn analogy and scaled by an average porosity).
- 4. Heat of hydration loading is defined via the hygro-thermal concrete material properties.
- 5. Concrete relative humidity RH in TMPE, TMP and TPDSP is internally converted to capillary pressure (Pc).

Restrictions

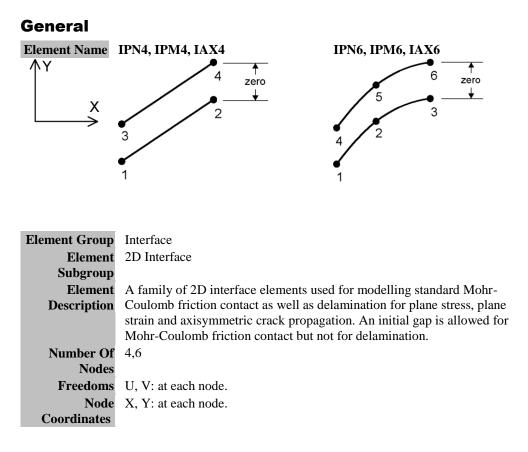
- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio
- □ Certain combinations of permeability and convection boundary water vapour transfer coefficient may result in problems that do not converge.

Recommendations on Use

The solid hygro-thermal elements may be used to analyse continuum problems where the response is fully 3D (i.e. it cannot be approximated using the plane or axisymmetric elements). These elements are generally used for problems involving the heat of hydration of concrete, and are normally used in a hygro-thermal-structural coupled analysis.

Chapter 11 : Interface Elements.

2D Interface Element



Geometric Properties

Not applicable to plane strain and axisymmetric elements. For plane stress t1..tn for each node

Material Properties

Linear	Not applicable
Matrix	Not applicable
Joint	Not applicable
Concrete	Not applicable
Elasto-Plastic	Not applicable
Creep	Not applicable

Damage	Not applicable	
Viscoelastic	Not applicable	
Shrinkage	Not applicable	
Interface	Interface	MATERIAL PROPERTIES NONLINEAR 25
	Interface	MATERIAL PROPERTIES INTERFACE
Rubber	Not applicable	
Generic Polymer	Not applicable	
Composite	Not applicable	

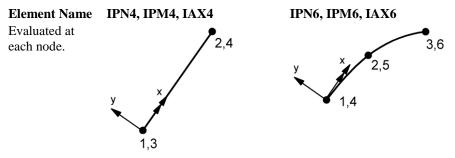
Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V: at each node.
Concentrated	CL	Concentrated loads. Px, Py: at each node.
Loads		
Element Loads	Not applicable.	
Distributed Loads	Not applicable.	
Body Forces	Not applicable.	
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay: at nodes.
Initial	Not applicable.	
Stress/Strains		
Residual Stresses	Not applicable.	
Target	Not applicable.	
Stress/Strains		
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not applicable.	
Loads		

LUSAS Output

Solver	Stress (default): shear and direct tractions.
	Strain: shear and direct relative displacements
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes



Sign Convention

A positive traction occurs if the local relative displacement (with respect to the first line of the element) is a positive value, i.e. for the quadratic elements at nodes 3 > 6 the local relative displacement, Ez, would be positive if (Dz3 - Dz6) > 0, where Dzi is the local displacement at node i.

Formulation

Geometric Nonlinearity

Total Lagrangian	Not applicable.
Updated	Not applicable.
Lagrangian	
Eulerian	Not applicable.
Co-rotational	Applicable to IPN4 and IAX4 elements.

Integration Schemes

StiffnessDefault.2 (Newton Cotes) (IPN4, IPM4, IAX4) 3 (Newton-Cotes) (IPN6, IPM6, IAX6)Fine.As default

Mass Modelling

Not applicable.

Options

- 62 Continue solution if more than one negative pivot occurs
- 64 Non-symmetric solver
- 229 Co-rotational geometric non-linearity.
- 252 Suppress pivot warning messages.
- 261 Select the root with the lowest residual norm with arc-length.

Notes on use in delamination analyses

- 1. When defining the transient analysis control the arc-length procedure should be adopted with the option to select the root with the lowest residual norm [option 261].
- 2. It is recommended that fine integration [option 18] is selected for the parent elements.
- 3. The nonlinear convergence criteria should be selected to converge on the residual norm.
- 4. Option 62, Continue solution if more than one negative pivot occurs, should be selected to continue if more than one negative pivot is encountered and option 252 should be used to suppress pivot warning messages from the solution process.
- 5. The non-symmetric solver is selected automatically when mixed mode delamination is specified.
- 6. Although the solution is largely independent of the mesh discretisation, to avoid convergence difficulties it is recommended that at least 2 elements are placed in the process zone.

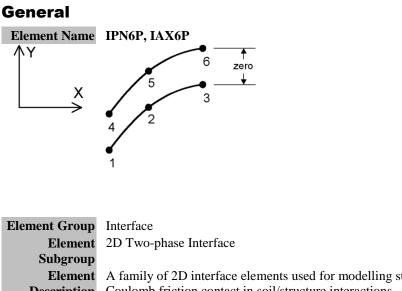
Restrictions

None.

Recommendations on Use

These elements may be used to model contact between two bodies. For delamination problems they should be placed at sites of potential delamination between 2D plane and axisymmetric continuum elements. The non-symmetric solver should be used.

2D Two Phase Interface Element



Licitent	2D Two phase interface
Subgroup	
Element	A family of 2D interface elements used for modelling standard Mohr-
Description	Coulomb friction contact in soil/structure interactions.
Number Of	6
Nodes	
Freedoms	U, V, P: at end nodes, U,V at middle nodes.
Node	X, Y: at each node.

Coordinates

Geometric Properties

Not applicable to plane strain and axisymmetric elements. For plane stress t1..tn for each node

Material Properties

Linear	Not applicable
Matrix	Not applicable
Joint	Not applicable
Concrete	Not applicable
Elasto-Plastic	Not applicable
Creep	Not applicable
Damage	Not applicable
Viscoelastic	Not applicable

Shrinkage Interface	Not applicable Interface	MATERIAL PROPERTIES NONLINEAR 25
	Interface	MATERIAL PROPERTIES INTERFACE
Rubber	Not applicable	
Generic Polymer	Not applicable	
Composite	Not applicable	
Two-Phase	Interface	TWO PHASE MATERIAL INTERFACE

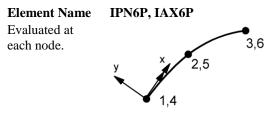
Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, P: at end nodes, U,V at middle nodes.
Concentrated Loads	CL	Concentrated loads. Px, Py, Q: at end nodes, Px, Py at middle nodes.
Element Loads	Not applicable.	
Distributed Loads	Not applicable.	
Body Forces	Not applicable.	
Velocities	VELO	Velocities. Vx, Vy: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay: at nodes.
Initial	Not applicable.	
Stress/Strains		
Residual Stresses	Not applicable.	
Target	Not applicable.	
Stress/Strains		
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not applicable.	
Loads		

LUSAS Output

Solver	Stress (default): shear and direct tractions.
	Strain: shear and direct relative displacements
Modeller	See <u>Results Tables (Appendix K)</u> .

Local Axes



Sign Convention

A positive traction occurs if the local relative displacement (with respect to the first line of the element) is a positive value, i.e. for the quadratic elements at nodes 3 > 6 the local relative displacement, Ez, would be positive if (Dz3 - Dz6) > 0, where Dzi is the local displacement at node i.

Formulation

Geometric Nonlinearity

Total Lagrangian	Not applicable.
Updated	Not applicable.
Lagrangian	
Eulerian	Not applicable.
Co-rotational	Not applicable.

Integration Schemes

StiffnessDefault.3 (<u>Newton-Cotes</u>)Fine.As default

Mass Modelling

Not applicable.

Options

64 Non-symmetric solver

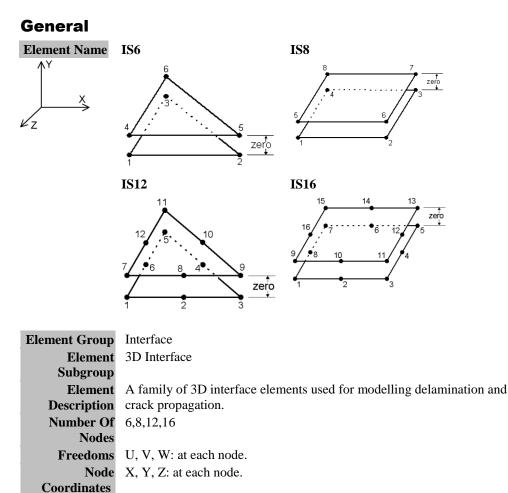
Restrictions

None.

Recommendations on Use

These elements should be used to model soil/structure and soil/soil interactions. The nonsymmetric solver should be used.

3D Interface Element



Geometric Properties

Not applicable (a zero thickness is assumed).

Material Properties

Linear	Not applicable
Matrix	Not applicable
Joint	Not applicable

Concrete	Not applicable	
Elasto-Plastic	Not applicable	
Creep	Not applicable	
Damage	Not applicable	
Viscoelastic	Not applicable	
Shrinkage	Not applicable	
Interface	Interface	MATERIAL PROPERTIES NONLINEAR 25
	Interface	MATERIAL PROPERTIES INTERFACE
Rubber	Not applicable	
Generic Polymer	Not applicable	
Composite	Not applicable	

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, W: at each node.
Concentrated Loads	CL	Concentrated loads. Px, Py, Pz: at each node.
Element Loads	Not applicable.	
Distributed Loads	Not applicable.	
Body Forces	Not applicable.	
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay, Az: at nodes.
Initial Stress/Strains	Not applicable.	
Residual Stresses	Not applicable.	
Target	Not	
Stress/Strains	applicable.	
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	
Field Loads	Not applicable.	

Temp DependentNotLoadsapplicable.

LUSAS Output

Solver	Stress (default): shear tractions in X and Y, and direct tractions.
	Strain: relative displacements in X, Y and Z directions.
Modeller	See Results Tables (Appendix K).

Local Axes **Element Name** IS6 IS8 4,8 3,7 3,6 Evaluated at each node. 2.6 2,5 1,4 **IS12 IS16** 7,15 5,11 6,14 5,13 Evaluated at each node. 4,12 6,12 4.10 3,1 2,8 <u>3</u>,9 1.7

Sign Convention

A positive traction occurs if the local relative displacement (with respect to the first surface of the element) is a positive value, i.e. for the IS16 element at nodes 3 > 11 the local relative displacement, Ez, would be positive if (Dz11 - Dz3) > 0, where Dzi is the local displacement at node i.

Formulation

Geometric Nonlinearity

Total Lagrangian	Not applicable.
Updated	Not applicable.
Lagrangian	
Eulerian	Not applicable.
Co-rotational	Applicable to IS6 and IS8 elements.

Integration Schemes

Stiffness	Default.	3x3 (Newton-Cotes) (IS16), 2x2 (Newton Cotes) (IS8), 7-point cubic
		(IS12), 3-point (IS6)
	Fine.	As default

Mass Modelling

Not applicable.

Options

- 62 Continue solution if more than one negative pivot occurs.
- 64 Non-symmetric solver.
- **229** Co-rotational geometric non-linearity.
- 252 Suppress pivot warning messages
- 261 Select the root with the lowest residual norm with arc-length.

Notes on Use

- 1. When defining the transient analysis control the arc-length procedure should be adopted with the option to select the root with the lowest residual norm [option 261].
- 2. It is recommended that fine integration [option 18] is selected for the parent elements.
- 3. The nonlinear convergence criteria should be selected to converge on the residual norm.
- 4. Option 62, Continue solution if more than one negative pivot occurs, should be selected to continue if more than one negative pivot is encountered and option 252 should be used to suppress pivot warning messages from the solution process.

- 5. The non-symmetric solver is selected automatically when mixed mode delamination is specified.
- 6. Although the solution is largely independent of the mesh discretisation, to avoid convergence difficulties it is recommended that at least 2 elements are placed in the process zone.

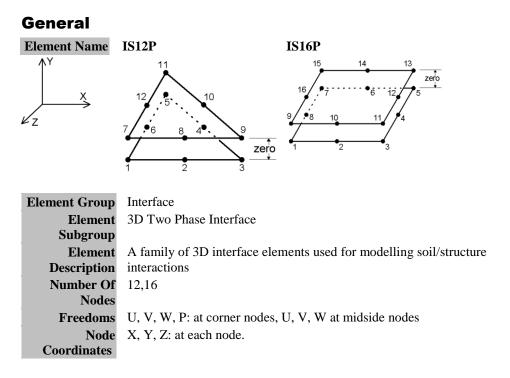
Restrictions

None.

Recommendations on Use

These elements should be used at places of potential delamination between 3D continuum elements. The non-symmetric solver should be used.

3D Two Phase Interface Element



Geometric Properties

Not applicable (a zero thickness is assumed).

Material Properties

Linear	Not applicable
Matrix	Not applicable
Joint	Not applicable
Concrete	Not applicable
Elasto-Plastic	Not applicable
Creep	Not applicable
Damage	Not applicable
Viscoelastic	Not applicable
Shrinkage	Not applicable
Interface	Interface

MATERIAL PROPERTIES NONLINEAR 25

erface	MATERIAL PROPERTIES INTERFACE
erface	TWO PHASE MATERIAL INTERFACE
t applicable	
t applicable	
t applicable	
t	applicable applicable

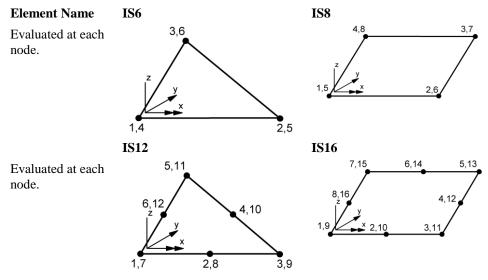
Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, W, Q: at corner nodes U,V,W at midside nodes.
Concentrated Loads	CL	Concentrated loads. Px, Py, Pz, Q: at corner nodes, Px, Py, Pz at midside nodes.
Element Loads	Not applicable.	
Distributed Loads	Not applicable.	
Body Forces	Not applicable.	
Velocities	VELO	Velocities. Vx, Vy, Vz: at nodes.
Accelerations	ACCE	Acceleration Ax, Ay, Az: at nodes.
Initial	Not	
Stress/Strains	applicable.	
Residual Stresses	Not applicable.	
Target	Not	
Stress/Strains	applicable.	
Temperatures	TEMP, TMPE	Temperatures at nodes/for element. T, 0, 0, 0, To, 0, 0, 0
Overburden	Not applicable.	
Phreatic Surface	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent Loads	Not applicable.	

LUSAS Output

Solver	Stress (default): shear tractions in X and Y, and direct tractions.
	Strain: relative displacements in X, Y and Z directions.
Modeller	See Results Tables (Appendix K).

Local Axes



Sign Convention

A positive traction occurs if the local relative displacement (with respect to the first surface of the element) is a positive value, i.e. for the IS16 element at nodes 3 > 11 the local relative displacement, Ez, would be positive if (Dz11 - Dz3) > 0, where Dzi is the local displacement at node i.

Formulation

Geometric Nonlinearity

Total Lagrangian	Not applicable.
Updated	Not applicable.
Lagrangian	
Eulerian	Not applicable.
Co-rotational	Applicable to IS6 and IS8 elements.

Integration Schemes

StiffnessDefault.3x3 (Newton-Cotes) (IS16), 2x2 (Newton Cotes) (IS8), 7-point cubic
(IS12), 3-point (IS6)Fine.As default

Mass Modelling

Not applicable.

Options

64 Non-symmetric solver.

Restrictions

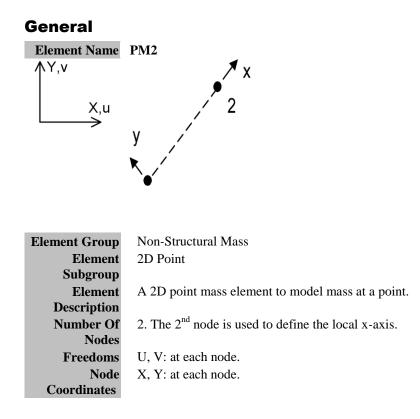
None.

Recommendations on Use

These elements should be used to model soil/structure and soil/soil interactions. The non-symmetric solver should be used.

Chapter 12 : Non-Structural Mass Elements

2D Point Mass Element



Geometric Properties

Not applicable.

Material Properties

Linear	Not applicable	
Matrix	Not applicable	
Joint	Not applicable	
Mass	2D	MATERIAL PROPERTIES MASS 2 1
Concrete	Not applicable	
Elasto-Plastic	Not applicable	
Creep	Not applicable	
Damage	Not applicable	
Viscoelastic	Not applicable	

ShrinkageNot applicableRubberNot applicableGeneric PolymerNot applicableCompositeNot applicableFieldNot applicable

Loading

Prescribed CBF Value Constant body forces for element. Xcbf, Ycbf, Zcbf (applied as accelerations)

LUSAS Output

None

Local Axes

The 2nd node is used to define the local x-axis.

Sign Convention

□ Not applicable.

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Not applicable.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

105 Lumped mass matrix.

Notes on Use

1. Use to model point mass in a structure.

Restrictions

None.

Recommendations on Use

The 2D point mass element can be used to model point masses occur in a 2D structure.

3D Point Mass Element

General	
Element Name	PM3
∱ Υ,ν	♠ x
X,u	2 •
	1 , 7 3
	' ∲ > y
Element Course	Non Structural Mass
-	Non-Structural Mass
Element	3D Point
Subgroup	A 2D maint many alamant to madel many at a maint
Element Description	A 3D point mass element to model mass at a point.
-	2. The Ond we do is used to define the level of suit. The Ond and Ond we do
	3. The 2nd node is used to define the local x-axis. The 2nd and 3rd node define the local x y plane.
	define the local x-y plane.
	U, V, W: at each node.
Node	X, Y, Z: at each node.
Coordinates	

Geometric Properties

Not applicable.

Material Properties

Linear	Not applicable
Matrix	Not applicable
Joint	Not applicable
Mass	3D.
Concrete	Not applicable
Elasto-Plastic	Not applicable
Creep	Not applicable

MATERIAL PROPERTIES MASS 3 1

Damage	Not applicable
Viscoelastic	Not applicable
Shrinkage	Not applicable
Rubber	Not applicable
Generic Polymer	Not applicable
Composite	Not applicable

Loading

Constant body forces for element. Xcbf, Ycbf, Zcbf (applied as accelerations)

Output

None

Local Axes

The 2^{nd} node is used to define the local x-axis. The 2^{nd} and 3^{rd} node define the local x-y plane.

Sign Convention

□ Not applicable.

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Not applicable.

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

105 Lumped mass matrix.

Notes on Use

1. Use to model point mass in a structure.

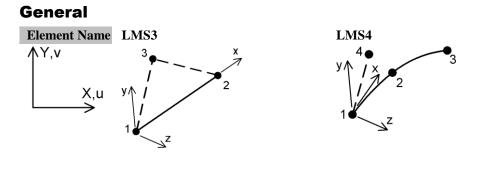
Restrictions

None.

Recommendations on Use

The 3D point mass element can be used to model point masses occur in a 3D structure.

3D Line Mass Elements



Element Group	Non-Structural Mass
Element	3D Line
Subgroup	
Element	3D straight (LMS3) and curved (LMS4) line mass elements to model
Description	mass along an edge. The elements can accommodate varying mass along
	the length.
	3 (LMS3). The 3^{rd} node is used to define the local x-y plane.
Nodes	4 (LMS4). The 4 th node is used to define the local x-y plane.
End Releases	
Freedoms	U, V, W, θx , θy , θz : at each active node (see <i>Notes</i>).
Node	X, Y, Z : at each node.
Coordinates	

Geometric Properties

Not applicable.

Material Properties

Linear	Not applicable
Matrix	Not applicable
Joint	Not applicable.
Mass	3D.
Concrete	Not applicable
Elasto-Plastic	Not applicable
Creep	Not applicable
Damage	Not applicable

MATERIAL PROPERTIES MASS 3 2 (or 3)

Viscoelastic	Not applicable
Shrinkage	Not applicable
Rubber	Not applicable
Generic Polymer	Not applicable
Composite	Not applicable

Loading

Prescribed Value CBF

Constant body forces for element. Xcbf, Ycbf, Zcbf (applied as accelerations)

Output

None

Local Axes

□ Standard Line Element

Sign Convention

□ Not applicable.

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Mass Default. 2-point Fine 2-point (LMS2), 3-point (LMS3)

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- **18** Invokes fine integration rule.
- **105** Lumped mass matrix.

Notes on Use

- 1. Use to model mass on an edge in a structure.
- 2. There is no mass associated with the rotational degrees of freedom θx , θy , θz ; these freedoms are used purely to orientate the directions of the local element axes. If the LMS3/LMS4 elements are connected to an element that does not possess the same rotational degrees of freedom (e.g. the edge of a continuum element), then the rotational degrees of freedom will automatically be restrained

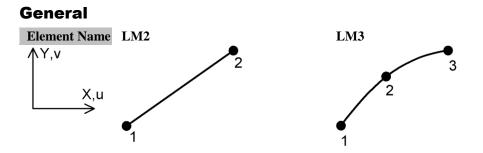
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature

Recommendations on Use

3D line mass elements can be used to model masses along an edge in a 3D structure.

2D Line Mass Elements



Element Group	Non-Structural Mass
Element	2D Line
Subgroup	
Element	2D straight (LM2) and curved (LM3) line mass elements to model mass
Description	along an edge. The elements can accommodate varying mass along the
	length.
Number Of	2 (LM2). 3 (LM3).
Nodes	
End Releases	
Freedoms	U, V: at each node.
Node	X, Y: at each node.
Coordinates	

Geometric Properties

Not applicable.

Material Properties

Linear	Not applicable
Matrix	Not applicable
Joint	Not applicable
Mass	2D.
Concrete	Not applicable
Elasto-Plastic	Not applicable
Creep	Not applicable
Damage	Not applicable

MATERIAL PROPERTIES MASS 2 2 (or 3)

Viscoelastic	Not applicable
Shrinkage	Not applicable
Rubber	Not applicable
Generic Polymer	Not applicable
Composite	Not applicable

Loading

Prescribed Value CBF

Constant body forces for element. Xcbf, Ycbf, Zcbf (applied as accelerations)

Output

None

Local Axes

□ Standard Line Element

Sign Convention

□ Not applicable.

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Mass Default. 2-point Fine 2-point (LM2), 3-point (LM3)

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

- **18** Invokes fine integration rule.
- 105 Lumped mass matrix.

Notes on Use

1. Use to model mass on an edge in a structure.

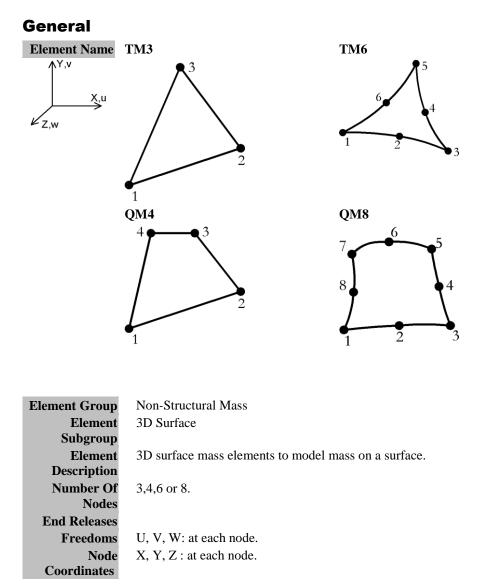
Restrictions

- □ Ensure mid-side node centrality
- □ Avoid excessive element curvature

Recommendations on Use

2D line mass elements can be used to model masses along an edge in a 2D structure.

Surface Mass Elements



Geometric Properties

Not applicable.

Material Properties

Linear	Not applicable	
Matrix	Not applicable	
Joint	Not applicable	
Mass	3D	MATERIAL PROPERTIES MASS 3 (3,4,6 or 8)
Concrete	Not applicable.	
Elasto-Plastic	Not applicable.	
Creep	Not applicable	
Damage	Not applicable	
Viscoelastic	Not applicable	
Shrinkage	Not applicable	
Rubber	Not applicable	
Generic Polymer	Not applicable	
Composite	Not applicable.	

Loading

Prescribed	Value	CBF	

Constant body forces for element. Xcbf, Ycbf, Zcbf (applied as accelerations)

Output

None

Local Axes

□ Standard Surface Element

Sign Convention

Not applicable.

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Mass	Default.	1-point (TM3), 3-point (TM6), 4-point (QM4,QM8)
	Fine	3-point (TM3, TM6), 4-point (QM4), 9-point (QM8)

Mass Modelling

- □ Consistent mass (default).
- □ Lumped mass.

Options

18	Invokes fine integration rule.
105	Lumped mass matrix.

Notes on Use

1. Use to model mass on a surface in a structure.

Restrictions

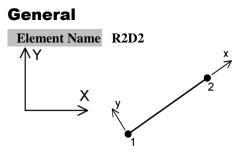
- Ensure mid-side node centrality
- □ Avoid excessive element curvature
- □ Avoid excessive aspect ratio

Recommendations on Use

The surface mass elements can be used to model masses on a surface 3D structures.

Chapter 13 : Rigid Slideline Elements

Rigid Slideline Surface 2D Elements



Element Group	Rigid
Element	2D Rigid Slideline Surface
Subgroup	
Element	2D Rigid Slideline Surface elements capable of modelling non-
Description	deformable surfaces in a contact analysis.
Number Of	2
Nodes	
Freedoms	U, V at each node
Node	X, Y at each node.
Coordinates	

Geometric Properties

Not applicable.

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
Loading		
Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V at each node.
Concentrated	Not applicable.	
Loads		
Element Loads	Not applicable.	
Distributed Loads	Not applicable.	
Body Forces	Not applicable.	
Velocities	VELO	Velocities. Vx, Vy at nodes.

Accelerations	ACCE	Acceleration Ax, Ay at nodes.
Initial	Not applicable.	
Stress/Strains		
Residual Stresses	Not applicable.	
Temperatures	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not applicable.	
Loads		

LUSAS Output

Solver	Displacements & Reactions only.
Modeller	Displacements & Reactions only.

Formulation

Geometric Nonlinearity

Total Lagrangian	Depends on the other surface (deformable surface) which is in contact with the rigid surface. See the related section for the deformable surface elements.
Updated	As above.
Lagrangian	
Eulerian	As above.
Co-rotational	As above.

Integration Schemes

Not applicable.

Mass Modelling

Not applicable.

Restrictions

- A rigid slideline surface cannot contact another rigid slideline surface.
- Rigid slideline surface elements do not accept external applied forces.

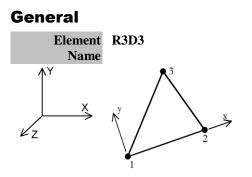
Notes on use

- 1. All the rigid slideline surface element nodes must be fully restrained.
- 2. There is no stress and strain calculation for these elements.
- 3. If rigid slideline surfaces are defined there is no need to assign geometric and material properties to these elements. However, when using automatic contact surfaces, linear elastic isotropic material properties need to be assigned.
- 4. For saving analysis time a one pass contact algorithm can be used. In this case only the penetration of the deformable surface into the rigid slideline surface is checked. To avoid the penetration of the rigid surface into the deformable surface use either the default two pass algorithm or a finer mesh on the deformable surface.

Recommendations on Use

These elements should be used when one of the surfaces which come into contact is nondeformable. Using these elements will make the analysis faster.

Rigid Slideline Surface 3D Elements



R3D4

Element Group	Rigid
Element	3D Rigid Slideline Surface
Subgroup	
Element	3D Rigid Slideline Surface elements capable of modelling non-
Description	deformable surfaces in a contact analysis.
Number Of	3/4
Nodes	
Freedoms	U, V, W at each node.
Node	X, Y, Z at each node.
Coordinates	

Geometric Properties

Not applicable.

Material Properties

Linear	Isotropic:	MATERIAL PROPERTIES (Elastic: Isotropic)
Loading		
Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V, W at each node.
Concentrated	Not applicable.	
Loads		
Element Loads	Not applicable.	
Distributed Loads	Not applicable.	
Body Forces	Not applicable.	

Velocities	VELO	Velocities. Vx, Vy, Vz at nodes.
Accelerations	ACCE	Acceleration Ax, Ay, Az at nodes.
Initial	Not applicable.	
Stress/Strains		
Residual Stresses	Not applicable.	
Temperatures	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not applicable.	
Loads		

LUSAS Output

Solver	Displacements & Reactions only.
Modeller	Displacements & Reactions only.

Formulation

Geometric Nonlinearity

Total Lagrangian	Depends on the other surface (deformable surface) which is in contact with the rigid surface. See the related section for the deformable surface elements.
Updated	As above.
Lagrangian	
Eulerian	As above.
Co-rotational	As above.

Integration Schemes

Not applicable.

Mass Modelling

Not applicable.

Restrictions

- A rigid slideline surface cannot contact another rigid surface.
- Rigid slideline surface elements do not accept external applied forces.

Notes on use

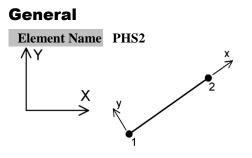
- 1. All the rigid slideline surface element nodes must be fully restrained.
- 2. There is no stress and strain calculation for these elements.
- 3. If rigid slideline surfaces are defined there is no need to assign geometric and material properties to these elements. However, when using automatic contact surfaces, linear elastic isotropic material properties need to be assigned.
- 4. For saving analysis time a one pass contact algorithm can be used. In this case only the penetration of the deformable surface into the rigid slideline surface is checked. To avoid the penetration of the rigid surface into the deformable surface use either the default two pass algorithm or a finer mesh on the deformable surface.

Recommendations on Use

These elements should be used when one of the surfaces which come into contact is nondeformable. Using these elements will make the analysis faster.

Chapter 14 : Phreatic Elements

Phreatic Surface 2D Elements



Element Group	Phreatic surface
Element	2D Phreatic Surface
Subgroup	
Element	2D Phreatic surface elements for defiing phreatic surface
Description	
Number Of	2
Nodes	
Freedoms	U, V at each node
Node	X, Y at each node.
Coordinates	

Geometric Properties

Not applicable.

Material Properties

Not applicable.

Loading

Prescribed Value	PDSP, TPDSP	Prescribed variable. U, V at each node.
Concentrated	Not applicable.	
Loads		
Element Loads	Not applicable.	
Distributed Loads	Not applicable.	
Body Forces	Not applicable.	
Velocities	VELO	Velocities. Vx, Vy at nodes.

Accelerations	ACCE	Acceleration
Initial	Not applicable.	
Stress/Strains		
Residual Stresses	Not applicable.	
Temperatures	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not applicable.	
Loads		

Acceleration Ax, Ay at nodes.

LUSAS Output

Not applicable.

Formulation

Geometric Nonlinearity

Not applicable.

Integration Schemes

Not applicable.

Mass Modelling

Not applicable.

Restrictions

Not applicable.

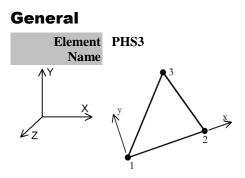
Notes on use

- 1. All the phreatic surface element nodes must be fully restrained.
- 2. There are no stress or strain calculations.
- 3. There is no need to assign geometric and material properties.
- 4. The phreatic surface elements are used with the Phreatic Surface load type and are used to define the location and extent of a phreatic surface.

Recommendations on Use

These elements are for use in geotechnical problems for the definition of the nodal pore-water pressures and hydrostatic loads.

Phreatic Surface 3D Elements



PHS4

Element Group	Phreatic Surface
Element	3D Phreatic Surface
Subgroup	
Element	3D Phreatic surface elements for defiing phreatic surface.
Description	
Number Of	3/4
Nodes	
Freedoms	U, V, W at each node.
Node	X, Y, Z at each node.
Coordinates	

Geometric Properties

Not applicable.

Material Properties

Not applicable.

Loading

PDSP, TPDSP	Prescribed variable. U, V, W at each node.
Not applicable.	
Not applicable.	
Not applicable.	
Not applicable.	
	Not applicable. Not applicable. Not applicable.

Velocities	VELO	Velocities. Vx, Vy, Vz at nodes.
Accelerations	ACCE	Acceleration Ax, Ay, Az at nodes.
Initial	Not applicable.	
Stress/Strains		
Residual Stresses	Not applicable.	
Temperatures	Not applicable.	
Field Loads	Not applicable.	
Temp Dependent	Not applicable.	

LUSAS Output

Not applicable.

Formulation

Geometric Nonlinearity

Loads

Not applicable.

Integration Schemes

Not applicable.

Mass Modelling

Not applicable.

Restrictions

Not applicable.

Notes on use

- 1. All the phreatic surface element nodes must be fully restrained.
- 2. There are no stress or strain calculations.
- 3. There is no need to assign geometric and material properties.
- 4. The phreatic surface elements are used with the Phreatic Surface load type and are used to define the location and extent of a phreatic surface.

Recommendations on Use

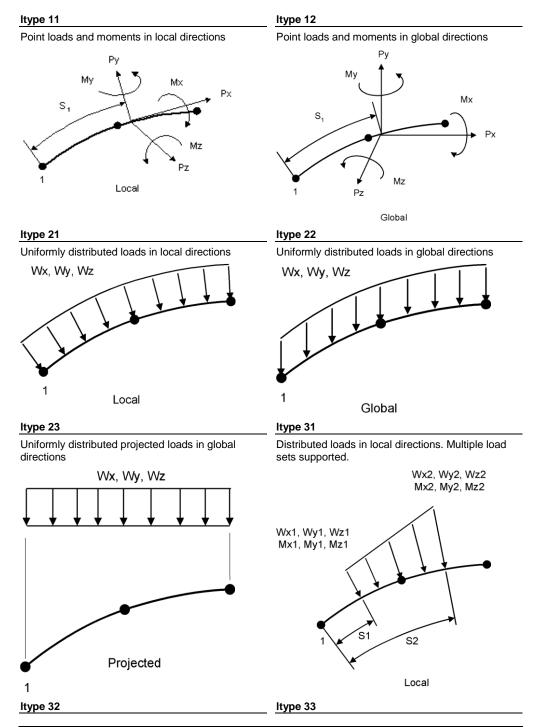
These elements are for use in geotechnical problems for the definition of the nodal pore-water pressures and hydrostatic loads.

Appendix A : Element and Pressure Loads.

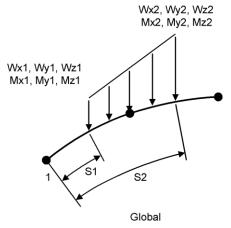
ELDS Element Loads

These are referred to as Internal Beam Point Loads and Internal Beam Distributed Loads within LUSAS Modeller.

Parameter	Description
ltype	Element load type
S1, S2	Distances to specified loads
Px, Py, Pz	Point loads in local/global directions
Mx, My, Mz	Point moments in local/global directions
Wx, Wy, Wz	Distributed loads in local/global directions



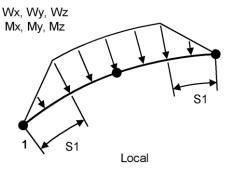
Distributed loads in global directions. Multiple load sets supported.



Itype 41

Trapezoidal loads in local directions

Definition only supported in LUSAS Solver. In LUSAS Modeller trapezoidal beam loads are defined in accordance with ltype 31.



Itype 43

Trapezoidal projected loads in global directions

Definition only supported in LUSAS Solver. In LUSAS Modeller trapezoidal beam loads are defined in accordance with ltype 33.

Distributed projected loads in global directions. Multiple load sets supported.

Wx2, Wy2, Wz2

Mx2, My2, Mz2

ltype 42

Wx1, Wy1, Wz1

Mx1, My1, Mz1

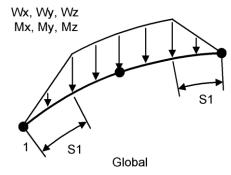
Trapezoidal loads in global directions

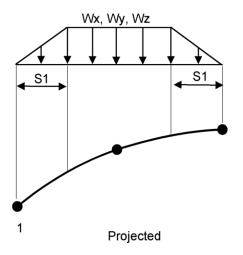
s1

Definition only supported in LUSAS Solver. In LUSAS Modeller trapezoidal beam loads are defined in accordance with ltype 32.

S2

Global

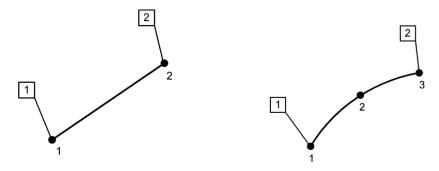




ENVT/TDET Environmental Boundary Conditions

Contains some or all of:

Parameter	Description
Tenv	External environmental temperature.
hc	Convective heat transfer coefficient.
RH	Radiative heat transfer coefficient.
hv	Vapour mass transfer coefficient.
т	Temperature for element.

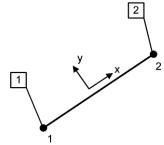


Face Numbering Convention for Thermal Bars

Note

The environmental temperature loading for node 2 cannot be specified for a 3 noded bar.

FLD Face loading applied to thermal bars



Face number = local node number

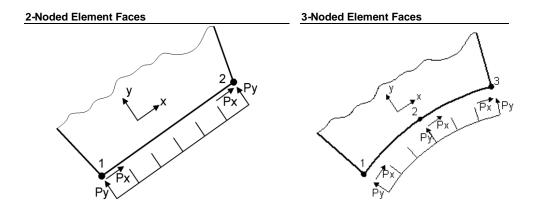
Face Numbering Convention for Thermal Bars

Face Loads On 2D Continuum Elements

Parameter	Description

Р

Yx, Py	Face pressures defined at nodes in local x, y
	directions



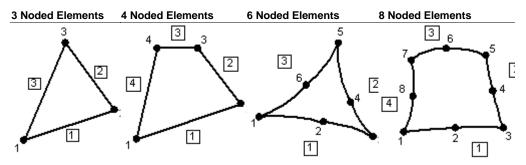
Notes

• In structural analysis note that the direction of the normal face load is not consistent between 2D and 3D continuum elements. For 2D continuum elements it is from the

face towards the interior of the element. For 3D elements it is in the opposite direction - from the face of the element outwards.

• Face loads for explicit dynamics elements are constant, i.e. the average of the input nodal pressures

Face Numbering Convention



Face Loads On 3D Continuum Elements

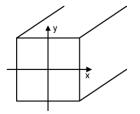
coordinate directions

Parameter	Description
Px. Pv. Pz	Face pressures defined at nodes in local x. v directions acting positively in the local

Note

- In structural analysis note that the direction of the normal face load is not consistent between 2D and 3D continuum elements. For 2D continuum elements it is from the face towards the interior of the element. For 3D elements it is in the opposite direction from the face of the element outwards.
- Face loads for explicit dynamics elements are constant, i.e. the average of the input nodal pressures.+

Local Face Coordinates

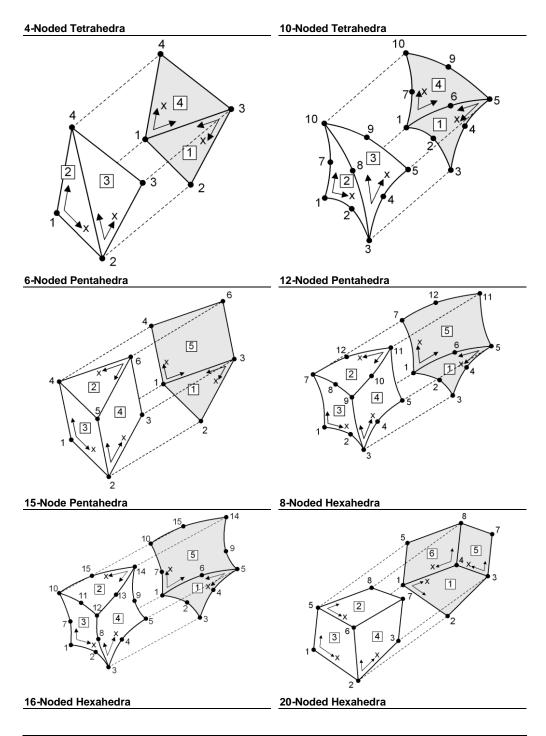


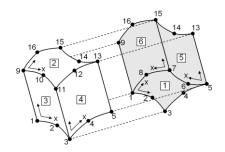
Face Numbering Convention

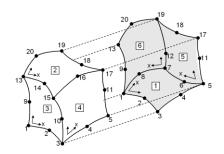
The following diagrams show exploded view of the various 3D elements. The grey faces show the element external faces that can be seen from a single perspective point, the white faces depict the internal faces from the same view point.

Notes

• The views of the internal faces show the x-axis direction from the inside. Take care when converting this to a view from the outside of the element.







UDL Loads on Shells

Appendix B : Element Restrictions.

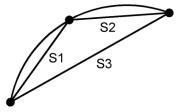
Mid-side Node Centrality

The mid-length node must be equidistant from the end nodes. Mid-side nodes may be automatically corrected for elements with global translational mid-side node freedoms using Option 49. The mid-side node is moved along the existing element edge until it is positioned centrally.

Excessive Element Curvature

Elements must not be excessively curved. A warning will be invoked (but the analysis will continue) if the element curvature is not in accordance with the following inequalities:

i) ABS (S1-S2) / (S1+S2) < 0.05
ii) (S1+S2) / S3 < 1.02</pre>

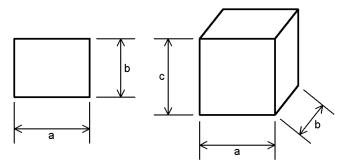


Where the function ABS returns the absolute value of the arguments.

Excessive Aspect Ratios

An aspect ratio can be defined as the ratio of the longest to shortest element side lengths, such that:

- \square R = max (a/b, b/a) for surface elements (e.g. 2D continuum, plates and shells)
- \square R = max (a/b, b/a, c/a, c/b, ...) for three dimensional solid elements



Elements must not have an excessive aspect ratio. A warning will be invoked (but the analysis will continue) if the element aspect ratio is greater than 10.

In general, severe distortion of an element will affect the accuracy of the stress distribution through an element. The type of stress field being imposed is also of importance, since a badly shaped element will still yield a good distribution in the presence of a constant uniaxial stress field, but not when subjected to a full stress field in which any of the components have a significant variation across the element.

The force equilibrium for the element will always be satisfied.

Excessive Warping

The four nodal points defining quadrilateral surface elements should be coplanar. However a small out of plane tolerance is permitted to allow a slightly warped shape according to

z < 0.01(L12)

where \mathbf{z} is the out of plane distance of a node,

and L12 is the length between the first and second nodes.

If the above inequality is exceeded a warning will be issued but the analysis will proceed.

Appendix C : Local Element Axes.

Standard Joint Element

Local x-axis The local x-axis is defined by the vector between the first and the third nodes of the element topology.

Note.

The third node must be different from nodes 1 and 2 of the topology.

Standard Line Element

Local x axis The local x-axis lies along the element in the direction in which the element nodes are defined. For curved elements the local x-axis is the tangent to the curve.

Local y axis The local xy plane is either defined by a dummy node and the two end nodes, or (in the absence of a dummy node), defined by the two end nodes and the central node. For the latter case, the local y-axis is perpendicular to the x-axis and on the positive convex side.

Local z axis The local z-axis forms a right-handed set with the local xy plane.

For cross-section beams the top surface is defined by the local +ve z direction.

Note

Default line axes are defined in Modeller with the local x axis of the element following the line direction. The element local z is then defined in the XZ plane unless the local x axis is aligned to the global Z axis in which case the element local z axis is aligned with the global Y axis.

Standard Surface Element

Local x axis For 3 or 4 noded elements the local x-axis is defined by a line joining the first and second element nodes. For 6 and 8 noded elements the local x-axis is the tangent to the curve between the first 3 nodes.

Local y axis The local xy-plane is defined by the remaining nodes, the local y-axis being perpendicular to the x-axis and forming a right-handed set with the x-axis and the xy plane.

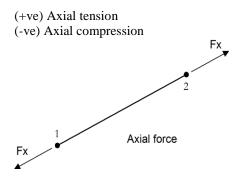
Local z-axis The local z-axis forms a right-handed set with the local x and y-axes. For shell elements the top surface is defined by the local +ve z direction.

Appendix D : Sign Conventions.

The sign convention for forces, moments, stresses, rotations, eccentricities and potentials for different element types is documented in the following section headings.

Standard Bar Element

Axial force



Standard Beam Element

Numerically Integrated Beam Elements

Axial force

- (+ve) Axial tension
- (-ve) Axial compression

Bending Moment

(+ve) Hogging moment (Top of beam in tension)

(-ve) Sagging moment (Bottom of beam in tension)

Note: The top/bottom of the beam is determined by the element axes.

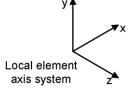
Torsion

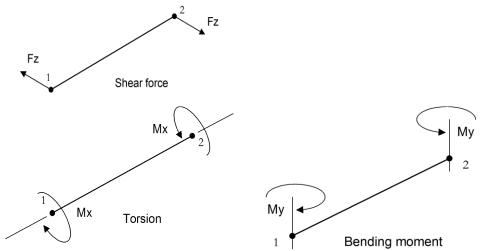
(+ve) Rotation at 1st node greater than rotation at other end node (-ve) Rotation at 1st node smaller than rotation at other end node

Grillage Elements

End Forces and Rotations

Positive end forces and rotations for grillage elements are those acting on the element nodes in local directions, and are as follows:





Note that when a reference path has been specified, additional force/moment components are available, and for this situation the x, y, and z element axes relate to longitudinal, transverse and vertical terms respectively. For instance My will relate to MF (longitudinal) - the flexural moment in longitudinal members that are following the path and MF (transverse) - the flexural moment in the transverse members that are orthogonal or skewed in relation to the reference path. Similarly, Fz will relate to FV (longitudinal) - the force in the vertical direction for longitudinal members that are following the path and FV (transverse) - the vertical direction for transverse members that are orthogonal or skewed in relation to the reference path.

Internal forces

These forces follow the sign convention for numerically integrated beams.

Axial force	Bending Moment	Torsion
Not applicable	(+ve) Sagging moment (-ve) Hogging moment	(+ve) Rotation at 1st node greater than rotation at other end node(-ve) Rotation at 1st node smaller than rotation at other end node

Sign convention in Modeller for bending moment

(+ve) Top of beam in tension

(-ve) Bottom of beam in tension

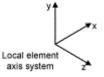
Where the top/bottom of the beam are determined by the element axes

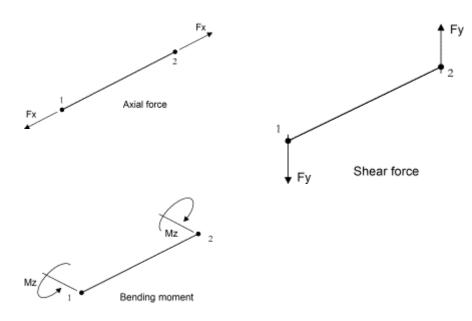
See <u>numerically integrated beam sign convention</u>.

2D Engineering Beam Elements

End Forces and Rotations

Positive end forces and rotations for 2D engineering beams are those acting on the element nodes in local directions, and are as follows:





Internal forces

These forces follow the sign convention for numerically integrated beams.

Axial force	Bending Moment
(+ve) Axial tension	(+ve) Hogging moment
(-ve) Axial compression	(-ve) Sagging moment

Sign convention in Modeller for bending moment

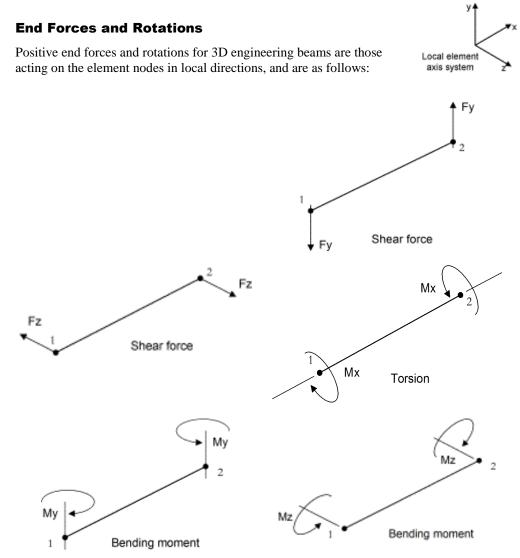
(+ve) Top of beam in tension

(-ve) Bottom of beam in tension

Where the top/bottom of the beam are determined by the element axes

See <u>numerically integrated beam sign convention</u>.

3D Engineering Beam Elements



Internal forces

These forces follow the sign convention for numerically integrated beams.

Axial force	Bending Moment	Torsion
(+ve) Axial tension (-ve) Axial compression	(+ve) Hogging moment (-ve) Sagging moment	(+ve) Rotation at 1st node greater than rotation at other end node(-ve) Rotation at 1st node smaller than rotation at other end node

Sign convention in Modeller for bending moment

(+ve) Top of beam in tension

(-ve) Bottom of beam in tension

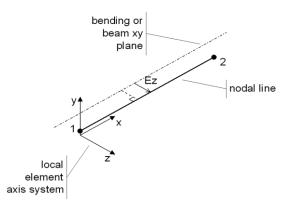
Where the top/bottom of the beam are determined by the element axes

See <u>numerically integrated beam sign convention</u>.

Standard Beam Eccentricities

Eccentricities are optional geometric properties for some elements and may be specified if the nodal line of the element does not lie along the required bending line/plane for the structural component being modelled.

Measurement of Ez (see diagram) is **from** the required bending plane (the beam xy plane) **to** the nodal line in the local element axis z-direction. If a beam xy plane is required such that it has negative local z coordinates relative to the nodal line, the eccentricity is positive.



Similarly, measurement of Ey is **from** the required bending plane (the beam xz plane) **to** the nodal line in the local element axis y-direction. If a beam xz plane is required such that it has negative local y coordinates relative to the nodal line, the eccentricity is positive.

σv

σΧ

σχν

σxy

σ×

Х

Standard 2D Continuum Element

Direct stress

(+ve) Tension (-ve) Compression

Shear stress

(+ve) Shear into XY quadrant (-ve) Shear into XY quadrant

Note. Positive stress values are shown.

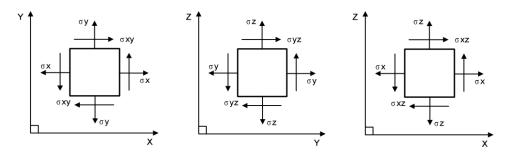


Direct stress

(+ve) Tension (-ve) Compression

Shear stress

(+ve) Shear into XY, YZ and XZ quadrants (-ve) Shear into XY, YZ and XZ quadrants



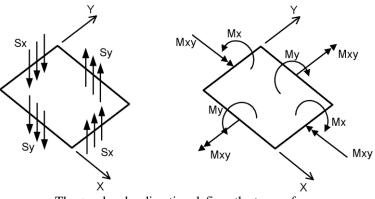
Note. Positive stress values shown.

Standard Plate Element

Flexural stress

(+ve) Hogging moment (producing +ve stresses on the element top surface)

(-ve) Sagging moment (producing -ve stresses on the element top surface)



The +ve local z-direction defines the top surface.

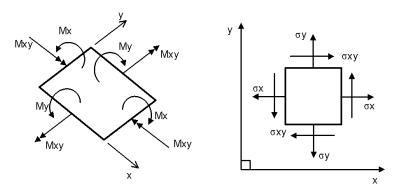
Thin Shell Element

Membrane stress

(+ve)	Direct tension
(-ve)	Direct compression
(+ve)	In-plane shear into xy quadrant
(-ve)	In-plane shear into xy quadrant

Flexural stress

- (+ve) Hogging moment (producing +ve stresses on the element top surface)
- (-ve) Sagging moment (producing -ve stresses on the element top surface)

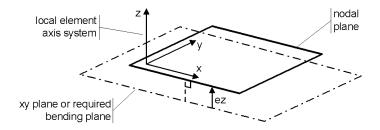


Notes

- Positive stress values shown.
- The +ve local z-direction defines the top surface.

Thin Shell Eccentricity

Eccentricity is an optional geometric property for this element type and may be specified if the nodal plane of the element does not lie along the required bending plane for the structural component being modelled.

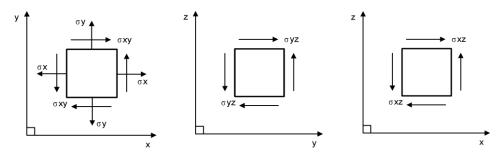


Measurement of ez is **from** the required bending plane **to** the nodal plane in the local element axis z-direction.

Thick Shell Element

Thick shell stress

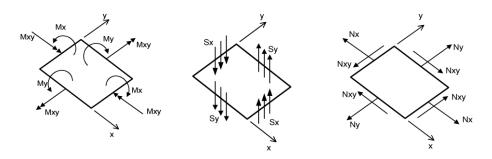
Direct stress	(+ve) (-ve)	Tension Compression
Shear stress	(+ve) (-ve)	As shown in the following images In the reverse directions in following images



Stress Resultant

- Membrane stress (+ve) Direct tension
 - (-ve) Direct compression
 - (+ve) In-plane shear into xy quadrant
 - (-ve) In-plane shear into xy quadrant
- Flexural stress
 (+ve)
 Hogging moment (producing +ve stresses on the element top surface)

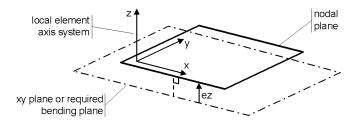
 (-ve)
 Sagging moment (producing -ve stresses on the element top surface)



The +ve local z-direction defines the top surface.

Thick Shell Eccentricity

Eccentricity is an optional geometric property for this element type and may be specified if the nodal plane of the element does not lie along the required bending plane for the structural component being modelled.

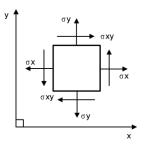


Measurement of ez is **from** the required bending plane **to** the nodal plane in the local element axis z-direction.

Standard Membrane Element

Direct stress	(+ve)	Tension
	(-ve)	Compression
Shear stress	(+ve)	Shear into xy quadrant

(-ve) Shear into xy quadrant



Standard Field Element

Potential

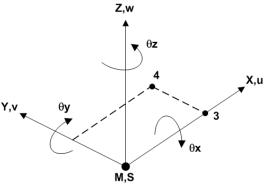
(+ve) +ve field value, dT/dx rate of change of field in x direction

Standard Joint Element

Direct force : (+ve) Tension and (-ve) Compression

Spring Moment : (+ve) for positive rotational spring strain and (-ve) for negative rotational spring strain

The sign of joint results is dependent upon both the element direction(that is which geometry is the master, and which is the slave) and the orientation of the local coordinate axes chosen.



Coincident Master and Slave nodes, M = Master, S= Slave

Compression	Tension	Negative Moment	Positive Moment
Mu > Su	Su > Mu	$M_{\theta x} > S_{\theta x}$	$S_{\theta x} > M_{\theta x}$
Mv > Sv	Sv > Mv	$M_{\theta y} > S_{\theta y}$	$S_{\theta y} > M_{\theta y}$
Mw > Sw	Sw > Mw	$M_{\theta z} > S_{\theta z}$	$S_{\theta z} \!\!> \! M_{\theta z}$

Appendix E : Thick Shell Notation.

Thick Shell Nodal Rotation

Problems with Singularities

In general, five degrees of freedom will be associated with each shell node: three translations and two rotations. The first axis of rotation will be defined by one of the global axes. The second axis of rotation is defined by the vector product of the selected global axis and the nodal normal.

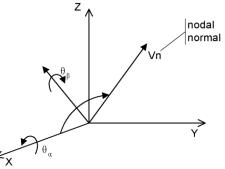
Choosing one global axis to define the first rotation is not possible for all cases as singularities can occur depending on the orientation of the shell. As the topology of the shell cannot be known a means of choosing suitable rotations after the shell orientation has been defined must be provided.

How the Nodal Systems are Defined

The axis defining the θ_{α} rotation is chosen by examining the global components of the nodal normal. The smallest (absolute) component of the normal vector defines the global axis to be chosen as the first axis of rotation. The vector product of this axis and the nodal normal defines

the axis for the second rotation θ_{β} . If the nodal normal coincides with the global Z axis, the

global X axis will be chosen to define θ_{α} . In this instance, the X and Y components will both be



minimum values. When two components define the same minimum value the order of priority for selection of the axis is X, Y, Z. Note that, in general, the axes of rotation and the nodal normal will form a non-orthogonal left-handed set. The rotations are indicated in the

following figure where the global x axis has been used to define θ_{α} :

Five or Six Degrees of Freedom at a Node

LUSAS Solver will automatically select five degrees of freedom at a node, with rotations defined as above, unless:

- □ The maximum angle between the normals of adjacent elements meeting at the node is greater than 20 degrees. The value of 20 degrees is selected by default and may be changed using the SYSTEM parameter SHLANG.
- □ Beam, joint or other shell element types are connected to the node
- □ <u>Concentrated loads</u> or <u>support conditions</u> have been specified at the node using LUSAS Modeller
- □ Option 278 has been specified
- □ Six degrees of freedom have been selected for the node within the NODAL FREEDOMS data chapter If six degrees of freedom are used at a node the rotations will relate to the global axes, θX , θY and θZ unless TRANSFORMED FREEDOMS have been specified. It is recommended that the default value for SHLANG is retained wherever possible.

When are Six Degrees of Freedom Necessary?

Rotations relating to global axes will be required in the following circumstances:

- □ When a branched shell connection exists in the structure to be analysed. LUSAS Solver will automatically detect this and assign six degrees of freedom to nodes along the branch connection.
- □ When connecting with other element types. Six degrees of freedom will automatically be assigned to shell nodes connected to beams, joints or other shell element types.

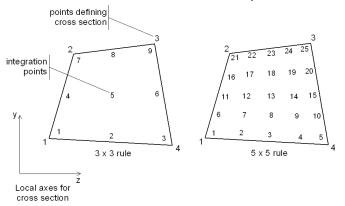
□ When boundary conditions or loading cannot be easily specified using the above definition of rotations, e.g. when applying moments or using symmetry.

If the rotations $\theta \alpha$, θ_{β} will not allow the required loading or symmetry conditions to be applied, rotations about global axes may be enforced using NODAL FREEDOMS. The use of TRANSFORMED FREEDOMS will then allow the rotations to be related to a more convenient local orthogonal set if necessary. If six degrees of freedom at a node are enforced using NODAL FREEDOMS (i.e. not set automatically by LUSAS Solver) singularities may occur if the **in-plane rotation** (about the normal) **is not restrained**.

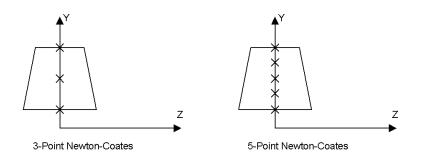
Appendix F : Newton Coates Integration.

Newton-Cotes Integration Points

For beam elements BMX3, BSX4 and BXL4 the rigidity is computed by integration of the cross section. The default integration employs a 3x3 Newton Cotes rule for linear materials and a 5x5 rule for nonlinear materials. These may be altered by the user within the GEOMETRIC PROPERTIES definition. The locations of the default integration points are shown in the accompanying diagram, together with the local axes for the beam cross section (note the different corner numbering). The integration points are equally spaced along a particular natural ordinate for the section. The integration point numbers shown correspond with those given in the stress output for the element. More information on the cross sectional integration for these elements is available in the *LUSAS Theory Manual*.



Newton-Cotes Integration Points for 3D Elements



Newton-Cotes Integration Points for 2D Elements

Appendix G : Shear Area and Torsional Constant.

Shear Areas

In beams of small span to depth ratio, the shear stresses are likely to be high and the resulting deflection due to shear may not be negligible. The shear area is used to control the amount of shear deformation which will occur (Asz, Asy). For various sections, approximate values are as follows:

- **\Box** Rectangular beams = 5A/6
- \Box I-beams (along web direction) = Area of web
- □ I-beams (along flange direction) = Area of flanges
- \Box Thin walled, hollow circular section = A/2
- $\Box \quad \text{Solid circular section} = 9A/10$
- \Box No shear deformation = 1000A

Note

- If Asz or Asy equal zero, mechanisms may occur.
- For elements which support this geometric input, shear deformation effects may be removed by assigning an artificially large value.
- The section property calculator in Modeller can be used to accurately compute shear areas

Torsional Constant

The torsional constant provides a measure of the torsional rigidity of a line member. Approximate values are as follows:

Solid circle

(equivalent to the polar moment of inertia)

$$\frac{\pi r^4}{2}$$

where \mathbf{r} is the radius of the circle

Hollow circle

$$\frac{\pi}{2}(r_2^4 - r_1^4)$$

where r2 is the outer radius and r1 is the inner radius

Solid square = 0.1406a⁴

where a is the side length

Solid rectangle =

$$ab^{3}\left[\frac{16}{3} - 3.36 \frac{b}{a}\left(1 - \frac{b^{4}}{12a^{4}}\right)\right]$$

where **2a** is the length of the longest side and **2b** is the length of the shortest side

Equilateral triangle

where **a** is the side length

Rectangular tube

$$\frac{2 \cdot t_1 \cdot t_2 \cdot (a - t_2)^2 (b - t_1)^2}{a t_2 + b t_1 - t^2 _2 - t^2 _1}$$

where

a is the length of the longest side

t1 is the thickness of the longest side

b is the length of the shortest side

t2 is the thickness of the shortest side

Thin rectangle

 $\frac{1}{3}$ bt³

where **b** is the rectangle length and **t** is the rectangle length thickness

Any section consisting of thin rectangles

$$\frac{1}{3}\Sigma$$
 bt³

Solid ellipse

$$\frac{\pi a^3 b^3}{a^2 + b^2}$$

where 2a is the longest dimension

and $\mathbf{2b}$ is the shortest dimension

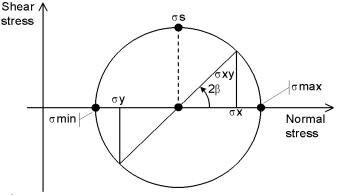
Note

• The section property calculator in Modeller can be used to accurately compute torsional constants

Appendix H : Principal Stress Output.

Output Notation for Principal Stresses

For a bi-axial stress state, the Mohr's circle representation of a stress field is:



where:

smax is the maximum principal stress.

Smin is the minimum principal stress

 ${\bf Ss}$ is the maximum shear stress

 β defines the orientation of the principal axis (the plane on which the principal stresses act).

sx, σ y, σ xy represent an arbitrary two dimensional stress state.

Appendix I : Mass Lumping.

Mass Lumping in LUSAS

Non-Structural mass elements are used to define a lumped mass at a point, or a distributed mass along a line and over a surface.

See Non-Structural Mass Elements in the Modeller Reference Manual for more details.

Appendix J : Moments of Inertia.

Moments of Inertia Definitions

Second moment of area about line yy

Second moment of area about line zz

$$I_{zz} = \int y^2 dA$$

Product moment of inertia of section

(=0 for sections symmetric about **either** yy or zz)

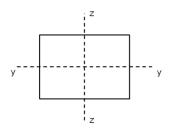
First moment of area about yy

(=0 for sections symmetric about yy)

First moment of area about zz

$$I_z = \int y dA$$

(=0 for sections symmetric about zz)



Note

- The above definitions are for a section defined in the two dimensional yz plane. Similar expressions apply for a section in the three dimensional space.
- For a beam with eccentricity e from the nodal line, then:

$$I_{zz} = Ae^2 + I_{na}$$
 and $I_z = eA$

where $|_{na}$ is the second moment of area about the centroidal axis.

• For the purpose of the moment inertia definitions above only, the eccentricity is measured **from the nodal line to the required bending plane** (the beam's xy plane in the figure above). For example, if a beam xy plane is required such that it has negative local z coordinates relative to the nodal line, the eccentricity to be used above is negative.

Appendix K : Results Tables.

Key to Element Results Tables

This section contains the notation for the results in the Results Tables. Some results are available in local and global directions depending on the element type. The case of the direction indicator associated for each term in the table will indicate its default direction for that element. Lower case indicates local element directions and upper case indicates that results are available in global directions by default.

Displacements

- **DX** Displacement in X direction
 - **DY** Displacement in Y direction
 - **DZ** Displacement in Z direction
- **RSLT** Resultant displacement
- THX Rotation about X
- THY Rotation about Y
- THZ Rotation about Z

Note: Rotations are output in radians.

Velocities and Accelerations

- VX Velocity in X direction
- VY Velocity in Y direction
- VZ Velocity in Z direction
- **RSLT** Resultant velocity

THL1First loof rotationTHL2Second loof rotationDUHierarchical disp. at mid-nodeDTHXHierarchical rotation at mid-nodePRESPore PressureTHwRate of change of twisting angle (warping beams)

- AX Acceleration in X direction
- AY Acceleration in Y direction
- $\mathbf{AZ} \quad \text{Acceleration in } Z \text{ direction}$
- **RSLT** Resultant acceleration

VC Results calculator values

Strains

х

- **EX** Direct strain in X direction
- EY Direct strain in Y direction
- **EZ** Direct strain in Z direction
- EXY Shear strain in XY plane
- EYZ Shear strain in YZ plane
- EZX Shear strain in XZ plane
- EMa Maximum principal strain
- EMin Minimum principal strain
 - E1 Major principal strain
 - E2 Intermediate principal strain
 - E3 Minor principal strain
- Eabs Signed largest value of principal strain

Strains: Top/Middle/Bottom (TMB)

- **EX** Direct strain in X direction
- EY Direct strain in Y direction
- **EZ** Direct strain in Z direction
- EXY Shear strain in XY plane
- **EYZ** Shear strain in YZ plane
- **EXZ** Shear strain in XZ plane

Plastic Strains

- **EPX** Plastic direct strain in X direction
- **EPY** Plastic direct strain in Y direction
- **EPZ** Plastic direct strain in Z

- **Bx** Bending strain (curvature) about x axis
- **By** Bending strain (curvature) about y axis
- **Bz** Bending strain (curvature) about z axis
- Bxy Bending or torsional strain into xy plane
- **Byz** Bending or torsional strain into yz plane
- **Bxz** Bending or torsional strain into xz plane
- BMax Maximum principal bending strain
- BMin Minimum principal bending strain
 - β Angle between E1 and X axis
 - **EE** Equivalent strain (von Mises)
 - EI Maximum shear strain
 - **EV** Volumetric strain
- E1 Major principal strain
- E2 Intermediate principal strain
- E3 Minor principal strain
- Eabs Signed largest value of principal strain
 - β Angle between E1 and X axis
 - EE Equivalent strain (von Mises)
 - EI Maximum shear strain
 - EP1 Major principal strain
 - EP2 Intermediate principal plastic strain
 - EP3 Minor principal plastic strain

direction

- **EPXY** Plastic shear strain in XY plane
- **EPYZ** Plastic shear strain in YZ plane
- **EPZX** Plastic shear strain in ZX plane
- **EPMax** Maximum principal plastic strain
- **EPMin** Minimum principal plastic strain

Creep Strains

- ECX Creep direct strain in X directionECY Creep direct strain in Y
- direction
- ECZ Creep direct strain in Z direction
- **ECXY** Creep shear strain in XY plane
- ECYZ Creep shear strain in YZ plane
- ECZX Creep shear strain in ZX plane
- ECMax Maximum principal creep strain
- ECMin Minimum principal creep strain

Rubber Stretches

- StchX Direct stretch tensor in X direction
- StchY Direct stretch tensor in Y direction
- StchZ Direct stretch tensor in Z direction
- StchXY Shear stretch tensor in XY plane
- StchYZ Shear stretch tensor in YZ plane
- StchXZ Shear stretch tensor in XZ

EPabs	Signed largest value of principal plastic strain
β	Angle between EP1 and X axis
EPE	Equivalent plastic strain (von Mises)
EPI	Maximum shear strain
CWMax	Maximum crack width
EFSMax	Maximum equivalent fracture strain

- EC1 Major principal creep strain
- EC2 Intermediate principal creep strain
- EC3 Minor principal creep strain
- Ecabs Signed largest value of principal creep strain
 - β Angle between EC1 and X axis
- ECE Equivalent creep strain (von Mises)
- ECI Maximum shear creep strain
- Stch1 Major principal stretch
- Stch2 Intermediate principal stretch
- Stch3 Minor principal stretch
- StchAbs Signed largest value of principal stretch
 - β Angle between Stch1 and X axis
 - StchE Equivalent stretch

	plane
StchMax	Maximum principal stretch
StchMin	Minimum principal stretch

Strains: Interface Elements

- **Ex** Shear relative displacement in local x direction
- **Ez** Direct relative displacement in the thickness direction

Stresses: Continuum Elements

- **SX** Direct stress in global X direction
- SY Direct stress in global Y direction
- SZ Direct stress in global Z direction
- **SXY** Shear stress in Y-direction on a plane normal to X
- **SYZ** Shear stress in yz plane
- SXZ Shear stress in xz plane
- **SMax** Maximum principal stress
- SMin Minimum principal stress

Force/Moment: Bar and Beam Elements

- **Fx** Force in local x direction
- Fy Force in local y direction
- **Fz** Force in local z direction

Fb

- Mx Moment about local x directionMy Moment about local y direction
- Mz Moment about local z direction
- **Mb** Bi-moment (warping)

Stresses: Bar and Beam Elements

Bi-shear or torque (warping)

Sx(Fx)	Stress due to axial	Sx(Fx, My)	Stress due to axial force and
	force in x		bending about y
Sx(My)	Stress due to bending	Sx(Fx, Mz)	Stress due to axial force and
	about y		bending about y
Sx(Mz)	Stress due to bending	Sx(Fx, My, Mz)	Stress due to axial force and
	about z		bending about y and z
Sx(My, Mz)	Stress due to bending		
-	about y and z		

StchI Maximum shear stretch

direction

dP Pressure difference

Ey Shear relative displacement in local y

- **S1** Major principal stress
- S2 Intermediate principal stress
- S3 Minor principal stress
- Sabs Signed largest value of principal stress
 - β Angle between E1 and x axis
 - SI Maximum shear stress
 - SE Equivalent stress (von Mises)
- **Pres** Pore pressure

Force/Moment: Plate Elements (per unit width)

- **SX** Shear force in global YZ plane
- SY Shear force in global XZ plane
- MX Moment in global X
- MY Moment in global Y
- MXY Twisting moment in global XY plane
- Mmax Major principal moment
- Mmin Minor principal moment
 - β Angle between MMax and X axis
 - MI Maximum shear moment
- Mabs Signed largest value of moment
 - ME Equivalent moment

Force/Moment: Membrane and Shell Elements (per unit width)

- $\mathbf{N}\mathbf{x}$ In-plane force in local x direction
- Ny In-plane force in local y direction
- Nxy In-plane shear force
- NMax Major principal in-plane force
- NMin Minor principal in-plane force
- Nβετα Angle between NMax and x axis
 - NI Maximum in-plane shear force
 - NE Equiv stress resultant (von Mises)
 - Nabs Signed largest value of in-plane force
 - \mathbf{Sx} Shear force in local yz plane
 - Sy Shear force in local xz plane

Stresses: Top/Middle/Bottom (TMB)

- SX Direct stress in global X direction
- SY Direct stress in global Y direction
- SZ Direct stress in global Z direction
- **SXY** Shear stress in XY plane
- SYZ Shear stress in YZ plane
- **SXZ** Shear stress in XZ plane

- S1 Major principal stress
- S2 Intermediate principal stress
- S3 Minor principal stress
- Sabs Signed largest value of principal stress
 - SI Maximum shear stress
 - SE Equivalent stress (von Mises)

- Mx Moment in local x direction
- My Moment in local y direction
- Mxy Twisting moment in local xy plane
- Mmax Major principal moment
- **Mmin** Minor principal moment
- Mβετα Angle between MMax and X axis
 - MI Maximum shear moment
 - ME Equivalent moment
 - Mabs Signed largest value of moment

Stresses: Interface Elements

- Sx Shear traction in local x direction Sy Shear traction
- Sz Direct traction in thickness direction

Force/Moment: Wood-Armer (per unit width for Shells)

- Mx(T) Top surface local x moment
- My(T) Top surface local y moment
- **Mx(B)** Bottom surface local x moment
- My(B) Bottom surface local y moment
- **Util(T)** Top surface utilisation factor
- Util(B) Bottom surface utilisation factor
- MUtil(T) Top surface utilisation factor for bending only
- MUtil(B) Bottom surface utilisation factor for bending only

- Nx(T) Top surface local x force
- Ny(T) Top surface local y force
- Nx(B) Bottom surface local x force
- Ny(B) Bottom surface local y force
- Fc(T) Top surface concrete force
- Fc(B) Bottom surface concrete force

Force/Moment: Wood-Armer (per unit width for Plates and Grillages)

- MX(T) Top surface global X moment
- MY(T) Top surface global Y moment
- MX(B) Bottom surface global X moment
- MY(B) Bottom surface global Y moment
- MUtil(T) Top surface utilisation factor for bending only
- MUtil(B) Bottom surface utilisation factor for bending only

Additional Force/Moment Components

Note for influence analysis when a reference path has been specified, additional force/moment components are available for selection when transforming results. These are not listed for relevant elements in the Results tables.

FV	Force in Vertical direction for	MF Flexural Moment in
(longitudinal)	longitudinal members that are	(longitudinal) longitudinal members that
	following the reference path	are following the reference
		path
FV	Force in Vertical direction for	MF Flexural Moment in
(transverse)	transverse members that are	(transverse) transverse members that are

- Sy Shear traction in local y direction
- **O** Flow

Sy Shear traction in local y direction

PHIC Results calculator values

qX Field flux in X direction

qY Field flux in Y direction

qZ Field flux in Z direction

Fluxes

orthogonal or skewed in relation to the reference path

orthogonal or skewed in relation to the reference path

Stresses: Interface Elements

- **Sx** Shear traction in local x direction
- Sz Direct traction in the thickness direction

Concrete Results

Max Crack width	ESFmax	Max fracture strain
Shrinkage strain	EPthm	Thermal strain
Temperature	Fcomp	Compressive strength
tensile strength	Young	Young's modulus
Creep strain in global X	ECY	Creep strain in global Y
Creep strain in global Z		

Potential

CWmax EPshk Temp Ftens ECX ECZ

HI Field variable	Field va	P
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T Temperature

Gradients

- GX Field gradient in X direction
- GY Field gradient in Y direction
- GY Field gradient in Z direction

Hygro-Thermal Results

SW	Water saturation	RoWC	Water content
PV	Vapour pressure	DH	Degree of hydration at day 28
Por	Porosity	TefH	Effective time of hydration
ТС	Thermal conductivity	PMD	Water permeability [m/s]
HR	Relative humidity of concrete		

Reactions / Residual Forces

FX Force in X direction

FY	Force in Y direction	FDU	Force due to hierarchical displacement
FZ	Force in Z direction	MDX	Moment due to hierarchical rotation
RSLT	Resultant force		
MX	Moment about X axis	QC	Flow at a point (field problems)
MY	Moment about Y axis	VFLW	Velocity of Flow

Reaction Stress

PX Stress due to reaction in X direction	I
---	---

PY Stress due to reaction in Y direction

Fatigue Parameters

Damage A measure of damage LogLife Log repeats to failure

Note. The fatigue facility uses Miner's rule, that is:

 $n1/N1 + n2/N2 + \cdots + ni/Ni = Damage$

where Damage is the damage variable and is usually taken as unity (experiment usually gives values between 0.7 and 2.2). ni is the number of cycles of stress applied to the structure and Ni is the life corresponding to the stress. Loglife is the log (base 10) of the life expectancy of the structure according to the loading and the number of cycles specified. Life is measured in terms of cycles.

PZ Stress due to reaction in Z direction

Damage Parameters

DDAMA	Damage variable	DAMAM	Damage consistency parameter
CCURD	Damage threshold	DFUNC	Damage function

Note. Damage parameters are only available when a damage model is in use.

Strain Energy and Plastic Work

SED Strain energy density (StEngD) PWD Plastic work density

Note. Strain energy density and plastic work density values can be accessed if turned on by selecting **Calculate Strain Energy and Plastic Work Densities** from the **Results > Options** dialog or by using the command: **SET RESULTS ENERGY**.

Adaptive Error

Eadp Adaptive error.

Note. Adaptive error results are only available when an adaptive results column is set. See the LUSAS User Manual for more details.

State Variables

State variables can be accessed with the command:

SET RESULTS STATE_VARIABLES istvb nsvcmp isvloc

Where istvb is the type of state variable required, nsvcmp is the number of state variables required, and isvloc is the start location of the first state variable required.

The results columns for these state variables vary according to the results type set. The column descriptors have the following prefixes:

- D PL Plastic, Rubber
- **CR** Creep
- **DM** Damage

- followed by the number of the state variable required. For example, if four creep state variables are required, the column descriptors will be CR1, CR2, CR3 and CR4.

Key to Slideline Results Components

This section contains the notation for slideline results. Note that slideline results components are not listed in the results tables.

TanGapFrcx	Tangential gap force in local x direction	NrmPen	Penetration normal to contact surface
TanGapFrcy	Tangential gap force in local y direction	ContStatus	In-contact/out-of-contact status
RsltTanGFc	Resultant tangential gap force	ContacArea	Nodal contact area
NrmGapForc	Gap force normal to contact surface	Contact	In-contact/out-of-contact status
ForceX	Contact force in system x direction	Zone	Zonal contact parameter
ForceY	Contact force in system y direction	ZnCnDetDst	Zonal contact detection distance
ForceZ	Contact force in system z direction	IntStfCoef	Contact stiffness coefficient
RsltForce	Resultant contact force	TanForcex	Tangential contact force in local x direction
ContStresx	Contact stress in local x direction	TanForcey	Tangential contact force in local y direction
ContStresy	Contact stress in local y direction	RsltTanFrc	Resultant tangential contact force
ContPress	Contact pressure normal to contat surface	NrmForce	Contact force normal to contact surface
ContStiff	Contact stiffness		

Transforming Results Directions

Important: Some results entities can be transformed. The results components will use alternative suffixes if results are calculated relative to a system other than the global axis set. The element results tables show the default results directions for all elements with lower case subscripts being used for local results.

See the <u>Local and Global Results</u> in the *LUSAS Modeller User Manual* for details of results transformation procedures.

2D Structural Bars **BAR2**, **BAR3**

Entity					C	ompone	ent				
Displacement	DX	DY	RSLT								
Force/Moment	FX	Fabs	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp
Strain	EX	Eabs	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
Loading	FX	FY	RSLT								
Reaction	FX	FY	RSLT								
Residual Force	FX	FY	RSLT								
Reaction Stress											
Velocity	VX	VY	RSLT								
Acceleration	AX	AY	RSLT								
Plastic Strain	EPX	EPabs	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
Creep Strain	ECX	ECabs	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
Rubber Stretches											
TMB Stress											
TMB Strain											
TMB Plastic Strain											
TMB Creep Strain											

3D Structural Bars **BRS2**, **BRS3**

Entity					C	ompone	ent				
Displacement	DX	DY	DZ	RSLT							
Force/Moment	FX	Fabs	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp
Strain	EX	Eabs	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
Loading	FX	FY	FZ	RSLT							
Reaction	FX	FY	FZ	RSLT							
Residual Force	FX	FY	FZ	RSLT							
Reaction Stress											
Velocity	VX	VY	VZ	RSLT							
Acceleration	AX	AY	AZ	RSLT							
Plastic Strain	EPX	EPabs	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
Creep Strain	ECX	ECabs	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
Rubber Stretches											
TMB Stress											
TMB Strain											
TMB Plastic Strain											
TMB Creep Strain											

2D Engineering Grillage Thick Beam GRIL

Entity							Cor	npone	nt				
Displacement	DZ	RSLT	THX	THY									
Force/Moment	Fz	Mx	My	Mx(T)	My(T)	Mx(B)	My(B)	Util(T)	Util(B)	Damage	LogLife	SED	Eadp
Strain													
Loading	FZ	RSLT	MX	MY									
Reaction	FZ	RSLT	MX	MY									
Residual Force													
Reaction Stress													
Velocity	VZ	RSLT											
Acceleration	ΑZ	RSLT											
Plastic Strain													
Creep Strain													
Rubber Stretches													
TMB Stress													
TMB Strain													
TMB Plastic Strain													
TMB Creep Strain													

Note: Wood-Armer results are only available for plotting /printing at nodes. They are not available unaveraged at nodes within elements or at Gauss points.

2D Thick Beam Elements **BMI2**, **BMI3**, **BMI2X**, **BMI3X**

Entity						Con	nponen	t				
Displacement	DX	DY	RSLT	THZ								
Force/Moment	Fx	My	Mz	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp
Strain	Ex	Exy	Bz	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
Loading	FX	FY	RSLT	MZ								
Reaction	FX	FY	RSLT	MZ								
Residual Force	FX	FY	RSLT	MZ								
Reaction Stress												
Velocity	VX	VY	RSLT									
Acceleration	AX	AY	RSLT									
Plastic Strain	EPx	EPxy	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp			
Creep Strain	ECx	ECxy	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp			
Rubber Stretches	Sx	Sy										
TMB Stress	Ex	Exy										
TMB Strain	EPx	EPxy										
TMB Plastic Strain	ECx	ECxy										

Note: Plastic and creep strains are only available for BMI2X and BMI3X elements with the appropriate material models.

3D Thick Beam Elements <u>BMI21</u>, <u>BMI22</u>, <u>BMI31</u>, <u>BMI33</u>, <u>BMX21</u>, <u>BMX22</u>, <u>BMX31</u>, <u>BMX33</u>

Entity							Com	ponent	t						
Displacement	DX	DY	DZ	RSLT	THX	THY	THZ								
Force/Moment	Fx	My	Mz	Mx	My	Mz	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp
Strain	Ex	By	Bz	Bx	Ву	Bz	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
Loading	FX	FY	FZ	RSLT	MX	MY	MZ								
Reaction	FX	FY	FZ	RSLT	MX	MY	MZ								
Residual Force	FX	FY	FZ	RSLT	MX	MY	MZ								
Reaction Stress															
Velocity	VX	VY	VZ	RSLT											
Acceleration	AX	AY	AZ	RSLT											
Plastic Strain	EPx	EPxy	EPzx	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp					
Creep Strain	ECx	ECxy	ECzx	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp					
Rubber Stretches															
TMB Stress															
TMB Strain															
TMB Plastic Strain															

Note: Plastic and creep strains are only available for BMX21, BMX31, BMX22, BMX33 elements with the appropriate material models.

3D Thick Beam Elements with Torsional Warping <u>BMI21W</u>, <u>BMI22W</u>, <u>BMI31W</u>, <u>BMI33W</u>, <u>BMX21W</u>, <u>BMX22W</u>, <u>BMX31W</u>, <u>BMX33W</u>

																_
Entity								Comp	onent							
Displacement	DX	DY	DZ	RSLT	THX	THY	THY	THw								
Force/Moment	Fx	My	Mz	Mx	Му	Mz	Fb	Mb	Damage	LogLife	DDAMA	CURR D	DAMA M	DFUN C	SED PWI) Eadp
Strain	Ex	By	Bz	Bx	Ву	Bz	Efb	Emb	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp	
Loading	FX	FY	FZ	RSLT	MX	MY	MZ									
Reaction	FX	FY	FZ	RSLT	MX	MY	MZ	Mw								
Residual Force	FX	FY	FZ	RSLT	MX	MY	MZ									
Reaction Stress																
Velocity	VX	VY	VZ	RSLT												
Acceleration	AX	AY	AZ	RSLT												
Plastic Strain	EPx	EPxy	EPzx	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
Creep Strain	ECx	ECxy	ECzx	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
Rubber Stretches																
TMB Stress																
TMB Strain																
TMB Plastic Strain																

Note: Plastic and creep strains are only available for BMX21W, BMX31W, BMX22W, BMX33W elements with the appropriate material models.

2D Kirchhoff Thin Beams **BM3**, **BMX3**

Entity						Com	ponent					
Displacement	DX	DY	RSLT	THZ	DU							
Force/Moment	Fx	Fy	Mz	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp
Strain	Ex	Ey	Bz	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
Loading	FX	FY	RSLT	MZ	FDU							
Reaction	FX	FY	RSLT	MZ	FDU							
Residual Force	FX	FY	RSLT	MZ	FDU							
Reaction Stress												
Velocity	VX	VY	RSLT									
Acceleration	AX	AY	RSLT									
Plastic Strain	EPx	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
Creep Strain	ECx	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
Rubber Stretches												
TMB Stress												
TMB Strain												
TMB Plastic Strain												
TMB Creep Strain												

Note: Plastic and creep strains are only available for BMX3 elements with the appropriate material models.

3D Kirchhoff Thin Beams **BS3**, **BS4**, **BSX4**

Entity							С	ompor	nent					
Displacement	DX	DY	DZ	RSLT	THX	THY	THZ	DU	DTHX					
Force/Moment	Fx	Му	Mz	Tzx	Тху	Fy	Fz	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED PWD
(continued)	Eadp													
Strain	Ex	By	Bz	Bzx	Bxy	Ey	Ez							
(continued)	Eadp													
Loading	FX	FY	FZ	RSLT	MX	MY	MZ	FDU	MDX					
Reaction	FX	FY	FZ	RSLT	MX	MY	MZ	FDU	MDX					
Residual Force	FX	FY	FZ	RSLT	MX	MY	MZ	FDU	MDX					
Reaction Stress														
Velocity	VX	VY	VZ	RSLT										
Acceleration	AX	AY	AZ	RSLT										
Plastic Strain	EPx	EPxy	EPzx	EPyz	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp			
Creep Strain	ECx	ECxy	ECzx	ECyz	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp			
Rubber Stretches														
TMB Stress														
TMB Strain														
TMB Plastic Strain														
TMB Creep Strain														

Note: Plastic and creep strains are only available for BSX4 elements with the appropriate material models.

3D Semiloof Thin Beams <u>BSL3</u>, <u>BSL4</u>, <u>BXL4</u>

Entity							(Compo	nent						
Displacement	DX	DY	DZ	RSLT	THX	THY	THZ	THL1	THL2						
Force.Moment	Fx	My	Mz	Tzx	Тху	Fy	Fz	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD
(continued)	Eadp														
Strain	Ex	By	Bz	Bzx	Bxy	Ey	Ez	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp	
Loading	FX	FY	FZ	RSLT	MX	MY	MZ	ML1	ML2						
Reaction	FX	FY	FZ	RSLT	MX	MY	MZ	ML1	ML2						
Residual Force	FX	FY	FZ	RSLT	MX	MY	MZ	ML1	ML2						
Reaction Stress															
Velocity	VX	VY	VZ	RSLT											
Acceleration	AX	AY	AZ	RSLT											
Plastic Strain	EPx	EPxy	EPyz	EPzx	DDAM A	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
Creep Strain	ECx	ECxy	ECyz	ECzx	DDAM A	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
Rubber Stretches															
TMB Stress															
TMB Strain															
TMB Plastic Strain															
TMB Creep Strain															

Note: Plastic and creep strains are only available for BXL4 elements with the appropriate material models.

Plane Strain Beam Elements **BMI2N**, **BMI3N**

Entity						Comp	onent				
Displacement	DX	DY	RSLT	THZ							
Stress	Nx	Nz	Mx	Mz	Nxy	NMax	NMin	Ns	β	Nabs	Ne
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
Strain	Ex	Ez	Bx	Bz	Exy	EMax	EMin	EI	β	Eabs	EE
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
Loading	FX	FY	RSLT	MZ							
Reaction	FX	FY	RSLT	MZ							
Residual Force	FX	FY	RSLT	MZ							
Reaction Stress	PX	PY									
Velocity	VX	VY	RSLT								
Acceleration	AX	AY									
Plastic Strain											
Creep Strain											
Rubber Stretches											
TMB Stress	Sx	Sz	Sxy	SMax	Smin	SI	β	Sabs	SE		
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
TMB Strain	Ex	Ez	Exy	EPmax	EMin	El	β	Eabs	ECE		
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
TMB Plastic Strain	EPx	EPz	EPxy	EPMax	EPMin	EPI	β	EPabs	ECE		
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
TMB Creep Strain	ECx	ECz	ECxy	ECMax	ECMin	ECI	β	ECabs	ECE		
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				

2D Continuum (Plane Stress) <u>TPM3/6</u>, <u>QPM4/8</u>, <u>QPM4M</u>, <u>TPK6</u>, <u>QPK8</u>

Entity						Comp	onent					
Displacement	DX	DY	RSLT									
Stress	SX	SY	SXY	SMax	SMin	SI	β	Sabs	SE			
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp			
Strain	EX	EY	EXY	EMax	EMin	EI	β	Eabs	EE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp					
Loading	FX	FY	RSLT									
Reaction	FX	FY	RSLT									
Residual Force	FX	FY	RSLT									
Reaction Stress	PX	PY										
Velocity	VX	VY	RSLT									
Acceleration	AX	AY	RSLT									
Plastic Strain	EPX	EPY	EPXY	EPMax	EPMin	EPI	β	EPabs	EPE	CWMax	EFSMax	
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp					
Creep Strain	ECX	ECY	ECXY	ECMax	ECMin	ECI	β	ECabs	ECE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp					
Rubber Stretches	StchX	StchY	StchXY	StchMax	StchMin	Stchl	β	StchAbs	StchE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp					
TMB Stress												
TMB Strain												
TMB Plastic Strain												
TMB Creen Strain												

TMB Creep Strain

Notes:

Rubber stretches are only available for QPM4M elements with rubber material models. Strains are not available for this element when using rubber materials.

Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Models (105 and 109) are used.

2D Continuum Plane Stress (Explicit Dynamics) <u>TPM3E</u>, <u>QPM4E</u>

Entity					Con	nponent			
Displacement	DX	DY	RSLT						
Stress	SX	SY	SXY	SMax	SMin	SI	β	Sabs	SE
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp
Strain	EX	EY	EXY	EMax	EMin	El	β	Eabs	EE
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
Loading	FX	FY	RSLT						
Reaction	FX	FY	RSLT						
Residual Force	FX	FY	RSLT						
Reaction Stress	PX	PY							
Velocity	VX	VY	RSLT						
Acceleration	AX	AY	RSLT						
Plastic Strain	EPX	EPY	EPXY	EPMax	EPMin	EPI	β	EPabs	EPE
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
Creep Strain	ECX	ECY	ECXY	ECMax	ECMin	ECI	β	ECabs	ECE
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
Rubber Stretches									
TMB Stress									
TMB Strain									
TMB Plastic Strain									
TMB Creep Strain									

2D Continuum (Plane Strain) <u>TPN3/6</u>, <u>QPN4/8</u>, <u>TNK6</u>, <u>QNK8</u>, <u>QPN4M</u>

Entity						Comp	onon						
-	D.Y	5.7	DOI T			Comp	onen	L					
Displacement	DX	DY	RSLT										
Stress	SX	SY	SXY	SZ	S1	S2	S3	SI	Sabs	SE			
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
Strain	EX	EY	EXY	ΕZ	E1	E2	E3	EI	Eabs	EE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
Loading	FX	FY	RSLT										
Reaction	FX	FY	RSLT										
Residual Force	FX	FY	RSLT										
Reaction Stress	PX	PY											
Velocity	VX	VY	RSLT										
Acceleration	AX	AY	RSLT										
Plastic Strain	EPX	EPY	EPXY	EPZ	EP1	EP2	EP3	EPI	EPabs	EPE	CWMax	EFSMax	
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
Creep Strain	ECX	ECY	ECXY	ECZ	EC1	EP2	EC3	ECI	ECabs	ECE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
Rubber Stretches	StchX	StchY	StchXY	StchZ	Stch1	Stch2	Stch3	Stchl	StchAbs	StchE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
TMB Stress													
TMB Strain													
TMB Plastic Strain										_			
TMB Creep Strain													

TMB Creep Strain

Notes:

Rubber stretches are only available for QPN4M elements with rubber material models. Strains are not available for this element when using rubber materials.

Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Models (105 and 109) are used.

2D Continuum (Plane Strain) **QPN4L**

Entity	Component										
Displacement	DX	DY	RSLT								
Stress	SX	SY	SXY	SZ	S1	S2	S3	SI	SE		
Strain	StchX	StchY	StchXY	StchZ	Stch1	Stch2	Stch3	Stchl	StchE		
Loading	FX	FY	RSLT								
Reaction	FX	FY	RSLT								
Residual Force	FX	FY	RSLT								
Reaction Stress	PX	PY									
Velocity	VX	VY	RSLT								
Acceleration	AX	AY	RSLT								
Plastic Strain	EPX	EPY	EPXY	EPZ	EP1	EP2	EP3	EPI	EPE		
Creep Strain											
Rubber Stretches	StchX	StchY	StchXY	StchZ	Stch1	Stch2	Stch3	Stchl	StchE		
TMB Stress											
TMB Strain											
TMB Plastic Strain											
TMB Creep Strain											

2D Plane Strain Two Phase Continuum TPN6P, QPN8P

Entity					(Compo	nent						
Displacement	DX	DY	RSLT	Pres									
Stress	SX	SY	SXY	SZ	PRES	S1	S2	S3	SI	Sabs	SE		
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
Strain	EX	EY	EXY	EZ	EV	E1	E2	E3	EI	Eabs	EE		
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
Loading	FX	FY	RSLT	Q									
Reaction	FX	FY	RSLT	Q									
Residual Force	FX	FY	RSLT										
Reaction Stress	PX	PY											
Velocity	VX	VY	RSLT										
Acceleration	AX	AY	RSLT										
Plastic Strain	EPX	EPY	EPXY	EPZ	EP1	EP2	EP3	EPI	EPabs	EPE	CWMax	EFSMax	
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
Creep Strain	ECX	ECY	ECXY	ECZ	EC1	EP2	EC3	ECI	ECabs	ECE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
Rubber Stretches													
TMB Stress													
TMB Strain													
TMB Plastic Strain													
TMB Creep Strain													

Notes

Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Model (Model 109) is used.

2D Continuum Plane Strain (Explicit Dynamics) <u>TPN3E</u>, <u>QPN4E</u>

Entity					Comp	onent				
Displacement	DX	DY	RSLT							
Stress	SX	SY	SXY	SZ	S1	S2	S3	SI	Sabs	SE
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp	
Strain	EX	EY	EXY	EZ	E1	E2	E3	EI	Eabs	EE
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp			
Loading	FX	FY	RSLT							
Reaction	FX	FY	RSLT							
Residual Force	FX	FY	RSLT							
Reaction Stress	PX	PY								
Velocity	VX	VY	RSLT							
Acceleration	AX	AY	RSLT							
Plastic Strain	EPX	EPY	EPXY	EPZ	EP1	EP2	EP3	EPI	EPabs	EPE
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp			
Creep Strain	ECX	ECY	ECXY	ECZ	EC1	EP2	EC3	ECI	ECabs	ECE
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp			
Rubber Stretches										
TMB Stress										
TMB Strain										
TMB Plastic Strain										
TMB Creep Strain										

2D Continuum Axisymmetric Solid (Explicit Dynamics) <u>TAX3E</u>, <u>QAX4E</u>

Entity					Comp	onent				
Displacement	DX	DY	RSLT	Pres						
Stress	SX	SY	SXY	SZ	S1	S2	S3	SI	Sabs	SE
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp	
Strain	EX	EY	EXY	EZ	E1	E2	E3	EI	Eabs	EE
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp			
Loading	FX	FY	RSLT							
Reaction	FX	FY	RSLT							
Residual Force	FX	FY	RSLT							
Reaction Stress	PX	PY								
Velocity	VX	VY	RSLT							
Acceleration	AX	AY	RSLT							
Plastic Strain	EPX	EPY	EPXY	EPZ	EP1	EP2	EP3	EPI	EPabs	EPE
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp			
Creep Strain	ECX	ECY	ECXY	ECZ	EC1	EP2	EC3	ECI	ECabs	ECE
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp			
Rubber Stretches										
TMB Stress										
TMB Strain										
TMB Plastic Strain										
TMB Creep Strain										

2D Axisymmetric Solid Two Phase Continuum <u>TAX6P</u>, <u>QAX8P</u>

Entity					(Compo	nent						
Displacement	DX	DY	RSLT	Pres									
Stress	SX	SY	SXY	SZ	PRES	S1	S2	S3	SI	Sabs	SE		
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
Strain	EX	EY	EXY	EZ	EV	E1	E2	E3	EI	Eabs	EE		
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
Loading	FX	FY	RSLT	Q									
Reaction	FX	FY	RSLT	Q									
Residual Force	FX	FY	RSLT										
Reaction Stress	PX	PY											
Velocity	VX	VY	RSLT										
Acceleration	AX	AY	RSLT										
Plastic Strain	EPX	EPY	EPXY	EPZ	EP1	EP2	EP3	EPI	EPabs	EPE	CWMax	EFSMax	
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
Creep Strain	ECX	ECY	ECXY	ECZ	EC1	EP2	EC3	ECI	ECabs	ECE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
Rubber Stretches													
TMB Stress													
TMB Strain													
TMB Plastic Strain													
TMB Creep Strain													

Notes

Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Model (Model 109) is used.

2D Continuum Axisymmetric Solid Fourier <u>TAX3/6F</u>, <u>QAX4/8F</u>

Entity					Compor	nent				
Displacement	DX	DY	DZ	RSLT						
Stress	SX	SY	SXY	SZ	S1	S2	S3	SI	Sabs	SE
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	Eadp		
Strain	EX	EY	EXY	EZ	E1	E2	E3	EI	Eabs	EE
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	Eadp				
Loading	FX	FY	FZ	RSLT						
Reaction	FX	FY	FZ	RSLT						
Residual Force										
Reaction Stress	PX	PY								
Velocity	VX	VY	VZ	RSLT						
Acceleration	AX	AY	AZ	RSLT						
Plastic Strain										
Creep Strain										
Rubber Stretches										
TMB Stress										
TMB Strain										
TMB Plastic Strain										
TMB Creep Strain										

Axisymmetric Solid TAX3/6, QAX4/8, QAX4M, TXK6, QXK8

Entity						Comp	onent	t					
Displacement	DX	DY	RSLT										
Stress	SX	SY	SXY	SZ	S1	S2	S3	SI	Sabs	SE			
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
Strain	EX	EY	EXY	EZ	E1	E2	E3	El	Eabs	EE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
Loading	FX	FY	RSLT										
Reaction	FX	FY	RSLT										
Residual Force	FX	FY	RSLT										
Reaction Stress	PX	PY											
Velocity	VX	VY	RSLT										
Acceleration	AX	AY	RSLT										
Plastic Strain	EPX	EPY	EPXY	EPZ	EP1	EP2	EP3	EPI	EPabs	EPE	CWMax	EFSMax	
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
Creep Strain	ECX	ECY	ECXY	ECZ	EC1	EP2	EC3	ECI	ECabs	ECE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
Rubber Stretches	StchX	StchY	StchXY	StchZ	Stch1	Stch2	Stch3	Stchl	StchAbs	StchE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
TMB Stress													
TMB Strain													
TMB Plastic Strain													

TMB Creep Strain

Notes

Rubber stretches are only available for QAX4M elements with rubber material models. Strains are not available for this element when using rubber materials Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Models (105 and 109) are used.

Axisymmetric Solid Large Strain QAX4L

					•						
Entity					Compo	nent					
Displacement	DX	DY	RSLT	Pres							
Stress	SX	SY	SXY	SZ	S1	S2	S3	SI	Sabs	SE	
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
Strain	StchX	StchY	StchXY	StchZ	Stch1	Stch2	Stch3	Stchl	StchE		
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
Loading	FX	FY	RSLT								
Reaction	FX	FY	RSLT								
Residual Force	FX	FY	RSLT								
Reaction Stress	PX	PY									
Velocity	VX	VY	RSLT								
Acceleration	AX	AY	RSLT								
Plastic Strain	EPX	EPY	EPXY	EPZ	EP1	EP2	EP3	EPI	EPE		
Creep Strain											
Rubber Stretches	StchX	StchY	StchXY	StchZ	Stch1	Stch2	Stch3	Stchl	StchE		
TMB Stress											
TMB Strain											
TMB Plastic Strain											
TMB Creep Strain											

3D Solid Continuum <u>TH4/10</u>, <u>TH10S</u>, <u>PN6/12/15</u>, <u>PN6L/12L</u>, <u>HX8/16/20</u>, <u>HX8M</u>, <u>HX8L/16L</u>, <u>TH10K</u>, <u>PN15K</u>, <u>HX20K</u>

Entity						Compo	onent						
Displacement	DX	DY	DZ	RSLT									
Stress	SX	SY	SZ	SXY	SYZ	SZX	PRES	S1	S2	S3	SI	Sabs	SE
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
Strain	EX	EY	EZ	EXY	EYZ	EZX	EV	E1	E2	E3	EI	Eabs	EE
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
Loading	FX	FY	FZ	RSLT									
Reaction	FX	FY	FZ	RSLT									
Residual Force	FX	FY	FZ	RSLT									
Reaction Stress	PX	PY	ΡZ										
Velocity	VX	VY	VZ	RSLT									
Acceleration	AX	AY	AZ	RSLT									
Plastic Strain	EPX	EPY	EPZ	EPXY	EPYZ	EPZX	EP1	EP2	EP3	EPI	EPabs	EPE	
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp	CWMax	EFSMax				
Creep Strain	ECX	ECY	ECZ	ECXY	ECYZ	ECZX	EC1	EC2	EC3	ECI	ECabs	ECE	
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
Rubber Stretches	StchX	StchY	StchZ	StchXY	StchYZ	StchZX	Stch1	Stch2	Stch3	Stchl	StchAbs	StchE	
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
TMB Stress													
TMB Strain													
TMB Plastic Strain													
TMB Creep Strain													

Notes:

Rubber stretches are only available for HX8M elements with rubber material models. Strains are not available for this element when using rubber materials. Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Models (105 and 109) are used.

3D Solid Continuum Two Phase <u>TH10P</u>, <u>PN12P</u>, <u>PN15P</u>, <u>HX16P</u>, <u>HX20P</u>

Entity					C	Compor	nent					
Displacement	DX	DY	DZ	RSLT	Pres							
Stress	SX	SY	SZ	SXY	SYZ	SZX	S1	S2	S3	SI	Sabs	SE
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp			
Strain	EX	EY	EZ	EXY	EYZ	EZX	E1	E2	E3	EI	Eabs	EE
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp					
Loading	FX	FY	FZ	RSLT	Q							
Reaction	FX	FY	FZ	RSLT	Q							
Residual Force	FX	FY	FZ	RSLT								
Reaction Stress	PX	PY	ΡZ									
Velocity	VX	VY	VZ	RSLT								
Acceleration	AX	AY	AZ	RSLT								
Plastic Strain	EPX	EPY	EPZ	EPXY	EPYZ	EPZX	EP1	EP2	EP3	EPI	EPabs	EPE
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp	CWMax	EFSMax			
Creep Strain	ECX	ECY	ECZ	ECXY	ECYZ	ECZX	EC1	EC2	EC3	ECI	ECabs	ECE
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp					
Rubber Stretches												
TMB Stress												
TMB Strain												
TMB Plastic Strain												
TMB Creep Strain												

Notes

Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Model (Model 109) is used.

3D Solid Continuum Explicit Dynamics <u>TH4E</u>, <u>PN6E</u>, <u>HX8E</u>

Entity					Comr	oonent						
-	DV	DV	57			Joneni						
Displacement	DX	DY	DZ	RSLT	Pres							
Stress	SX	SY	SZ	SXY	SYZ	SZX	S1	S2	S3	SI	Sabs	SE
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp			
Strain												
Loading	FX	FY	FZ	RSLT								
Reaction	FX	FY	FZ	RSLT								
Residual Force	FX	FY	FZ	RSLT								
Reaction Stress	PX	PY	ΡZ									
Velocity	VX	VY	VZ	RSLT								
Acceleration	AX	AY	AZ	RSLT								
Plastic Strain												
Creep Strain												
Rubber Stretches												
TMB Stress												
TMB Strain												
TMB Plastic Strain												
TMB Creep Strain												

Isoflex Thin Plates <u>TF3</u>, <u>QF4</u>

Entity							Com	pone	nt						
Displacement	DZ	RSLT	THX	THY											
Stress	MX	MY	MXY	MMax	MMin	MI	β	Nabs	ME	Mx(T)	My(T)	Mx(B)	My(B)	Util(T)	Util(B)
(continued)	Damage	LogLife	SED	PWD	Eadp										
Strain	BX	BY	BXY	BMax	BMin	BI	β	Eabs	BE	SED	PWD	Eadp			
Loading	FZ	RSLT	MX	MY											
Reaction	FZ	RSLT	MX	MY											
Residual Force	FZ	RSLT	MX	MY											
Reaction Stress	ΡZ														
Velocity	VZ	RSLT													
Acceleration	AZ	RSLT													
Plastic Strain															
Creep Strain															
Rubber Stretches															
TMB Stress	SX	SY	SXY	SMax	SMin	SI	β	Sabs	SE	Damage	LogLife	SED	PWD	Eadp	
TMB Strain	EX	EY	EXY	EMax	EMin	EI	β	Eabs	EE	SED	PWD	Eadp			
TMB Plastic Strain															

TMB Creep Strain

Isoflex Thick Plates **QSC4**

Entity							Com	oonen	t						
-	D7		TUV	TUN			00111	Jonen	•						
Displacement	DZ	RSLT	THX	THY											
Stress	MX	MY	MXY	Sx	Sy	MMax	MMin	MI	β	Nabs	ME	Mx(T)	My(T)	Mx(B)	My(B)
(continued)	Util(T)	Util(B)	Damage	LogLife	SED	PWD	Eadp								
Strain	BX	BY	BXY	EZX	EYZ	BMax	BMin	BI	β	Eabs	BE	SED	PWD	Eadp	
Loading	FZ	RSLT	MX	MY											
Reaction	FZ	RSLT	MX	MY											
Residual Force	FZ	RSLT	MX	MY											
Reaction Stress	PZ														
Velocity	VZ	RSLT													
Acceleration	AZ	RSLT													
Plastic Strain															
Creep Strain															
Rubber Stretches															
TMB Stress	SX	SY	SXY	SMax	SMin	SI	β	Sabs	SE	Damage	LogLife	SED	PWD	Eadp	
TMB Strain	EX	EY	EXY	EMax	EMin	EI	β	Eabs	EE	SED	PWD	Eadp			
TMB Plastic Strain															

TMB Creep Strain

Mindlin Thick Plates <u>TTF6, QTF8</u>

Entity							Со	npone	nt						
Displacement	DZ	RSLT	THX	THY											
Stress	MX	MY	MXY	Sx	Sy	MMax	MMin	MI	β	Nabs	ME	Mx(T)	My(T)	Mx(B)	My(B)
(continued)	Util(T)	Util(B)	Damage	LogLife	SED	PWD	Eadp								
Strain	BX	BY	BXY	EZX	EYZ	BMax	BMin	BI	β	Eabs	BE	SED	PWD	Eadp	
Loading	FZ	RSLT	MX	MY											
Reaction	FZ	RSLT	MX	MY											
Residual Force	FZ	RSLT	MX	MY											
Reaction Stress	PZ														
Velocity	VZ	RSLT													
Acceleration	AZ	RSLT													
Plastic Strain															
Creep Strain															
Rubber Stretches															
TMB Stress	SX	SY	SXY	SMax	SMin	SI	β	Sabs	SE	Damage	LogLife	SED	PWD	Eadp	
TMB Strain	EX	EY	EXY	EMax	EMin	EI	β	Eabs	EE	SED	PWD	Eadp			
TMB Plastic Strain															

TMB Creep Strain

2D Axisymmetric Membranes **BXM2**, **BXM3**

Entity					Comp	onent			
Displacement	DX	DY	RSLT		- • · · · P				
Stress	Sx	Sz	SMax	SMin	SI	β	Sabs	SE	
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp
Strain	Ex	Ez	EMax	EMin	EI	β	Eabs	EE	
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
Loading	FX	FY	RSLT						
Reaction	FX	FY	RSLT						
Residual Force	FX	FY	RSLT						
Reaction Stress	PX	PY							
Velocity	VX	VY	RSLT						
Acceleration	AX	AY	RSLT						
Plastic Strain	EPx	EPz	EPMax	EPMin	EPI	β	EPabs	EPE	
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
Creep Strain	ECx	ECz	ECMax	ECMin	ECI	β	ECabs	ECE	
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
Rubber Stretches									
TMB Stress									
TMB Strain									
TMB Plastic Strain									
TMB Creep Strain									

Note: Rubber models are available for use with the BXM2 element, however strains are output and rubber stretches are not available.

3D Space Membranes <u>TSM3</u>, <u>SMI4</u>

Entity					Co	ompone	nt					
Displacement	DX	DY	DZ	RSLT								
Stress	Nx	Ny	Nxy	NMax	NMin	Ns	β	Nabs	Ne			
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp			
Strain	Ex	Ey	Exy	EMax	EMin	El	β	Eabs	EE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp					
Loading	FX	FY	FZ	RSLT								
Reaction	FX	FY	FZ	RSLT								
Residual Force	FX	FY	FZ	RSLT								
Reaction Stress	PX	PY	PZ									
Velocity	VX	VY	VZ	RSLT								
Acceleration	AX	AY	AZ	RSLT								
Plastic Strain												
Creep Strain												
Rubber Stretches												
TMB Stress	SX	SY	SZ	SXY	SYZ	SZX	S1	S2	S3	SI	Sabs	SE
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp					
TMB Strain	EX	EY	EZ	EXY	EYZ	EZX	E1	E2	E3	El	Eabs	EE
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp					
TMB Plastic Strain												
TMB Creep Strain												

2D Thin Axisymmetric Shells **BXS3**

Entity					(Componer	nt				
Displacement	DX	DY	RSLT	THZ	DU						
Stress	Nx	Nz	Mx	Mz	Ny	NMax	NMin	Ns	β	Nabs	Ne
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
Strain	Ex	Ez	Bx	Bz	Ey	EMax	EMin	El	β	Eabs	EE
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
Loading	FX	FY	RSLT	MZ	FDU						
Reaction	FX	FY	RSLT	MZ	FDU						
Residual Force	FX	FY	RSLT	MZ	FDU						
Reaction Stress	PX	PY									
Velocity	VX	VY	RSLT								
Acceleration	AX	AY									
Plastic Strain											
Creep Strain											
Rubber Stretches											
TMB Stress	Sx	Sz	SMax	SMin	SI	β	Sabs	SE			
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
TMB Strain	Ex	Ez	EPMax	EMin	EI	β	Eabs	EE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
TMB Plastic Strain	EPx	EPz	EPMax	EPMin	EPI	β	EPabs	EPE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
TMB Creep Strain	ECx	ECz	ECMax	ECMin	ECI	β	ECabs	ECE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				

2D Thick Axisymmetric Shells **BXSI2**, **BXSI3**

Entity						Comp	onent				
Displacement	DX	DY	RSLT	THZ							
Stress	Nx	Nz	Mx	Mz	Nxy	NMax	NMin	Ns	β	Nabs	Ne
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
Strain	Ex	Ez	Bx	Bz	Exy	EMax	EMin	EI	β	Eabs	EE
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
Loading	FX	FY	RSLT	MZ							
Reaction	FX	FY	RSLT	MZ							
Residual Force	FX	FY	RSLT	MZ							
Reaction Stress	PX	PY									
Velocity	VX	VY	RSLT								
Acceleration	AX	AY									
Plastic Strain											
Creep Strain											
Rubber Stretches											
TMB Stress	Sx	Sz	Sxy	SMax	SMin	SI	β	Sabs	SE		
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp		
TMB Strain	Ex	Ez	Exy	EPMax	EMin	El	β	Eabs	EE		
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
TMB Plastic Strain	EPx	EPz	EPxy	EPMax	EPMin	EPI	β	EPabs	EPE		
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				
TMB Creep Strain	ECx	ECz	ECxy	ECMax	ECMin	ECI	β	ECabs	ECE		
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp				

3D Flat Thin Shells <u>TS3</u>, <u>QSI4</u>

Entity						C	Compor	nent							
Displacement	DX	DY	DZ	RSLT	THX	THY	THZ								
Stress	Nx	Ny	Nxy	Мх	Му	Мху	NMax	NMin	Ns	β	Nabs	Ne	Nx(T)/ Mx(T)	Ny(T)/ Ny(T)	Nx(B)/ Mx(B)
(continued)	Ny(B)/ My(B)	Util(T)	Util(B)	MUtil(T)	MUtil(B)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	Fc(T)	Fc(B)	Eadp
Strain	Ex	Ey	Exy	Bx	Ву	Bxy	EMax	EMin	EI	β	Eabs	EE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	Eadp									
Loading	FX	FY	FZ	RSLT	MX	MY	MZ								
Reaction	FX	FY	FZ	RSLT	MX	MY	MZ				_				
Residual Force	FX	FY	FZ	RSLT	MX	MY	MZ								
Reaction Stress	PX	PY	ΡZ												
Velocity	VX	VY	VZ	RSLT											
Acceleration	AX	AY	AZ	RSLT											
Plastic Strain															
Creep Strain															
Rubber Stretches															
TMB Stress	SX	SY	SZ	SXY	SYZ	SZX	S1	S2	S3	SI	Sabs	SE			
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	Eadp							
TMB Strain	EX	EY	EZ	EXY	EYZ	EZX	E1	E2	E3	EI	Eabs	EE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp								
TMB Plastic Strain															
TMB Creep Strain															

3D Flat Thin Nonlinear Shell <u>TSR6</u>

Entity						Co	mponer	nt							
Displacement	DX	DY	DZ	RSLT	THL1										
Stress	Nx	Ny	Nxy	Mx	Му	Мху	NMax	NMin	Ns	β	Nabs	Ne	Nx(T)/ Mx(T)	Ny(T)/ Ny(T)	Nx(B)/ Mx(B)
(continued)	Ny(B)/ My(B)	Util(T)	Util(B)	MUtil(T)	MUtil(B)	Damage	LogLife	DDAM A	CURR D	DAMA M	DFUN C	SED	PWD	Fc(T)	Fc(B)
Eadp															
Strain	Ex	Ey	Exy	Bx	By	Bxy	EMax	EMin	EI	β	Eabs	EE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp								
Loading	FX	FY	FZ	RSLT	ML1										
Reaction	FX	FY	FZ	RSLT	ML1										
Residual Force	FX	FY	FZ	RSLT	ML1										
Reaction Stress	PX	PY	PZ												
Velocity	VX	VY	VZ	RSLT											
Acceleration	AX	AY	AZ	RSLT											
Plastic Strain															
Creep Strain															
Rubber Stretches															
TMB Stress	SX	SY	SZ	SXY	SYZ	SZX	S1	S2	S3	SI	Sabs	SE			
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	Eadp							
TMB Strain	EX	EY	EZ	EXY	EYZ	EZX	E1	E2	E3	EI	Eabs	EE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp								
TMB Plastic Strain	EPX	EPY	EPZ	EPXY	EPYZ	EPZX	EP1	EP2	EP3	EPI	EPabs	EPE	CWMa x	EFSMa x	
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp								
TMB Creep Strain	ECX	ECY	ECZ	ECXY	ECYZ	ECZX	EC1	EC2	EC3	ECI	ECabs	ECE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp								

Notes

TMB Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Model (Model 109) is used.

Semiloof Shells <u>TSL6</u>, <u>QSL8</u>

Entitut						~				_		_			
Entity	5.4	51					ompo	nent							
Displacement	DX	DY	DZ	RSLT	THL1	THL2									
Stress	Nx	Ny	Nxy	Mx	Му	Мху	NMax	NMin	Ns	β	Nabs	Ne	Nx(T)/ Mx(T)	Ny(T)/ My(T)	Nx(B)/ Mx (B)
(continued)	Ny(B)/ My(B)	Util(T)	Util(B)	MUtil(T)	MUtil(B)	Damage	LogLife	DDAMA	CURR D	DAMAM	DFUNC	SED	PWD	Fc(T)	Fc(B)
(continued)	Eadp														
Strain	Ex	Ey	Exy	Bx	Ву	Bxy	EMax	EMin	EI	β	Eabs	EE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp								
Loading	FX	FY	FZ	RSLT	ML1	ML2									
Reaction	FX	FY	FZ	RSLT	ML1	ML2									
Residual Force	FX	FY	FZ	RSLT	ML1	ML2									
Reaction Stress	PX	PY	ΡZ												
Velocity	VX	VY	VZ	RSLT											
Acceleration	AX	AY	AZ	RSLT											
Plastic Strain															
Creep Strain															
Rubber Stretches															
TMB Stress	SX	SY	SZ	SXY	SYZ	SZX	S1	S2	S3	SI	Sabs	SE			
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
TMB Strain	EX	EY	EZ	EXY	EYZ	EZX	E1	E2	E3	EI	Eabs	EE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp								
TMB Plastic Strain	EPX	EPY	EPZ	EPXY	EPYZ	EPZX	EP1	EP2	EP3	EPI	EPabs	EPE	CWMax	EFSMa x	
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp								
TMB Creep Strain	ECX	ECY	ECZ	ECXY	ECYZ	ECZX	EC1	EC2	EC3	ECI	ECabs	ECE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp								

Notes

TMB Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Model (Model 109) is used.

3D Thick Shells TTS3, TTS6, QTS4, QTS8

Entity							Compo	onent							
Displacement	DX	DY	DZ	RSLT	THX	THY	THZ								
Stress	Nx	Ny	Nxy	Mx	Му	Мху	Sx	Sy	NMax	NMin	β	Nab s	NE	Nx(T)/ Mx(T)	Ny(T)/ My(T)
(continued)	Nx(B)/Mx(B)	Ny(B)/ My(B)	Util(T)	Util(B)	MUtil(T)	MUtil(B)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFU NC	SED	PWD	Fc(T)
(continued)	Fc(B)	Eadp													
Strain															
Loading	FX	FY	FZ	RSLT	MX	MY	MZ								
Reaction	FX	FY	FZ	RSLT	MX	MY	MZ								
Residual Force	FX	FY	FZ	RSLT	MX	MY	MZ								
Reaction Stress	PX	PY	ΡZ												
Velocity	VX	VY	VZ	RSLT											
Acceleration	AX	AY	AZ	RSLT				_				_			
Plastic Strain															
Creep Strain															
Rubber Stretches															
TMB Stress	SX	SY	SZ	SXY	SYZ	SZX	S1	S2	S3	SI	Nabs	SE			
(continued)	Damage	LogLife	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp						
TMB Strain	EX	EY	EZ	EXY	EYZ	EZX	E1	E2	E3	EI	Eabs	EE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp								
TMB Plastic Strain	EPX	EPY	EPZ	EPXY	EPYZ	EPZX	EP1	EP2	EP3	EPI	EPabs	EPE	CWMa x	EFSMa x	
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp								
TMB Creep Strain	ECX	ECY	ECZ	ECXY	ECYZ	ECZX	EC1	EC2	EC3	ECI	ECabs	ECE			
(continued)	DDAMA	CURRD	DAMAM	DFUNC	SED	PWD	Eadp								

Notes

TMB Plastic strain components CWMax and EFSMax are only available when the Smoothed Multi-crack Concrete Model (Model 109) is used.

2D Joints (for Bars, Plane Stress and Plane Strain) JNT3

Entity					Compon	ent		
Displacement	DX	DY	RSLT					
Stress	Fx	Fy	Damage	LogLife	SED	PWD	Eadp	
Strain	Ex	Ey	SED	PWD	Eadp			
Loading	FX	FY	RSLT					
Reaction	FX	FY	RSLT					
Residual Force	FX	FY	RSLT					
Reaction Stress								
Velocity	VX	VY	RSLT					
Acceleration	AX	AY	RSLT					
Plastic Strain	EPx	EPy	SED	PWD	Eadp			
Creep Strain								
Rubber Stretches								
TMB Stress								
TMB Strain								
TMB Plastic Strain								
TMB Creep Strain								

2D Joints (for Engineering and Kirchhoff Beams) JPH3

Entity					Comp	onent		
Displacement	DX	DY	RSLT	THZ				
Stress	Fx	Fy	Mz	Damage	LogLife	SED	PWD	Eadp
Strain	Ex	Ey	Bz	SED	PWD	Eadp		
Loading	FX	FY	RSLT	MZ				
Reaction	FX	FY	RSLT	MZ				
Residual Force	FX	FY	RSLT	MZ				
Reaction Stress								
Velocity	VX	VY	RSLT					
Acceleration	AX	AY	RSLT					
Plastic Strain	EPx	EPy	BPz	SED	PWD	Eadp		
Creep Strain								
Rubber Stretches								
TMB Stress								
TMB Strain								
TMB Plastic Strain								
TMB Creep Strain								

2D Joints (for Grillage Beams and Plates) <u>JF3</u>

Entity					Compo	onent		
Displacement	DZ	RSLT	THXZ	THY				
Stress	Fz	Mx	My	Damage	LogLife	SED	PWD	Eadp
Strain	Ez	Bx	Ву	SED	PWD	Eadp		
Loading	FZ	RSLT	MX	MY				
Reaction	FZ	RSLT	MX	MY				
Residual Force	FZ	RSLT	MX	MY				
Reaction Stress								
Velocity	VZ	RSLT						
Acceleration	AZ	RSLT						
Plastic Strain	EPx	EPy	BPz	SED	PWD	Eadp		
Creep Strain								
Rubber Stretches								
TMB Stress								
TMB Strain								
TMB Plastic Strain								
TMB Creep Strain								

2D Joints (for Axisymmetric Solids) JAX3

Entity					Compone	ent			
Displacement	DX	DY	RSLT						
Stress	Fx	Fy	Damage	LogLife	SED	PWD	Eadp		
Strain	Ex	Ey	SED	PWD	Eadp				
Loading	FX	FY	RSLT	MZ					
Reaction	FX	FY	RSLT	MZ					
Residual Force	FX	FY	RSLT	MZ					
Reaction Stress									
Velocity	VX	VY	RSLT						
Acceleration	AX	AY	RSLT						
Plastic Strain	EPx	EPy	SED	PWD	Eadp				
Creep Strain									
Rubber Stretches									
TMB Stress									
TMB Strain									
TMB Plastic Strain								 	
TMB Creep Strain									

2D Joints (for Axisymmetric Shells) <u>JXS3</u>

Entity					Comp	onent		
Displacement	DX	DY	RSLT	THZ				
Stress	Fx	Fy	Mz	Damage	LogLife	SED	PWD	Eadp
Strain	Ex	Ey	Bz	SED	PWD	Eadp		
Loading	FX	FY	RSLT	MZ				
Reaction	FX	FY	RSLT	MZ				
Residual Force	FX	FY	RSLT	MZ				
Reaction Stress								
Velocity	VX	VY	RSLT					
Acceleration	AX	AY	RSLT					
Plastic Strain	EPx	EPy	BPz	SED	PWD	Eadp		
Creep Strain								
Rubber Stretches								
TMB Stress								
TMB Strain								
TMB Plastic Strain								
TMB Creep Strain								

3D Joints (for general 3 dof connection) JNT4, JL43

					•				
Entity					Com	ponent			
Displacement	DX	DY	DZ	RSLT					
Stress	Fx	Fy	Fz	Damage	LogLife	SED	PWD	Eadp	
Strain	Ex	Ey	Ez	SED	PWD	Eadp			
Loading	FX	FY	FZ	RSLT					
Reaction	FX	FY	FZ	RSLT					
Residual Force	FX	FY	FZ	RSLT					
Reaction Stress									
Velocity	VX	VY	VZ	RSLT					
Acceleration	AX	AY	AZ	RSLT					
Plastic Strain	EPx	EPy	EPz	SED	PWD	Eadp			
Creep Strain									
Rubber Stretches									
TMB Stress									
TMB Strain									
TMB Plastic Strain									
TMB Creep Strain									

(for Bars, Solids, Space Membranes and Semiloof Shell Corners)

3D Joints (for general 6 dof connection) <u>JSH4</u>, <u>JL46</u>

(for Engineering, Kirchhoff and Semiloof Beam End Nodes)

Entity							Compon	ent			
Displacement	DX	DY	DZ	RSLT	THX	THY	THZ				
Stress	Fx	Fy	Fz	Mx	My	Mz	Damage	LogLife	SED	PWD	Eadp
Strain	Ex	Ey	Ez	Bx	By	Bz	SED	PWD	Eadp		
Loading	FX	FY	FZ	RSLT	MX	MY	MZ				
Reaction	FX	FY	FZ	RSLT	MX	MY	MZ				
Residual Force	FX	FY	FZ	RSLT	MX	MY	MZ				
Reaction Stress											
Velocity	VX	VY	VZ	RSLT							
Acceleration	AX	AY	AZ	RSLT							
Plastic Strain	EPx	EPy	EPz	BPx	BPy	BPz	SED	PWD	Eadp		
Creep Strain											
Rubber Stretches											
TMB Stress											
TMB Strain											
TMB Plastic Strain											
TMB Creep Strain											

3D Joints (for Semiloof Element Mid-side Nodes) JSL4

Entity						Com	ponent			
Displacement	DX	DY	DZ	RSLT	THL1	THL2				
Stress	Fx	Fy	Fz	M1	M2	Damage	LogLife	SED	PWD	Eadp
Strain	Ex	Ey	Ez	B1	B2	SED	PWD	Eadp		
Loading	FX	FY	FZ	RSLT	ML1	ML2				
Reaction	FX	FY	FZ	RSLT	ML1	ML2				
Residual Force	FX	FY	FZ	RSLT	ML1	ML2				
Reaction Stress										
Velocity	VX	VY	VZ	RSLT						
Acceleration	AX	AY	AZ	RSLT						
Plastic Strain	EPx	EPy	EPz	BP1	BP2	SED	PWD	Eadp		
Creep Strain										
Rubber Stretches										
TMB Stress										
TMB Strain										
TMB Plastic Strain										
TMB Creep Strain										

Thermal Bars <u>BFD2/3</u>, <u>BFS2/3</u>, <u>BFX2/3</u>

Entity	Component
Potential	PHI
Gradient	Gx Eadp
Flux	qx Eadp
Reaction	Q

Thermal Links <u>LFD2</u>, <u>LFS2</u>, <u>LFX2</u>

Entity				Component		
Potential	PHI					
Gradient	n.a.	Eadp				
Flux	qx	Eadp				
Reaction	Q					

Plane and Axisymmetric Field <u>TFD3/6</u>, <u>QFD4/8</u>, <u>TXF3/6</u>, <u>QXF4/8</u>

Entity				Component
Potential	PHI			
Gradient	Gx	Gy	Eadp	
Flux	qx	qy	Eadp	
Reaction	Q			

Solid Field <u>TF4/10</u>, <u>PF6/12/15</u>, <u>HF8/16/20</u>, <u>TF10S</u>, <u>PF6C/12C</u>, <u>HF8C/16C</u>

Entity					Component
Potential	PHI				
Gradient	Gx	Gy	Gz	Eadp	
Flux	qx	qy	qz	Eadp	
Reaction	Q				

Plane and Axisymmetric Hygro-Thermal <u>THT3/6</u>, <u>QHT4/8</u>, <u>TXHT3/6</u>, <u>QXHT4/8</u>

Entity				Comp	onent					
Nodal variable	Т									
Temperature flux	qX	qY	qZ	RSLT						
Water vapour flux	JVX	JyY	JVZ	RSLT						
Liquid water flux	JWX	JWY	JWZ	RSLT						
Temperature gradient	GTX	GTY	GTZ	RSLT						
Water saturation gradient	GWX	GWY	GWZ	RSLT						
Other hygro-thermal results	SW	ROWC	PV	DH	TEFH	POR	тс	PMD	Hr	

Hygro-thermal results components:

SW = Water saturation ROWC = Liquid water content PV = Water vapour pressure DH = Degree of hydration TEFH = Effective time of hydration POR = Porosity TC = Thermal conductivity PMD = Water permeabilityHr = Relative humidity

Solid Hygro-Thermal <u>THT4/10</u>, <u>PHT6/12/16</u>, <u>HHT8/16/20</u>

Entity				Comp	onent					
Nodal variable	Т									
Temperature flux	qX	qY	qZ	RSLT						
Water vapour flux	JVX	JyY	JVZ	RSLT						
Liquid water flux	JWX	JWY	JWZ	RSLT						
Temperature gradient	GTX	GTY	GTZ	RSLT						
Water saturation gradient	GWX	GWY	GWZ	RSLT						
Other hygro-thermal results	SW	ROWC	PV	DH	TEFH	POR	TC	PMD	Hr	

Hygro-thermal results components:

SW = Water saturation ROWC = Liquid water content PV = Water vapour pressure DH = Degree of hydration TEFH = Effective time of hydration POR = Porosity TC = Thermal conductivity PMD = Water permeabilityHr = Relative humidity

2D Interface Element <u>IPN4</u>, <u>IPN6</u>, <u>IAX4</u>, <u>IAX6</u>

Entity				Com	nponent
Displacement	Dx	Dy	RSLT		
Stress	Sx	Sy	Damage	LogLife	Eadp
Strain	Ex	Ey	Eadp		
Loading	Fx	Fy	RSLT	MZ	
Reaction	Fx	Fy	RSLT	MZ	
Residual Force	Fx	Fy	RSLT		
Reaction Stress					
Velocity	Vx	Vy	RSLT		
Acceleration	Ax	Ay	RSLT		
Plastic Strain					
Creep Strain					
Rubber Stretches					
TMB Stress					
TMB Strain					
TMB Plastic Strain					
TMB Creep Strain					

2D Two Phase Interface Elements <u>IPN6P</u>, <u>IPN8P</u>

Entity					Compone	nt
Displacement	Dx	Dy	RSLT	Press		
Stress	Sx	Sy	Q	Damage	LogLife	Eadp
Strain	Ex	Ey	dP	Eadp		
Loading	Fx	Fy	RSLT			
Reaction	Fx	Fy	RSLT	Q		
Residual Force	Fx	Fy	RSLT	Q		
Reaction Stress						
Velocity	Vx	Vy	RSLT			
Acceleration	Ax	Ay	RSLT			
Plastic Strain						
Creep Strain						
Rubber Stretches						
TMB Stress						
TMB Strain						
TMB Plastic Strain						
TMB Creep Strain						

3D Interface Element IS6 IS8 IS12 IS16

Entity					Component
Displacement	Dx	Dy	RSLT		
Stress	Sx	Sy	Sz	Ez	Eadp
Strain	Ex	Ey	Eadp		
Loading	Fx	Fy	RSLT		
Reaction	Fx	Fy	RSLT		
Residual Force	Fx	Fy	RSLT		
Reaction Stress					
Velocity	Vx	Vy	RSLT		
Acceleration	Ax	Ay	RSLT		
Plastic Strain					
Creep Strain					
Rubber Stretches					
TMB Stress					
TMB Strain					
TMB Plastic Strain					
TMB Creep Strain					

3D Two Phase Interface Element <u>IS12P</u>, <u>IS16P</u>

Entity					Compo	nent
Displacement	Dx	Dy	Dz	RSLT	Press	
Stress	Sx	Sy	Q	Damage	LogLife	Eadp
Strain	Ex	Ey	Ez	dP	Eadp	
Loading	Fx	Fy	Fz	RSLT		
Reaction	Fx	Fy	Fz	RSLT	Q	
Residual Force	Fx	Fy	Fz	RSLT	Q	
Reaction Stress						
Velocity	Vx	Vy	Vz	RSLT		
Acceleration	Ax	Ay	Az	RSLT		
Plastic Strain						
Creep Strain						
Rubber Stretches						
TMB Stress						
TMB Strain						
TMB Plastic Strain						
TMB Creep Strain						

Appendix L : Joint Element Compatibility.

Joint Element Compatibility and Notes

Joint elements are compatible with the following elements:

Joint Element	Compatible Finite Elements					
JNT3	Bars	BAR2, BAR3				
	2D Plane Stress	<u>TPM3, TPM6, QPM4, QPM8, TPK6, QPK8, QPM4M, TPM3E, QPM4E, </u>				
	2D Plane Strain	<u>TPN3, TPN6, QPN4, QPN8, TNK6, QNK8, TPN6P, QPN8P, QPN4M, QPN4L</u>				
<u>JPH3</u>	2D Beams	<u>BMI2, BMI21, BMI2N, BMI3N, BMI3, BMI3N, BMI2X, BMI3X, BM3, BMX3</u>				
<u>JF3</u>	2D Grillage	GRIL				
	2D Plates	<u>TF3, QF4, TF6, QSC4, TTF6, QTF8</u>				
JNT4	3D Bars	<u>BRS2,</u> <u>BRS3,</u>				
	3D Solids	<u>TH4, TH10, PN6, PN12, PN15, HX8, HX16, HX20,</u> <u>TH10P, PN12P, PN15P, HX16P, HX20P, HX8M, PN6L,</u> <u>PN12L , HX8L, HX16L, TH10S</u>				
	Space	<u>TSM3, SMI4</u>				

Joint Element	Compatible Finite Elements					
	Membranes					
	3D Shell	TSR6 (corner nodes)				
<u>JL43</u>	Semiloof Shells	TSL6, QSL8 (corner nodes)				
<u>JSH4</u>	3D Beams	BS3, BS4, BSX4, BMI21, BMI31, BMI22, BMI33, BMX21, BMX31, BMX22, BMX33, BMI21W, BMI22W, BMI31W, BMI33W, BMX21W, BMX22W, BMX31W, BMX33W				
	3D Shells	<u>TS3, QSI4, TTS3, TTS6, QTS4, QTS8</u>				
<u>JL46</u>	Semiloof Beams	BSL3, BSL4, BXL4 (corner nodes)				
JSL4	Semiloof Beams	BSL3, BSL4, BXL4 (mid-side nodes)				
	Semiloof Shells	QSL8, TSL6 (mid-side nodes)				
JAX3	Axisymmetric Solids	<u>TAX3, TAX6, QAX4, QAX8, TAX6P, QAX8P, TAX3E, QAX4E, TAX6P, TXK6, QXK8, QAX4M, QAX4L</u>				
JXS3	Axisymmetric Shells	<u>BXS3, BXSI2, BXSI3,</u>				

Notes on the use of Joints

1. The nodes of a joint element need not be coincident, but for correct response the distance between them should be as small as possible. This is particularly important with joint elements which contain rotational degrees of freedom, since the stiffness matrix is not formulated using engineering beam theory. This means that a joint moment is independent of both shear force and its length. For instance, the moment calculated with a joint length of zero will remain the same magnitude at any other joint length. These effects can be exacerbated significantly in dynamic analyses (e.g. eigenvalue extraction or Hilber dynamics). Non-coincident nodes will lead to additional forces in the solution which are not in equilibrium (usually small and swamped, but could be significant sometimes). It is not recommend to have joints "hanging off" the side of a modelled structure, having a large stiffness associated.

- 2. If eccentricity is defined for a joint element (JPH3/JSH4/JL46), the joint will behave in the same manner as an infinitesimally short eccentric beam.
- 3. Joints do not support any geometric nonlinearity. They may be used, however, in geometrically nonlinear analyses but will themselves remain geometrically linear (that is, infinitesimal strain is assumed and large deformation effects are ignored).
- 4. The strain for a joint element is measured as follows:
 - Strain measure = (displacement for 2nd node) (displacement for 1st node)
 - This strain being measured in the local axis system. Therefore, if node 1 is restrained, node 2 would need to be displaced in the negative local (x/y/z) direction to generate compressive contact forces.
- 4. The rotation output for a joint element is measured in radians.

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LUSAS, Forge House, 66 High Street, Kingston upon Thames, Surrey, KT1 1HN, UK Tel: +44 (0)20 8541 1999 | Fax: +44 (0)20 8549 9399 | info@lusas.com | www.lusas.com