Rail Track-Structure Interaction to UIC774-3

For LUSAS version:	20.0						
For software product(s):	LUSAS Bridge						
With product option(s):	Nonlinear, Rail Track						
Note: The example exceeds the limits of the LUSAS Teaching and Training Version.							

Description

This example examines the track-structure interaction between a braking train and a single span bridge. It considers the cases where the trainset is just about to enter the left-side side of the structure through to the front of the train being 90m beyond the right-hand side. It approximates (as far as the original test data allows) testcase E1-3 which can be found in Appendix D.1 of the UIC774-3 Code of Practice.



Objectives

The output requirements of the analysis are:

□ Maximum relative displacement between the track and the structure in the longitudinal direction (relative railbed displacement).

- Peak axial rail stresses.
- □ Peak longitudinal reactions at the abutments.

Keywords

UIC774-3, Track-Structure Interaction, TSI, Rail, Railbed

Associated Files

Associated files can be downloaded from the user area of the LUSAS website.



These two files are intended for copying to a project folder if a rail track model is to be defined from scratch.

□ **UIC_Template.xlsx** or **UIC_Template.xls** UIC774-3 Microsoft Excel input spreadsheet (unpopulated) for copying to a projects folder and using with this worked example.

These files below are also provided and are intended for copying to a projects folder if results processing only and not spreadsheet data input is of interest:

- □ UIC E1-3 Analysis.xlsx or UIC E1-3 Analysis.xls UIC774-3 Microsoft Excel input spreadsheet populated with data defined in this example. If used, continue at the section titled *Modelling / Running an Analysis*.
- □ UIC E4-6 Analysis.xlsx or UIC E4-6 Analysis.xls UIC774-3 Microsoft Excel input spreadsheet populated with data defined in this example. This is for use for a further investigation with the same model as built by the preceding spreadsheet.

Defining Model Data

The LUSAS Rail Track Analysis software option automatically builds LUSAS models suitable for track/structure interaction analysis. It does so from data defined in Microsoft Excel spreadsheets.

If you wish to build the model used in the worked example from a predefined populated spreadsheet continue at the section titled <u>Modelling / Running an Analysis</u>.

Otherwise, to see the processes involved in defining data to build a model from scratch:

- Ensure the supplied Microsoft Excel spreadsheet named UIC_Template.xlsx (use UIC_Template.xls if using an older version of Microsoft Excel) is present in a working projects folder where the track-structure interaction model is to be built.
- Rename the spreadsheet to **UIC E1-3 Analysis.xlsx** if using Microsoft Excel 2007 and above or rename to **UIC E1-3 Analysis.xls** if the other file was copied and you are using an older version of Microsoft Excel.

• Open the spreadsheet in Microsoft Excel.

The modelling spreadsheet contains six worksheets titled:

- Decks, Tracks and Embankment
- **Structure Definition**
- **Geometric Properties**
- Material Properties
- □ Interaction and Expansion Joint
- □ Loading



Note. Data should only be entered into the yellow regions of the Microsoft Excel spreadsheet to define the modelling and analysis requirements. Numeric values in the white cells are automatically populated according to data entered in other worksheets. These cells are protected from editing or user input. Data tips and other details relating to cells can often be seen by hovering over a cell.



Note. Whilst it is recommended that an unpopulated spreadsheet is used with this example, populated spreadsheets are also supplied for those not wishing to enter all details as listed or for use if any errors are encountered with user-input into the general spreadsheet that cannot easily be fixed. A spreadsheet compatible for an installed version of Microsoft Excel should be copied to the working folder where the track-structure interaction example model is to be created.

Defining Decks, Tracks and Embankment Lengths

- Pick the **Decks**, **Tracks and Embankment** worksheet.
- Enter 1 for the Number of Decks.
- Enter 1 for the Number of Tracks.

	Al 🔹 🔿 🏂 Decks, Tra	cks and Embankr	nent		×
	A	В	С	D	-
1	Decks, Tracks and Embankment	Units : m			
2		-			
3	Number of Decks	1			
4	Number of Tracks	1			
5	Left Embankment Length	300			
6	Left Embankment Ballast Type	1			
7	Right Embankment Length	300			
8	Right Embankment Ballast Type	1			
9	Length of Decks Only / Total Length (m)	60	660		
10					-
н -	Decks, Tracks and Embankment / Strue	turi 4	1	•	1

- The UIC774-3 Code of Practice specifies the embankment lengths for the test cases to be 300m. Enter **300** for both the **Left Embankment Length** and **Right Embankment Length**.
- Only a single ballast type will be defined for both the track-embankment-interaction and the track-structure-interaction in the model. Enter 1 for the ID number of the Left Embankment Ballast Type and the Right Embankment Ballast Type.

Note that the **Length of Decks Only** and **Total Length** cells are populated using data on this and another worksheet. These cells are protected on this worksheet.

Defining the Structure

• Pick the **Structure Definition** worksheet.

- The left abutment has a stiffness of 600000kN/m according to test case E1-3. Enter **600** for the **Spring Support for each Abutment/Pier** for the left end of the deck because the units for the worksheet entry are kN/mm.
- No bearing behaviour is modelled in the E1-3 test case so enter **R** for the **Bearing Springs on Top of each Pier** for the left end of the deck.
- The first and only span of the deck has a free support in the longitudinal direction and can be specified through either no restraint in the spring support for the abutment / pier or through no restraint in the bearing springs. For this example the condition has been modelled using no restraint in the bearing springs.
- Enter **R** for the **Spring Support for each Abutment/Pier** for the first span of the deck.
- Enter **F** for the **Bearing Springs on Top of each Pier** for the first span of the deck.
- Enter 60 for the Span Length.
- Enter 1 for the **Geometric Assignment**. This ID will match a geometric definition in the **Geometric Properties** worksheet covered next.
- Enter 1 for the Material Assignment. This ID will match a material definition in the Material Properties worksheet covered later.
- Enter 1 for the **Ballast Type**. This ID will match a ballast definition in the **Interaction and Expansion Joint** worksheet covered later.



Note. No data is input for the **Bearing Offset from End of Deck** entry as the bearings in the UIC774-3 E1-3 test case are at the extreme ends of the deck. UIC774-3 only considers the situation where the bearings are at the extreme end of the deck but this is not the situation in reality and location of the bearings away from the ends can significantly affect the behaviour of the track-structure-interaction. The Rail Track Analysis in LUSAS allows the bearings to be placed inboard of the deck end which is demonstrated in another worked example.

The worksheet should look like this:

	A1 A1												
-	A	В	С	D	E	F	G	Н	1	L	M	N	
1	Structure	e Definition	Units : Pie	r Height : r	n : Bearing	springs on	top of each	pier: kN/n	nm, Span L	ength : m			
2		,											
3			Spring Support for each Abutment /Pier	Pier Height	Pier Geo. Assign.	Pier Mat. Assign	Bearing Springs on Top of each Pier	Bearing Offset from End of Deck	Span Length	Geo. Assign.	Mat. Assign.	Ballast Type	
4		Left End	600				R						
5		Span 1	R				F		60	1	1	1	
6		Span 2											
7	_	Span 3					ļ						
8	×	Span 4											
9	ă	Span 5											
10		Span b											-
11		Span /											-
12		Span 8											-
1.4		Span 9 Number of Supports for the Deck / Length	2				2		co				-
14		Number of Supports for the Deck/ Length	- 2				- 2		00				
10		Shon 1											-
17		Span 2											-
18		Span 2 Snan 3											
19	2	Span 4											-
20	Š.	Span 5											F.
21	Ō	Span 6											
22		Span 7											
23		Span 8											
24		Span 9											
25		Number of Supports for the Deck / Length	0				0		0				
26		Left End											
27		Span 1								COLORAD CERTIFICATION OF COLORADO		COLORADO CONTRACTOR	
28		Span 2											-
14 -	I N N D	ecks, Tracks and Embankment 📃 Structure Definit	tion / Geo	metric Prop	ierties 🖉 I	vlaterial 🕕 🖣)	•



Note. If more spans were present in the deck or the structure consisted of multiple decks this information would be entered into this worksheet.

The UIC774-3 fundamental tests do not incorporate the modelling of piers as part of the structure, so these are not included in this example. LUSAS offers two methods of modelling piers when these need to be represented in the structure:

- □ The first method represents the pier through the equivalent stiffness, which should be entered into the **Spring Support for each Abutment/Pier** entry and is calculated in accordance with Clause 1.3.2.2 in the UIC774-3 Code of Practice.
- □ The second method physically includes the pier in the finite element model and requires additional data entry into the columns for the **Pier Height**, **Pier Geometric Assignment** and **Pier Material Assignment**.

For further details see the Rail Track Analysis User Manual.



Defining the Geometric Properties for the Structure

• Pick the **Geometric Properties** worksheet.

The first line of data should always be called **Rail** and contains the geometric properties for the rail track. All other lines define the geometric properties for the unique IDs used in the **Structure Definition** worksheet.

The details of the rail used in the UIC774-3 test cases are not provided so it has been assumed that the track is formed of two UIC 60 rails and for the purposes of this example the properties are obtained by doubling the values from the LUSAS section library to give the total value per track. Enter the following values for the rail track:

- Enter **0.01534126** for the area (A) in m^2 of the two rails of the track.
- Enter **6.07756E-5** for the second moment of inertia about the horizontal y-axis (**Iyy**) in m⁴.
- Enter **1.024324E-5** for the second moment of inertia about the vertical z-axis (**Izz**) in m⁴.
- Enter **4.42698E-6** for the torsional constant (**J**) in m⁴.
- Enter **8.43488E-3** for the shear area for the y-direction (Asy) in m².
- Enter **6.0307E-3** for the shear area for the z-direction (**Asz**) in m².
- Enter 0 for the **Eccentricity** in the rail in m.
- Enter Track with 2 UIC 60 Rails in the Description for the rails.



Note. The UIC774-3 Code of Practice assumes that a 2D analysis is performed where the longitudinal and vertical behaviours of the track and structure are of interest. The current rail track analysis also assumes a 2D analysis but for its solution it requires the features of an element type which is only available in 3D in LUSAS. The properties entered into the worksheet therefore require geometric properties for all freedoms of the 3D element and the lateral behaviour and torsion the properties for two rails have been assumed to be twice those of the single rail. This will be discussed further in the **Modelling Discussion** section that follows.

Some of the properties for the 2D bending behaviour of the deck are provided in Appendix D.1 of the code of practice. As for the track rails, while the analysis is 2D the elements used are 3D so dummy properties have been included for the lateral behaviour and torsion of the deck although these will not affect the results obtained. In the model it has therefore been assumed that these properties are equal to the values provided for the vertical behaviour. Enter the following values for the deck:

- Enter **1** for the ID in the first column to match the geometric assignment ID for the deck in the **Structure Definition** worksheet.
- Enter 6 for the **Depth of Section** in m.
- Select **Steel Deck** from the **Component Type** list. In the UIC774-3 E1-3 test case the deck section is primarily made from steel 'I' sections and the material properties (see next section) provided in the test case match this.
- Enter **0.74** for the area (**A**) in m².
- Enter 2.59 for the second moment of inertia about the horizontal y-axis (Iyy) in m⁴.
- Enter **2.59** for the second moment of inertia about the vertical z-axis (**Izz**) in m⁴.
- Enter **2.59** for the torsional constant (**J**) in m⁴.
- Enter **740** for the shear area for the y-direction (**Asy**) in m². The UIC774-3 test cases do not indicate whether shear deformations were included in the calculation of the target results, so these have been ignored by setting the shear area to 1000*A in accordance with the *Element Reference Manual*.
- Enter **740** for the shear area for the z-direction (**Asz**) in m².
- Enter 1.21 for the Eccentricity in the deck in m. The UIC774-3 test cases assume that the track is at the top surface of the section and the neutral axis ordinate specified is from the base of the section. The depth of the section is 6m and the neutral axis ordinate is 4.79m giving an eccentricity of 6 4.79 = 1.21m.
- Enter **Deck Cross-Section** in the **Description** for the deck.

Modelling Discussion

While the UIC774-3 Code of Practice treats the track-structure interaction as a 2D problem the rail track analysis software uses 3D thick beam elements for the modelling of this problem but restrains the out of plane behaviour thus reducing it back to an equivalent 2D analysis. In the definition of the geometric properties for the track rails and structure the rail track analysis software therefore requires all of the 3D geometric properties to be defined for the worksheet. The properties entered for I_{zz} , J and A_{sy} will be used in the analysis, but these will not affect the results. They should however be set to similar magnitudes to the properties in I_{yy} and A_{sz} which are used for the bending deflection and shear deflection in the geometric properties to avoid mechanisms.

The properties for a single UIC 60 rail were taken from the LUSAS KS Rails section library. Since only the vertical bending of the track is considered the combined geometric section properties for the two rails of the track can be calculated by doubling the values for the single rail. These combined values are the ones entered into the **Rail** properties section of the Geometric Properties worksheet



Note. The doubling of the I_{zz} , J and A_{sy} properties could be considered to be inappropriate but since these properties are not used in the effective 2D analysis their doubling is considered acceptable.

	A1	f_{x}	Material f	Material Properties						
	A	В	С	D	E	F	G			
1	Material Pro	perties	Units : N, n							
2										
3			E	v	ρ	æ	Description			
4		Rail	210000	0.3	0	1.20E-05	Rails			
5		1	210000	0.3	0	1.00E-05	Deck			
6										
7								- 11		
8								- 84		
9								-88		
10								_		
	↔ → I / Geon	netric Prope	arties Ma	terial Prop	erties 🖉 I	i Interaction ar	nd Expanii 4			
Dee			1							

Defining the Material Properties for the Structure

• Pick the Material Properties worksheet.

The first line of data should always be called **Rail** and contains the material properties for the rail track. All other lines define the material properties for the unique IDs used in the **Structure Definition** worksheet.

Enter the following values for the rail:

- Enter **210000** for the Young's modulus (E) in N/mm² which is equivalent to a value of 210 GPa.
- Enter **0.3** for the Poisson's ratio (**v**).

- Enter 0 for the mass density (ρ) . Setting this to the representative value allows the self-weight deflections to be calculated for the structure and track system if they are required but it is not used for the track-structure interaction analysis.
- Enter **1.20E-5** for the coefficient of thermal expansion (α) see note below.
- Enter **Rails** in the **Description** for the rails.

Enter the following values for the deck:

- Enter 1 for the ID in the first column to match the material assignment ID for the deck in the **Structure Definition** worksheet.
- Enter **210000** for the Young's modulus (**E**) in N/mm².
- Enter **0.3** for the Poisson's ratio (**v**).
- Enter **0** for the mass density (**ρ**).
- Enter **1.0E-5** for the coefficient of thermal expansion (α).
- Enter **Deck** in the **Description** for the material properties.



Note. The documentation accompanying the UIC774-3 test cases does not mention the exact material properties that were used for the rail track in the target solutions and also does not mention the Poisson's ratio or coefficient of thermal expansion used for the track / deck. The Poisson's ratio has therefore been assumed to be identical for both and the coefficient of thermal expansion used for the deck is identical to the value mentioned in Example 1 in Appendix C.1 of the UIC774-3 Code of Practice and mentioned elsewhere within the Code of Practice.

From the temperature behaviour of a restrained bar, it can, however, be back calculated that the coefficient of thermal expansion for the track was 1.2E-5 to obtain a target compressive stress of 126 MPa in the track alone under thermal loading. To replicate the exact test case the example has therefore used this coefficient of thermal expansion and accurate UIC60 track properties.

Defining the Track-Structure Interaction and Expansion Joint Properties for the Structure



- Pick the Interaction and Expansion Joint worksheet.
- Enter 0 for the eccentricity between the rail and slab as the UIC774-3 test cases in Appendix D.1 are assumed to have their centre of gravity coincident with the top of the reinforced concrete slab of the deck.
- Enter **0.5** for the Parametric Distance of Interaction Joint from Rail. For modelling with no eccentricity between the rail and the slab this parameter is not used but they are placed halfway between the rail and slab by default for eccentric track if entry is blank.



Note. The UIC774-3 test cases assume that the track is ballasted without specifying the exact interaction properties that are to be used. It is therefore assumed that the value of u_0 in the test cases is equal to 2mm which is the representative value for a sleeper in ballast (as opposed to 'frozen' ballast track) indicated in Clause 1.2.1.2.

Enter the following values for the longitudinal bilinear spring characteristics for **Ballast Type ID 1** – (Only ballast type ID 1 has been assigned in the **Decks, Tracks and Embankment** and the **Structure Definition** worksheets):

- Enter **10** for the **Unloaded Elastic Spring Stiffness** in the longitudinal direction in kN/m/mm. The resistance parameter for the unloaded track is 20kN/m in the test and this gives a stiffness of 20kN/m / 2mm = 10kN/m/mm (see note above).
- Enter 20 for the Unloaded Yield Force in the longitudinal direction in kN/m.
- Enter **1.0E-6** for the **Unloaded Hardening Stiffness** in the longitudinal direction in kN/m/mm.
- Enter **30** for the **Loaded Elastic Spring Stiffness** in the longitudinal direction in kN/m/mm. The resistance parameter for the unloaded track is 60 kN/m in the test and this gives a stiffness of 60kN/m / 2mm = 30 kN/m/mm (see note above).
- Enter 60 for the Loaded Yield Force in the longitudinal direction in kN/m.
- Enter **1.0E-6** for the **Loaded Hardening Stiffness** in the longitudinal direction in kN/m/mm.



Note. The interaction springs are modelled using nonlinear joints with elasticperfectly plastic behaviour in the longitudinal direction. This is achieved using the elasto-plastic uniform tension and compression material. The hardening stiffness should always be set to a very small value to avoid numerical instabilities.

• Ensure that there is no data specified in the **Rail Expansion Joints** region of the worksheet.

	A1 • 6 fx Loading												
	A	В	С	D	E	F	G	Н		J			
1	Loading	Units : Temperature : Ce	lsius , Load F	osition/Leng	h : m , Load	: kN/m							
2													
3			Amount										
4		Concrete Deck											
5	Temperature Loads	Steel Deck	35										
6		User Deck	50										
1		Rails	50										
8													
9		Num	hor of Train L	anding Group	o to Analyca	1							
11		Num	Der of Train L	bauing Group	s to Analyse								
12											<u> </u>		
13				Train Lo	ading Group:	1							
14													
		Number of Track									Num		
15		Loading Locations	16								Loac		
16		Loading Type	Track Selection to be Loaded	Parametric Starting Position for Loadings	Parametric End Position for Loadings	Amount (per unit length)	Loaded Length	Starting Location of Loading for First Analysis	Finishing Location of Loading for Last Analysis	Location Increment for each Analysis			
17		Braking	1	0	300	20	300	0	150	10			
18		Vertical	1	0	300	80	300	0	150	10	· · · · · · · · · · · · · · · · · · ·		
19													
20											• •••••		
21											•		
23	Train Loads												
24													
25											-		
H.	🕩 🕨 📈 Material Prope	rties 📈 Interaction and	Expansion Joir	nt Loadir	ig / 🞾 🖊	I 4 I							

Defining the Trainset Loading for the Structure

- Pick the **Loading** worksheet.
- Enter 35 for the **Temperature** variation of the **Steel Deck** in °C (to match the **Component Type** in the **Geometric Properties** worksheet).
- Enter **50** for the **Temperature** variation of the **Rails** in °C.



Note. If both steel and concrete deck constructions were present within the structure, then these component types would be specified in the **Geometric Properties** worksheet and any appropriate temperature variations can then be specified and applied using the input for each component type.

For the UIC774-3 E1-3 test case the single 300m long trainset travels from the lefthand abutment of the 60m long deck to 90m past the right-hand abutment of the deck, a total distance of 150m. For the example this trainset passage will be broken up into 10m increments.



- Enter 1 for the Number of Train Loading Groups to Analyse as only the single Train Loading Group is being considered. A Train Loading Group can consist of different trainsets on each track (usually one braking and one accelerating for a two-track structure) and the Rail Track Analysis tool can analyse different trainsets / movements of trainsets within multiple Train Loading Groups in the same analysis see another worked example.
- In the first Train Loading Group, enter 16 for the Number of Track Loading Locations based on the formula Number of track loading locations = (Travel / Increment) + 1 giving (150 / 10) + 1 = 16.
- Enter **Braking** for the **Loading Type** in the first row of loading.
- Enter 1 in the **Track Selection to be Loaded** since there is only a single track in the analysis.
- Enter **0** for the **Parametric Starting Position for Loadings** (in m) to indicate the left-hand limit of the trainset loading.
- Enter **300** for the **Parametric End Position for Loadings** (in m) to indicate the right-hand limit of the trainset loading. The train is 300m long in the test case.
- Enter **20** for the **Amount (per unit length)** to apply 20kN/m horizontal braking forces acting to the right for the trainset moving from left to right.
- Enter 0 for the **Starting Location of Loading for First Analysis** to place the trainset in a location where it is just about to enter the deck structure for the first analysis, recalling that the left-hand embankment is 300m long.
- Enter **150** for the **Finishing Location of Loading for Last Analysis** to place the right-hand extent of the trainset 90m past the 60m deck span for the last analysis.
- Enter Vertical for the Loading Type in the second row of loading.
- Enter 1 in the **Track Selection to be Loaded** since there is only a single track in the analysis.
- Enter **0** for the **Parametric Starting Position for Loadings** (in m) to indicate the left-hand limit of the trainset loading.
- Enter **300** for the **Parametric End Position for Loadings** (in m) to indicate the right-hand limit of the trainset loading. The train is 300m long in the test case.
- Enter **80** for the **Amount (per unit length)** to apply 80 kN/m vertically downwards for the trainset.
- Enter 0 for the **Starting Location of Loading for First Analysis** to place the trainset in a location where it is just about to enter the deck structure for the first analysis, recalling that the left-hand embankment is 300m long.

- Enter **150** for the **Finishing Location of Loading for Last Analysis** to place the right-hand extent of the trainset 90m past the 60m deck span for the last analysis.
- Save the spreadsheet and close the Microsoft Excel application.



Note. The horizontal and vertical loading of the trainset in the test cases have identical configurations. More complex trainset loading configurations and acceleration loading can be also specified (see the *Rail Track Analysis User Manual* for more information).

Modelling / Running an Analysis

All of the model construction and analysis is automatically performed by the Rail Track Analysis software option but, to do so, a blank LUSAS model must be initially created or a suitable existing LUSAS model (that was created by the Rail Track Analysis option) must be opened.

Running LUSAS Modeller

For details of how to run LUSAS Modeller, see the heading *Running LUSAS Modeller* in the *Introduction to LUSAS Worked Examples* document.

Creating a Temperature-only Model

An initial temperature-only analysis can form the basis for carrying out more than one track-structure interaction analysis with different trainset loading configurations being used. For large analyses time savings can result from not having to re-run a temperature analysis for each trainset loading.

- Enter **UIC774_testcase** for the model's name.
- Select an analysis catgory of **3D** and click **OK**.

This model is created solely to allow the Rail Track Analysis option to be selected. It is not used after the option has been run.

- Enter a model filename of **E1-3_TemperatureOnly**
- Enter the filename of the Microsoft Excel spreadsheet you created for the model building and analysis (e.g. UIC E1-3 Analysis.xlsx) or browse for it using the Browse... button in the Microsoft Excel spreadsheet or

UIC774-3 Model Builder									
Model filename	E1-3_TemperatureOnly								
Microsoft Excel spreadsheet or	C:\Users\Projects\UIC E1-3 Analysis.xlsx Browse								
Datch text file NOTE: LUSAS model will be built and run in the current working directory									
Current working directory: C:\Users\geoff\Documents\Lusas200\Projects									
Element size 2									
Apply temperature and rail loa	ds in same analysis								
Vait for solution									
	OK Cancel Help								

batch text file input. If the full folder information is not entered it will be assumed

New...

File

Bridge

Rail Track Analysis

Build Model..

>

UIC774-3

that the Microsoft Excel spreadsheet is in the current working folder which is reported in the dialog.

If wanting to build the model from a supplied spreadsheet, select the file **UIC E1-3 Analysis.xlsx** that was downloaded and placed in a folder of your choosing.

- Ensure an Element size of **2** is specified which will create elements of a maximum length of 2m in the LUSAS model.
- Ensure that the **Apply temperature and rail loads in same analysis** option is <u>not</u> selected.
- Ensure the Wait for solution option is selected and click the OK button.

Assuming that there have been no errors in the input for the Microsoft Excel spreadsheet the Rail Track Analysis software option will automatically generate a LUSAS model (shown below) from the spreadsheet data and run a rail track analysis for temperature-only loading.



If the Rail Track Analysis software option detected errors with modelling data these will be reported and must be corrected prior to re-running the Rail Track Analysis option.



Note. If the intention was to only perform this analysis and investigate the thermal effects, then post-processing could be performed on the results of the analysis. In addition, if the **Apply temperature and rail loads in same analysis** option was selected the combined temperature and rail track loading results would now be available. For this example, we will however be using this temperature only analysis as a starting point for more than one track-structure interaction analysis so no post-processing will be performed at this stage.

Applying Trainset Rail Loading to the Temperature Model

The temperature only model will now be used as the starting point for the application of the trainset rail loading that needs to be considered for the track-structure interaction analysis.

Bridge Rail Track Analysis UIC774-3 > Apply Rail Loads... • Select the **Apply train loads to current model** option as we have just performed the temperature only analysis and will use this model as the base model for the application of the trainset rail loading. If this option is not selected the original temperature only

UIC774-3 Apply Rail Loads	×
Apply train loads to current n	nodel
Original model filename	Browse
Rail load model filename	E1-3_TemperatureAndRailLoads
Rail load Microsoft Excel spreadsheet or batch text file	C:\Users\Projects\UIC E1-3 Analysis.xlsx Browse
✓ Wait for solution	
	OK Cancel Help

analysis model name would need to be supplied.

- Enter E1-3_TemperatureAndRailLoads as the Rail load model filename.
- Enter the **UIC E1-3 Analysis.xlsx** (or UIC E1-3 Analysis.xls) filename of the Microsoft Excel spreadsheet created for the analysis or browse for it using the **Browse...** button in the **Microsoft Excel spreadsheet or batch text file** input. If the full folder information is not entered it will be assumed that the Microsoft Excel spreadsheet is in the current working folder.
- If wanting to apply train loads from a supplied spreadsheet, select the file **UIC E1-3 Analysis.xlsx** that was downloaded and placed in a folder of your choosing.
- Ensure the **Wait for solution** option is selected.
- Click the **OK** button and choose **No** to saving the changes to the current model as no manual changes have been made.

Assuming that there have been no errors in the trainset loading input for the Microsoft Excel spreadsheet the Rail Track Analysis software option will now automatically generate a LUSAS model with a separate analysis for each train position being considered (16 in total) and run a track-structure analysis for the combined temperature and trainset rail loading using the trainset loading information defined in the spreadsheet.

Note. If both the temperature and trainset rail loads were applied to the original model the software would detect this and report that the original model is not a valid temperature-only model. If this were to happen, repeat the model building process above before reattempting to apply the trainset rail loading to the analysis.

If errors were detected...

If errors were detected with the modelling data, or the post-processing in the next section gives different results, the values in the spreadsheet should be corrected before re-selecting the previous Rail Track Analysis menu item. If it proves impossible for you to correct the errors reported a populated spreadsheet file is provided to enable you to create the model and run an analysis successfully. You may download this file from the user area of the LUSAS website.



□ UIC E1-3 Analysis.xlsx (.xls) is a populated spreadsheet containing all input data for the example.

A spreadsheet compatible for an installed version of Microsoft Excel should be copied to the working project folder where the track-structure interaction example model is to be created, and the **Bridge > Rail Track Analysis UIC774-3 > Apply Rail Loads** menu item re-selected.

Viewing the Results

If the analyses were run from within LUSAS Modeller with the 'Wait for solution' option set, the results for each train position analysis considered will be added to the Treeview.

Automatic Extraction of Results into Microsoft Excel

The Rail Track Analysis option provides a post-processing tool that automatically extracts the results of the analyses into tabular form in Microsoft Excel and generates commonly required graphs and tables of quantities that can be compared against prescribed limits for the track-structure interaction.

Bridge	UIC774-3 Post Processor	×
Rail Track Analysis UIC774-3 > Extract Results to Excel	Filename E1-3_PostProcess Working folder © Current © User defined	
	Save in C:\Users\geoff\Documents\Lusas200\Projects Brc Dutrut control	owse
	Included model extent: All tracks : All Train Loading Groups : All track length Image: Constant of the second se	odify
	WARNING: Do not perform any Copy & Paste actions during the post-processing as this could lead to incorrect extraction and proces the results by Microsoft Excel Defaults OK Cancel	sing of Help

- Enter E1-3_PostProcess for the Filename. Note that no *.xlsx or *.xls extension is required.
- Ensure the **Working folder** is set to **Current** to place the post-processing Microsoft Excel spreadsheet into the same folder as the analyses.

• Ensure the **Output Control** is reporting that "All tracks : All Train Loading Groups : All track length" are included in the model extent.

For a new model being post-processed for the first time this should always be the case. If previous selective post-processing has been carried out on the model, and the model saved, that choice will have been stored for use again by the post-processor. The included model extent must be updated by clicking the **Modify** button and revising the selection. Clicking the **Defaults** button in the **Modify Included Output** dialog will return the included model extent to "All tracks : All Train Loading Groups : All track length" if needed.

- Ensure the **Output Control** is reporting that the **Generate envelopes and peak** result tables in Microsoft Excel when processing groups option is selected.
- Ensure the **Output Control** is reporting that the **Generate charts in Microsoft Excel** option is selected.

If previous customised post-processing has been carried out on the model and the model saved the choice of charts created may have been changed from the defaults and will have been stored for use again by the post-processor. The choice of charts created must be updated by clicking the **Options** button and the included charts revised. Clicking the **Defaults** button in the **Chart Options** dialog will return the chart options to the defaults.

Prior to clicking the OK button please note the following cautions:



Caution. You should not have any other Microsoft Excel windows open while the post-processing is carried out. Starting Microsoft Excel or opening another Microsoft Excel spreadsheet while the post-processing is running will break the connection between Modeller and Microsoft Excel resulting in an error and termination of the post-processing.



Caution. Do not carry out any Copy or Paste actions <u>in any application</u> whilst results are being extracted during the post-processing process as this could lead to incorrect extraction and processing of the results by Microsoft Excel.

• Click the **OK** button.

The automatic Rail Track Analysis post-processor will now extract the results from the loaded analysis results and generate the Microsoft Excel spreadsheet in the working folder.



Note. An estimate of the time to complete the post-processing for each worksheet can be obtained by watching the progress bar at the bottom of the Modeller window. Post-processing of all the results will occupy the LUSAS licence for this time.

• Open the spreadsheet E1-3_PostProcess in Microsoft Excel.

Since the creation of envelopes was specified earlier the results spreadsheet will contain seven worksheets that contain the results from the analyses. Note that some versions of Excel may only show the tabs for the last created worksheets and hide the previous worksheets. If this is the case, other worksheets can be seen by pressing the 'back' arrow at the bottom of the worksheet window.

The worksheets created are titled:

- □ Track 1
- **Decks**
- **Envelope Track 1**
- **Envelope** Decks
- **Railbed Check**
- □ Longitudinal Reactions Check
- Rail Stresses Check

Peak Relative Railbed Displacement

For a continuously welded rail (CWR) track the typical criteria to be met for the relative railbed displacements is quoted in Clause 1.5.3 of UIC774-3 which states that:

"The maximum permissible displacement between rail and deck or embankment under braking and/or acceleration forces is 4 mm"

To permit checking of this criteria railbed displacements are included in the **Track 1** worksheet which reports all of the relative railbed displacements calculated for the track-structure interaction model.

• Click on the **Track 1** worksheet tab.

Maximum and minimum values are reported in the summaries at the top of the sets of results, values over the structure are graphed in the top chart, and individual values along the length of the track are reported in tabular form – as shown below.



Since the option to create envelopes in Microsoft Excel was chosen when the postprocessor was run the spreadsheet includes additional post-processing of the relative railbed displacement in the form of envelopes and a table of peak values for each trainset position.

For the envelopes worksheet the output is identical to the tabular and chart output for the individual results in the analyses. Six envelopes are generated by the postprocessor, namely:

- **Envelope Temperature Only (Max)**
- **Envelope Temperature Only (Min)**
- **D** Envelope Temperature and Train (Max)
- **D** Envelope Temperature and Train (Min)
- **Envelope All Configurations (Max)**
- **Envelope All Configurations (Min)**



Note. The **All Configurations** envelope provides an envelope over all loading configurations that are present in the analysis which in this case is temperature only and combined temperature and train loading. If valid basic combinations were also present an additional maximum / minimum envelope would be presented for these results and the results from these basic combinations would also be included within the **All Configurations** envelope.

Concentrating on the envelopes for the combination of the temperature and trainset loading, these are illustrated in the following figure.



• Click on the **Envelope** - **Track 1** worksheet tab.

Zooming into the summary tables at the top of the columns of results and charts (see images that follow) allows the extraction of the peak relative railbed displacements of +0.00343 m movement of the track to the right relative to the base of the ballast over the deck, +0.00675 m movement of the track to the right relative to the base of the ballast over the whole track length and -0.01747 m movement of the track to the left relative to the base of the ballast over the whole track length and deck.

	Æ	AF	AG	AH	AI	AJ	AK	AL	AM	AN	AO
1											
2											
3	Model	Filename:	E1-3_TemperatureAndRailLoads.mdl								
4	Model	Directory:	C:\Projects\Example\								
5	м	odel Date:	25/04/2019								
6	Mo	del Units:	N,m,kg,s,C								
7											
8	Envelope	- Tempera	ture and Train (Max)								
9					Maxi	mum			Mini	mum	
10				Value	Element	Node	Dist (m)	Value	Element	Node	Dist (m)
10 11			Disp X (m)	Value 0.01064295	Element	Node 334	Dist (m) 328	Value 0	Element	Node 5	Dist (m) 0
10 11 12			Disp X (m) Disp Y (m)	Value 0.01064295 0.00106426	Element	Node 334 332	Dist (m) 328 326	Value 0 -0.00008	Element	Node 5 163	Dist (m) 0 158
10 11 12 13			Disp X (m) Disp Y (m) Rot RZ (rad)	Value 0.01064295 0.00106426 0.00140170	Element	Node 334 332 364	Dist (m) 328 326 358	Value 0 -0.00008 -7.827E-07	Element	Node 5 163 332	Dist (m) 0 158 326
10 11 12 13 14			Disp X (m) Disp Y (m) Rot R2 (rad) Rel. Disp of Railbed over Decks (m)	Value 0.01064295 0.00106426 0.00140170 0.00343076	Element	Node 334 332 364 306	Dist (m) 328 326 358 300	Value 0 -0.00008 -7.827E-07 -0.016551	Element	Node 5 163 332 366	Dist (m) 0 158 326 360
10 11 12 13 14 15			Disp X (m) Disp Y (m) Rot RZ (rad) Rel. Disp of Railbed over Decks (m) Rel. Disp of Railbed whole Track (m)	Value 0.01064295 0.00106426 0.00140170 0.00343076 0.00674795	Element	Node 334 332 364 306 366	Dist (m) 328 326 358 300 360	Value 0 -0.00008 -7.827E-07 -0.016551 -0.016551	Element	Node 5 163 332 366 366	Dist (m) 0 158 326 360 360
10 11 12 13 14 15 16			Disp X (m) Disp Y (m) Rot RZ (rad) Rel. Disp of Railbed over Decks (m) Rel. Disp of Railbed whole Track (m) Fx (N)	Value 0.01064295 0.00106426 0.00140170 0.00343076 0.00674795 -866303.2	Element 304	Node 334 332 364 306 366 303	Dist (m) 328 326 358 300 360 298	Value 0 -0.00008 -7.827E-07 -0.016551 -0.016551 -2388322.7	Element 398	Node 5 163 332 366 366 366 366	Dist (m) 0 158 326 360 360 360
10 11 12 13 14 15 16 17			Disp X (m) Disp Y (m) Rot R2 (rad) Rel. Disp of Railbed over Decks (m) Rel. Disp of Railbed whole Track (m) Fx (N) Fr (N)	Value 0.01064295 0.00106426 0.00106426 0.00343076 0.00674795 -866303.2 8277.52791	Element	Node 334 332 364 306 366 303 364	Dist (m) 328 326 358 300 360 298 358	Value 0 -0.00008 -7.827E-07 -0.016551 -0.016551 -2388322.7 -1.3246197	Element 398 326	Node 5 163 332 366 366 366 319	Dist (m) 0 158 326 360 360 360 312
10 11 12 13 14 15 16 17 18			Disp X (m) Disp Y (m) Ret RZ (rad) Rel. Disp of Railbed over Decks (m) Fel. Disp of Railbed whole Track (m) Fx (N) Fz (N) My (Nm)	Value 0.01064295 0.00106426 0.00140170 0.00343076 0.00674795 -865303.2 8277.52791 5057.96072	Element 304 394 398	Node 334 332 364 306 366 303 364 366	Dist (m) 328 326 358 300 360 298 358 358 360	Value 0 -0.00008 -7.827E-07 -0.016551 -2388322.7 -1.3246197 -1.767E-13	Element	Node 5 163 332 366 366 366 319 201	Dist (m) 0 158 326 360 360 360 312 196

AT	AU	AV	AW	AX	AY	AZ	BA	BB	BC	BD	
Envelope	- Temperat	ture and Train (Min)									
				Maxi	mum		Minimum				
			Value	Element	Node	Dist (m)	Value	Element	Node	Dist (m)	
		Disp X (m)	0.00450569		343	336	0		5	0	
		Disp Y (m)	0		5	0	-0.02317		337	330	
		Rot RZ (rad)	8.685E-20		199	194	0.0010000	•	308	302	
		Rel. Disp of Railbed over Decks (m)	0.00060485		306	300	-0.0174726		366	360	
		Rel. Disp of Railbed whole Track (m)	0.0027513		366	360	-0.0174726		366	360	
		Fx (N)	-1589508.5	326	319	312	-2943585	398	366	360	
		Fz (N)	1.5559E-12	198	198	192	-8085.4214	398	366	360	
		My (Nm)	6 65069694	31/	310	304	-1440 2929	392	362	356	
		iaià (iain)	0.03000004	314	010	004	14012525			000	
	AT Envelope	AT AU	AT AU AV Envelope - Temperature and Train (Min) Envelope - Temperature and Train (Min) Disp X (m) Disp Y (m) Rel. Disp of Railbed over Decks (m) Rel. Disp of Railbed over Decks (m) Fr (N) Fr (N) May (Min)	AT AU AV AW Envelope - Temperature and Train (Min)	AT AU AV AW AX Envelope - Temperature and Train (Min)	AT AU AV AW AX AY Envelope - Temperature and Train (Min)	AT AU AV AW AX AY AZ Envelope - Temperature and Train (Min) Image: Constraint of the second secon	AT AU AV AW AX AY AZ BA Envelope - Temperature and Train (Min)	AT AU AV AW AX AY AZ BA BB Image: Ima	AT AU AV AW AX AY AZ BA BB BC Image: Image	

The peak relative railbed displacement is therefore -0.01747 m which compares well with the UIC774-3 E1-3 test case published result of -1.73E-2 m with a difference of +0.98%.

In addition to the envelope worksheet, the peak relative railbed displacement can also be found in the **Railbed Check** worksheet as shown below.

• Click on the **Railbed Check** worksheet tab.

This shows that the peak relative railbed displacement occurs when the braking trainset is placed at the 5^{th} position when the front of the 300 m long trainset is just over halfway across the 60 m deck. This is highlighted in bold blue text in the worksheet.

<u>Check of Longitudinal Relative Displacement of Railbed (Relative Displacement between Rails and Deck)</u>		
3 Job Title: UIC 774-3 Model: E1-3 TemperatureAndReilLoads		
4 Analysis Filename: E1.3.TemperatureAndRailLoads*Position 1 -> E1.3.TemperatureAndRailLoads*Position 16		
5 Model Directory: CVProject//Ecample		
6 Analysis Bate: 25/04/2019 → 25/04/2019		
7 Model Units: N.m.kg.s.C		
8		
9 Track 1		
Distance from Left End Distance from Left End Peak Relative	Distance from Left En	1
Analysis ID Results Filename Loading Type Starting During of the Model to the United Starting	Deals Disabarrantee of Structure for Peak	Description of peak
set up rostout of units internet in the cashe of the set of the se	Displacement (m)	location
10		
11 1 EL_3_TemperatureAndRailLoads*Position 1.mys Temperature Only 0.016503638	1 6	0 RH Abutment
12 1 EL_S_TemperatureAndRailLeads*Position 1.mys Braking 0 300 0.016550996	1 6	0 RH Abutment
13 2 E1_3_TemperatureAndRailLeads*Position 2.nys Braking 10 310 0.016837662	1 6	0 RH Abutment
14 B La_g_TemperatureAndRailLoads*Position 3.mys Braking 20 920 0.017203035	1 6	0 RH Abutment
15 Contraction of the contract on the contract		o fill Abutu at
16 5 EL_3_TemperatureAndRailLoads'Position S.mys Braking 40 340 0.017472607	1 0	0 RH Abutment
17 01123615	1	o kh Abdorienc
18 7 EL_3_TemperatureAndReilLoads*Position 7.mys Braking 60 360 0.016883199	1 6	0 RH Abutment
19 8 EL_3_TemperatureAndRailLeads*Position 8 mys 8 raking 70 870 0.01225313	1 6	0 RH Abutment
20 9 L1_3_TemperatureAndRailLaads*Position 9 mys Braking 80 360 0.017358581	1 1	0 RH Abutment
21 10 EL_S_TEMPERATURANDANILINAS**POSITION 10 Mys Braking 90 S90 ULIT/33008	1 1	U RH Abutment
22 11 II_3_TemperatureAndRailLaads'Position 11 mys Braking 100 400 0.017925405	1 1	0 RH Abutment
28 12 L1_3_TemperatureAndMailLaadS Mostton 12 m/s Braking 110 410 0.017819955	1 0	UKH ADUTMENT
24 13 IL_3_TemperatureIndRailLads'Position 13 m/s Braking 120 420 0.017317706	1 0	0 RH Abutment
20 14 L1_3_temperatureAndAsiLaadS*Position 14.m/s Braking 130 430 0.0171664	1 0	u Kri Abutment
20 20	1	u kn Aputment



Note. The peak relative railbed displacement in test case E1-3 is 0.01747 m or 17.47 mm which would be greater than the limit stated in Clause 1.5.3 of the UIC774-3 code of practice. All of the test cases in Appendix D.1 of the code of practice exceed this limit.

Peak Axial Rail Stresses

For a continuously welded rail track with UIC 60 rails the typical criteria to be met for the rail stress are quoted in Clause 1.5.2 of UIC774-3 which states that:

"The maximum permissible additional compressive rail stress is 72 N/mm²"

and

"The maximum permissible additional tensile rail stress is 92 N/mm²"

To permit checking of these criteria rail axial stress values are included in the **Track 1** Microsoft Excel worksheet.

• Click on the **Track 1** worksheet tab.

Maximum and minimum values are reported in the summaries at the top of the sets of results, values over the track length are graphed in the bottom chart, and the individual values along the length of the track are reported in tabular form – as highlighted in the following figure.

For the temperature-only loadcase (Increment 1) the maximum and minimum stresses observed in the rail track were -100.13MPa in compression and -154.97MPa in compression (lower graph). This most compressive value compares well with the value of -156.67MPa from the E1-3 test case (equal to -126MPa from the temperature in the rail and -30.67MPa from the temperature in the deck) with a percentage difference of -1.08%. For the temperature and trainset rail loading loadcase (Increment 2) for the first position of the train loading the maximum and minimum stresses observed in the rail track were -102.23MPa in compression and -155.68MPa in compression (lower graph), not to dissimilar to the temperature only results since the train loading is only just entering the bridge for this position.



Now, concentrating on the envelopes for the combination of the temperature and trainset loading to find the worst effects of all train loading positions:

• Click on the **Envelope - Track 1** worksheet tab.

Maximum and minimum stresses observed in the rail track were -56.47MPa in compression and -191.87MPa in compression. The value of -191.87MPa compares well with the UIC774-3 E1-3 test case published results of -182.4MPa to -190.07MPa with a difference of between 0.95% and 5.19% (depending upon the calculation method).

	AE	AF	AG	AH	Al	AJ	AK	AL	AM	AN	AO	
1												
2												
3	Model	Filename:	E1-3_TemperatureAndRailLoads.mdl									
4	Model	Directory:	C:\Projects\Example\									
5	M	odel Date:	25/04/2019									
6	Ma	del Units:	N, m, kg, s, C									
7												
8	Envelope	- Temperat	ture and Train (Max)									
9					Махі	mum		Minimum				
10				Value	Element	Node	Dist (m)	Value	Element	Node	Dist (m)	
11			Disp X (m)	0.01064295		334	328	0		5	0	
12			Disp Y (m)	0.00106426		332	326	-0.00008		163	158	
13			Rot RZ (rad)	0.00140178		364	358	-7.827E-07		332	326	
14			Rel. Disp of Railbed over Decks (m)	0.00343076		306	300	-0.016551		366	360	
15			Rel. Disp of Railbed whole Track (m)	0.00674795		366	360	-0.016551		366	360	
16			Fx (N)	-866303.2	304	303	298	-2388322.7	398	366	360	
17			Fz (N)	8277.52791	394	364	358	-1.3246197	326	319	312	
18			My (Nm) 👩	5057.96072	398	366	360	-1.767E-13	202	201	196	
19			Rail Stress (MPa)	-56.468843	304	303	298	-155.6797	398	366	360	

	AT	AU	AV	AW	AX	AY	AZ	BA	BB	BC	BD
1											
2											
З											
4											
5											
6											
7											
8	Envelope	- Tempera	ture and Train (Min)								
9					Maxi	mum			Mini	mum	
10				Value	Element	Node	Dist (m)	Value	Element	Node	Dist (m)
10 11			Disp X (m)	Value 0.00450569	Element	Node 343	Dist (m) 336	Value 0	Element	Node 5	Dist (m) 0
10 11 12			Disp X (m) Disp Y (m)	Value 0.00450569 0	Element	Node 343 5	Dist (m) 336 0	Value 0 -0.02317	Element	Node 5 337	Dist (m) 0 330
10 11 12 13			Disp X (m) Disp Y (m) Rot RZ (rad)	Value 0.00450569 0 8.685E-20	Element	Node 343 5 199	Dist (m) 336 0 194	Value 0 -0.02317 -0.0013208	Element	Node 5 337 308	Dist (m) 0 330 302
10 11 12 13 14			Disp X (m) Disp Y (m) Rot R2 (rad) Rel. Disp of Railbed over Decks (m)	Value 0.00450569 0 8.685E-20 0.00060485	Element	Node 343 5 199 306	Dist (m) 336 0 194 300	Value 0 -0.02317 -0.0013208 -0.0174726	Element	Node 5 337 308 366	Dist (m) 0 330 302 360
10 11 12 13 14 15			Disp X (m) Disp Y (m) Rot RZ (rad) Rel. Disp of Railbed over Decks (m) Rel. Disp of Railbed whole Track (m)	Value 0.00450569 0 8.685E-20 0.00060485 0.0027513	Element	Node 343 5 199 306 366	Dist (m) 336 0 194 300 360	Value 0 -0.02317 -0.0013208 -0.0174726 -0.0174726	Element	Node 5 337 308 366 366	Dist (m) 0 330 302 360 360
10 11 12 13 14 15 16			Disp X (m) Disp Y (m) Rot RZ (rad) Rel. Disp of Railbed over Decks (m) Rel. Disp of Railbed whole Track (m) Fx (N)	Value 0.00450569 0 8.685E-20 0.00060485 0.0027513 -1589508.5	Element 326	Node 343 5 199 306 366 319	Dist (m) 336 0 194 300 360 312	Value 0 -0.02317 -0.0013208 -0.0174726 -2943585	Element	Node 5 337 308 366 366 366 366	Dist (m) 0 330 302 360 360 360 360
10 11 12 13 14 15 16 17			Disp X (m) Disp Y (m) Rot R2 (rad) Rel. Disp of Railbed over Decks (m) Rel. Disp of Railbed whole Track (m) Fx (N) Fz (N)	Value 0.00450569 0 8.685E-20 0.00060485 0.0027513 -1589508.5 1.5559E-12	Element 326 198	Node 343 5 199 306 366 319 198	Dist (m) 336 0 194 300 360 312 192	Value 0 -0.02317 -0.0013208 -0.0174726 -0.0174726 -2943585 -8085.4214	Element 398 398	Node 5 337 308 366 366 366 366 366	Dist (m) 0 330 302 360 360 360 360 360
10 11 12 13 14 15 16 17 18			Disp X (m) Disp Y (m) Rot RZ (rad) Rel. Disp of Railbed over Decks (m) Fel. Disp of Railbed whole Track (m) Fx (N) Fz (N) My (Nm)	Value 0.00450569 0 8.685E-20 0.00060485 0.0027513 -1589508.5 1.5559E-12 6.65068684	Element 326 198 314	Node 343 5 199 306 366 319 198 310	Dist (m) 336 0 194 300 360 312 192 304	Value 0 -0.02317 -0.0013208 -0.0174726 -2943585 -8085.4214 1440.2929	Element	Node 5 337 308 366 366 366 366 366 366 362	Dist (m) 0 330 302 360 360 360 360 360 360 356

In addition to the envelope worksheet, the peak axial stresses in the rails can also be found in the **Rail Stresses Check** worksheet.

• Click on the **Rail Stresses Check** worksheet tab.

This worksheet shows that the peak most compressive axial stress of 191.87MPa occurs when the braking trainset is placed at the 9th position when the front of the 300m long trainset is 20m past the right-hand abutment side of the deck. The peak most tensile axial stress occurs at the 7th position. Both peaks are highlighted in bold blue text in the worksheet.

A	В	0	D	E	F	G	н	1	J	К	
1		Check of Axial Rail Stress									
2											
3	Job Title:	UIC 774-9 Model: E1-9 TemperatureAndRailLoads									
4	Analysis Filename:	E1 3 TemperatureAndRailLoads*Position 1> E1 3 TemperatureAndRailL	ads-Position 16								
5	Model Directory:	C\Projects\Example									
6	Analysis Date:	25/04/2019> 25/04/2019									
7	Model Units:	N,m,kg.s,C									
0											
9				Track 1							
10	ānalysis ID	Besults Filenance	Loading Type	Distance from Left End of the Model to the Starting Position of the Loading (m)	Distance from Left End of the Model to the Finishing Position of the Loading (m)	Peak Most Tensile Asial Stress of Rail (MPa)	Track Number with Peak Most Tensile Stress	Distance from Left End of Structure for Peak Most Tensile Stress (m)	Description of peak location	Peak Most Compressive Axial Stress of Rail (MPa)	T Pea
11	1	E1_3_TemperatureAndRailLoads=Position 1 mys	Temperature Only			-100 1257527	1	12	Within Deck 1	-154 9742044	
12	1	E1_3_TemperatureAndRailLoads*Position 1 mys	Braking	0	900	-102.2324235	1	12	Within Deck 1	-155.6796954	
19	2	E1_3_TemperatureAndRailLoads*Position 2 mys	braking	10	910	-103.4844307	1	6	Within Deck 1	-157.7774518	
14	3	E1_3_TemperatureAndRailLoads*Position 3 mys	Braking	20	320	-90.90988516	1	0	LH Abutment	-161.7865228	
15	4	E1_3_TemperatureAndRailLoads*Position 4.mys	Braking	30	390	-78.11942256	1	-2	LH Embankment	-166.9983607	
16	5	E1_3_TemperatureAndRailLoads*Position 5.mys	Braking	40	340	-67.08736253	1	-2	LH Embankment	-172.3095564	
17		Cl. 2. Temperature in d'aillea de Pealter Conye	2 milling		200	50 71550714			UI Contraction and	-177.1055101	
10	7	E1_3_TemperatureAndRailLoads=Position 7.mys	Braking	64	360	-56.46884276	1	-2	LH Enbankment	-101.3501432	-
19	7		and the second s							100 7/64443	-
20	,	E1_3_TemperatureAndRailLoads=Position 9.mys	Braking		380	-58.30649193	1	-2	LH Embankment	-191.873747	
21	10	sr"2"Lewberaunewickencosos-sosie eu 10 wéa	practing	×	350	-58.22724014		14	LH EMBARKMENC	-191 #522565	
22	11	£1_3_TemperatureAndRailLoads=Position 11.mys	Braking	100	400	-58.17855474	1	-2	LH Embankment	-191 1933324	
23	12	E1_3_TemperatureAndRailLoads*Position 12.mys	Braking	110	410	-58.15709833	1	-2	LH Embankment	-191.0792201	-
24	13	E1_3_TemperatureAndRailLoads*Position 13.mys	braking	120	420	-58.14548348	1	-2	LHEmbankment	-191.0334043	-
25	14	E1_3_TemperatureAndRailLoads=Position 14.mys	Braking	130	430	-58.14513314	1	-2	LH Embankment	-191.0155887	-
26	15	E1_3_TemperatureAndRailLoads*Position 15.mys	Braking	140	440	-58.14384446	1	-2	LH Embankment	-191.0087419	-
27	16	E1_3_TemperatureAndRailLoads*Position 16.mys	braking	150	I 450	-58.14334839	1	2	LHEmbankment	-191.0061217	1

Peak Longitudinal Reactions at the Abutments

The left-hand abutment provides all of the longitudinal restraint to the deck of the structure and the peak longitudinal reactions at this abutment are now investigated.

When post-processing, the option to create the envelopes in Microsoft Excel was chosen which caused an additional worksheet tabulating the peak longitudinal reactions for all of the analyses to be created.

• Click on the Longitudinal Reactions Check worksheet tab.

The first row shows a longitudinal reaction for the left-hand abutment under temperature only loading of 695.8kN. This compares well with the E1-3 test case published value of 700.12kN with a difference of -0.62%.

The worksheet also shows the longitudinal reactions for all of the train loading positions and indicates that the peak longitudinal reaction occurs when the braking trainset is placed at the 9th position (highlighted in bold blue text in the worksheet) when the front of the 300m long trainset is 20m past the right-hand abutment side of the deck. This trainset position gives a reaction of 929.1kN which compares well with the UIC774-3 E1-3 test case published result of 874.42kN with a difference of +6.25%.

A	В	с	D	E	F	G	н
1		Check of Longitudinal Reactions					
2	-						
3	Job Title	UIC 774-3 Model: E1-3 TemperatureAndRailLoads					
4	Analysis Filename	E1_3_TemperatureAndRailLoads*Position 1> E1_3_TemperatureAndRailLoads	"Position 16				
5	Model Directory	C\Projects\Example					
6	Analysis Date	25/04/2019> 25/04/2019					
7	Model Units	N,m,kg,s,C					
8							
9				Track 1			
				Distance from Left End	Distance from Left End		Abutment (Disc
	Analysis ID	Deculty Elisabete	Londles Tures	of the Model to the	of the Model to the	Peak Longitudinal	Abutment / Pier
	Anarysis ID	Results Filename	Loading Type	Starting Position of	Finishing Position of	Reaction (N)	Number with Peak
10	_			the Loading (m)	the Loading (m)		Reaction
11		E1_3_TemperatureAndRailLoads*Position 1.mys	Temperature Only			695795.7944	LH Abutment
12		ET_3_LemberatureworkenFoads. Losition 1 w/k	Braking	0	300	64/276.7736	LH ADUTMENT
13		E1_3_TemperatureAndRailLoads"Position 2.mys	Braking	10	310	634918.2367	LH Abutment
14		E1_3_TemperatureAndRailLoads*Position 3.mys	Braking	20	320	726055.4141	LH Abutment
15		E1_3_TemperatureAndRailLoads"Position 4.mys	Braking	30	330	823514.9025	LH Abutment
16		E1_3_TemperatureAndRailLoads*Position 5.mys	Braking	40	340	874241.0395	LH Abutment
17		E1_3_TemperatureAndRailLoads"Position 6.mys	Braking	50	350	860909.3369	LH Abutment
18		E1_3_TemperatureAndRailLoads"Position 7.mys	Braking	60	360	807346.0805	LH Abutment
19		E1_9_Temperature/indRoilLoads*Position 0-mys	Braking	70	070	982080.1657	Utilbutment
20		E1_3_TemperatureAndRailLoads~Position 9.mys	Braking	80	380	929089.9928	LH Abutment
21	-	E1_3_TEMPERATORATIONALCOADS POSITION 10.Mys	Braking	90	390	923839.8467	LH ADUCIMENC
22	1	E1_3_TemperatureAndRailLoads*Position 11.mys	Braking	100	400	920614.2933	LH Abutment
23	1	E1_3_TemperatureAndRailLoads"Position 12.mys	Braking	110	410	919192.8348	LH Abutment
24	1	E1_3_TemperatureAndRailLoads*Position 13.mys	Braking	120	420	918622.1261	LH Abutment
25	1	E1_3_TemperatureAndRailLoads*Position 14.mys	Braking	130	430	918400.2098	LH Abutment
26	1	E1_3_TemperatureAndRailLoads*Position 15.mys	Braking	140	440	918314.9418	LH Abutment
27	1	E1_3_TemperatureAndRailLoads"Position 16.mys	Braking	150	450	918282.3555	LH Abutment

• Close the Microsoft Excel application.

Alternative Analyses with Same Temperature Only Model

If further studies are required on the same structure for identical temperature conditions but with different trainset loading the Rail Track Analysis option can make use of the temperature only analysis from a previous analysis for a new one. For small structures the time saving from avoiding the reconstruction of an identical track-structure interaction model will generally not be significant but where the structure is very long and has many decks and spans this time saving can become significant.

Applying Alternative Trainset Rail Loading



UIC774-3 test case E4-6 (shown above) is very similar to the one for test case E1-3. The only difference between the two tests is the direction that the braking trainset is travelling. As a result, the temperature only model from test case E1-3 can and will be used as the starting point for the application of the alternative trainset rail loading that needs to be considered for the E4-6 track-structure interaction analysis.

Defining the Trainset Loading for the Structure

If you wish to use the predefined populated spreadsheet for this part of the example continue at the section entitled *Applying the Trainset Rail Loading to the Analysis*.

Otherwise:

- Copy the UIC E1-3 Analysis.xlsx (or UIC E1-3 Analysis.xls) Microsoft Excel spreadsheet created for the E1-3 test case and save it as a new Microsoft Excel spreadsheet with the filename UIC E4-6 Analysis.xlsx (or UIC E4-6 Analysis.xls).
- Open the spreadsheet in Microsoft Excel.



- Pick the **Loading** worksheet.
- Enter -20 in the Amount (per unit length) for the trainset braking loading to indicate that the braking load is now acting to the left for a trainset that is travelling from right to left.
- Enter 360 for the Starting Location of Loading for First Analysis of both the Braking and Vertical loading to place the trainset in a location where it is just

about to enter the deck structure for the first analysis, recalling that the left-hand embankment is 300m long and the deck is 60m long.

- Enter **210** for the **Finishing Location of Loading for Last Analysis** of both the **Braking** and **Vertical** loading to place the left-hand extent of the trainset 90m past the 60m deck span for the last analysis.
- Save the spreadsheet and close the Microsoft Excel application.

Applying the Trainset Rail Loading to the Analysis

The E1-3 temperature only model can now be specified along with the updated rail load spreadsheet containing the revised trainset loading for the Rail Track Analysis software option to carry out an analysis for this test case.

Ensure that the **Apply train loads to current model** option is <u>not</u> selected. The current model loaded is a combined temperature and trainset rail loads model for the E1-3 analysis and should not be used.

UIC774-3 Apply Rail Loads		×
Apply train loads to current m	odel	
Original model filename	E1-3_TemperatureOnly.mdl	Browse
Rail load model filename	E4-6_TemperatureAndRailLoads	
Rail load Microsoft Excel spreadsheet or batch text file	C:\Users\Projects\UIC E4-6 Analysis.xlsx	Browse
Wait for solution		
	OK Cancel	Help

- Enter E1-3_TemperatureOnly.mdl for the Original model filename which holds the temperature only analysis from the previous section or browse for it using the **Browse...** button. If the full folder is not specified, then it will be assumed that the model is in the current working folder.
- Enter E4-6_TemperatureAndRailLoads as the Rail load model filename.
- Enter the **UIC E4-6 Analysis.xlsx** (or **UIC E4-6 Analysis.xls**) filename of the Microsoft Excel spreadsheet created for the analysis or browse for it using the **Browse...** button in the **Microsoft Excel spreadsheet or batch text file** input. If the full folder information is not entered it will be assumed that the Microsoft Excel spreadsheet is in the current working folder.
- Ensure the **Wait for solution** option is selected.
- Click the **OK** button and choose **No** when asked to save the changes to the current model since there have been no manual changes to it.

Assuming that there have been no errors in the input for the Microsoft Excel spreadsheet the Rail Track Analysis software option will automatically generate a LUSAS model from the spreadsheet data and run a rail track analysis for the alternative trainset positions defined by the spreadsheet data.

Bridge Rail Track Analysis UIC774-3 > Apply Rail Loads...

If errors were detected...

If errors were detected with the modelling data or the post-processing in the next section gives different results the values in the spreadsheet should be corrected before re-selecting the previous Rail Track Analysis menu item. If it proves impossible for you to correct the errors reported a populated spreadsheet file is provided to enable you to create the model and run an analysis successfully.

1.00	

Bridge

Rail Track Analysis UIC774-3

UIC E4-6 Analysis.xlsx (.xls) is a populated spreadsheet containing all input data for this stage of the example.

A spreadsheet compatible for an installed version of version of Microsoft Excel should be copied to the working folder where the track-structure interaction example model is to be created, and the Bridge > Rail Track Analysis UIC774-3 > Apply Rail Loads menu item re-selected.

Automatic Extraction of Results into Microsoft Excel

ail Track Analysis C774-3 >	Filename E4-6_PostProcess	
Extract Results to Excel	Working folder © Current © User defined	-
	Save in C. Ausers georr Documents ALBas2004Projects Output control Included model extent: All tracks : All Train Loading Groups : All track length Image: Control Contrecontrol Control Control Control Control Control Contro	Modify
	WARNING: Do not perform any Copy & Paste actions during the post-processing as this could lead to incorrect extraction and pr the results by Microsoft Excel Defaults OK Cancel	ocessing of Help

- Enter **E4-6 PostProcess** for the Filename. ٠
- Ensure the Working folder is set to Current to place the post-processing • Microsoft Excel spreadsheet into the same folder as the analyses.
- Ensure the Output Control is reporting that "All tracks : All Train Loading Groups : All track length" are included in the model extent.
- Ensure the **Output Control** is reporting that the **Generate envelopes and peak** result tables in Microsoft Excel when processing groups option is selected.

• Ensure the **Output Control** is reporting that the **Generate charts in Microsoft Excel** option is selected.



Caution. As previously noted earlier in this example, prior to clicking the OK button ensure that no Excel applications are open and no copying and pasting of data in any application is done whilst the post-processing is carried out.

• Click the **OK** button and choose **No** when asked to save the changes to the current model since there have been no manual changes to it.

The automatic post-processor will now extract the results from the loaded analysis results and generate a new Microsoft Excel spreadsheet in the working folder.

- In your project folder, open the spreadsheet **E4-6_PostProcess.xlsx** in Microsoft Excel.
- If necessary, pressing the 'back' arrow at the bottom of the worksheet window to see all the worksheets created.

Peak Relative Railbed Displacement

A	В	c	D	E	F	G	н	1	J	K	L	-
1		Check of Longitudinal Relative Displacement of	Railbed (Relativ	e Displacement	t between Rail	s and Deck)						
2												
2	Job Tit	le: UIC 724-3 Model: E4-6 TemperatureAndBailLoads										
4	Anabula Ellanan	the Stephene State of the State	https://tion.16									
	Madel Directo	er. CAlifernia auf Al Decomental Locar 102 Decients	AS POSICION 20									
5	Anabaia Da	12/03/09/09/04/00/00/00/00/00/00/00/00/00/00/00/00/										
7	Model Uni	he. N m kn s C										
0		an mining as										
9				Track 1								
						Peak Relative						
10	Analysis ID	Results Filename	Loading Type	Distance from Left End of the Model to the Starting Position of the Loading (m)	Distance from Left End of the Model to the Finishing Position of the Loading (m)	Longitudinal Displacement between Rail and Slab (m)	Track Number with Peak Displacement	Distance from Left End of Structure for Peak Displacement (m)	Description of peak location			
11		1 64 6 TemperatureAndRailLoads"Position 1.mys	Temperature Only			0.016503638	1	60	RH Abutment			
12		1 64 6 TemperatureAndRailLoads"Position 1.mys	Braking	360	660	0.016966656	1	60	RH Abutment			
13		2 E4_6_TemperatureAndRailLoads*Position 2.mys	Braking	350	650	0.016943296	1	60	RH Abutment			
14		3 E4_6_TemperatureAndRailLoads"Position 3.mys	Braking	340	640	0.016955869	1	60	RH Abutment			
15		4 E4_6_TemperatureAndRailLoads"Position 4.mys	Braking	330	630	0.017039662	1	60	RH Abutment			1
16		5 E4_6_TemperatureAndRailLoads"Position 5.mys	Braking	320	620	0.01718389	1	60	RH Abutment			
17		6 E4_6_TemperatureAndRailLoads*Position 6.mys	Braking	310	610	0.017314468	1	60	RH Abutment			
18		7 64_6_TemperatureAndRailLoads"Position 7.mys	Braking	300	600	0.017256511	1	60	RH Abutment			
19		8 64_6_TemperatureAndRailLoads*Position 8.mys	Braking	290	590	0.017156105	1	60	RH Abutment			
20		9 64_6_TemperatureAndRailLoads*Position 9.mys	Braking	280	580	0.017135178	1	60	RH Abutment			
21		10 E4_6_TemperatureAndRailLoads*Position 10.mys	Braking	270	570	0.01712915	1	60	RH Abutment			
22		11 64_6_TemperatureAndRailLoads"Position 11.mys	Braking	260	560	0.017127127	1	60	RH Abutment			
23		12 64_6_TemperatureAndRailLoads"Position 12.mys	Braking	250	550	0.017126395	1	60	RH Abutment			
24		13 E4_6_TemperatureAndRailLoads"Position 13.mys	Braking	240	540	0.017126121	1	60	RH Abutment			
25		14 E4_6_TemperatureAndRailLoads*Position 14.mys	Braking	230	530	0.017126018	1	60	RH Abutment			
26		15 64_6_TemperatureAndRailLoads*Position 15.mys	Braking	220	520	0.017125979	1	60	RH Abutment			
27		16 E4_6_TemperatureAndRailLoads*Position 16.mys	Braking	210	510	0.017125964	1	60	RH Abutment			
28												
29												
30												
31												
32												
33												
54												-1
23												-1
30										_		
IA A P N To	ack 1 / Decks / Envel	ope - Track 1 / Envelope - Decks Railbed Check / Longitudinal Reactions Check	/ Rail Stresses Check /							÷	_	

• Click on the **Railbed Check** worksheet tab.

From this worksheet the peak relative railbed displacement is shown to be 0.01731m when the braking trainset is placed at the 6th position where it is 10 m from the left-hand abutment of the deck. This peak relative railbed displacement compares well with the UIC774-3 E4-6 test case published result of 1.78E-2 m with a difference of -2.75%.

Peak Axial Rail Stresses

• Click on the Rail Stresses Check worksheet tab.

A	B	c	D	E	F	G	н	1	1	K
3	Job Title:	UIC 774-3 Model: E4-6_TemperatureAndRailLoads								
4	Analysis Filename:	E4_6_TemperatureAndRailLoads"Position 1->E4_6_TemperatureAndRailL	oads"Position 16							
5	Model Directory:	C:\Users\paul_b\Documents\Lusas190\Projects								
6	Analysis Date:	13/02/2020> 13/02/2020								
7	Model Units:	N,m,kg,s,C								
8										
9				Track 1						
10	Analysis ID	Results Filename	Loading Type	Distance from Left End of the Model to the Starting Position of the Loading (m)	Distance from Left End of the Model to the Finishing Position of the Loading (m)	Peak Most Tensile Axial Stress of Rail (MPa)	Track Number with Peak Most Tensile Stress	Distance from Left End of Structure for Peak Most Tensile Stress (m)	Description of peak location	Peak Most Compressive Axial Stress of Rail (MPa)
11	1	E4_6_TemperatureAndRailLoads"Position 1.mys	Temperature Only			-100.1257527		1 12	Within Deck 1	-154.9742044
12	1	E4_6_TemperatureAndRailLoads"Position 1.mys	Braking	360	660	-101.3885546		1 12	Within Deck 1	-157.4084021
13	2	E4_6_TemperatureAndRailLoads"Position 2.mys	Braking	350	650	-101.9662701		10	Within Deck 1	-154.6567528
14	3	E4_6_TemperatureAndRailLoads"Position 3.mys	Braking	340	640	-101.9964012		10	Within Deck 1	-154.7082981
15	4	E4_6_TemperatureAndRailLoads"Position 4.mys	Braking	330	630	-100.6591995	1.	8	Within Deck 1	-157.4690882
16	5	E4_6_TemperatureAndRailLoads"Position 5.mys	Braking	320	620	-97.71739788		1 6	Within Deck 1	-161.388184
17	6	E4_6_TemperatureAndRailLoads=Position 6.mys	Braking	310	610	-94.74874128		4	Within Deck 1	-164.5527583
18	7	E4_6_TemperatureAndRailLoads"Position 7.mys	Braking	300	600	-93.12381969		L 0	LH Abutment	-163.688271
19	8	E4_6_TemperatureAndRailLoads"Position 8.mys	Braking	290	590	-86.36359552		ı 0	UH Abutment	-161.7294661
20	2	E4_6_TemperatureAndRailLoads"Position 9.mys	Braking	280	580	-84.95461087		u 0	LH Abutment	-161.3212078
21	10	E4_6_TemperatureAndRailLoads"Position 10.mys	Braking	270	570	-84.5487352		L 0	LH Abutment	-161.203604
22	11	E4_6_TemperatureAndRailLoads"Position 11.mys	Braking	260	560	-84.41253008		L 0	LH Abutment	-161.1641382
23	12	64_6_TemperatureAndRailLoads"Position 12.mys	Braking	250	550	-84.36325544		0	LH Abutment	-161.1493607
24	13	E4_6_TemperatureAndRailLoads*Position 13.mys	Braking	240	540	-84.34484571		0	LH Abutment	-161.1445263
25	14	E4_6_TemperatureAndRailLoads"Position 14.mys	Braking	230	530	-84.33787823		0	UH Abutment	-161.1425073
26	15	E4_6_TemperatureAndRailLoads"Position 15.mys	Braking	220	520	-84.3352279		L 0	LH Abutment	-161.141739
27	16	E4_6_TemperatureAndRailLoads"Position 16.mys	Braking	210	510	-84.33421757		L 0	UH Abutment	-161.1414451
28										
29										
30										
31										
32										
33										
34										
35										
36										
37										
38										
N & P PI To	ark 1 / Decks / Envelope	- Track 1 / Frueinne - Decks / Raibed Check / Longitudinal Reactions Chec	Rail Stresses Check	3/	14					

From this worksheet the peak axial rail stress is shown to be -164.55MPa when the braking trainset is placed at the 6th position where it is 10 m from the left-hand abutment of the deck. This peak rail stress compares well with the UIC774-3 E4-6 test case published result of -162.06 MPa with a difference of 1.5%.

Peak Longitudinal Reactions at the Abutments

	A	B	C	D	E	F	G	н
1			Check of Longitudinal Reactions					
2								
3		Job Title	: UIC 774-3 Model: E4-6 TemperatureAndRailLoads					
4		Analysis Filename	: E4 6 TemperatureAndRailLoads"Position 1> E4 6 TemperatureAndRailLoad	"Position 16				
5		Model Directory	C:\Users\paul b\Documents\Lusas190\Projects					
6		Analysis Date	: 13/02/2020> 13/02/2020					
7		Model Units	s: N,m,kg,s,C					
8								
9					Track 1			
		Analysis ID	Results Filename	Loading Type	Distance from Left End of the Model to the Starting Position of	Distance from Left End of the Model to the Finishing Position of	Peak Longitudinal Reaction (N)	Abutment / Pier Number with Peak
10					the Loading (m)	the Loading (m)		Reaction
11	_		1 E4_6_TemperatureAndRailLoads"Position 1.mys	Temperature Only			695795.7944	LH Abutment
12			1 E4_6_TemperatureAndRailLoads"Position 1.mys	Braking	360	660	722728.8459	LH Abutment
13			2 E4_6_TemperatureAndRailLoads"Position 2.mys	Braking	350	650	868862.637	LH Abutment
14			3 E4_6_TemperatureAndRailLoads"Position 3.mys	Braking	340	640	1107096.072	LH Abutment
15			4 E4_6_TemperatureAndRailLoads"Position 4.mys	Braking	330	630	1420184.793	LH Abutment
16		1 1	5 E4_6_TemperatureAndRailLoads"Position 5.mys	Braking	320	620	1767865.812	LH Abutment
17			6 E4_6_TemperatureAndRailLoads"Position 6.mys	Braking	310	610	2085606.512	LH Abutment
18			7 E4_6_TemperatureAndRailLoads"Position 7.mys	Braking	300	600	2322152.489	LH Abutment
19			8 E4_6_TemperatureAndRailLoads"Position 8.mys	Braking	290	590	2403571.083	LH Abutment
20			9 E4_6_TemperatureAndRailLoads"Position 9.mys	Braking	280	580	2420540.588	LH Abutment
21		1	0 E4_6_TemperatureAndRailLoads"Position 10.mys	Braking	270	570	2425428.869	LH Abutment
22		1	1 E4_6_TemperatureAndRailLoads"Position 11.mys	Braking	260	560	2427069.295	LH Abutment
23		1	2 E4_6_TemperatureAndRailLoads"Position 12.mys	Braking	250	550	2427662.748	LH Abutment
24		1	3 E4_6_TemperatureAndRailLoads"Position 13.mys	Braking	240	540	2427884.47	LH Abutment
25		1	4 E4_6_TemperatureAndRailLoads"Position 14.mys	Braking	230	530	2427968.382	LH Abutment
26		1	5 E4_6_TemperatureAndRailLoads*Position 15.mys	Braking	220	520	2428000.295	LH Abutment
27		1	6 E4_6_TemperatureAndRailLoads"Position 16.mys	Braking	210	510	2428012.444	LH Abutment

• Click on the Longitudinal Reactions Check worksheet tab.

From this worksheet the peak reaction is shown to be 2428.01kN when the braking trainset is placed at the last position where the front of it is 90m past the left-hand abutment of the deck. This peak reaction compares well with the UIC774-3 E4-6 test case published result of 2196.1kN with a difference of $\pm 10.56\%$ which is within the 20% limit specified in the code of practice. The maximum reaction is also comparable with the alternative calculation method which gives 2373.47kN ($\pm 2.3\%$ difference).

• Close the Microsoft Excel application.

File Close

• Choose **No** when asked to save the changes to the current model since there have been no manual changes to it and we want to preserve the original model built by the Rail Track Analysis software.

This completes the example.

A general discussion follows, along with information about how to model a structure with multiple decks.

General Modelling Discussion and Accuracy of Results

The modelling of the structure and approach embankments in this example is relatively crude to ensure that the track-structure analysis is carried out within a reasonable length of time. As a result, the accuracy of some results, such as the rail stresses, may have been reduced slightly.

Refinement of the modelling will improve the accuracy of the solution at the cost of increased computer memory requirements and increased modelling / analysis and post-processing time. The following table shows the improvement of accuracy for the two test cases when element sizes of less than 2m and trainset location increments of less than 10m are used. For the UIC774-3 code of practice the computed values should be within -10% and +20% (if on the safe side) and based on this all results pass the criterion when compared against the UIC774-3 global / complete analyses results.

Description	Test	Railbed	Reaction	Rail Stress
	Case	Displacement		
2m Elements	E1-3	0.01747 m	929.09 kN	-191.87 MPa
16 Location		+0.98%	+6.25%	+5.19%
Increments of 10m	E4-6	0.01731 m	2428.0 kN	-164.55 MPa
		-2.75%	+10.56%	+1.54%
1m Elements	E1-3	0.01747 m	927.45 kN	-193.06 MPa
16 Location		+0.98%	+6.06%	+5.84%
Increments of 10m	E4-6	0.01732 m	2428.1 kN	-165.37 MPa
		-2.70%	+10.56%	+2.04%
2m Elements	E1-3	0.01748 m	929.09 kN	-191.87 MPa
31 Location		+1.04%	+6.25%	+5.19%
Increments of 5m	E4-6	0.01733 m	2428.0 kN	-165.04 MPa
		-2.64%	+10.56%	+1.84%
1m Elements	E1-3	0.01748 m	927.45 kN	-193.06 MPa
31 Location		+1.04%	+6.06%	+5.84%
Increments of 5m	E4-6	0.01733 m	2428.1 kN	-165.78 MPa
		-2.64%	+10.56%	+2.30%
2m Elements	E1-3	0.01748 m	929.64 kN	-191.92 MPa
151 Location		+1.04%	+6.32%	+5.22%
Increments of 1m	E4-6	0.01733 m	2428.0 kN	-165.04 MPa
		-2.64%	+10.56%	+1.84%
1m Elements	E1-3	0.01748 m	927.61 kN	-193.07 MPa
151 Location		+1.04%	+6.08%	+5.85%
Increments of 1m	E4-6	0.01733 m	2428.1 kN	-165.80 MPa
		-2.64%	+10.56%	+2.31%
0.5m Elements	E1-3	0.01748 m	927.00 kN	-193.65 MPa
301 Location		+1.04%	+6.01%	+6.17%
Increments of 0.5m	E4-6	0.01733 m	2428.1 kN	-166.23 MPa
		-2.64%	+10.56%	+2.57%

In the previous table the meshing and increment size can be seen to have a less significant effect on the railbed displacement and reactions obtained than on the rail

stress values. This is because the Finite Element solution is a displacement method and reactions should be in equilibrium with the applied load which is constant. All element sizes shown can be seen to satisfy the accuracy of the rail stresses against the fundamental test cases in UIC774-3 but a refinement of both the mesh and the train position incrementation potentially allows a more accurate capture of the value of the maximum stress and location of the trainset where the maximum rail stress occurs but at the cost of analysis time. All results in the table are very similar, however, for the range of element sizes presented from 0.5 m up to the UIC774-3 maximum recommended element size of 2.0 m.

Modelling a Structure with Multiple Decks

To model a structure with multiple decks spreadsheet data similar to that shown on the following pages would need to be defined.

The input for the support conditions / pier at the end of one deck / start of the next deck must be identical or an input error will occur. Bearing conditions for the decks at the individual supports / piers can of course be different – see the Rail Track User Manual for more information on the input requirements.

Values are for illustration purposes only.



	A1	✓										
	A	В	С	D	E	F	G	Н	I	L	M	N
1	Structure	Definition	Units : Pie	r Height : r	n : Bearing	springs on	top of each	pier : kN/r	nm, Span L	ength : m		
2			Spring									
			Support	Dior	Dior Coo	Dior Mot	Bearing	Bearing	Chan	Can	Mot	Polloct
			for each	Height	Assian.	Assign	on Top of	from End	Length	Assign.	Assign.	Type
2			Abutment (Dior				each Pier	of Deck				
4		Left End	R				R					
5		Span 1	1200				F		60	1	1	1
6		Span 2										
8	-	Span 3 Span 4										
9	eck.	Span 5			1							
10		Span 6										
11		Span 7 Span 8										
13		Span 9										
14		Number of Supports for the Deck / Length	2				2		60			
15		Left End Shop 1	1200				R		60	1	1	1
17		Span 2	1000				F		80			
18		Span 3										
19	- K	Span 4										
20	å	Span 5 Span 6										
22		Span 7										
23		Span 8										
24		Span 9 Number of Sunnorts for the Deck / Length	2				2		60			
26		Left End	1000				R					
27		Span 1	950				F		60	1	1	1
28		Span 2										
30	θ.	Span 5										
31	Dect	Span 5										
32		Span 6										
34		Span 7 Span 8										
35		Span 9										
36		Number of Supports for the Deck / Length	2				2		60			
37		Left End Snan 1	950				F R		ഖ	1	1	1
39		Span 2	1100									· · · · ·
40	-	Span 3										
41	, s	Span 4 Span 5										
43	ă	Span 6										
44		Span 7										
45		Span 8 Snan 9										
47		Number of Supports for the Deck / Length	2				2		60			
48	ĺ	Left End	1100				R					
49		Span 1 Span 2	R				F		60	1	1	1
51		Span 3										
52	ις γ	Span 4										
53	Dec	Span 5										
55		Span 7										
56		Span 8										
57		Span 9										
58		number of Supports for the Deck / Length	2				2		60			
14	De De	cks, Tracks and Embankment 📃 Structure Defini	tion 🖉 Geo	metric Prop	perties 📈 I	Material (I 🔳		_				•



	A1	- (•	f_x	Material F	Properties			¥
	A	В	С	D	E	F	G	
1	Material Pro	perties	Units : N, n					
2								
3			E	v	ρ	æ	Description	
4		Rail	210000	0.3	0	1.20E-05	Rails	
5		1	210000	0.3	0	1.00E-05	Deck	
6								
7								
8								
9								
10								
11		netric Prone	erties Ma	terial Pron	erties I	nteraction ar	d Expand 4	
		nethe Prope	ardes <u>T</u> illa	centar Prop		riteraction a		



	A1 v stating										
A		В	C	D	E	F	G	Н	1	J	-
1	Loading	Units : Temperat		Position/Leng							
2											
3			Amount								
4		Concrete Deck									
5	Temperature Loads	Steel Deck	3	<u>.</u>							
6		User Deck									
/		Ralls		4							_
8		1		-							
10		Number of Train Loading Groups to Analyse									
11					a to Analyse						
12				-							<u> </u>
13				Train Lo	ading Group:	1					
14				1	¥						
		Number of Track	k								Num
15		Loading Location	ins 73	3							Load
16		Loading Ty	Track Selection to be Loaded	Parametric Starting Position for Loadings	Parametric End Position for Loadings	Amount (per unit length)	Loaded Length	Starting Location of Loading for First Analysis	Finishing Location of Loading for Last Analysis	Location Increment for each Analysis	
17		Braking		0	300	20	300	0	360	5	
18		Vertical1		0	300	80	300	0	360	5	
19											
20											
21											
23	Train Loads										• • • • • • • • • • • • • • • • • • • •
24											
25											
📧 🔸 🕨 / Material Properties / Interaction and Expansion Joint Loading / 🗊 / 💷 🚺											